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(54) **ULTRASONIC TRANSDUCER ELECTRODE ASSEMBLY**

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See application file for complete search history.

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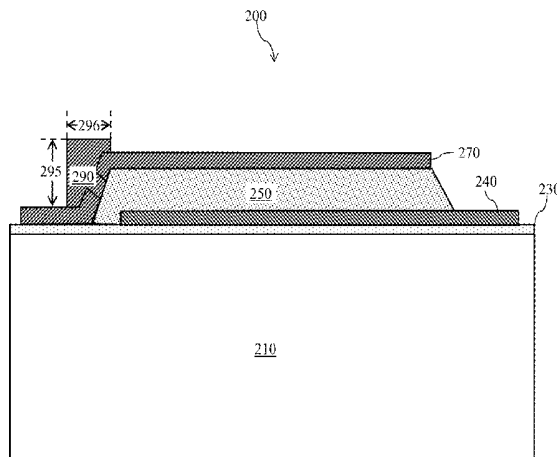
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*Primary Examiner* — Thomas Dougherty

(57) **ABSTRACT**

The present disclosure provides a method of fabricating an ultrasound transducer. A substrate having a first side and a second side opposite the first side is provided. A bottom electrode is formed over the first side of the substrate. A piezoelectric element is formed over the bottom electrode. The piezoelectric element has a chamfered sidewall. A top electrode is formed over the piezoelectric element. A step metal element is formed over a portion of the top electrode proximate to the chamfered sidewall of the piezoelectric element.

**20 Claims, 19 Drawing Sheets**



**Related U.S. Application Data**

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| (51) | <b>Int. Cl.</b>   |   |
|      | <i>A61B 8/12</i> (2006.01)  |   |
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|      | <i>H01L 41/09</i> (2006.01)   |   |
|      | <i>H01L 41/29</i> (2013.01)   |   |
|      | <i>B06B 1/06</i> (2006.01)  |   |
|      | <i>A61B 8/08</i> (2006.01)  |   |
| (52) | <b>U.S. Cl.</b>   |   |
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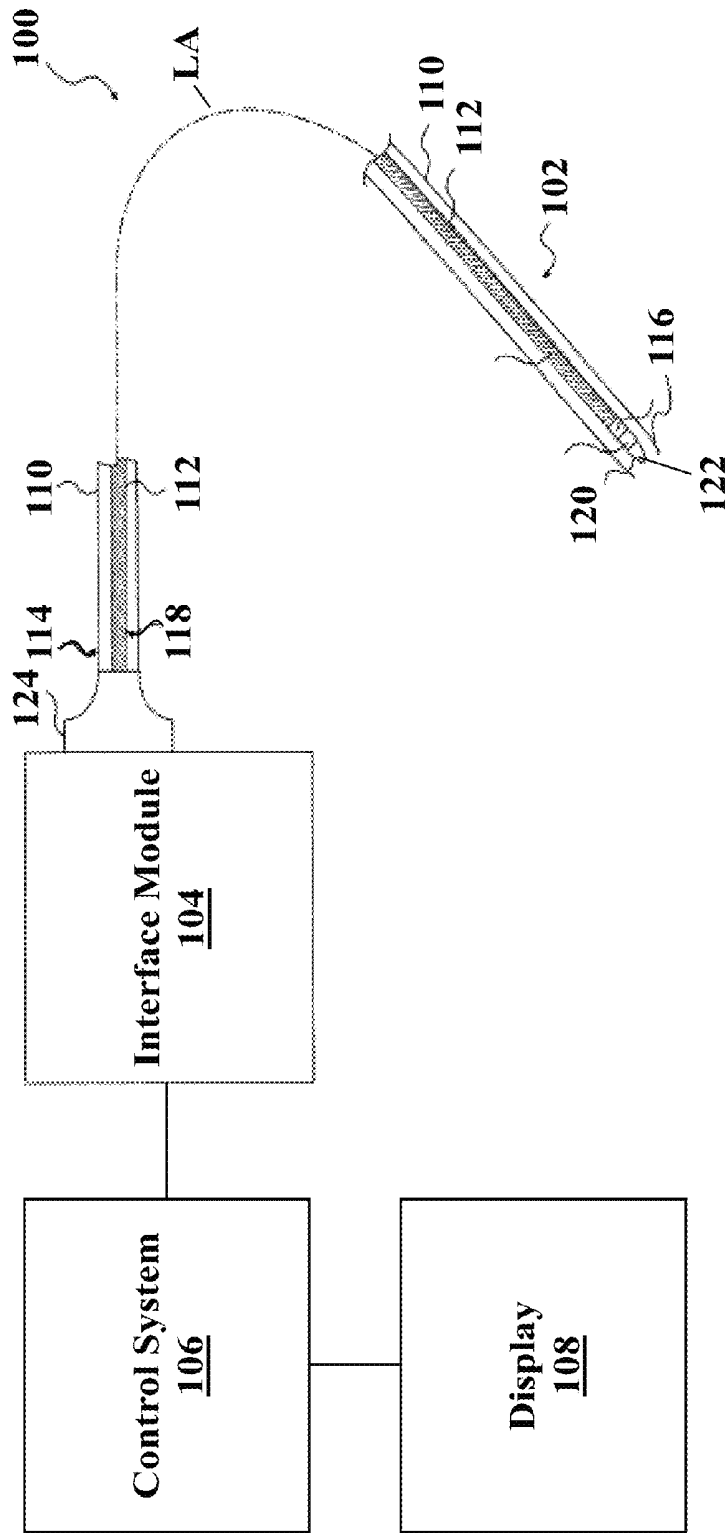


