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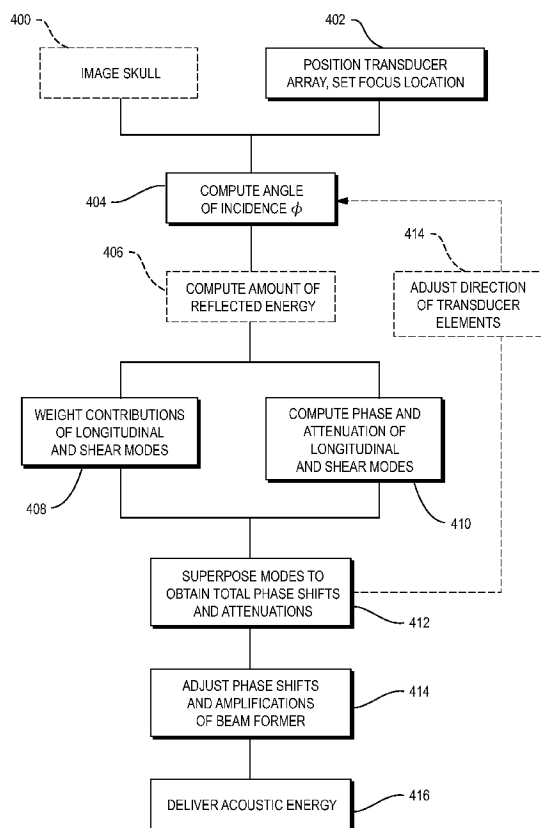


FIG. 4

(57) Abstract: Systems and methods for focusing ultrasound through the skull into the brain for diagnostic or therapeutic purposes may be improved by utilizing both longitudinal and shear waves. The relative contribution of the two modes may be determined based on the angle of incidence.



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## MULTIMODE ULTRASOUND FOCUSING FOR MEDICAL APPLICATIONS

### RELATED APPLICATIONS

[0001] This application claims priority to and the benefit of co-pending U.S. Patent Application Serial No. 12/425,698, filed on April 17, 2009, the entire disclosure of which is incorporated by reference herein.

### BACKGROUND

5 [0002] Ultrasound penetrates well through soft tissues and, due to its short wavelengths, can be focused to spots with dimensions of a few millimeters. As a consequence of these properties, ultrasound can and has been used for a variety of diagnostic and therapeutic medical purposes, including ultrasound imaging and non-invasive surgery of many parts of the body. For example, by heating diseased (e.g., cancerous) tissue using ultrasound, it is often possible  
10 to ablate the diseased portions without causing significant damage to surrounding healthy tissue.

[0003] The noninvasive nature of ultrasound surgery is particularly appealing for the treatment of brain tumors. Moreover, coherent, non-invasive focusing of ultrasound through the human skull has been considered as a tool for targeted drug delivery to the brain, improved  
15 thrombolytic stroke treatment, blood flow imaging, the detection of internal bleeding, and tomographic brain imaging. However, the human skull has been a barrier to the clinical realization of many of these applications. Impediments to transcranial procedures include strong attenuation and the distortions caused by irregularities in the skull's shape, density, and sound speed, which contribute toward destroying the ultrasound focus and/or decreasing the  
20 ability to spatially register received diagnostic information.

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[0004] Several minimally invasive or noninvasive aberration-correction techniques for transskull focusing overcome the focusing difficulties at least partially. Minimally invasive approaches may use receiving probes designed for catheter insertion into the brain to measure the amplitude and phase distortion caused by the skull, and then correct the ultrasound beam using an array of transducers. An alternative, completely noninvasive approach uses X-ray computed tomography (CT) images, rather than receiving probes, to predict the wave distortion caused by the skull.

[0005] Noninvasive focusing with a therapeutic array has been demonstrated at frequencies of about 2 MHz with a longitudinal wave propagation model. The velocity of these waves is approximately 2700 m/s in the skull, and about 1500 m/s in water and soft tissue. Due to this ratio, sound that arrives at the skull under an incident angle above about 30°, the critical angle, is reflected. The amplitude of the focus therefore drops when the focus is directed close to the skull surface. As shown in FIGS. 1A and 1B, a treatment envelope 100 is defined as the region accessible to ultrasound from a sufficient number of transducers 102 to enable treatment.

Whereas the effect of reflection is minimal when the target area is deep within the brain (FIG. 1A), since it lies inside the treatment envelope 100, reflection becomes problematic when the target is outside the envelope 100 (FIG. 1B). In the latter case, only a small number of transducers can reach the target area without reflection, and the closer the target is to the skull, the more transducers will be completely excluded from treatment due to reflection.

[0006] The treatment envelope 100 can be extended by reducing the frequency, e.g., to 0.2 MHz, and employing shear waves. Shear waves are largely absorbed in the skull at frequencies between 0.5 MHz and 4 MHz; at lower frequencies, however, their absorption is reduced to about that of longitudinal modes. Moreover, at 0.2 MHz, the sound velocity of shear waves in

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water (~1500 m/s) is comparable to that in the skull (~1400 m/s), thereby essentially eliminating the problem of reflection above a critical angle.

[0007] Previous methods of utilizing shear waves have calculated the phase shifts and amplitude attenuation associated with an originally longitudinal mode that is converted to a shear mode upon encountering the skull, and converted back to a longitudinal mode when entering the soft tissue of the brain. This approach is limited to large incidence angles at which no longitudinal mode is excited in the skull, or is otherwise inaccurate. In order to optimize focusing properties and maximize the amount of energy available in the focus, the coexistence of longitudinal and transverse modes ought to be taken into consideration.

## SUMMARY

[0008] The present invention provides, in various embodiments, methods and apparatus for ultrasound focusing utilizing both longitudinal and shear modes. While developed mostly for non-invasive brain surgery and imaging, the approach of the invention may also be applied to other parts of the body requiring the penetration of ultrasound through a bone or cartilage interface. In transcranial applications, a transducer array emits longitudinal sound waves, which split into longitudinal and transverse components when entering the skull. The ratio of these two components depends on the frequency and the incidence angle. At the interface of the skull with the soft brain tissue, the transverse wave, or shear wave, is converted back to a longitudinal wave, or pressure wave, and both longitudinal components contribute to the ultrasound focus in the brain. Methods embodying the invention compute and correct for a phase shift and/or amplitude attenuation experienced by the waves during their propagation through the skull and brain.

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[0009] In a first aspect, the invention provides, in various embodiments, a method for delivering ultrasound waves to a target through at least one tissue layer, which defines a first and a second interface. The waves have both a shear component and a longitudinal component through the first tissue layer. The method involves weighting energy contributions from the shear component and the longitudinal component based on an incident angle of the waves at the first interface and, optionally, further based on a frequency of the waves and/or on an acoustic response of the first layer. The method may also include the computation of a coefficient for the reflection of the waves at the first interface of the first tissue layer. Furthermore, the method includes the steps of computing phase shifts, and optionally attenuation coefficients, associated with the shear component and the longitudinal component, and compensating for the phase shifts and/or attenuations based on the weightings when delivering the ultrasound waves. The compensation step may, in some embodiments, also account for the geometry, thickness, density, and/or acoustic response of the first tissue layer. This first tissue layer corresponds in certain embodiments to a patient's skull. The method may involve providing a model of the first tissue layer (and any additional tissue layers), on which the compensation step may be based. Such a model may be obtained using computer tomography or magnetic resonance imaging. In certain embodiments, the model contains locally parallel layers.

