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**(54) ULTRASOUND IMAGE FORMATION AND/OR RECONSTRUCTION USING MULTIPLE FREQUENCY WAVEFORMS**

ULTRASCHALLBILDERZEUGUNG UND/ODER -REKONSTRUKTION UNTER VERWENDUNG VON WELLENFORMEN MIT MEHREREN FREQUENZEN

FORMATION ET/OU RECONSTRUCTION D'IMAGES PAR ULTRASONNS AU MOYEN DE FORMES D'ONDE À FRÉQUENCES MULTIPLES

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**US-B1- 6 172 939 US-B1- 6 494 839**

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**Description**

## BACKGROUND

5 **[0001]** The disclosure herein relates generally to ultrasound imaging. More particularly, the disclosure herein pertains to ultrasound imaging methods and systems for use in, e.g., diagnostic and/or therapy applications (e.g., imaging of complex media, such as blood vessels and/or regions proximate thereto, disc tissues, brain structures, etc.).

10 **[0002]** Ultrasound imaging is gaining increased attention not only as a way to detect cardiovascular diseases, but also for the evaluation of response to new anti-atherosclerotic therapies (see, Ainsworth, et al., "3D ultrasound measurement of change in carotid plaque volume - A tool for rapid evaluation of new therapies," *Stroke*, vol. 36, no. 9, pp. 1904-1909, SEP 2005). Intravascular ultrasound (IVUS) has been shown to provide an effective tool in measuring the progression or regression of atherosclerotic disease in response to therapies. However, IVUS is invasive, potentially risky, and more expensive than noninvasive imaging with ultrasound.

15 **[0003]** Advanced imaging modes on ultrasound scanners have led to increased interest in imaging important quantities, such as, wall shear rate (WSR) using Doppler (see, Blake, et al., "A method to estimate wall shear rate with a clinical ultrasound scanner," *Ultrasound in Medicine and Biology*, vol. 34, no. 5, pp. 760-764, MAY 2008) and tissue/wall motion (see, Tsou et al., "Role of ultrasonic shear rate estimation errors in assessing inflammatory response and vascular risk," *Ultrasound in Medicine and Biology*, vol. 34, no. 6, pp. 963-972, JUN 2008; Karimi et al., "Estimation of Nonlinear Mechanical Properties of Vascular Tissues via Elastography," *Cardiovascular Engineering*, vol. 8, no. 4, pp. 191-202, DEC 2008; and Weitzel et al., "High-Resolution Ultrasound Elasticity Imaging to Evaluate Dialysis Fistula Stenosis," *Seminars In Dialysis*, vol. 22, no. 1, pp. 84-89, JAN-FEB 2009) using speckle tracking.

20 **[0004]** Recently, there has been increased interest in imaging flow in conjunction with computational fluid dynamic (CFD) modeling for evaluation of large artery hemodynamics (see, Steinman et al., "Flow imaging and computing: Large artery hemodynamics," *ANNALS OF BIOMEDICAL ENGINEERING*, vol. 33, no. 12, pp. 1704-1709, DEC 2005; Figueroa, et al., "A computational framework for fluid-solid-growth modeling in cardiovascular simulations," *Computer Methods in Applied Mechanics and Engineering*, vol. 198, no. 45- 46, pp. 3583 - 3602, 2009; and Taylor et al., "Open problems in computational vascular biomechanics: Hemodynamics and arterial wall mechanics," *Computer Methods in Applied Mechanics and Engineering*, vol. 198, no. 45-46, pp. 3514 - 3523, 2009). In this context, modeling fluid-solid interfaces has been defined as a challenge area in vascular mechanics.

25 **[0005]** The advent of piezo-composite transducer technology has allowed for the design and fabrication of effective dual-mode ultrasound arrays (DMUAs) for use in an ultrasound system capable of both image formation and generation of therapeutic high-intensity focused ultrasound (HIFU) beams. Such DMUAs have been used for pulse echo imaging. For example, traditional beamforming-based pulse echo image formation has been used in both analog and digital forms, which has led to improvement in image quality (e.g., such as with use of dynamic-beamforming available on many commercial scanners in the formation of ultrasound images). Further, for example, synthetic-aperture imaging and other more computationally based approaches have also been described and/or used (e.g., the Verasonics engine which is a software-based image formation tool and/or model).