FIG. 1

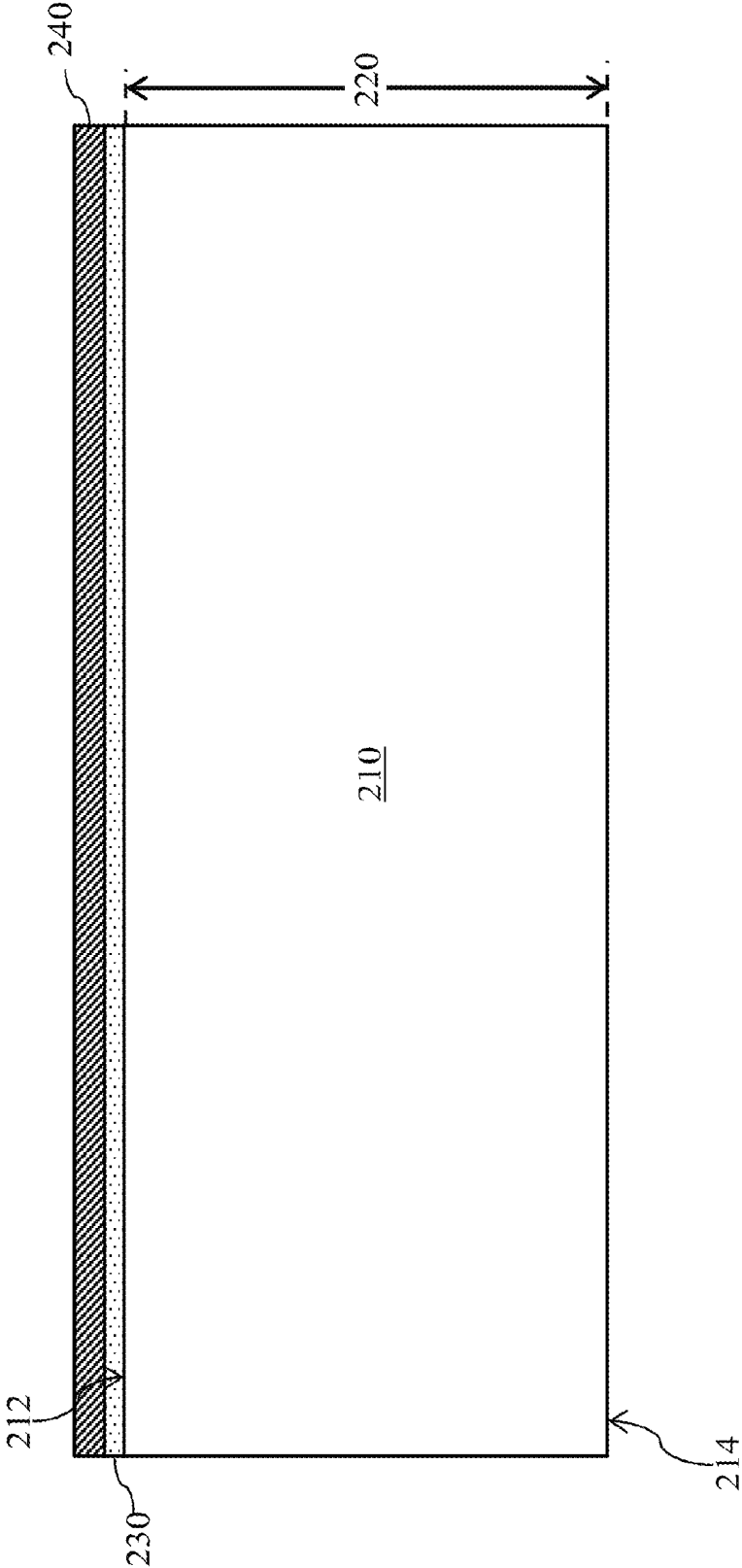


FIG. 2

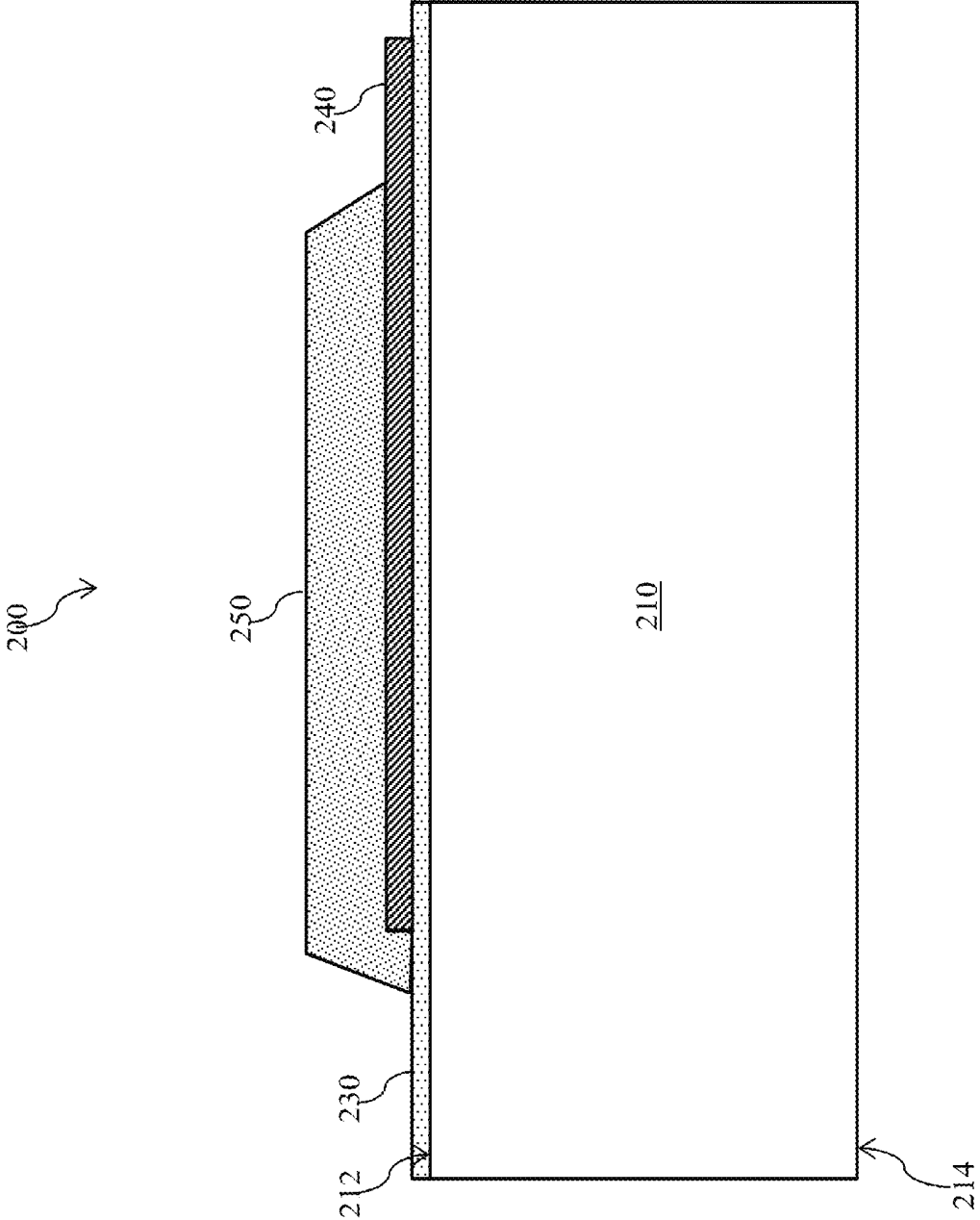


FIG. 3

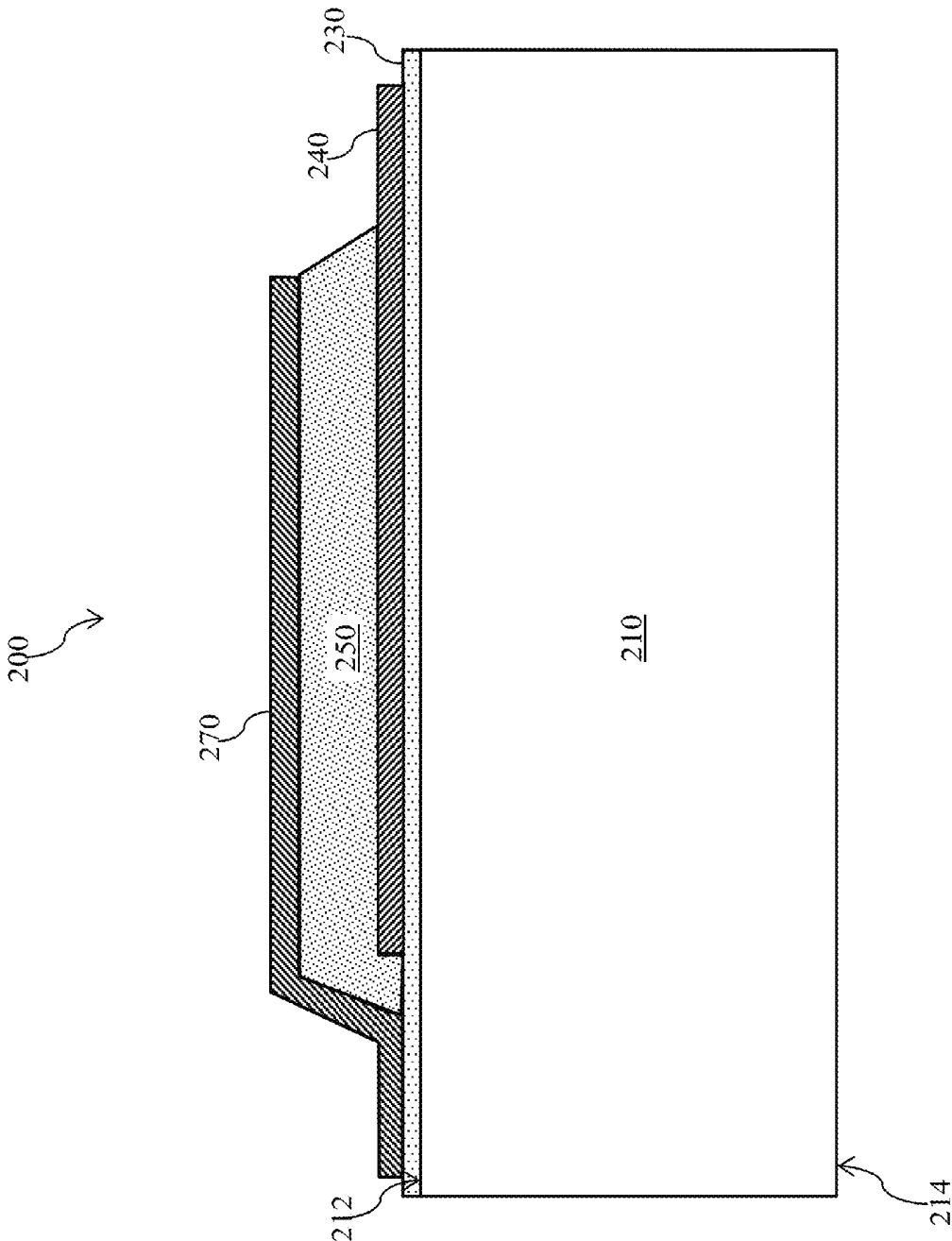


FIG. 4

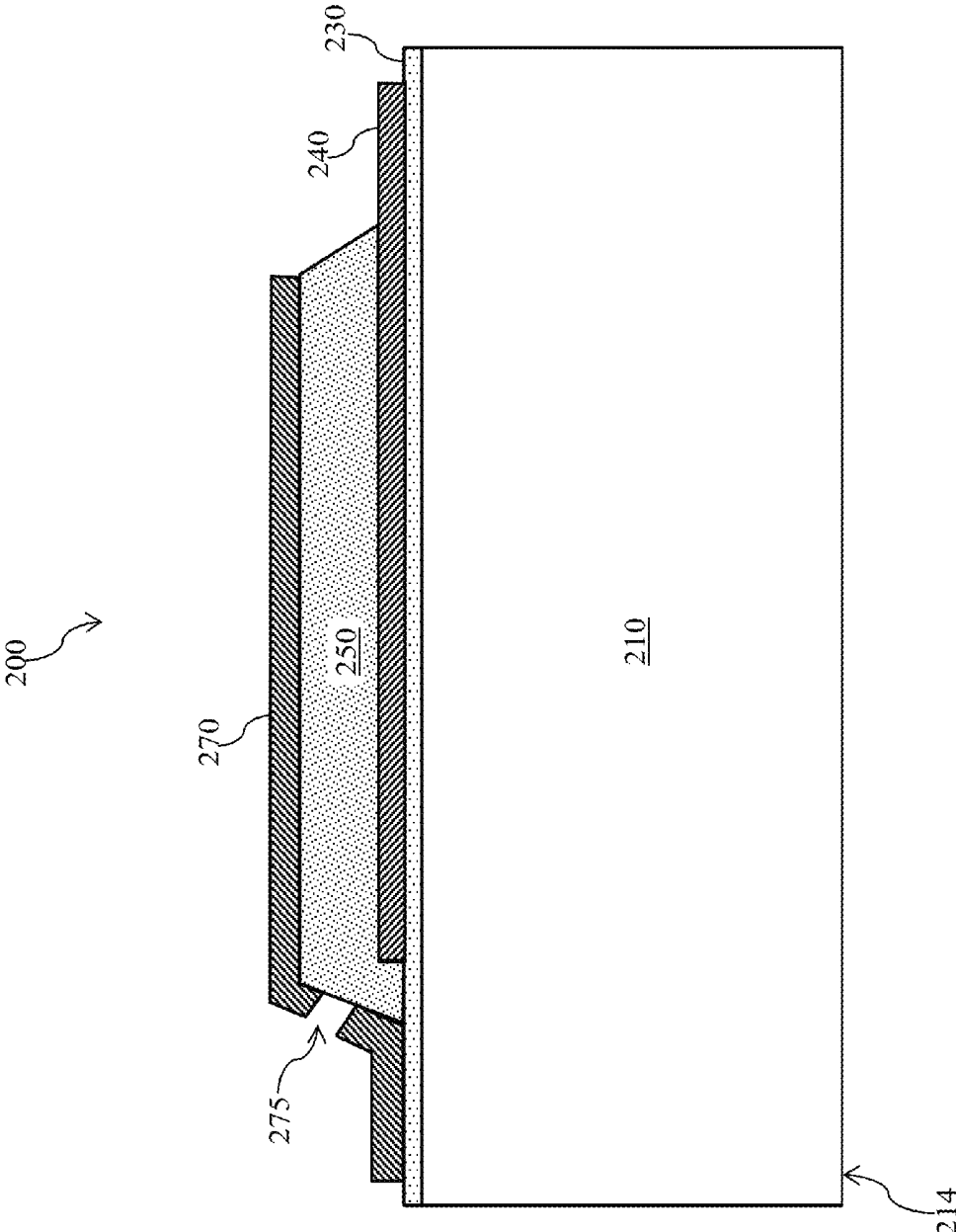


FIG. 5

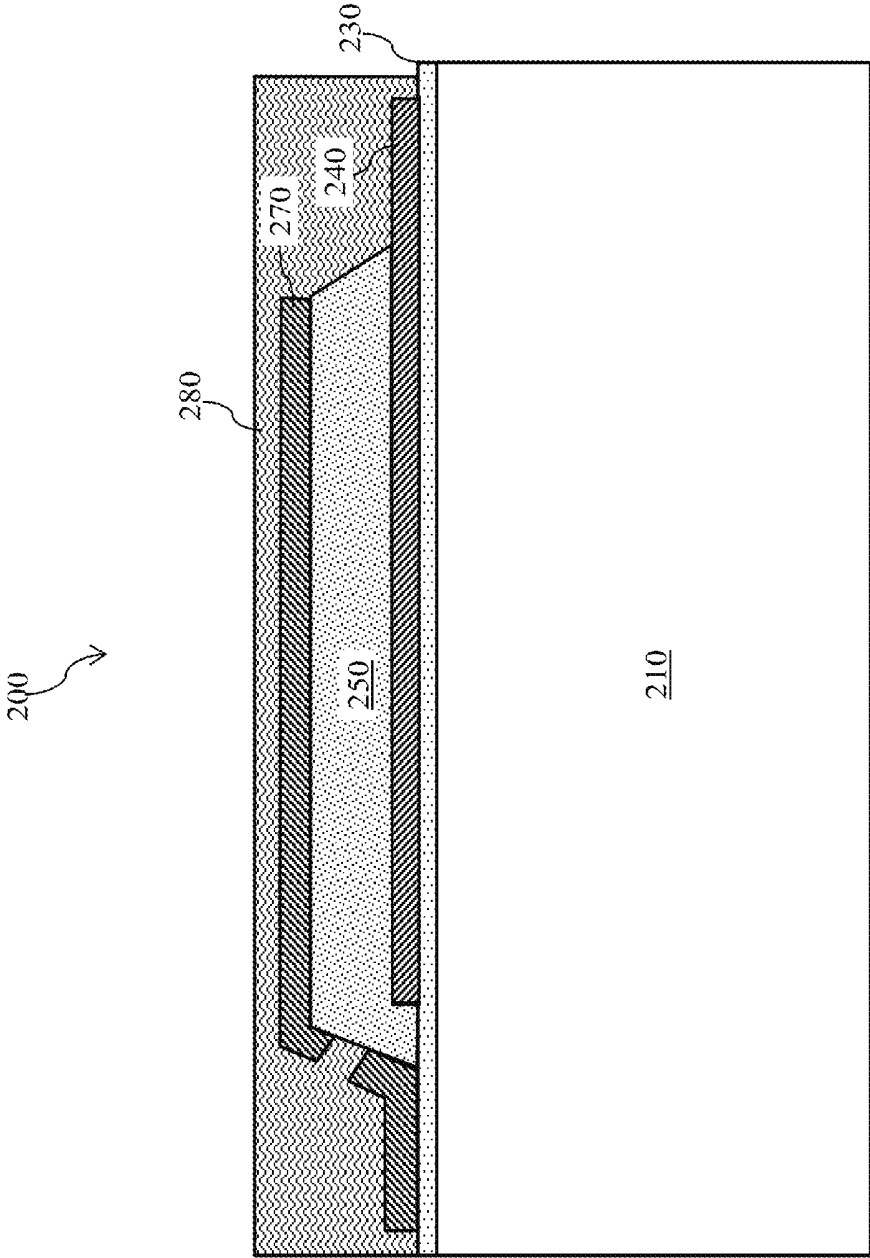


FIG. 6