[0010] In some embodiments, the weighting of energy contributions from the shear and longitudinal components is accomplished by determining a threshold angle, and setting the contribution from the shear component to zero for incident angles below the threshold angle and the contribution from the longitudinal component to zero for incident angles above or at the threshold angle. Alternatively, two threshold angles may be determined. In these alternative embodiments, the contribution from the shear mode is set to zero for incident angles below the smaller of the two threshold angles, and the contribution of the longitudinal mode is set to zero

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for angles above the larger of the two threshold angles. For incident angles between the threshold angles, the energy contributions of the two modes are computed by (e.g., linear) interpolation. In some embodiments, the weighting step is based on a relationship between energy contributions from the shear component and the longitudinal component that has been  
5 determined empirically over a range of incidence angles.

**[0011]** In certain embodiments, the ultrasonic wave incident upon the first interface is purely longitudinal, and excites a longitudinal and a shear component in the first tissue layer. The shear component, in turn, may excite a longitudinal wave at the second interface.

**[0012]** In various embodiments, the ultrasound waves are delivered by a phased array of  
10 transducers, whose outputs are adjusted according to the computed phase shifts and, if applicable, attenuations in the compensation step. The waves may have a frequency in the range from 100 kHz to 400 kHz.

**[0013]** In a second aspect, the invention provides, in various embodiments, a system for delivering multimode ultrasound waves to a target located inside an object that contains at least  
15 a first tissue layer defining a first and a second interface. The system includes a phased array of transducers arranged around the object, a controller computing phase shift compensations for the transducers, and a beam former in communication with the phased array of transducers for adjusting outputs of the transducers in accordance with the phase shift compensations computed by the controller. The controller receives data about the object and its location  
20 relative to the transducers, as well as about the location of the target, and uses this data to compute an incident angle at which waves emanating from the transducer arrive at the first interface. Based on the computed incidence angle, the controller computes weightings of the energy contributions from the shear component and the longitudinal component. It further

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calculates phase shifts for the two wave components, based on the incident angle and the data about the object, and uses these phase shifts in determining the phase shift compensations.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

[0014] The foregoing discussion and the following detailed description of embodiments of the invention can more readily be understood in conjunction with the accompanying drawings wherein:

[0015] FIGS. 1A and 1B are schematic diagrams illustrating ultrasound wave focusing for foci in the center and near the periphery of the brain, respectively;

[0016] FIG. 2 is a schematic diagram of a system for focusing ultrasound in accordance with various embodiments of the invention;

[0017] FIG. 3A is a computer tomography image of a skull section, and FIG. 3B is a schematic diagram of an enlarged view of the skull section illustrating acoustic wave propagation through the skull;

[0018] FIG. 4 is a flow chart illustrating a method for ultrasound focusing using longitudinal and transverse modes in accordance with various embodiments of the invention;

[0019] FIGS. 5A–5C are flow charts detailing the weighting step of FIG. 4 in accordance with various embodiments of the invention;

[0020] FIG. 6 is a graph illustrating an interpolation for the energy distribution between longitudinal and transverse waves in accordance with one embodiment of the invention; and

[0021] FIG. 7 is a graph showing empirical data for the energy distribution between longitudinal and transverse waves which may be used in accordance with one embodiment of the invention.



**DETAILED DESCRIPTION**

[0022] Ultrasound energy may be transmitted into a patient, for various medical purposes, using arrays of radiating transducer elements. The amplitudes of the waves emanating from the elements can affect how much energy penetrates the patient, and the relative phases and  
5 amplitudes of the waves can be controlled to focus the energy into a desired region, e.g., into a tumor. While penetrating the patient, the waves typically encounter several layers of tissues, e.g., bone, muscle, or fat, whose density and structure, and, consequently, ultrasound propagation properties, differ. Due to inhomogeneities and anisotropies in the tissues, the wave fronts are often distorted. Moreover, signals from different transducer elements may encounter  
10 different thicknesses and contours of materials, and possibly air-filled or liquid-filled pockets between transducer elements and the region to be imaged or treated, resulting in different phase shifts and attenuations. Compensating for these effects, by appropriate phase shifts and amplification factors imposed on the transducer elements, avoids deterioration of focusing properties.

15 [0023] FIG. 2 illustrates an exemplary ultrasound therapy system 200 for focusing ultrasound into a patient's brain through the skull S. The system 200 includes a phased array 202 of transducer elements 204, a beam former 206 driving the phased array, a controller 208 in communication with the beamformer, and a frequency generator 210 providing an input electronic signal for the beamformer. The system may further include an imager 212, such as a  
20 magnetic resonance imaging (MRI) device or a computer tomography (CT) device, for determining the structure of the patient's skull and brain.

[0024] The array 202 may comprise a single row or a matrix of transducer elements 204. In alternative embodiments, the transducer elements 204 may be arranged in a non-coordinated fashion. The array 202 may have a curved (e.g., spherical or parabolic) shape suitable for

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placing it on the surface of the skull S, or may include one or more planar or otherwise shaped sections. Its dimensions may vary, depending on the application, between millimeters and tens of centimeters. The transducer elements 204 of the array 202 may be piezoelectric ceramic elements, and may be mounted in silicone rubber or any other material suitable for damping the mechanical coupling between the elements 204. Piezo-composite materials, or generally any materials capable of converting electrical energy to acoustic energy, may also be used. To assure maximum power transfer to the transducer elements 204, the elements may be configured for electrical resonance at 50  $\Omega$ , matching input connector impedance.

**[0025]** The array 202 is coupled to the beamformer 206, which drives the individual transducer elements so that they collectively produce a focused ultrasonic beam or field. For n transducer elements, the beamformer 206 may contain n pairs of an amplifier 212 and a phase delay circuit 214, each pair driving one of the transducer elements. The beamformer 206 receives a radio frequency (RF) input signal, typically in the range from 0.1 MHz to 0.4 MHz, from frequency generator 210, which may, for example, be a Model DS345 generator available from Stanford Research Systems. The input signal may be split into n channels for the n amplifiers and delay circuits 212, 214 of the beamformer 206. In some embodiments, the frequency generator 210 is integrated with the beamformer 206. The radio frequency generator 210 and the beamformer 206 are configured to drive the individual transducer elements 204 of the array 206 at the same frequency, but at different phases and different amplitudes.

**[0026]** The amplification or attenuation factors and the phase shift  $\alpha$  imposed by the beamformer 206 serve to transmit and focus ultrasonic energy through the patient's skull S into a selected region of the patient's brain, and account for wave distortions induced in the skull and soft brain tissue. They are computed in the controller 208, which may provide the computational functions through software, hardware, firmware, hardwiring, or any combination

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thereof. For example, the controller 208 may utilize a general purpose, or special purpose, digital data processor programmed with software in a conventional manner in order to determine the phase shifts and amplification factors. In certain embodiments, the computation is based on detailed information about the structure, thickness, density, etc. of the skull. Such information may be obtained from the imager 212. Image acquisition may be three-dimensional or, alternatively, the imager 212 may provide a set of two-dimensional images suitable for constructing a three-dimensional image of the skull and brain from which thicknesses and densities can be inferred. Image-manipulation functionality may be implemented in the imager 212, in the controller 208, or in a separate device.