30 **[0006]** US 6172939 B1 describes a digital transmit beamformer system with multiple beam transmit capability having a plurality of multi-channel transmitters, each channel with a source of sampled, complex-valued initial waveform information representative of the ultimate desired waveform to be applied to one or more corresponding transducer elements for each beam. Each multi-channel transmitter applies beamformation delays and apodization to each channel's respective initial waveform information digitally, digitally modulates the information by a carrier frequency, and interpolates the information to the DAC sample rate for conversion to an analog signal and application to the associated transducer element(s).

35 **[0007]** However, to be able to noninvasively identify and treat target regions, improved ultrasound image formation is needed. Further, image reconstruction approaches to provide reconstructed images representative of one or more properties of the structure in the target regions (e.g., scattering function, speed of sound, attenuation, reflection coefficients, etc.). The reconstruction of these quantities reveals important features in the tissue architecture (e.g. healthy versus diseased vessel walls, extent of tissue change due to therapy, etc.) that cannot be obtained from conventional image formation.

40 **[0008]** The present invention solves the afore-mentioned problems by providing an ultrasound imaging method (30; 80) comprising:

45 providing a region of interest (ROI) in a subject;

50 defining a plurality of control points (CPs) within the region of interest (ROI), wherein at least a first portion of the control points (CPs) are associated with a first identifiable portion of the region of interest (ROI) and a second portion of the control points (CPs) are associated with a second identifiable portion of the region of interest (ROI) that is different than the first identifiable portion;

providing a transducer apparatus (22) comprising a plurality of ultrasound transducer elements, wherein each of the plurality of ultrasound transducer elements is configured to deliver ultrasound energy to the region of interest (ROI) in response to a waveform applied thereto;

generating a waveform for each ultrasound transducer element of the plurality of ultrasound transducer elements, wherein generating the waveform comprises:

selecting one or more imaging frequencies within a transducer apparatus bandwidth, each of the one or more imaging frequencies being a carrier of a pulse to be transmitted having a finite bandwidth within the transducer bandwidth and having a time duration; and

generating element frequency components for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element;

delivering ultrasound energy in pulse mode to the region of interest using the plurality of ultrasound transducer elements in response to waveforms generated for each of the plurality of ultrasound transducer elements;

receiving pulse-echo data at each ultrasound transducer element of a plurality of ultrasound transducer elements from the region of interest (ROI) in response to the delivered ultrasound energy to generate an image based thereon; separating pulse-echo components received from at least one of the first portion of the control points associated with the first identifiable portion of the region of interest and received from the second portion of the control points associated with the second identifiable portion of the region of interest;

determining at least one of a contrast ratio (CR) between the first and second identifiable portions based on the pulse-echo components received from the first portion of the control points (CPs) associated with the first identifiable portion of the region of interest (ROI) and the pulse-echo components received from the second portion of the control points (CPs) associated with the second identifiable portion of the region of interest (ROI) and a signal to noise ratio (SNR) based on pulse-echo components received from a reference portion of the region of interest (ROI) and pulse-echo components received from at least one of the first portion of the control points (CPs) and the second portion of the control points (CPs); and

modifying the waveform generated for one or more of the plurality of ultrasound transducer elements based on at least one of a comparison of the contrast ratio (CR) determined between the first and second identifiable portions to a threshold value and a comparison of the signal to noise ratio (SNR) to a threshold value, wherein modifying the waveform generated for one or more of the plurality of ultrasound transducer elements comprises at least one of adjusting gain at frequencies of the one or more frequencies located at one or more locations within the transducer apparatus bandwidth, and adjusting one or more pulse parameters including at least one of pulse duration, pulse shape, pulse amplitude, and pulse phase to adjust time-bandwidth product to maximize at least one of contrast ratio (CR) between the first and second identifiable portions of the region of interest (ROI) and a signal to noise ratio (SNR) from the region of interest (ROI).

**[0009]** Furthermore, the problems are solved by a system for ultrasound imaging (10) according to the present invention, comprising:

a transducer apparatus (22) comprising a plurality of ultrasound transducer elements, wherein each of the plurality of ultrasound transducer elements is configured to deliver ultrasound energy to a region of interest (ROI) in response to a waveform applied thereto resulting in pulse-echo data therefrom; and

means for providing a region of interest (ROI) in a subject configured to define a plurality of control points (CPs) within the region of interest (ROI), wherein at least a first portion of the control points (CPs) are associated with a first identifiable portion of the region of interest (ROI) and a second portion of the control points (CPs) are associated with a second identifiable portion of the region of interest (ROI) that is different than the first identifiable portion;