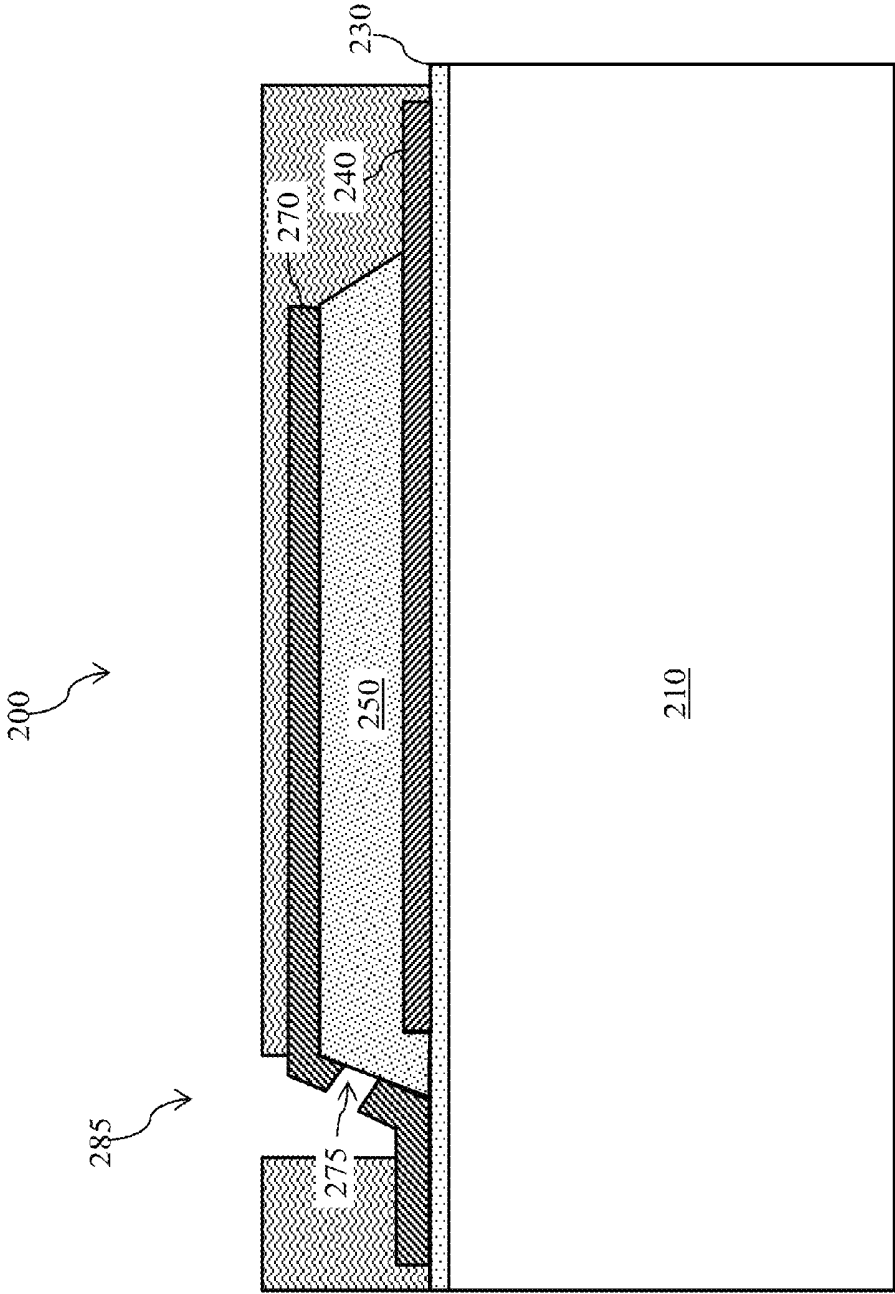


FIG. 7

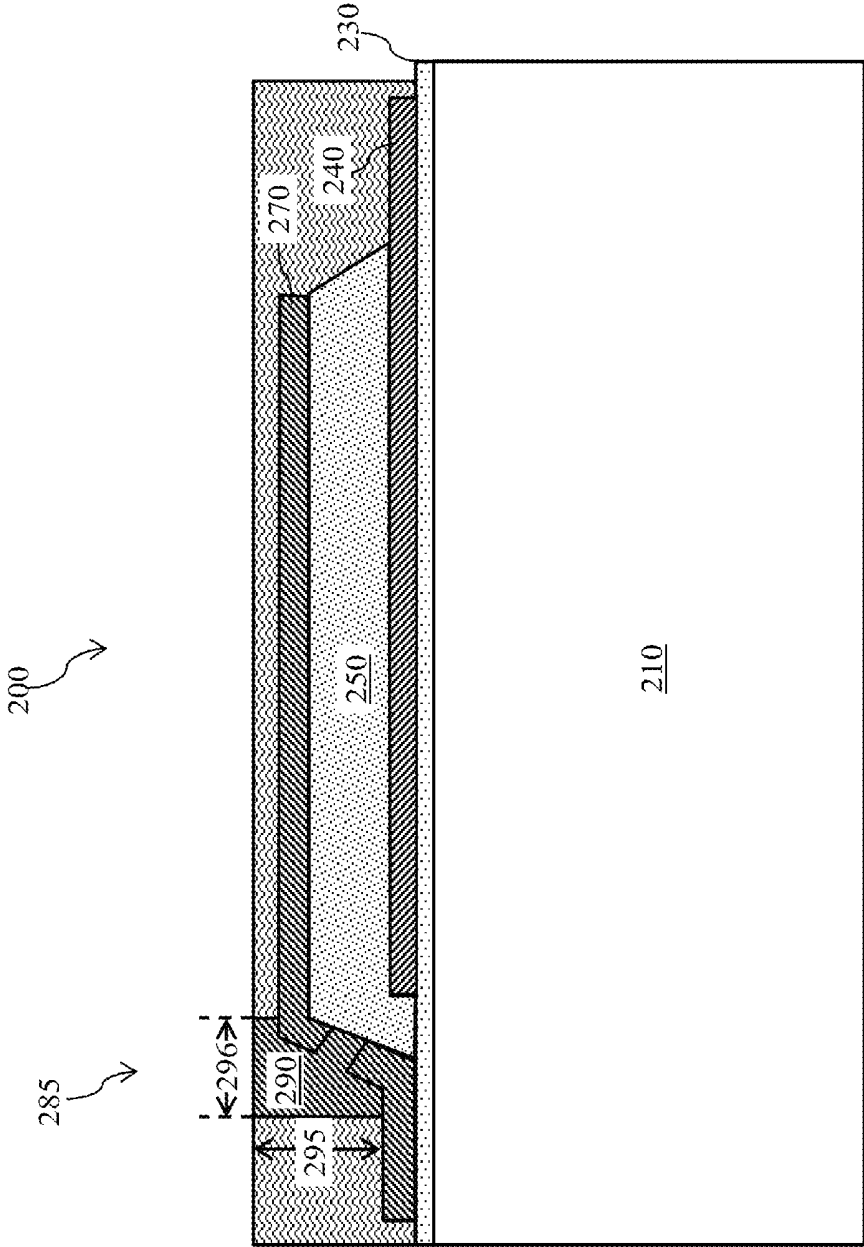


FIG. 8

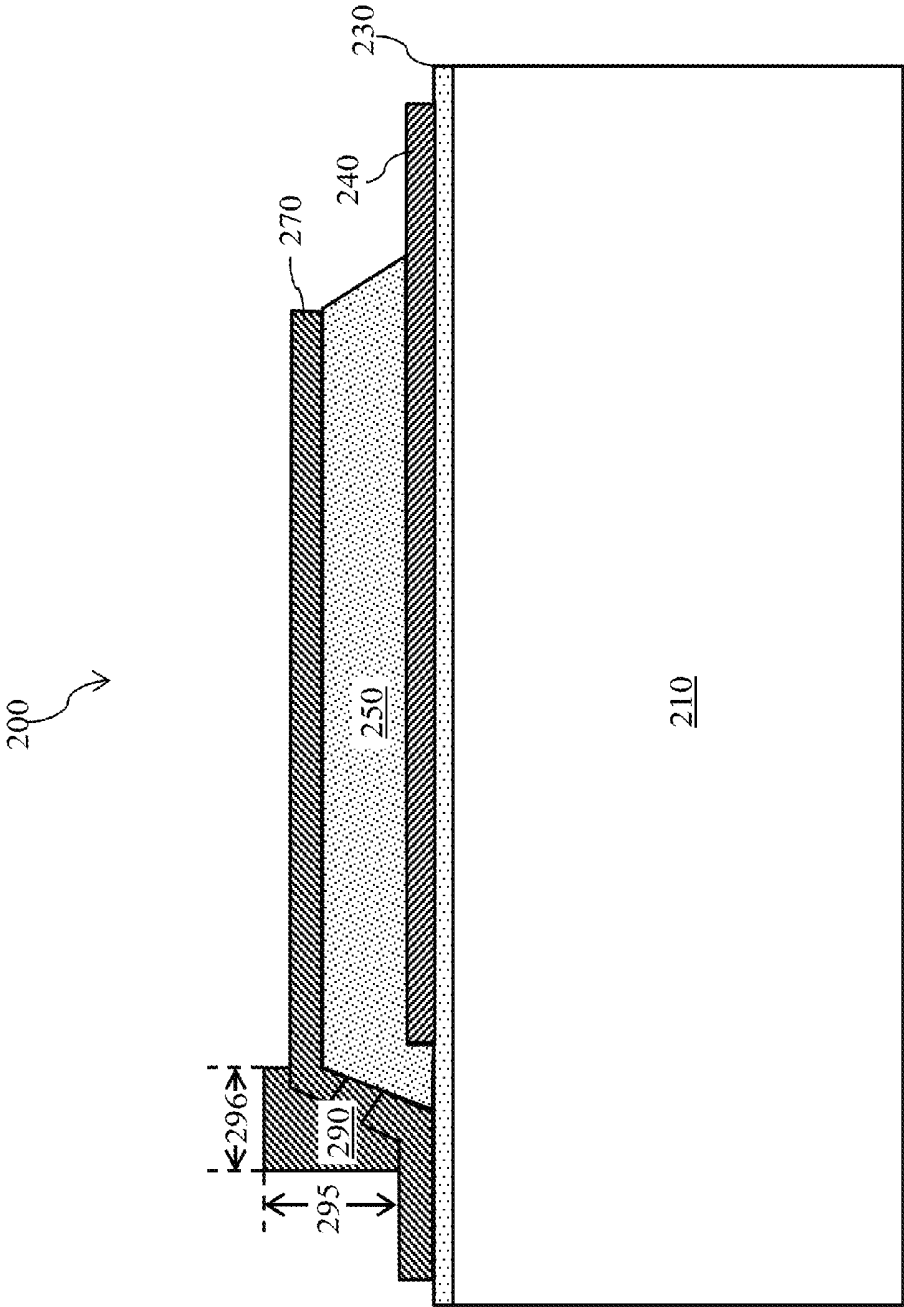


FIG. 9

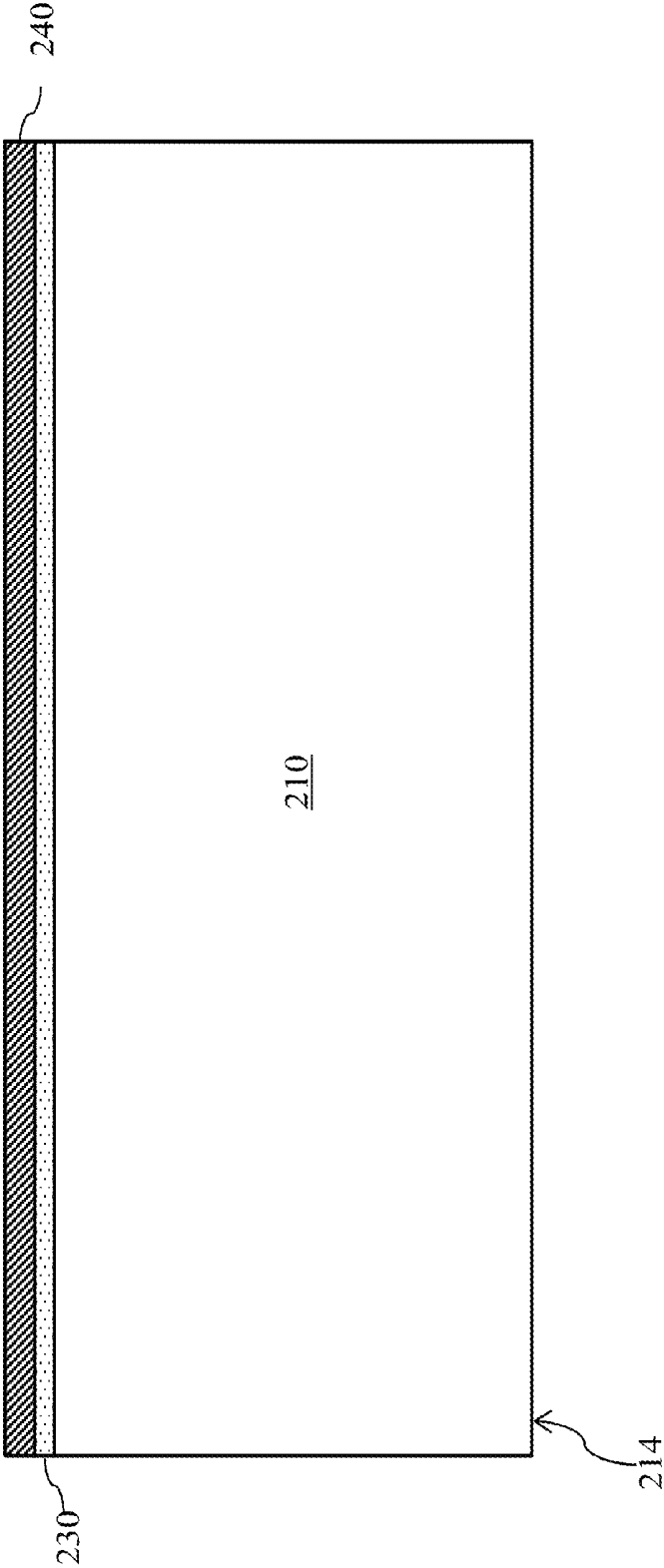


FIG. 10

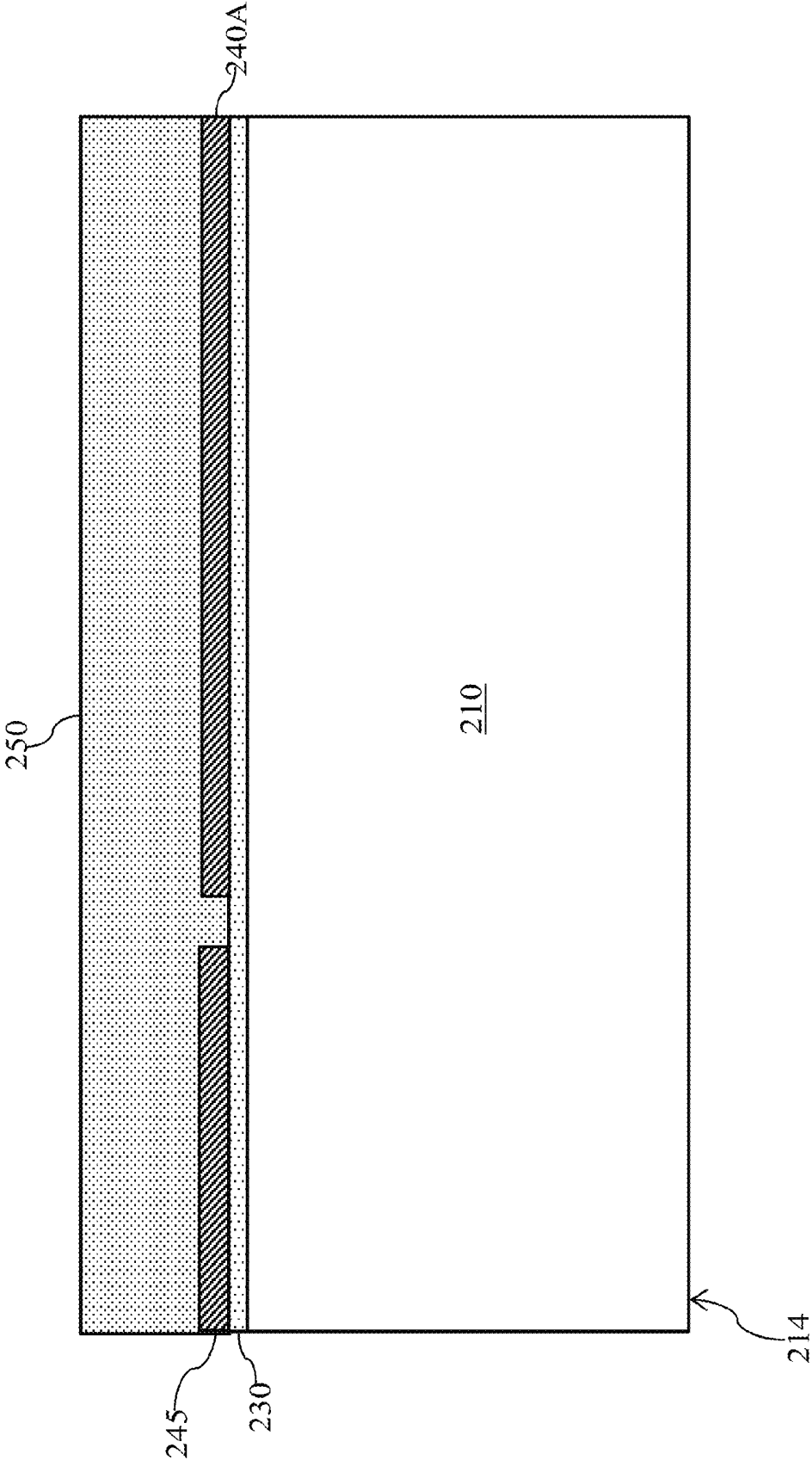


FIG. 11

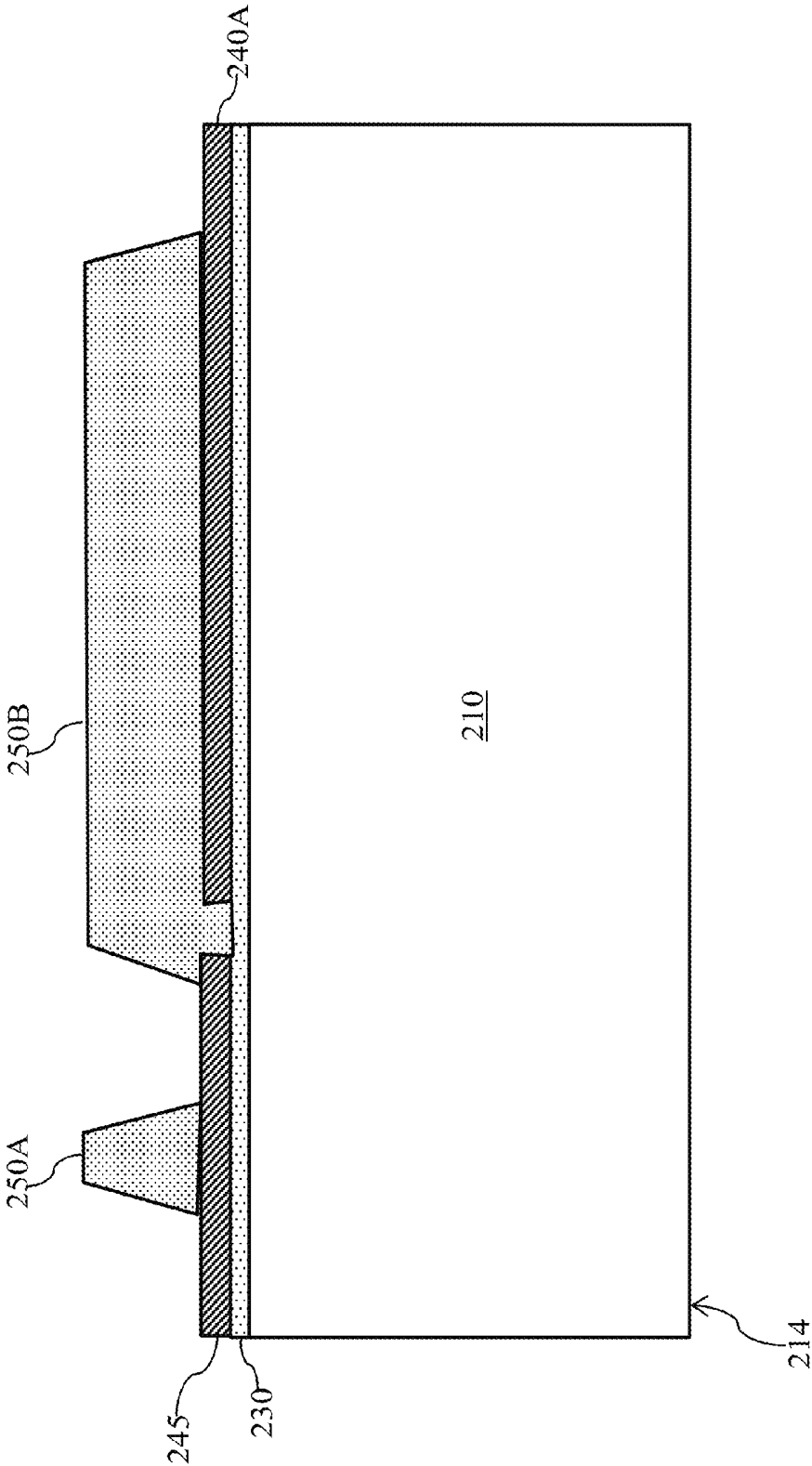