**[0027]** System 200 may be modified in many ways within the scope of the invention. For example, for diagnostic applications, the system may further include a detector device that measures transmitted or reflected ultrasound, and which may provide the signals it receives to the driver 208 for further processing. The reflection and transmission signals may also be used as feedback for the phase and amplitude adjustments of the beamformer 206. The system may contain a positioner for arresting the array 202 of transducer elements 204 with respect to the patient's skull S. In order to apply ultrasound therapy to body parts other than the brain, the transducer array 202 may take a different, e.g., a cylindrical, shape. In some embodiments, the transducer elements 204 are mounted movably and rotatably, providing mechanical degrees of freedom that can be exploited to improve focusing properties. Such movable transducers may be adjusted by conventional actuators, which may be driven by a component of controller 210 or by a separate mechanical controller.

**[0028]** Unlike many previous systems for focusing ultrasound through the skull, embodiments of the present invention utilize both longitudinal and shear waves. While water and soft brain tissue, for all practical purposes, only support longitudinal waves, shear waves

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can be excited in the much denser skull bone by longitudinal waves incident upon the skull surface. FIG. 3A shows a CT image of a skull section 300, in which the brightness level correlates with material density. The propagation of an ultrasound beam through the skull is illustrated schematically in FIG. 3B, which shows an enlarged section of the skull 300. A  
5 purely longitudinal wave  $L_I$  falling onto the outer skull surface 302 splits into a shear component  $S_{II}$  and a longitudinal component  $L_{II}$ . The relative contributions of these two components depend largely on the incidence angle. For wave frequencies between 100 kHz and 400 kHz, at angles below  $20^\circ$ , most of the energy of waves propagates in the longitudinal mode. At angles above  $40^\circ$ , the shear mode is predominant. In the intermediate regime,  
10 longitudinal and transverse modes co-exist. In general, part of the incident acoustic energy may be reflected (not shown). The remaining energy, which enters the skull, is partially absorbed, and partially propagated through the skull, depending on the frequency of the waves. For example, at frequencies above 500 kHz, most of the energy contained in the shear mode is absorbed and heats the skull. At frequencies between 100 kHz and 400 kHz, however, a  
15 significant fraction of the shear energy exits the skull at the interface 304 with the soft brain tissue, where it is transformed back into a longitudinal wave  $L_{III S}$ . The longitudinal wave  $L_{II}$  likewise penetrates the bone at such frequencies, and enters into the brain tissue as a longitudinal wave  $L_{III L}$ . The two components propagate through the skull 300 under different angles due to their different propagation velocities, and, consequently, enter the brain at  
20 different locations. In order to accurately adjust the amplitudes and phases of the transducer elements to focus the acoustic energy at the desired location, the energy contributions of both components are taken into consideration.

[0029] One approach to computing the propagation of longitudinal and shear waves through the skull involves numerically solving the Navier differential equation, which fully describes acoustic wave propagation, implying both longitudinal and transverse modes. Such a numerical simulation may be carried out, for example, using the finite elements method, and is therefore amenable to an arbitrary skull structure and geometry. It facilitates optimization of the phase and amplitude adjustments of the transducer elements for a particular patient, e.g., based on a CT scan of the patient's skull. However, this method is computationally expensive, and typically is performed off-line, i.e., during treatment planning.

[0030] Various alternative approaches are based on the analysis of the propagation of individual rays. For each transducer element, the path and phase shift of an acoustic ray starting at the element, passing through the skull bone, and arriving at the focal point is calculated. Using a simplified model of the skull which contains three locally parallel (e.g., concentric spherical) layers, corresponding to two cortical layers and a marrow layer in between, a closed analytical solution for the propagation of a ray through the skull may be obtained. Similarly, the propagation through other layers, e.g., soft brain tissue layers, may be calculated. The relations between incoming and outgoing waves for the various layers may be expressed in terms of transmission matrices, the product of which yields the overall transmission matrix for propagation from the transducer element to the focus. In this method, an acoustic ray is modeled as a planar wave, and includes both longitudinal and transverse modes.

[0031] A more realistic skull geometry can be accounted for in approaches that weight the contributions of longitudinal and shear modes, and calculate the propagation of these two modes separately. FIG. 4 illustrates separation methods in accordance with such approaches. In a first step 400, an image of the patient's head may be taken, e.g., by magnetic resonance

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imaging or computer tomography. Step 400 is optional, as an otherwise obtained model of the skull and brain may be substituted for the image. For certain applications, a simplified model, such as a series of concentric spherical layers, may suffice to focus ultrasound with adequate accuracy. In step 402, an array of transducer elements (see FIG. 2) is positioned with respect to the skull, and the desired focus of the acoustic energy is specified. The information about the skull geometry and structure and about the locations of transducer array and focus are used repeatedly throughout the following computational steps, which may be carried out by controller 208. First, an incident angle  $\phi$  of the acoustic wave onto the skull is computed for each transducer element (step 404). In an optional step 406, the amount of energy reflected from the skull may be calculated based on the angle. The contributions of the transmitted energy to the longitudinal and the shear modes, respectively, are weighted in step 408, as detailed further below. In step 410, wave propagation through the skull and brain, and the phase shift and attenuation resulting at the focus, are calculated separately for each mode. Then, the contributions of the two waves are added to determine an overall phase shift and attenuation for waves emanating from the transducer element (step 412). In embodiments wherein the transducer elements can be moved or rotated, they may then be adjusted to improve the focus (step 414), and steps 404 through 412 may be repeated. Once the total phase and/or attenuation are determined for each transducer element, they are employed, in step 416, to adjust the phase shifts  $\alpha$  and amplification factors in the beamformer. Finally, the transducer array is driven accordingly to deliver acoustic energy to the desired focus (step 418).

**[0032]** The weighting step 408 may be carried out in one of several ways of various levels of sophistication. FIGS. 5A–5C illustrate three exemplary methods. In approach 408a, shown in FIG. 5A, a threshold angle  $\theta$  is determined (step 500), and this angle separates a predominantly longitudinal regime from a predominantly transverse regime. The threshold

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angle may be chosen dependent on the frequency of the waves. For example, for acoustic waves at a frequency of around 0.2 MHz, a suitable threshold angle is  $30^\circ$ . The energy is assumed to be carried entirely by the longitudinal mode for incidence angles below the threshold angle, and entirely by the transverse mode for incidence angles above the threshold angle. Accordingly, the energy contribution of the shear wave is set to zero below the threshold angle (step 502), and the energy contribution of the longitudinal pressure wave is set to zero above the threshold angle (step 504).

**[0033]** FIG. 5B illustrates a more involved method 408b, involving three regimes — a longitudinal regime, a shear regime, and an overlap regime. In step 510, two threshold angles,  $\theta_1$  and  $\theta_2$ , are defined. For incidence angles  $\phi$  below the first, smaller threshold angle  $\theta_1$ , the shear component is set to zero (step 512), and for incidence angles above the second, larger threshold angle  $\theta_2$ , the longitudinal component is set to zero (step 514). At incidence angles between the first and second threshold angles, longitudinal and shear are assumed to coincide, and their relative contributions are determined by interpolation (step 516). For example, the fraction of the shear component may be set to increase linearly from zero percent at the first threshold angle,  $\theta_1$ , to one hundred percent at the second threshold angle,  $\theta_2$ , as illustrated in the diagram of FIG. 6. However, non-linear interpolations may also be used.