means for generating a waveform for each ultrasound transducer element of the plurality of ultrasound transducer elements, wherein the waveform generation means comprises:

means for selecting one or more imaging frequencies within a transducer apparatus bandwidth, each of the one or more imaging frequencies being a carrier of a pulse to be transmitted having a finite bandwidth within the transducer apparatus bandwidth and having a time duration; and

means for generating element frequency components for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element;

means for controlling delivery of ultrasound energy in pulse mode to the region of interest (ROI) using the plurality of ultrasound transducer elements in response to waveforms generated for each of the plurality of ultrasound transducer elements;

means for controlling capture of pulse-echo data at each ultrasound transducer element of a plurality of ultrasound transducer elements from the region of interest in response to the delivered ultrasound energy to generate an image based thereon;

5 means for separating pulse-echo components received from at least one of the first portion of the control points (CPs) associated with the first identifiable portion of the region of interest (ROI) and received from the second portion of the control points (CPs) associated with the second identifiable portion of the region of interest (ROI);

10 means for determining at least one of a contrast ratio (CR) between the first and second identifiable portions based on the pulse-echo components received from the first portion of the control points (CPs) associated with the first identifiable portion of the region of interest (ROI) and the pulse-echo components received from the second portion of the control points (CPs) associated with the second identifiable portion of the region of interest (ROI) and a signal to noise ratio (SNR) based on pulse-echo components received from a reference portion of the region of interest (ROI) and pulse-echo components received from at least one of the first portion of the control points (CPs) and the second portion of the control points (CPs); and

15 means for modifying the waveform generated for one or more of the plurality of ultrasound transducer elements based on at least one of a comparison of the contrast ratio (CR) determined between the first and second identifiable portions to a threshold value and a comparison of the signal to noise ratio (SNR) to a threshold value, wherein modifying the waveform generated for one or more of the plurality of ultrasound transducer elements comprises at least one of adjusting gain at frequencies of the one or more frequencies located at one or more locations within the transducer apparatus bandwidth, and adjusting one or more pulse parameters including at least one of pulse duration, pulse shape, pulse amplitude, and pulse phase to adjust time-bandwidth product to maximize at least one of contrast ratio (CR) between the first and second identifiable portions of the region of interest (ROI) and a signal to noise ratio (SNR) from the region of interest (ROI).

25 **[0010]** Further aspects and preferred embodiments of the invention are defined in the dependent claims.

**[0011]** In the following description, further embodiments, their advantages, and additional explanations of methods and systems suitable to be used with the invention are described

30 **[0012]** At least one embodiment of this disclosure relates to ultrasound image formation of a region of interest (e.g., a target region, such as a region including perivascular tissue). For example, in one or more embodiments of this disclosure, an ultrasound imaging architecture including a programmable transmit-receive chain allows for the application of transmit waveform design, together with pre- and post-beamforming filtering to achieve optimal image reconstruction of the scattering function in the target volume or region of interest (ROI). Such ultrasound imaging may make use of transmit waveform synthesis (or, more generally, wavefront synthesis) and post-beamforming filtering in the form of matched filtering or regularized inverse filtering. The performance of the system may be improved in one or more ways by coupling the waveform design and the pre- and post-beamforming filtering for detection, estimation, and high (super)-resolution image reconstruction. For example, mathematical operators described herein may allow for real-time implementation of enhancements to ultrasound imaging without requiring an excessive level of investment in transducer technology or hardware. For example, applications that require thousands of array elements with conventional beamforming may be achieved by reconstructive imaging and coded-wavefront design using arrays with a fraction of the channel count needed for the conventional case. One or more embodiments herein may allow for the use of the Fourier transform (FT) and, in particular, the discrete version of this the transform, the discrete Fourier transform (DFT), to simplify the imaging model and provide a computationally-efficient model for image reconstruction. In one or more embodiments, the use of a sliding eigenvalue (singular) decomposition of the ultrasound echo data at discrete frequencies makes it possible to derive imaging/reconstruction operators with high specificity to echo components resulting from the use of specifically-designed codes and/or from an assumed scattering structure. This approach may be beneficial in rejecting reverberations and beamforming artifacts without compromising spatial resolutions.