FIG. 12

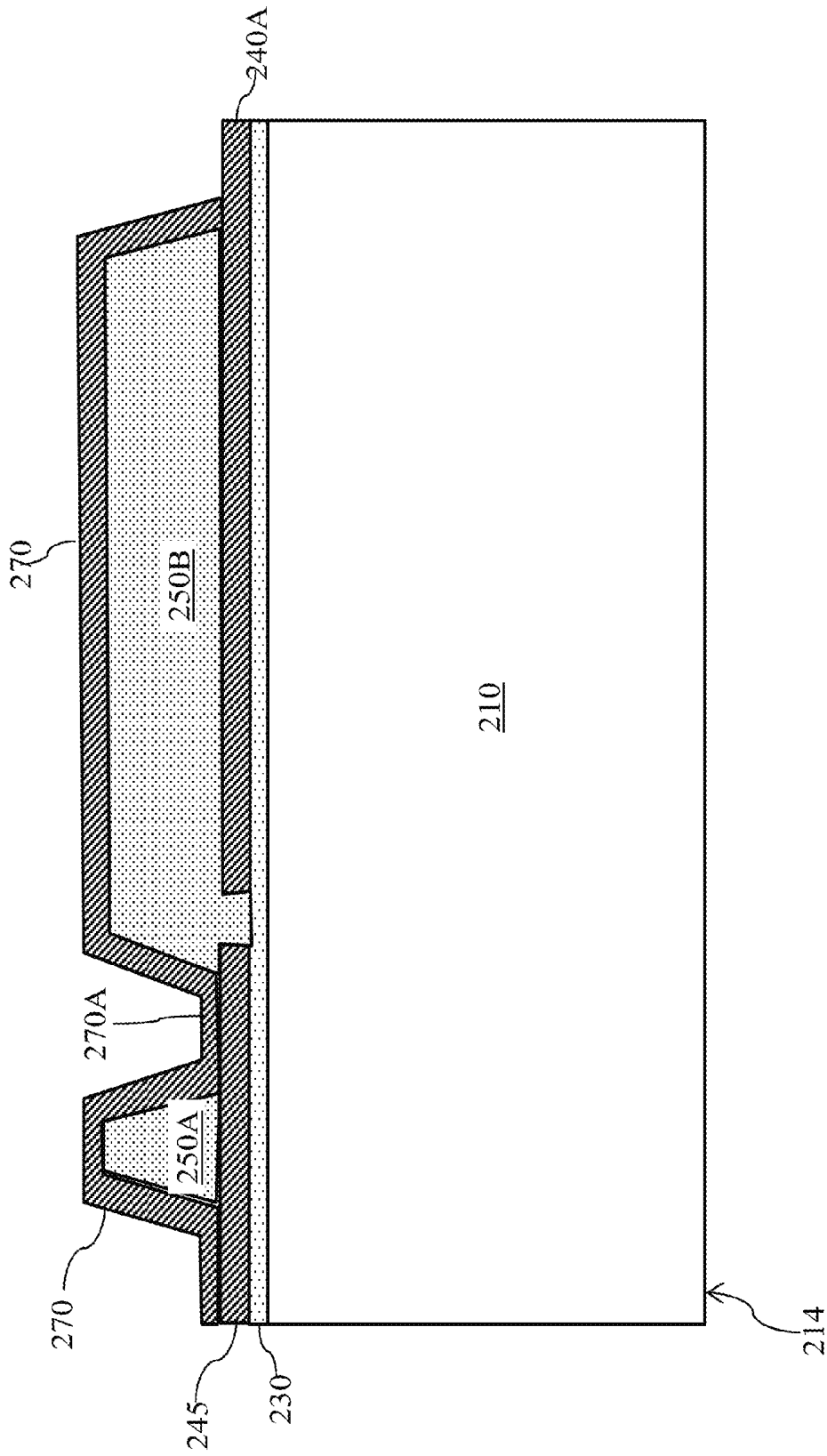


FIG. 13

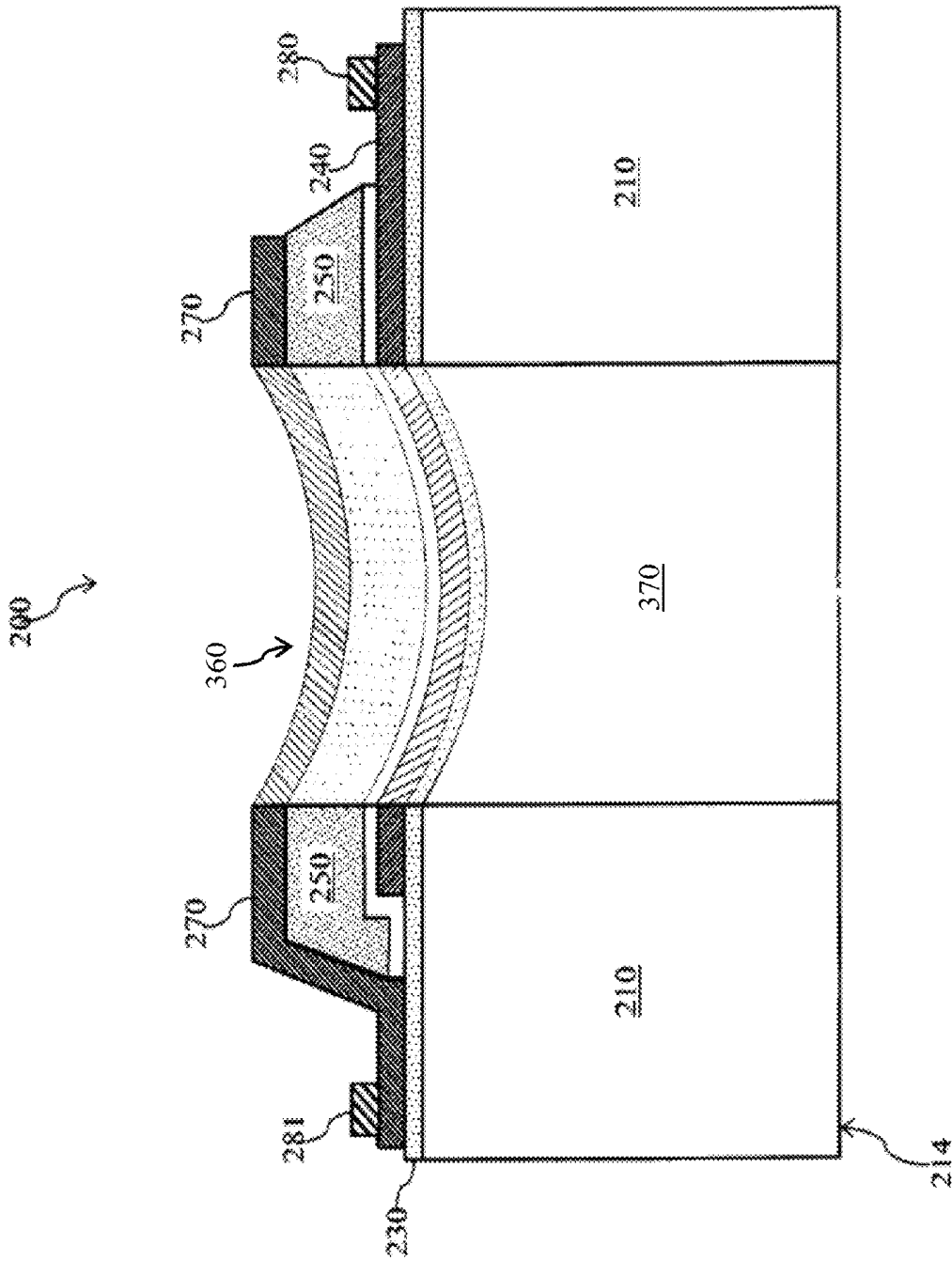


FIG. 14

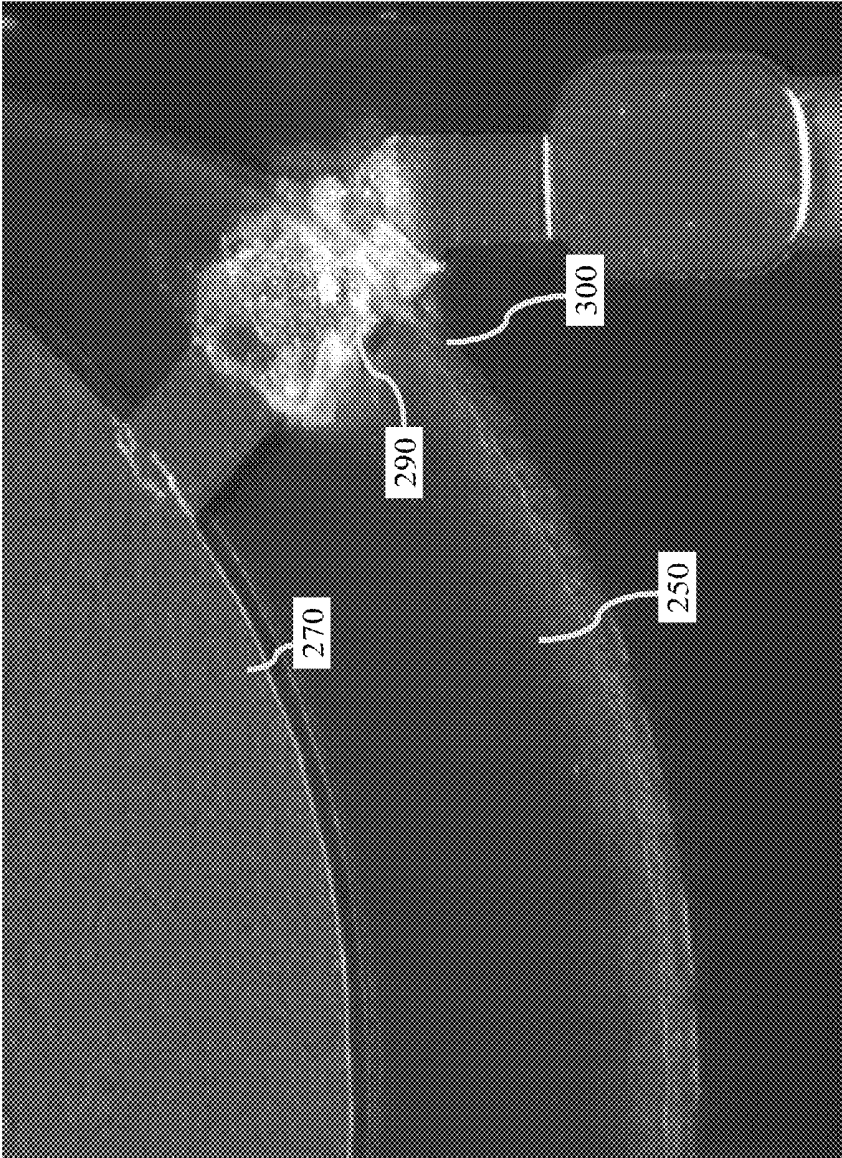


FIG. 15

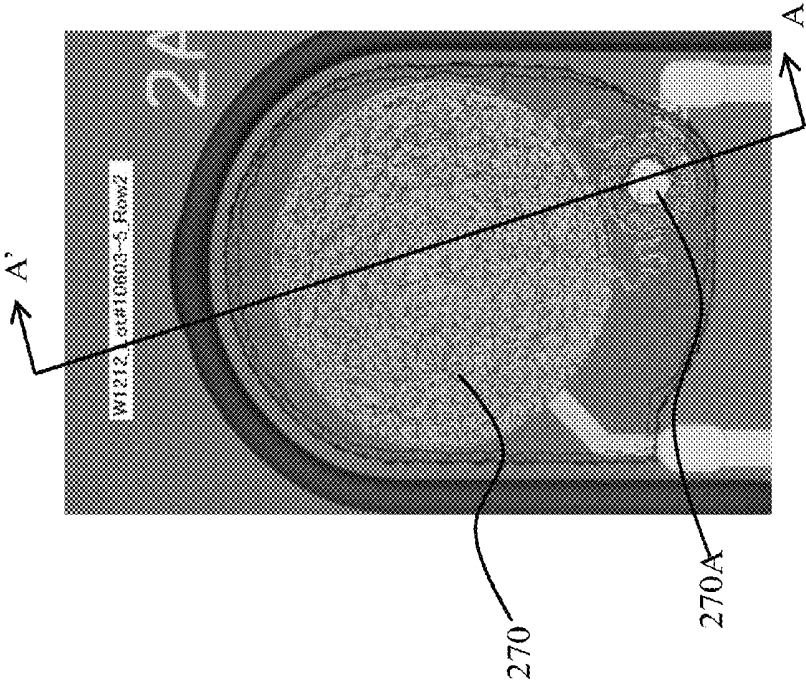


FIG. 16A

Via  
Serpentine  
Small Patch (one  
small)