**[0034]** In some embodiments, illustrated in FIG. 5C, the proportions of longitudinal and shear modes are determined empirically. Such methods 408c involve providing, in step 520, values for the contributions of both modes over a range of incident angles, e.g., in the form of a graph. FIG. 7 is an exemplary graph showing the fraction of the incident energy that propagates through the skull in the longitudinal and transverse modes, based on empirically gathered data. At about  $40^\circ$ , the energy of the longitudinal mode drops to zero. The energy of

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the transverse mode increases from zero at normal incidence to as significant fraction at about 40°, above which angle of incidence it predominates. In step 522, weighting factors for the longitudinal and the transverse component are determined for a particular incident angle based on, for example, the relationships shown in FIG. 7.

5 [0035] With renewed reference to FIG. 2, steps 404-412 are typically implemented by a suitable programmable processor and computer memory. The processor may be implemented in hardware or software, or a combination of both, within controller 208 or, alternatively, in a separate device such as a general-purpose computer. In addition, the operating program of system 200 may set aside portions of a computer's random access memory to provide control  
10 logic that effects one or more of the image capture, processing, and delivery of acoustic energy via transducer array 204. In such an embodiment, the program may be written in any one of a number of high-level languages, such as FORTRAN, PASCAL, C, C++, C#, Java, Tcl, or BASIC. Further, the program can be written in a script, macro, or functionality embedded in commercially available software, such as EXCEL or VISUAL BASIC. Additionally, the  
15 software can be implemented in an assembly language directed to a microprocessor resident on a computer. For example, the software can be implemented in Intel 80x86 assembly language if it is configured to run on an IBM PC or PC clone. The software may be embedded on an article of manufacture including, but not limited to, "computer-readable program means" such as a floppy disk, a hard disk, an optical disk, a magnetic tape, a PROM, an EPROM, or CD-  
20 ROM.

[0036] Although the present invention has been described with reference to specific details, it is not intended that such details should be regarded as limitations upon the scope of the invention, except as and to the extent that they are included in the accompanying claims.

[0037] What is claimed is:



**CLAIMS**

1. A method of delivering multimode ultrasound waves to a target through at least one tissue layer defining a first interface and a second interface, the waves having a shear component and a longitudinal component through the at least one tissue layer, the method comprising the steps of:

weighting energy contributions from the shear component and the longitudinal component based at least in part on an incident angle of the waves at the first interface; computing phase shifts associated with the shear component and the longitudinal component; and compensating for the phase shifts, based on the weightings, when delivering the ultrasound waves.

2. The method of claim 1 wherein the ultrasound waves are delivered by a phased array of transducers, the compensation step comprising adjusting outputs of the transducers in accordance with the phase shifts.

3. The method of claim 1 further comprising computing coefficients of attenuation associated with the longitudinal component and the shear component, and compensating for the attenuation when delivering the ultrasound waves.

4. The method of claim 1 further comprising computing a coefficient of reflection of the wave at the first interface, and compensating for the reflection when delivering the ultrasound waves.

5. The method of claim 1 wherein the weighting step is further based on a frequency of the ultrasound waves.

6. The method of claim 1 wherein the weighting step is further based on an acoustic response of the first layer.

7. The method of claim 1 wherein the compensating step is further based on at least one of a geometry, a thickness, a density, and an acoustic response of the first layer.

8. The method of claim 1 wherein the at least one tissue layer corresponds to a skull.

9. The method of claim 1 wherein the weighting step comprises:

determining a threshold angle; and

setting the energy contribution from the shear component to zero for incident angles smaller than the threshold angle; and

setting the energy contribution from the longitudinal component to zero for incident angles not smaller than the threshold angle.

10. The method of claim 1 wherein the weighting step further comprises:

determining a first threshold angle and a second threshold angle, the second threshold angle being greater than the first threshold angle;

setting the energy contribution from the shear component to zero for incident angles smaller than the first threshold angle; and

setting the energy contribution from the longitudinal component to zero for incident angles larger than the second threshold angle; and

computing the energy contributions from the shear component and the longitudinal component by interpolation for incident angles not smaller than the first threshold angle and not larger than the second threshold angle.

- 1 11. The method of claim 10 wherein the interpolation is linear.
- 1 12. The method of claim 1 wherein the weighting step is based on a relationship between  
2 energy contributions from the shear component and the longitudinal component determined  
3 empirically over a range of incident angles.
- 1 13. The method of claim 1 further comprising providing a model of the at least one tissue  
2 layer, and basing the compensation step on the model.
- 1 14. The method of claim 13 wherein the model comprises locally parallel layers.
- 1 15. The method of claim 13 wherein the model is obtained using at least one of computer  
2 tomography or magnetic resonance imaging.
- 1 16. The method of claim 1 wherein the ultrasound waves have a frequency in the range  
2 from 100 kHz to 400 kHz.
- 1 17. The method of claim 1 wherein the incident ultrasonic wave is purely longitudinal.
- 1 18. The method of claim 17 wherein the incident ultrasonic wave excites a longitudinal  
2 component and a shear component at the first interface.
- 1 19. The method of claim 18 wherein the shear component excites a longitudinal wave at the  
2 second interface.
- 1 20. A system for delivering multimode ultrasound waves to a target located inside an object  
2 that comprises at least a first layer defining a first interface and a second interface, the waves  
3 having a shear component and a longitudinal component through at least the first layer, the  
4 system comprising:
- 5 (a) a phased array of transducers arranged around the object;
- 6 (b) a controller for (i) receiving data about the object, its location relative to the  
7 transducers, and a location of the target, (ii) computing for each transducer, based on the data  
8 (1) an incident angle at which waves emanating from the transducer arrive at the first interface,

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9 (2) weightings of energy contributions from the shear component and the longitudinal  
10 component, based on the incident angle, and (3) phase shifts of the shear component and the  
11 longitudinal component, and (iii) computing phase shift compensations for the transducers  
12 based on the phase shifts of the shear components and the longitudinal components; and  
13 a beam former in communication with the controller and the phased array of transducers  
14 for adjusting outputs of the transducers in accordance with the phase shift compensations  
15 computed by the controller.