45 **[0013]** In one or more embodiments, a randomly distributed discrete set of frequencies is employed to adaptively design a coding scheme which is "matched to the spectral characteristics of the target region" while "utilizing the maximum bandwidth of the transducer system for optimal spatial and contrast resolutions." For example, such adaptive ultrasound may provide the ability to perform imaging and therapy in complex media, which is in many cases hampered by the use of conventional continuous wave (CW) or pulsed excitations on the therapy and imaging sides of the system. In one or more embodiments, the adaptive ultrasound system and method herein represents a unified approach to imaging and therapy using arbitrary waveform generation allowing for wavefront synthesis in the region of interest. For example, in principle, given the target size and depth together with a general understanding of its surroundings (e.g. bone, ligaments, etc.), a custom-designed DMUA with a relatively small number of elements to produce high quality focusing (e.g., for imaging and/or therapy) within the target while avoiding the critical structures in the path of the beams may be provided. Therefore, for example, lower back pain, stroke, cardiac ablation, renal denervation and any number of applications where precise ablation is sought may be performed using the systems and/or methods herein.

55 **[0014]** At least one embodiment of this disclosure relates to image reconstruction (e.g., of a portion of the region of

interest (e.g., as a region including perivascular tissue). For example, in one or more embodiments, a reconstructive approach is provided for pulsed ultrasound at single frequency. Such an exemplary single-frequency image reconstruction approach for pulse-mode ultrasound may have one or more of the following advantages. For example, by retaining the use of the pulsed nature of ultrasound the axial resolution of ultrasound may be maintained (e.g., axial resolution being determined by the transmit pulse shape). Further, for example, extracting a single frequency component of the pulse echo data at all depths, while accounting for transmit-receive beamforming models, allows for direct computation of a reflectivity map (e.g., which may be useful for analyzing the multilayer structure of blood vessels). This is in contrast to the difficulty in extracting reflectivity data from a full pulse packet echo due (e.g., a pulse packet being a group of frequencies forming a pulse initially traveling as a group, but their coherence being affected by dispersion in the propagation medium, frequency dependent scattering, attenuation, etc.) to the complexity of the structures. This may allow for some distinct advantages. For example, since reverberation is frequency-dependent, it may allow for more efficient dereverberation algorithms for improving image quality within the wall and in the lumen. Further, for example, a reliable model for reconstructing a property related to the multilayered nature of blood vessel may be important in analyzing vessels in a pre-disease state in a quantitative manner. Yet further, for example, the single-frequency echo components may provide a reliable way for separating speckle and specular reflections which may allow for quantitative ultrasound imaging of tissue architectures with high resolution (e.g., something that is currently impossible due to the almost inseparable speckle component in pulse packet form).

**[0015]** A computationally efficient algorithm for pulsed-mode single-frequency (PMSF) reconstruction may be implemented both in software and/or in hardware, e.g. on field programmable gate array (FPGA) circuitry of ultrasound scanners. Transmit and receive beams may be precomputed and tabulated at the frequency of interest and the region of interest within the image (see, e.g., Figures 6 and 7 herein).

**[0016]** One exemplary embodiment of an imaging method or system may include providing a running DFT computational block at a frequency of interest for each receiving element followed by a frequency-domain beamforming network (e.g., both of which may be implemented on an FPGA). Image reconstruction of the scattering function or other quantitative property of the ROI may be performed after the single-frequency image formation (e.g., which may be performed on a graphical processing unit (GPU)). Alternatively, a DFT processor may be deployed after beamforming and before the reconstruction block. In this case, the DFT and the reconstruction block may be performed on a GPU. In general, all three stages are computational stages and can be implemented in FPGA, GPU, multi-core CPUs or any appropriate processing unit(s) (see, e.g., Figure 6 herein).

**[0017]** One or more embodiments of methods or systems described herein may include one or more of the following features or processes: 1) real-time implementation of an adaptive algorithm to optimize the imaging performance (e.g., based on specified signal to noise ratio (SNR) and/or contrast ratio (CR) values for a given control-point selection); this may further include, for example, transmit and receive beamforming; 2) real-time frequency separation using DFT or other efficient methods (e.g., narrowband filtering); and 3) a reconstruction algorithm operating on single frequency pulse-mode (SFPM) data once the optimal formation has been achieved.