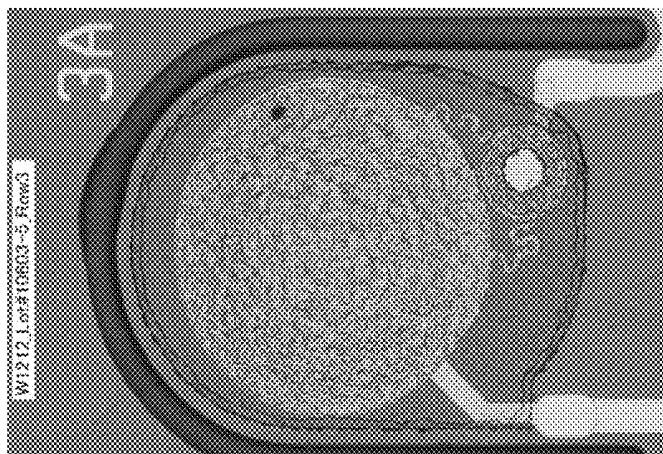


FIG. 16C

Via  
Serpentine  
Big Patch (two small)

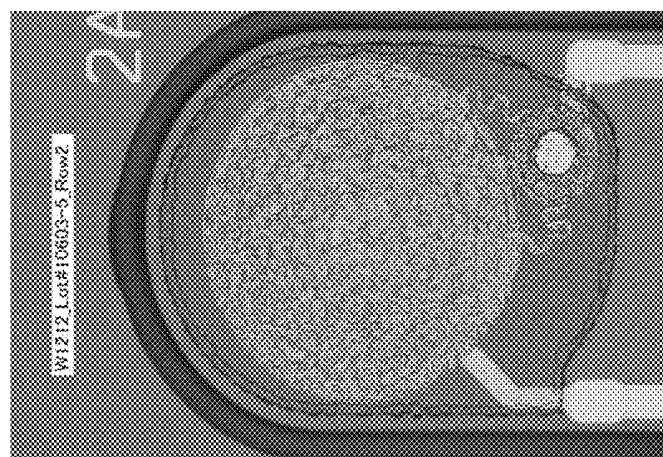


FIG. 16B

Via  
Fatty  
Small Patch (one  
small)

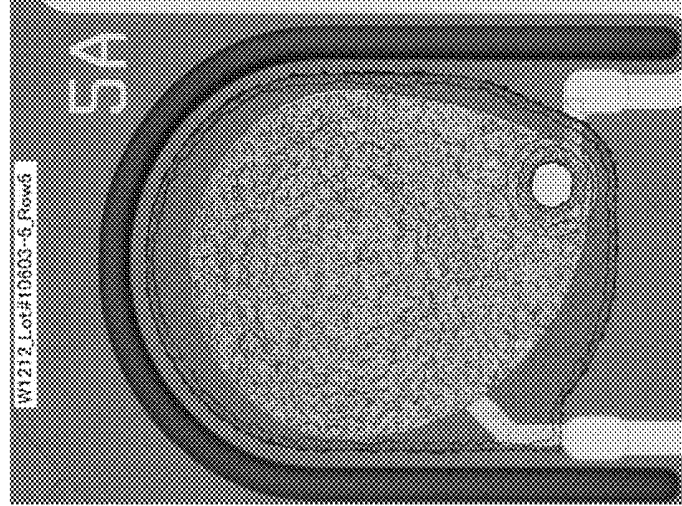


FIG. 16E

Via  
Fatty  
Big Patch (two small)