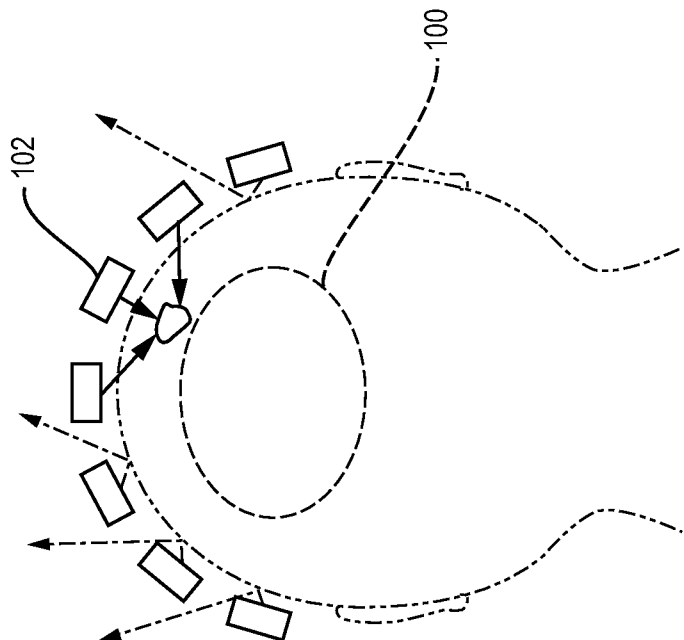


FIG. 1B

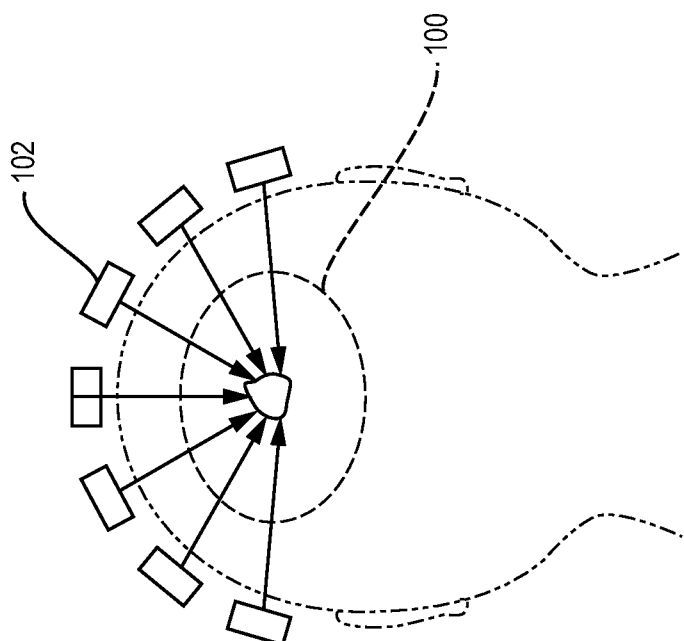


FIG. 1A

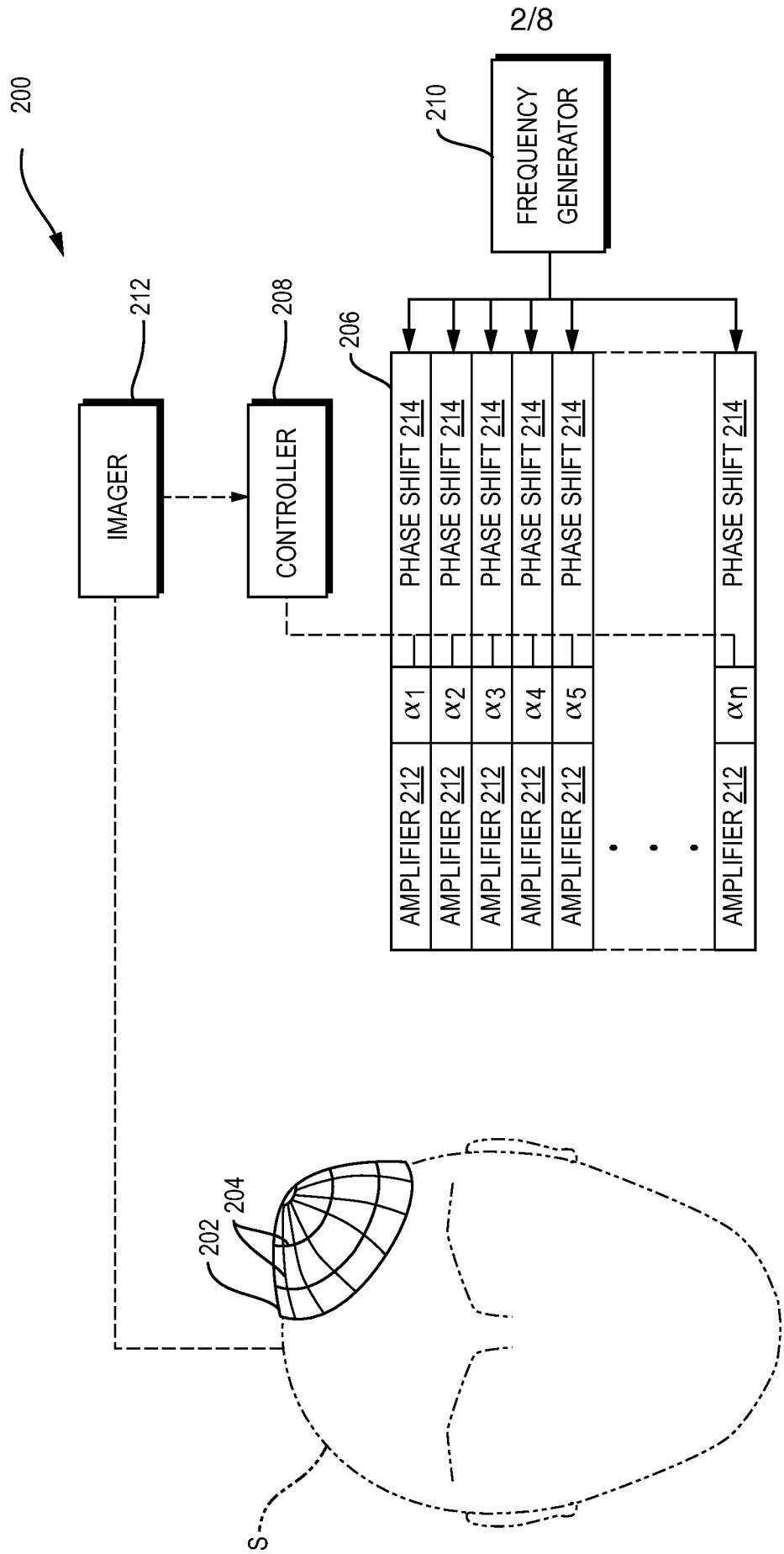


FIG. 2

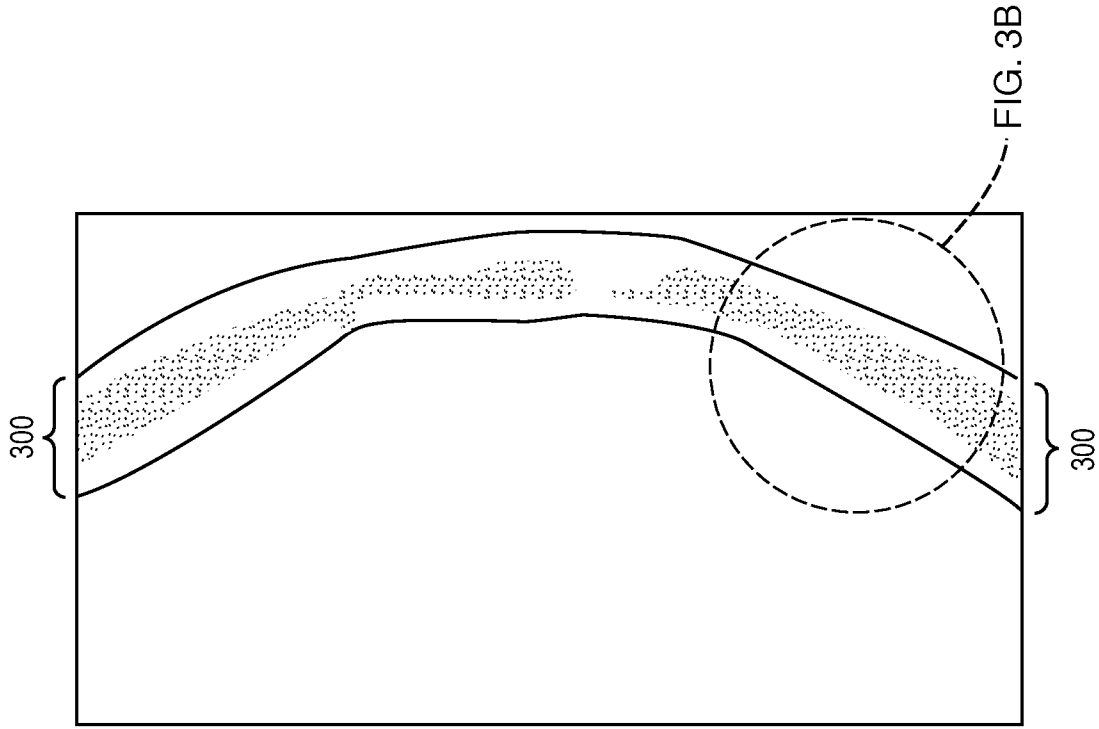


FIG. 3A

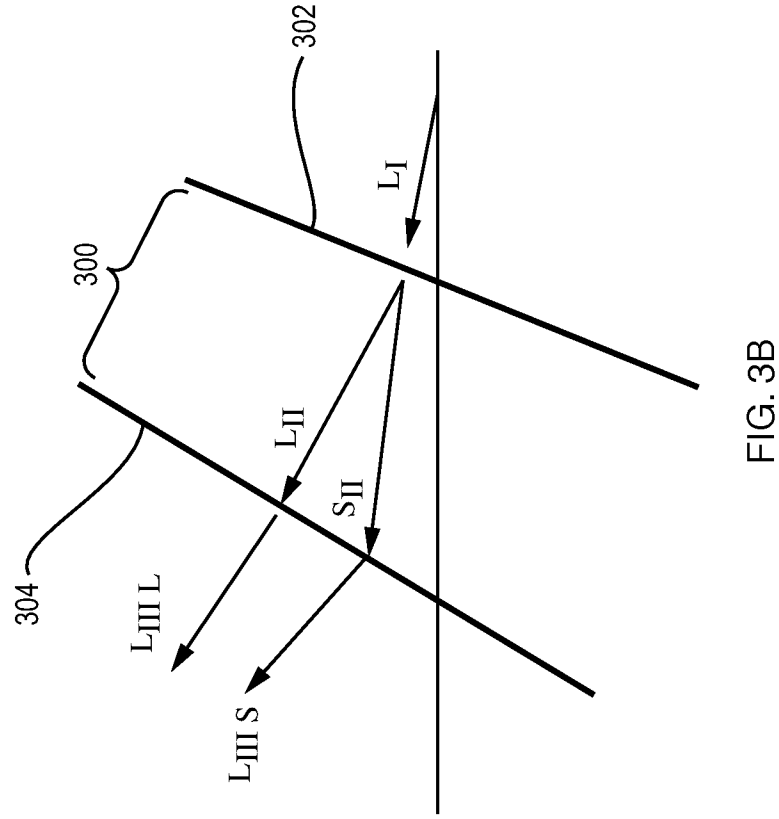


FIG. 3B