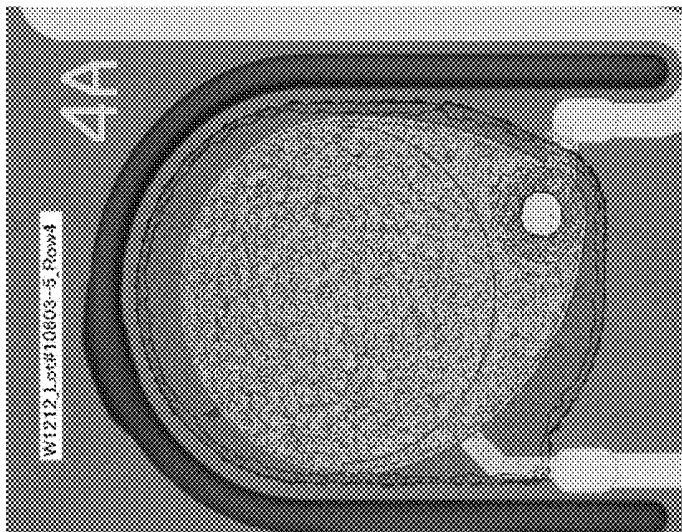


FIG. 16D

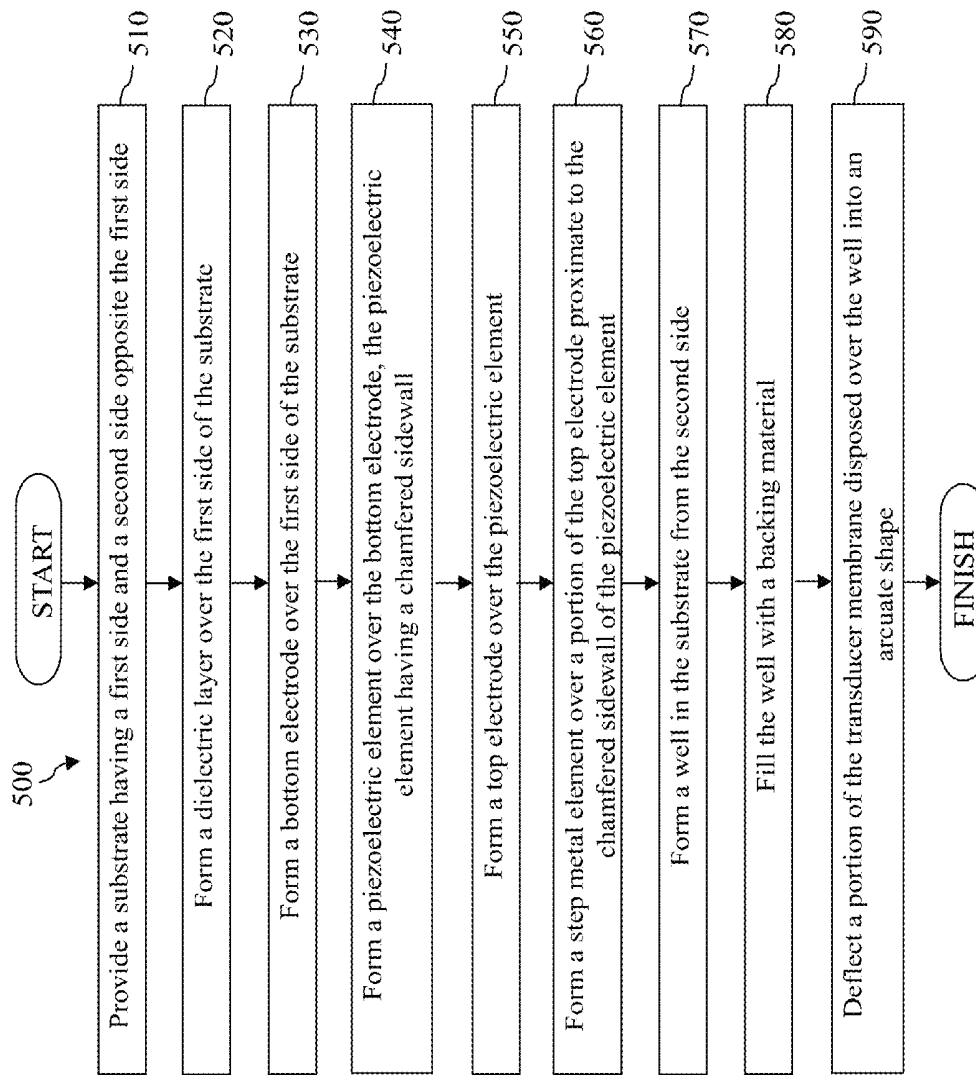


FIG. 17

## ULTRASONIC TRANSDUCER ELECTRODE ASSEMBLY

### PRIORITY DATA

This application is a division of U.S. patent application Ser. No. 15/094,717 No. 14/106,897, filed Dec. 16, 2013, now U.S. Pat. No. 9,312,470, which claims priority to Provisional Patent Application No. 61/747,498, filed Dec. 31, 2012, and entitled "Ultrasound Transducer Electrode Assembly," the disclosures of which are hereby incorporated by reference in their entireties.

### TECHNICAL FIELD

The present disclosure relates generally to intravascular ultrasound (IVUS) imaging, and in particular, to electrode assembly of an ultrasound transducer.

### BACKGROUND

Intravascular ultrasound (IVUS) imaging is widely used in interventional cardiology as a diagnostic tool for assessing a vessel, such as an artery, within the human body to determine the need for treatment, to guide intervention, and/or to assess its effectiveness. An IVUS imaging system uses ultrasound echoes to form a cross-sectional image of the vessel of interest. Typically, IVUS imaging uses a transducer on an IVUS catheter that both emits ultrasound signals (waves) and receives the reflected ultrasound signals. The emitted ultrasound signals (often referred to as ultrasound pulses) pass easily through most tissues and blood, but they are partially reflected as the result of impedance variations arising from tissue structures (such as the various layers of the vessel wall), red blood cells, and other features of interest. The IVUS imaging system, which is connected to the IVUS catheter by way of a patient interface module, processes the received ultrasound signals (often referred to as ultrasound echoes) to produce a cross-sectional image of the vessel where the IVUS catheter is located.

IVUS catheters typically employ one or more transducers to transmit ultrasound signals and receive reflected ultrasound signals. These transducers have electrodes that are used to apply electrical signals to the transducers. However, existing techniques of forming electrodes for transducers may have certain shortcomings. For example, the electrodes of conventional transducers may suffer from discontinuity problems.

Therefore, while conventional methods of forming transducer electrodes are generally adequate for their intended purposes, they have not been entirely satisfactory in every aspect.

### SUMMARY

Ultrasounds transducers are used in Intravascular ultrasound (IVUS) imaging to help assess medical conditions inside a human body. As a part of its operation, an ultrasound transducer has electrodes that are used to apply electrical signals to the transducer. However, conventional ultrasound transducers may suffer from drawbacks such as electrode discontinuity, which may interfere with the intended electrical operation of the transducer. The present disclosure is directed to an ultrasound transducer that utilizes a step metal element to overcome the electrode discontinuity issues associated with conventional ultrasound transducers. In more detail, the ultrasound transducer has a piezoelectric film that

is sandwiched between a top electrode and a bottom electrode. The top electrode is located on a top surface and a sidewall of the piezoelectric film. The portion of the top electrode located on the sidewall of the piezoelectric film is prone to suffer from discontinuity problems. Therefore, a step metal element—having the same material composition as the top electrode itself—is formed on the sidewall portion of the top electrode. The step metal element serves as a bridge in case electrical discontinuity occurs in the sidewall portion of the top electrode.

The present disclosure provides various embodiments of an ultrasound transducer for use in intravascular ultrasound (IVUS) imaging. An exemplary ultrasound transducer includes a substrate; a bottom electrode disposed over the substrate; a piezoelectric element disposed over the bottom electrode; a top electrode disposed over at least a top surface and a sidewall of the piezoelectric element; and a step metal element disposed over a sidewall of the top electrode.

The present disclosure further provides an ultrasound system. The ultrasound system includes: an imaging component that includes a flexible elongate member and a piezoelectric micromachined ultrasound transducer (PMUT) coupled to a distal end of the elongate member. The PMUT includes: a substrate having a front surface and a back surface opposite the first surface; a well located in the substrate, the well extending from the back surface of the substrate to, but not beyond, the front surface of the substrate, wherein the well is at least partially filled with a backing material; a transducer membrane disposed over the well, wherein the transducer member includes a piezoelectric element disposed between a top electrode and a bottom electrode; and a step metal element disposed over a sidewall of the piezoelectric element. The ultrasound system also includes an interface module configured to engage with a proximal end of the elongate member; and an ultrasound processing component in communication with the interface module.

The present disclosure further provides a method of forming an ultrasound transducer. The method includes: providing a substrate having a first side and a second side opposite the first side; forming a bottom electrode over the first side of the substrate; forming a piezoelectric element over the bottom electrode, the piezoelectric element having a chamfered sidewall; forming a top electrode over the piezoelectric element; and forming a step metal element over a portion of the top electrode proximate to the chamfered sidewall of the piezoelectric element.

Both the foregoing general description and the following detailed description are exemplary and explanatory in nature and are intended to provide an understanding of the present disclosure without limiting the scope of the present disclosure. In that regard, additional aspects, features, and advantages of the present disclosure will become apparent to one skilled in the art from the following detailed description.

### BRIEF DESCRIPTIONS OF THE DRAWINGS

Aspects of the present disclosure are best understood from the following detailed description when read with the accompanying figures. It is emphasized that, in accordance with the standard practice in the industry, various features are not drawn to scale. In fact, the dimensions of the various features may be arbitrarily increased or reduced for clarity of discussion. In addition, the present disclosure may repeat reference numerals and/or letters in the various examples. This repetition is for the purpose of simplicity and clarity

and does not in itself dictate a relationship between the various embodiments and/or configurations discussed.

FIG. 1 is a schematic illustration of an intravascular ultrasound (IVUS) imaging system according to various aspects of the present disclosure.

FIGS. 2-14 are diagrammatic cross-sectional side views of an ultrasound transducer at different stages of fabrication according to various aspects of the present disclosure.

FIG. 15 is a diagrammatic top view of a portion of a transducer according to various aspects of the present disclosure.

FIGS. 16A-16E are diagrammatic top views of various vias according to various aspects of the present disclosure.

FIG. 17 is a flowchart of a method of fabricating a transducer according to various aspects of the present disclosure.

### DETAILED DESCRIPTION

For the purposes of promoting an understanding of the principles of the present disclosure, reference will now be made to the embodiments illustrated in the drawings, and specific language will be used to describe the same. It is nevertheless understood that no limitation to the scope of the disclosure is intended. Any alterations and further modifications to the described devices, systems, and methods, and any further application of the principles of the present disclosure are fully contemplated and included within the present disclosure as would normally occur to one skilled in the art to which the disclosure relates. For example, the present disclosure provides an ultrasound imaging system described in terms of cardiovascular imaging, however, it is understood that such description is not intended to be limited to this application. In some embodiments, the ultrasound imaging system includes an intravascular imaging system. The imaging system is equally well suited to any application requiring imaging within a small cavity. In particular, it is fully contemplated that the features, components, and/or steps described with respect to one embodiment may be combined with the features, components, and/or steps described with respect to other embodiments of the present disclosure. For the sake of brevity, however, the numerous iterations of these combinations will not be described separately.

There are primarily two types of catheters in common use today: solid-state and rotational. An exemplary solid-state catheter uses an array of transducers (typically 64) distributed around a circumference of the catheter and connected to an electronic multiplexer circuit. The multiplexer circuit selects transducers from the array for transmitting ultrasound signals and receiving reflected ultrasound signals. By stepping through a sequence of transmit-receive transducer pairs, the solid-state catheter can synthesize the effect of a mechanically scanned transducer element, but without moving parts. Since there is no rotating mechanical element, the transducer array can be placed in direct contact with blood and vessel tissue with minimal risk of vessel trauma, and the solid-state scanner can be wired directly to the imaging system with a simple electrical cable and a standard detachable electrical connector.

An exemplary rotational catheter includes a single transducer located at a tip of a flexible driveshaft that spins inside a sheath inserted into the vessel of interest. The transducer is typically oriented such that the ultrasound signals propagate generally perpendicular to an axis of the catheter. In the typical rotational catheter, a fluid-filled (e.g., saline-filled) sheath protects the vessel tissue from the spinning trans-

ducer and driveshaft while permitting ultrasound signals to freely propagate from the transducer into the tissue and back. As the driveshaft rotates (for example, at 30 revolutions per second), the transducer is periodically excited with a high voltage pulse to emit a short burst of ultrasound. The ultrasound signals are emitted from the transducer, through the fluid-filled sheath and sheath wall, in a direction generally perpendicular to an axis of rotation of the driveshaft. The same transducer then listens for returning ultrasound signals reflected from various tissue structures, and the imaging system assembles a two dimensional image of the vessel cross-section from a sequence of several hundred of these ultrasound pulse/echo acquisition sequences occurring during a single revolution of the transducer.

FIG. 1 is a schematic illustration of an ultrasound imaging system 100 according to various aspects of the present disclosure. In some embodiments, the ultrasound imaging system 100 includes an intravascular ultrasound imaging system (IVUS). The IVUS imaging system 100 includes an IVUS catheter 102 coupled by a patient interface module (PIM) 104 to an IVUS control system 106. The control system 106 is coupled to a monitor 108 that displays an IVUS image (such as an image generated by the IVUS system 100).

In some embodiments, the IVUS catheter 102 is a rotational IVUS catheter, which may be similar to a Revolution® Rotational IVUS Imaging Catheter available from Volcano Corporation and/or rotational IVUS catheters disclosed in U.S. Pat. Nos. 5,243,988 and 5,546,948, both of which are incorporated herein by reference in their entirety. The catheter 102 includes an elongated, flexible catheter sheath 110 (having a proximal end portion 114 and a distal end portion 116) shaped and configured for insertion into a lumen of a blood vessel (not shown). A longitudinal axis LA of the catheter 102 extends between the proximal end portion 114 and the distal end portion 116. The catheter 102 is flexible such that it can adapt to the curvature of the blood vessel during use. In that regard, the curved configuration illustrated in FIG. 1 is for exemplary purposes and in no way limits the manner in which the catheter 102 may curve in other embodiments. Generally, the catheter 102 may be configured to take on any desired straight or arcuate profile when in use.

A rotating imaging core 112 extends within the sheath 110. The imaging core 112 has a proximal end portion 118 disposed within the proximal end portion 114 of the sheath 110 and a distal end portion 120 disposed within the distal end portion 116 of the sheath 110. The distal end portion 116 of the sheath 110 and the distal end portion 120 of the imaging core 112 are inserted into the vessel of interest during operation of the IVUS imaging system 100. The usable length of the catheter 102 (for example, the portion that can be inserted into a patient, specifically the vessel of interest) can be any suitable length and can be varied depending upon the application. The proximal end portion 114 of the sheath 110 and the proximal end portion 118 of the imaging core 112 are connected to the interface module 104. The proximal end portions 114, 118 are fitted with a catheter hub 124 that is removably connected to the interface module 104. The catheter hub 124 facilitates and supports a rotational interface that provides electrical and mechanical coupling between the catheter 102 and the interface module 104.

The distal end portion 120 of the imaging core 112 includes a transducer assembly 122. The transducer assembly 122 is configured to be rotated (either by use of a motor or other rotary devices or methods) to obtain images of the

vessel. The transducer assembly **122** can be of any suitable type for visualizing a vessel and, in particular, a stenosis in a vessel. In the depicted embodiment, the transducer assembly **122** includes a piezoelectric micromachined ultrasonic transducer (“PMUT”) transducer and associated circuitry, such as an application-specific integrated circuit (ASIC). An exemplary PMUT used in IVUS catheters may include a polymer piezoelectric membrane, such as that disclosed in U.S. Pat. No. 6,641,540, hereby incorporated by reference in its entirety. The PMUT transducer can provide greater than 75% bandwidth for optimum resolution in a radial direction, and a spherically-focused aperture for optimum azimuthal and elevation resolution.

The transducer assembly **122** may also include a housing having the PMUT transducer and associated circuitry disposed therein, where the housing has an opening that ultrasound signals generated by the PMUT transducer travel through. Alternatively, the transducer assembly **122** includes a capacitive micromachined ultrasonic transducer (“CMUT”). In yet another alternative embodiment, the transducer assembly **122** includes an ultrasound transducer array (for example, arrays having 16, 32, 64, or 128 elements are utilized in some embodiments).

The rotation of the imaging core **112** within the sheath **110** is controlled by the interface module **104**, which provides user interface controls that can be manipulated by a user. The interface module **104** can receive, analyze, and/or display information received through the imaging core **112**. It will be appreciated that any suitable functionality, controls, information processing and analysis, and display can be incorporated into the interface module **104**. In an example, the interface module **104** receives data corresponding to ultrasound signals (echoes) detected by the imaging core **112** and forwards the received echo data to the control system **106**. In an example, the interface module **104** performs preliminary processing of the echo data prior to transmitting the echo data to the control system **106**. The interface module **104** may perform amplification, filtering, and/or aggregating of the echo data. The interface module **104** can also supply high- and low-voltage DC power to support operation of the catheter **102** including the circuitry within the transducer assembly **122**.

In some embodiments, wires associated with the IVUS imaging system **100** extend from the control system **106** to the interface module **104** such that signals from the control system **106** can be communicated to the interface module **104** and/or vice versa. In some embodiments, the control system **106** communicates wirelessly with the interface module **104**. Similarly, it is understood that, in some embodiments, wires associated with the IVUS imaging system **100** extend from the control system **106** to the monitor **108** such that signals from the control system **106** can be communicated to the monitor **108** and/or vice versa. In some embodiments, the control system **106** communicates wirelessly with the monitor **108**.

FIGS. 2-14 are diagrammatic fragmentary cross-sectional side views of an example ultrasound transducer **200** to illustrate an electrode assembly for the transducer **200**. The FIGS. 2-14 correspond to different stages of fabrication in accordance with various aspects of the present disclosure. FIGS. 2-14 have been simplified for the sake of clarity to better understand the inventive concepts of the present disclosure.

The ultrasound transducers **200** can each be included in the IVUS imaging system **100** of FIG. 1, for example in the transducer assembly **122**. The ultrasonic transducer **200** has a small size and achieves a high resolution, so that it is well

suited for intravascular imaging. In some embodiments, the ultrasonic transducer **200** has a size on the order of tens or hundreds of microns, can operate in a frequency range between about 1 mega-Hertz (MHz) to about 135 MHz, and can provide sub 50 micron resolution while providing depth penetration of at least 10 millimeters (mm). Furthermore, the ultrasonic transducer **200** is also shaped in a manner to allow a developer to define a target focus area based on a deflection depth of a transducer aperture, thereby generating an image that is useful for defining vessel morphology, beyond the surface characteristics. The various aspects of the ultrasound transducer **200** and its fabrication are discussed in greater detail below.

In the depicted embodiment, the ultrasound transducer **200** is a piezoelectric micromachined ultrasound transducer (PMUT). In other embodiments, the transducer **200** may include an alternative type of transducer. Additional features can be added in the ultrasound transducer **200**, and some of the features described below can be replaced or eliminated for additional embodiments of the ultrasound transducer **200**.

As is shown in FIG. 2, the transducer **200** includes a substrate **210**. The substrate **210** has a surface **212** and a surface **214** that is opposite the surface **212**. The surface **212** may also be referred to as a front surface or a front side, and the surface **214** may also be referred to as a back surface or a back side. In the depicted embodiment, the substrate **210** is a silicon microelectromechanical system (MEMS) substrate. The substrate **210** includes another suitable material depending on design requirements of the PMUT transducer **200** in alternative embodiments. In the illustrated embodiments, the substrate **210** is a “lightly-doped silicon substrate.” In other words, the substrate **210** comes from a silicon wafer that is lightly doped with a dopant and as a result has a resistivity in a range from about 1 ohms/cm to about 1000 ohms/cm. One benefit of the “lightly-doped silicon substrate” **210** is that it is relatively inexpensive, for example in comparison with pure silicon or undoped silicon substrates. Of course, it is understood that in alternative embodiments where cost is not as important of a concern, pure silicon or undoped silicon substrates may also be used.

The substrate **210** may also include various layers that are not separately depicted and that can combine to form electronic circuitry, which may include various microelectronic elements. These microelectronic elements may include: transistors (for example, metal oxide semiconductor field effect transistors (MOSFET), complementary metal oxide semiconductor (CMOS) transistors, bipolar junction transistors (BJT), high voltage transistors, high frequency transistors, p-channel and/or n-channel field effect transistors (PFETs/NFETs)); resistors; diodes; capacitors; inductors; fuses; and/or other suitable elements. The various layers may include high-k dielectric layers, gate layers, hard mask layers, interfacial layers, capping layers, diffusion/barrier layers, dielectric layers, conductive layers, other suitable layers, or combinations thereof. The microelectronic elements could be interconnected to one another to form a portion of an integrated circuit, such as a logic device, memory device (for example, a static random access memory (SRAM)), radio frequency (RF) device, input/output (I/O) device, system-on-chip (SoC) device, other suitable types of devices, or combinations thereof.

An initial thickness **220** of the substrate **210** is measured between the surface **212** and the surface **214**. In some embodiments, an initial thickness **220** is in a range from about 200 microns (um) to about 1000 um.

A dielectric layer **230** is formed over the surface **212** and **214** of the substrate **210**. The dielectric layer **230** may be formed by a suitable deposition process known in the art, such as thermal oxidation, low temperature oxide deposition, chemical vapor deposition (CVD), physical vapor deposition (PVD), atomic layer deposition (ALD), or combinations thereof. The dielectric layer **230** may contain an oxide material or a nitride material, for example silicon oxide, phosphosilicate glass (PSG), silicon nitride, silicon oxynitride or combination thereof. The dielectric layer **230** provides a support surface for the layers to be formed thereon. The dielectric layer **230** also provides electrical insulation. In more detail, the substrate **210** in the illustrated embodiments is a "lightly-doped silicon substrate" that is relatively conductive, as discussed above. This relatively high conductivity of the substrate **210** may pose a problem when the transducer **200** is pulsed with a relatively high voltage, for example with an excitation voltage of about 60 volts to about 200 volts DC. This means that it is undesirable for a bottom electrode (discussed below in more detail) of the transducer **200** to come into direct contact with the silicon substrate **210**. According to the various aspects of the present disclosure, the dielectric layer **230** helps insulate the bottom electrode of the transducer **230** from the relatively conductive surface of the silicon substrate **210**.

A conductive layer **240** (i.e., the bottom electrode) is then formed over the dielectric layer **230**. The conductive layer **240** may be formed by a suitable deposition process such as sputtering, evaporation, CVD, PVD, ALD, etc. In the illustrated embodiment, the conductive layer **240** includes a metal or multiple metals material. For example, the metal or multiple metals material may include Titanium, Chromium, Gold, Aluminum, Platinum or combinations thereof.

Referring now to FIG. 3, the conductive layer **240** is patterned using techniques in a lift-off or photolithography process. Unwanted portions of the conductive layer **240** are removed as a part of the process. In some embodiments, the conductive layer can be deposited with a shadow mask to create a pattern.

A piezoelectric film **250** is then formed over the dielectric layer **230** and the conductive layer **240**. In various embodiments, the piezoelectric film **250** may include piezoelectric materials such as polyvinylidene fluoride (PVDF) or its co-polymers, polyvinylidene fluoride-trifluoroethylene (PVDF-TrFE), or polyvinylidene fluoride-tetrafluoroethylene (PVDF-TFE). Alternatively, polymers such as PVDF-CTFE and PVDF-CFE or sol-gel formed piezoelectric material may be used. In the illustrated embodiment, the piezoelectric material used in the piezoelectric film **250** contains PVDF-TrFE.

The piezoelectric film **250** is patterned to achieve a desired shape, for example the shapes shown in FIG. 3. Unwanted portions of the piezoelectric film **250** are removed in the patterning process. As a result, portions of the dielectric layer **230** and the conductive layer **240** are exposed. For reasons of simplicity, FIG. 3 only illustrates the piezoelectric film **250** after it has been patterned.

In the present embodiment, the piezoelectric film **250** is etched in a manner to form a chamfer to allow deposition for a top electrode to be formed. The chamfer may manifest itself as the trapezoidal sidewall shown in the cross-sectional view of FIG. 3. The chamfer allows a conductive layer **270** to be deposited over the piezoelectric film **250** with a lower likelihood of discontinuity. It is also understood that an adhesion-promoting layer (not illustrated herein) may be formed between the piezoelectric film **250** and the conductive layer **240** in some embodiments, so that the piezoelec-

tric film **250** is more likely to stick to the conductive layer **240**. One embodiment of the adhesion-promoting layer is discussed in detail in U.S. Provisional Application 61/745,212, titled "Methods and Apparatus for Focusing Miniature Ultrasound Transducers" to Dylan Van Hoven, filed on Dec. 21, 2012, the contents of which are incorporated by reference herein in its entirety.

Referring now to FIG. 4, a conductive layer **270** (i.e., the top electrode) is formed over the piezoelectric film **250** using a suitable deposition process known in the art. In the illustrated embodiment, the conductive layer **270** includes a metal or multiple metals material, such as Titanium, Chromium, Gold, Aluminum, Platinum or combinations thereof. After its deposition, the conductive layer **270** is patterned using techniques in a photolithography process. Unwanted portions of the conductive layer **270** are removed as a part of the photolithography process. For reasons of simplicity, FIG. 4 only illustrates the conductive layer **270** after it has been patterned.

The conductive layers **240** and **270** and the piezoelectric layer **250** (and the adhesion-promoting layer in embodiments where it is used) may collectively be considered a transducer membrane. It is understood that pad metals may also be formed to establish electrical connections on the conductive layers **240** and/or **270**, but these pad metals are not illustrated herein for reasons of simplicity.

A potential problem associated with the deposition of the conductive layer **270** (i.e., top electrode) is that there may be a discontinuity in the deposited conductive layer **270**. For example, referring now to FIG. 5, an example discontinuity **275** in the conductive layer **270** is shown. As discussed above, the piezoelectric film **250** is formed to have a chamfer partly to avoid such discontinuity **275**. Nevertheless, limitations in the metal deposition process and other imperfections may still lead to one or more discontinuities **275**. The discontinuity **275** may cause an electrical open condition. In other words, the conductive layer **270** may not be electrically connected to intended external devices due to the discontinuity **275**. This may prevent full electrical access to the transducer **200**.

According to various aspects of the present disclosure, the problems caused by the discontinuity **275** may be resolved using a step metal element. Step metal can be formed by a suitable deposition process such as sputtering, evaporation, CVD, PVD, ALD, etc., followed by lift-off or photolithography pattern process. The formation of the step metal is discussed below with reference to FIGS. 6-9.

Referring to FIG. 6, a photoresist material **280** is coated over the transducer **200**, including over the conductive layer **270**.

Referring now to FIG. 7, an opening **285** is formed in the photoresist material **280**. The opening **285** is configured to be wide enough to expose a sidewall portion of the conductive layer **270** (i.e., the portion of the top electrode formed on the sidewall of the piezoelectric film **250**). If the discontinuity **275** exists, the opening **285** exposes the discontinuity **275** as well.