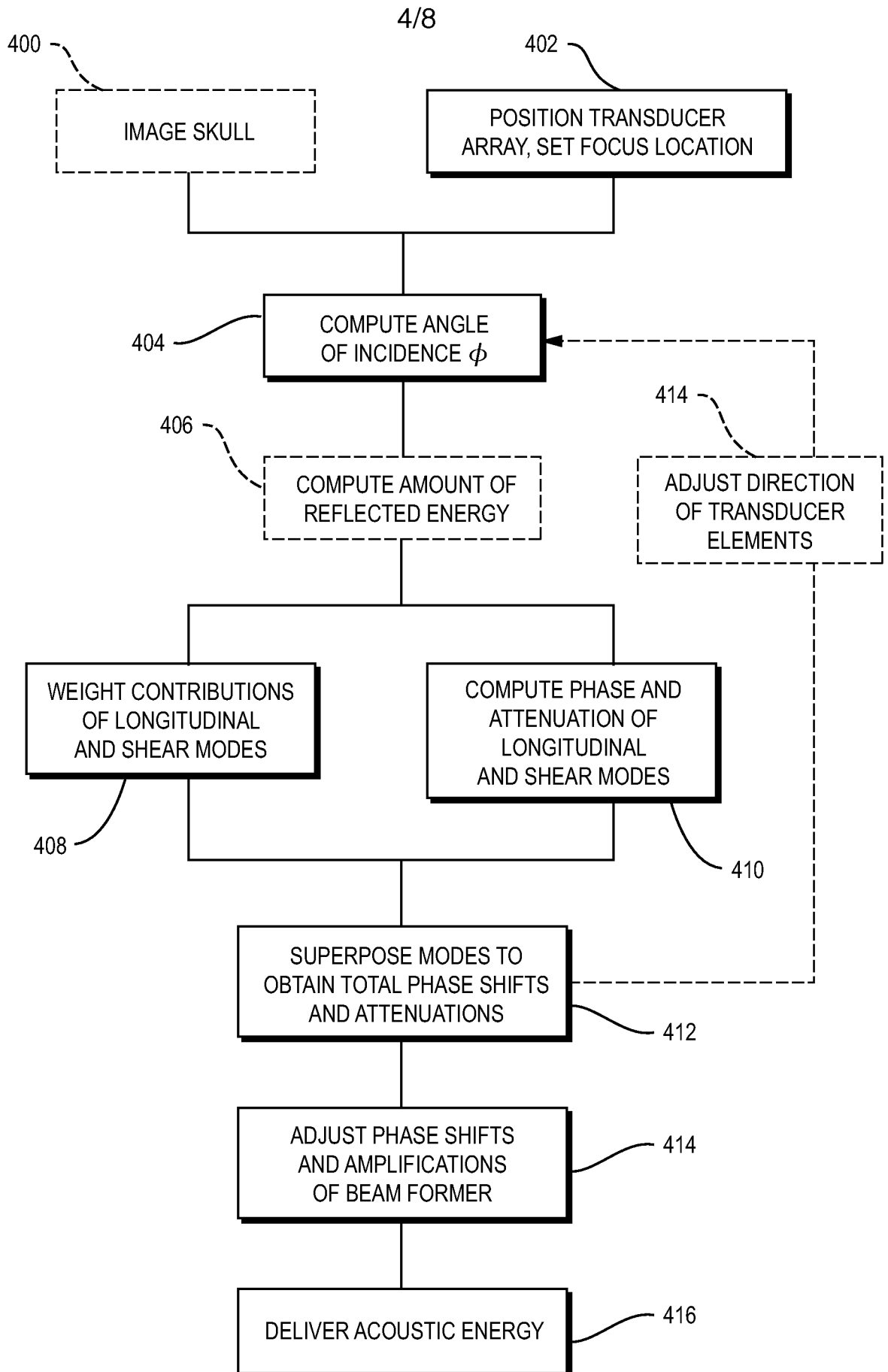
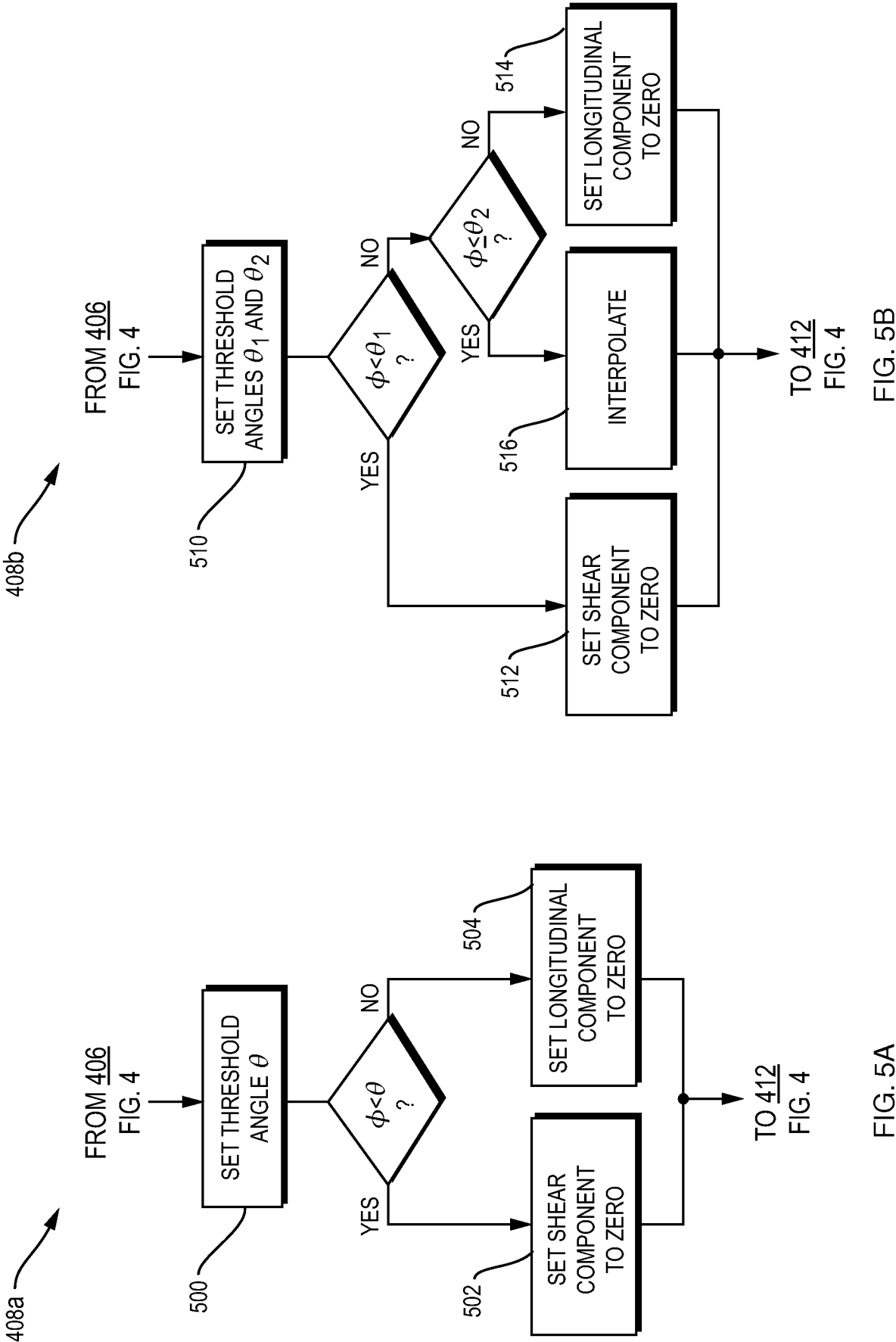
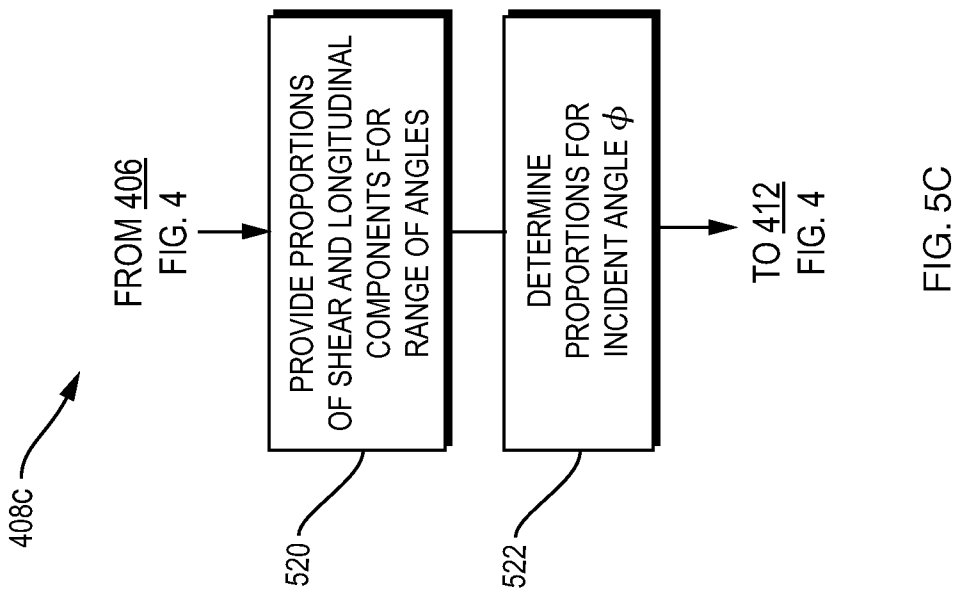


FIG. 4







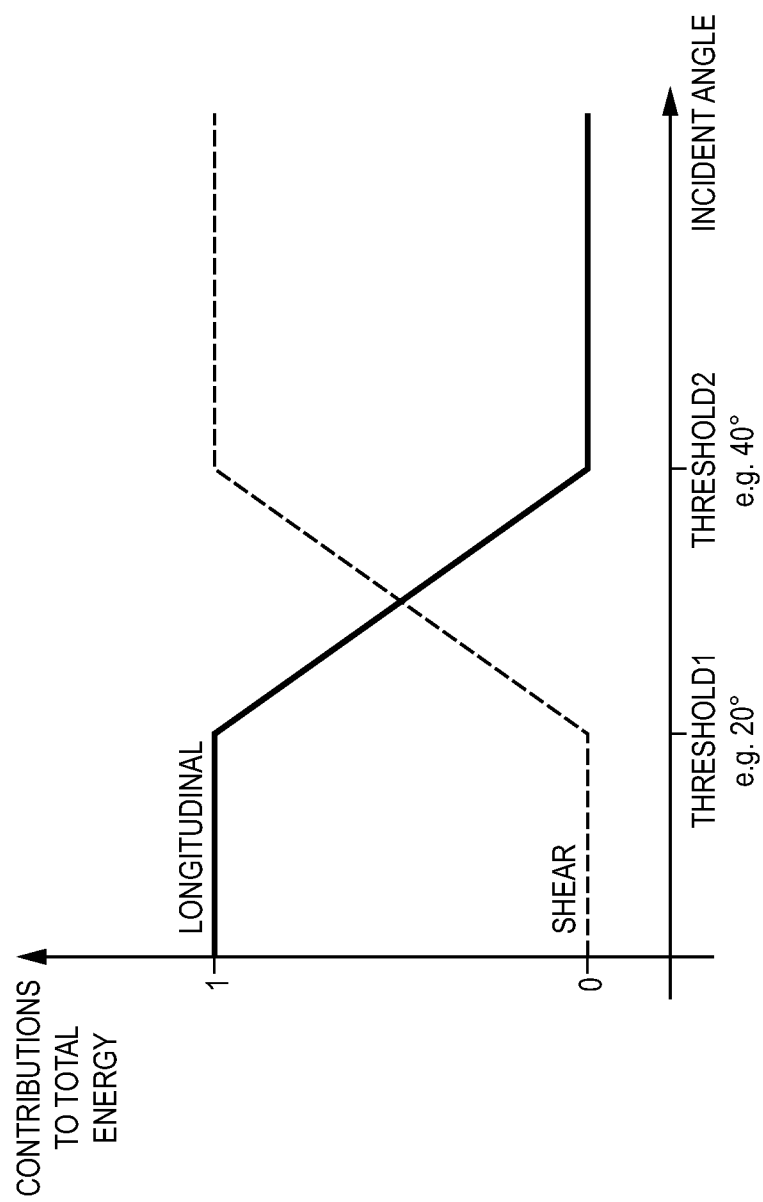


FIG. 6

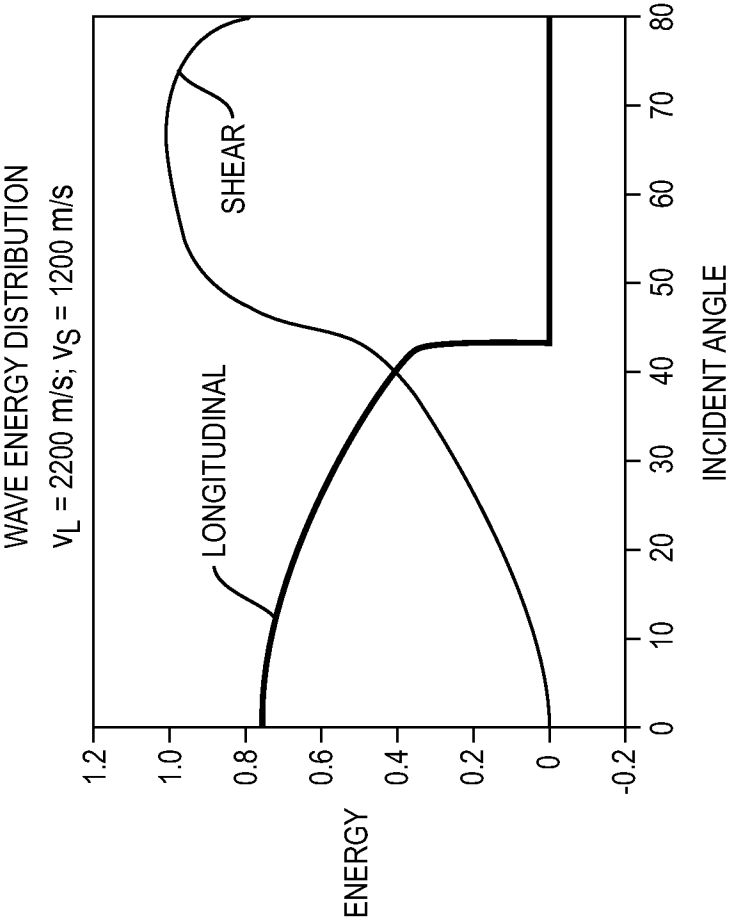


FIG. 7

# INTERNATIONAL SEARCH REPORT

International application No

PCT/IB2010/000971

**A. CLASSIFICATION OF SUBJECT MATTER**  
 INV. A61N7/00 A61N7/02  
 ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

A61N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EP0-Internal

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 03/013654 A1 (EXOGEN INC [US]) 20 February 2003 (2003-02-20) * abstract page 3, line 5 - page 4, line 3 page 15, line 4 - page 16, line 2 -----	20



Further documents are listed in the continuation of Box C.



See patent family annex.

\* Special categories of cited documents:

- \*A\* document defining the general state of the art which is not considered to be of particular relevance
- \*E\* earlier document but published on or after the international filing date
- \*L\* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- \*O\* document referring to an oral disclosure, use, exhibition or other means
- \*P\* document published prior to the international filing date but later than the priority date claimed

- \*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- \*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- \*Y\* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- \*G\* document member of the same patent family

Date of the actual completion of the international search

19 July 2010

Date of mailing of the international search report

29/07/2010

Name and mailing address of the ISA/

European Patent Office, P.B. 5818 Patentlaan 2  
 NL - 2280 HV Rijswijk  
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 Fax: (+31-70) 340-3016

Authorized officer

Kajzar, Anna

## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/IB2010/000971

### Box No. II Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☒ Claims Nos.: 1-19  
because they relate to subject matter not required to be searched by this Authority, namely:  
Rule 39.1(iv) PCT - Method for treatment of the human or animal body by therapy and surgery
2. ☐ Claims Nos.:  
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. ☐ Claims Nos.:  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

### Box No. III Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fees, this Authority did not invite payment of additional fees.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

#### Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee.
- ☐ The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation.
- ☐ No protest accompanied the payment of additional search fees.

# INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/IB2010/000971

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO 03013654	A1	20-02-2003	
		AT 306969 T	15-11-2005
		AU 2002329676 B2	02-11-2006
		CA 2456734 A1	20-02-2003
		DE 60206773 D1	24-11-2005
		DE 60206773 T2	06-07-2006
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		JP 4299128 B2	22-07-2009
		JP 2004537383 T	16-12-2004
		US 7429248 B1	30-09-2008

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专利名称(译)	多模超声聚焦用于医疗应用		
公开(公告)号	<a href="#">EP2429656A1</a>	公开(公告)日	2012-03-21
申请号	EP2010720818	申请日	2010-04-15
[标]申请(专利权)人(译)	因赛泰克有限公司		
申请(专利权)人(译)	InSightec的有限公司.		
当前申请(专利权)人(译)	InSightec的有限公司.		
[标]发明人	PRUS OLEG VITEK SHUKI		
发明人	PRUS, OLEG VITEK, SHUKI		
IPC分类号	A61N7/00 A61N7/02 A61B8/14		
CPC分类号	A61B8/14 A61B8/0816 A61B8/4455 A61B8/485 A61N7/02 A61N2007/0056 A61N2007/0078		
代理机构(译)	HARRISON GODDARD FOOTE		
优先权	12/425698 2009-04-17 US		
其他公开文献	EP2429656B1		
外部链接	<a href="#">Espacenet</a>		

#### 摘要(译)

通过利用纵波和剪切波可以改善用于将超声通过颅骨聚焦到大脑中用于诊断或治疗目的的系统和方法。可以基于入射角确定两种模式的相对贡献。