Referring now to FIG. 8, a step metal element **290** is formed in the opening **285**. The step metal element **290** has a substantially similar material composition as the conductive layer **270**. In other words, in the illustrated embodiment, the step metal element **290** includes one or more metals such as Titanium, Chromium, Gold, Aluminum, or combinations thereof. The step metal element **290** is formed to have a vertical dimension **295** and a lateral or horizontal dimension **296**. In some embodiments, the vertical dimension **295** is in

a range from about 0.5 um to about 2 um, and the lateral dimension 296 is in a range from about 30 um to about 100 um.

Referring now to FIG. 9, the photoresist material 280 is removed, for example through a photoresist stripping process. The step metal element 290 covers over the sidewall of the conductive layer 270 (top electrode). It can be seen that if any discontinuities such as the discontinuity 275 exist in the conductive layer 270, the step metal 290 would “cover up” the discontinuities. Stated differently, the step metal 290 in effect serves as a bridge for segments of the conductive layer 270 separated by the discontinuities. Consequently, electrical continuity is maintained throughout the conductive layer 270 due to the step metal 290.

It is understood that the step metal element 290 is formed on the sidewall of the conductive layer 270 because the sidewall of the conductive layer 270 has been identified as a segment of the conductive layer 270 where discontinuities are likely to occur. However, in alternative embodiments, the step metal element 290 (or other elements similar thereto) may be configured to form over other regions of the conductive layer 270, if those regions are also identified as likely to include discontinuities.

In addition to (or instead of) the step metal element 290, the present disclosure may also form a metal via to address the discontinuity issue discussed above, as discussed below in more detail with reference to FIGS. 10-14. For reasons of consistency and clarity, the same or similar components appearing in FIGS. 2-9 and 10-14 are labeled the same.

Referring now to FIG. 10, the dielectric layer 230 (discussed above with reference to FIG. 2) is formed over the substrate 210. The conductive layer 240 (discussed above with reference to FIG. 2) is then formed over the dielectric layer 230.

Referring now to FIG. 11, the conductive layer 240 is patterned into separate segments: a segment 240 and a segment 245. The segment 240 serves as the bottom electrode of the transducer 200 and will hereinafter be referred to as the bottom electrode 240A. The segment 245 serves as a bottom portion of the top electrode of the transducer 200 and will hereinafter be referred to as the top electrode segment 245. The piezoelectric film 250 is then formed over a portion of the bottom electrode 240A and over a portion of the top electrode segment 245. As discussed above, the piezoelectric film 250 may contain a PVDF material or another suitable polymer material.

Referring now to FIG. 12, the piezoelectric film 250 is patterned with a via through to the segment 245. The via separates the piezoelectric film into two separate components 250A and 250B in this cross-sectional view. In some embodiments, the component 250A is formed over the top electrode segment 245, and the component 250B is formed over the bottom electrode 240A. However, this may not necessarily be the case in different embodiments. As discussed above, to alleviate electrode discontinuity concerns, both the components 250A and 250B are formed to have a chamfer.

Referring now to FIG. 13, a conductive layer 270 is formed over the piezoelectric components 250A and 250B. The conductive layer 270 contains metal or multiple metals material, such as Titanium, Chromium, Gold, Aluminum, Platinum or combinations thereof. The conductive layer 270 serves as the top portion of the top electrode of the transducer 200 and will hereinafter be referred to as the top electrode segment 270.

As is shown in FIG. 13, a portion 270A of the top electrode segment 270 is formed on the top electrode

segment 245. This portion 270A may be referred to as a via 270A. The via 270A in effect increases the contact surface between the top electrode segment 270 (i.e., the top part of the top electrode) and the top electrode segment 245 (i.e., the bottom part of the top electrode). As a result, discontinuity is less likely to appear in the top electrode.

Additional processing steps may be performed to complete the fabrication of the transducer 200. For example, an opening or well may be etched into the substrate 210 from the back side 214. The opening or well may be filled with a backing material such as epoxy. The transducer membrane may also be deflected (for example by application of air pressure) into an arcuate shape such as illustrated in FIG. 14. These additional process steps are discussed in more detail in U.S. Provisional Application 61/745,212, titled “Methods and Apparatus for Focusing Miniature Ultrasound Transducers” to Dylan Van Hoven, filed on Dec. 21, 2012, the content of which is incorporated by reference herein in its entirety.

FIG. 15 is a simplified diagrammatic top view of a portion of the transducer 200 that illustrates an embodiment of the step metal element 290 discussed above with reference to FIGS. 8-9. For reasons of consistency and clarity, similar components are labeled the same in FIGS. 8-9 and 15. As discussed above, the piezoelectric film 250 is formed to have a chamfer, which is labeled with the reference numeral 300 herein to allow for better electrode continuity. A segment of the top electrode 270 spans over the chamfer 300. The step metal element 290 is formed on the chamfer 300 to ensure electrical continuity of the top electrode 270.

FIG. 16A is a simplified diagrammatic top view of a portion of the transducer 200 that illustrates an embodiment of the via 270A discussed above with reference to FIG. 13. For reasons of consistency and clarity, similar components are labeled the same in FIGS. 13 and 16A. The cross-sectional view of FIG. 13 is obtained by taking a cross-section from point A to A' in the top view of FIG. 16A. As is shown, the via 270A effectively increases a contact surface area between a top segment of the top electrode 270 and a bottom segment of the top electrode (not visible in FIG. 16A), thereby reducing risks of discontinuity.

It is also understood that in some embodiments, both the step metal element 290 and the via 270A may be implemented in a transducer 200 to further improve electrode continuity.

FIGS. 16B-16E illustrate diagrammatic top views of alternative embodiments of the via discussed above. For example, the embodiment shown in FIG. 16B illustrates a via serpentine big patch. The embodiment shown in FIG. 16C illustrates a via serpentine small patch. The embodiment shown in FIG. 16D illustrates a via fatty big patch. The embodiment shown in FIG. 16E illustrates a via fatty small patch. Regardless of the embodiment, however, it is understood that the big enhances the contact surface area for the top electrode and alleviates electrode discontinuity concerns.

FIG. 17 is a flowchart of a method 500 for fabricating an ultrasound transducer according to various aspects of the present disclosure. The method includes a step 510, in which a substrate is provided. The substrate has a first side and a second side opposite the first side. In some embodiments, the substrate contains silicon.

The method 500 includes a step 520, in which a dielectric layer is formed over the first side of the substrate. In some embodiments, the dielectric layer may include silicon oxide, silicon nitride, or silicon oxynitride.

The method 500 includes a step 530, in which a bottom electrode is formed over the entire surface of the substrate.

The bottom electrode may contain metal or multiple metals material, such as Titanium, Chromium, Gold, Aluminum, or combinations thereof. The bottom electrode may be patterned.

The method 500 includes a step 540, in which a piezoelectric element is formed over the bottom electrode. The piezoelectric element has a chamfered sidewall. In some embodiments, the piezoelectric element contains polyvinylidene fluoride (PVDF), polyvinylidene fluoride-trifluoroethylene (PVDF-TrFE), polyvinylidene fluoride-tetrafluoroethylene (PVDF-TFE), or sol-gel formed piezoelectric materials.

The method 500 includes a step 550, in which a top electrode is formed over the piezoelectric element. The top electrode may contain metal or multiple metals material, such as Titanium, Chromium, Gold, Aluminum, or combinations thereof. In some embodiments, the top electrode is formed to include: a top segment disposed over a top surface of the piezoelectric element; a bottom segment disposed over the substrate, the bottom segment being non-planar with the top segment; and a via coupling the top segment to the bottom segment. The via may be disposed directly on the bottom segment. The via may include a recessed portion of the top electrode.

The method 500 includes a step 560, in which a step metal element is formed over a portion of the top electrode on the chamfered sidewall of the piezoelectric element. The step metal element and the top electrode have substantially similar material compositions.

The method 500 includes a step 570, in which a well is formed in the substrate from the second side. The well may be formed by an etching process. In some embodiments, the well is formed so that the etching stops at the dielectric layer. In other embodiments, the well is formed so that the dielectric layer is also etched, and the etching stops at the bottom surface of the substrate.

The method 500 includes a step 580, in which the well is filled with a backing material. In some embodiments, the backing material includes an epoxy material.

The method 500 includes a step 590, in which the top electrode, the piezoelectric element, and the bottom electrode—collectively constituting a transducer membrane—is deflected so that a portion of the transducer membrane disposed over the well has an arcuate shape.

It is understood that some of the steps discussed above may be performed in different sequences. It is also understood that additional fabrication steps may be performed to complete the fabrication of the transducer. However, these additional fabrication steps are not discussed herein for reasons of simplicity.

Persons skilled in the art will recognize that the apparatus, systems, and methods described above can be modified in various ways. Accordingly, persons of ordinary skill in the art will appreciate that the embodiments encompassed by the present disclosure are not limited to the particular exemplary embodiments described above. In that regard, although illustrative embodiments have been shown and described, a wide range of modification, change, and substitution is contemplated in the foregoing disclosure. It is understood that such variations may be made to the foregoing without departing from the scope of the present disclosure. Accordingly, it is appropriate that the appended claims be construed broadly and in a manner consistent with the present disclosure.

What is claimed is:

1. A micromachined ultrasound transducer, comprising: a substrate;

a bottom electrode disposed over the substrate;  
a piezoelectric element disposed over the bottom electrode;

a top electrode disposed over at least a top surface and a sidewall of the piezoelectric element; and

a step metal element disposed over a sidewall of the top electrode.

2. The micromachined ultrasound transducer of claim 1, wherein the step metal element and the top electrode have substantially similar material compositions.

3. The micromachined ultrasound transducer of claim 1, wherein the piezoelectric element has a chamfer.

4. The micromachined ultrasound transducer of claim 1, further comprising: a well disposed in the substrate.

5. The micromachined ultrasound transducer of claim 4, wherein the well is at least partially filled with a backing material.

6. The micromachined ultrasound transducer of claim 4, wherein portions of the top electrode, the bottom electrode, and the piezoelectric element disposed over the well each have an arcuate shape.

7. The micromachined ultrasound transducer of claim 1, further comprising a dielectric layer disposed between the substrate and at least the bottom electrode.

8. The micromachined ultrasound transducer of claim 1, wherein the piezoelectric element contains polyvinylidene fluoride (PVDF), polyvinylidene fluoride-trifluoroethylene (PVDF-TrFE), or polyvinylidene fluoride-tetrafluoroethylene (PVDF-TFE).

9. The micromachined ultrasound transducer of claim 1, wherein the top electrode includes:

a top segment disposed over the top surface of the piezoelectric element;

a bottom segment disposed over the substrate, the bottom segment being non-planar with the top segment; and

a via coupling the top segment to the bottom segment.

10. The micromachined ultrasound transducer of claim 9, wherein the via is disposed directly on the bottom segment.

11. The micromachined ultrasound transducer of claim 9, wherein the via includes a recessed portion of the top electrode.

12. An ultrasound system, comprising:

an imaging component that includes a flexible elongate member and a piezoelectric micromachined ultrasound transducer (PMUT) coupled to a distal end of the elongate member, wherein the PMUT includes:

a substrate having a front surface and a back surface opposite the first surface;

a well located in the substrate, the well extending from the back surface of the substrate to, but not beyond, the front surface of the substrate, wherein the well is at least partially filled with a backing material;

a transducer membrane disposed over the well, wherein the transducer member includes a piezoelectric element disposed between a top electrode and a bottom electrode; and

a step metal element disposed over a sidewall of the piezoelectric element;

an interface module configured to engage with a proximal end of the elongate member; and

an ultrasound processing component in communication with the interface module.

13. The ultrasound system of claim 12, wherein the step metal element and the top electrode have substantially similar material compositions.

14. The ultrasound system of claim 12, wherein the piezoelectric element has a chamfer.

15. The ultrasound system of claim 12, wherein portions of the transducer membrane disposed over the well has an arcuate profile.

16. The ultrasound system of claim 12, further comprising a dielectric layer disposed between the substrate and the bottom electrode. 5

17. The ultrasound system of claim 12, wherein the piezoelectric element contains polyvinylidene fluoride (PVDF), polyvinylidene fluoride-trifluoroethylene (PVDF-TrFE), polyvinylidene fluoride-tetrafluoroethylene (PVDF-TFE) or sol-gel formed piezoelectric materials. 10

18. The ultrasound system of claim 12, wherein the top electrode includes:

a top segment disposed over a top surface of the piezoelectric element; 15

a bottom segment disposed over the substrate, the bottom segment being non-planar with the top segment; and a via coupling the top segment to the bottom segment.

19. The ultrasound system of claim 18, wherein the via is disposed directly on the bottom segment. 20

20. The ultrasound system of claim 18, wherein the via includes a recessed portion of the top electrode.

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摘要(译)

本公开提供了一种制造超声换能器的方法。提供具有第一侧和与第一侧相对的第二侧的基板。在衬底的第一侧上形成底部电极。在底部电极上形成压电元件。压电元件具有倒角侧壁。在压电元件上形成顶部电极。在靠近压电元件的倒角侧壁顶部电极的一部分上形成台阶金属元件。