**[0018]** One or more embodiments of methods or systems described herein may include one or more of the following features or processes (e.g., for image formation to provide an image of the reflectivity map for an object): generating one or more excitation vectors (e.g., each excitation vector may be generated using field synthesis at a single frequency of the one or more imaging frequencies within the transducer bandwidth); an excitation vector generated that may include an element frequency component corresponding to each ultrasound transducer element of the plurality of ultrasound transducer elements; comparing at least the signal to noise ratio to a threshold value and the waveform generated for one or more of the plurality of ultrasound transducer elements may be modified based on the comparison; comparing at least the contrast ratio determined between the first and second identifiable portions to a threshold value and the waveform generated for one or more of the plurality of ultrasound transducer elements may be modified based on the comparison; and the waveform generated may be modified for one or more of the plurality of ultrasound transducer elements by at least one of adjusting gain at frequencies of the one or more frequencies located at one or more locations within the transducer apparatus bandwidth, and/or adjusting one or more pulse parameters including at least one of pulse duration, pulse shape, pulse amplitude, and pulse phase to adjust time-bandwidth product to improve at least one of contrast ratio or signal to noise ratio.

**[0019]** One or more embodiments of methods or systems described herein may include one or more of the following features or processes relating to image formation for vascular structure. Such embodiments of methods or systems described herein may include one or more of the following features or processes: the first portion of the control points may be associated with a vessel wall of a vascular structure (e.g., of a living subject) and the second portion of the control points may be associated with a lumen defined at least in part by the vessel wall; the plurality of control points within the region of interest may further include a third portion of the control points associated with tissue surrounding the vessel wall of the vascular structure; and pulse-echo components received from the third portion of the control points associated with the tissue may be separated from the pulse-echo components received from other portions of the control points and at least a contrast ratio between the tissue and at least one of the vessel wall or lumen may be determined

for use in modifying the waveform generated for one or more of the plurality of ultrasound transducer elements.

**[0020]** One or more embodiments of methods or systems described herein may include one or more of the following features or processes related to image reconstruction (e.g., following image formation to provide an image of the reflectivity map for an object). Such embodiments of methods or systems described herein may include or such reconstruction processes may be used alone to provide a reconstructed image using one or more of the following features or processes: separating, from the pulse echo data received, at least a portion thereof received at each ultrasound transducer element from the region of interest in response to the delivered ultrasound energy corresponding to a single frequency of the one or more image frequencies and reconstructing an image representative of one or more properties in the region of interest from the separated pulse-echo data corresponding to the single frequency of the one or more image frequencies; and/or separating, from the pulse echo data received, one or more additional portions thereof received at each ultrasound transducer element from the region of interest in response to the delivered ultrasound energy corresponding to one or more additional single frequencies of the one or more image frequencies, reconstructing an image representative of one or more properties in the region of interest from the separated pulse-echo data corresponding to each of the single frequencies of the one or more image frequencies, and combining the reconstructed images corresponding to multiple frequencies within the transducer apparatus bandwidth.

**[0021]** Further, one or more embodiments of methods or systems described herein may include one or more of the following features or processes (e.g., related to delivering therapy): therapy may be delivered or the system may be configured to deliver therapy to a patient based on identification of at least one vascular characteristic of the region of interest in which at least one portion of a blood vessel is located. For example, the system may be configured to deliver therapy based on identification of the at least one vascular characteristic of the region of interest in which at least one portion of a blood vessel is located, the transducer apparatus used to deliver ultrasound energy and receive pulse-echo data may also be configured to generate ultrasonic energy to deliver therapy, etc.

**[0022]** One or more of the methods or systems may further include or may be configured to execute separating, from the pulse echo data received, one or more additional portions thereof received at each ultrasound transducer element from the region of interest in response to the delivered ultrasound energy corresponding to one or more additional single frequencies of the one or more image frequencies, reconstructing an image representative of one or more properties in the region of interest from the separated pulse-echo data corresponding to each of the single frequencies of the one or more image frequencies, and combining the reconstructed images corresponding to multiple frequencies within the transducer apparatus bandwidth (e.g., compounding of reconstructed images; wherein each reconstructed corresponds to a single frequency image of a plurality of image frequencies).

**[0023]** Further, one or more embodiments of the method or system (e.g., used to reconstruct images) may include generating element frequency components for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element by generating one or more excitation vectors (e.g., wherein generating the one or more excitation vectors may include generating each excitation vector using field synthesis at a single frequency of the one or more imaging frequencies within the transducer bandwidth). Further, the excitation vector generated may include an element frequency component corresponding to each ultrasound transducer element of the plurality of ultrasound transducer elements.

**[0024]** Further, in one or more embodiments of the method or system (e.g., used to reconstruct images) the region of interest may include a vessel wall of a vascular structure of the subject and a lumen defined at least in part by the vessel wall, and/or may include or be configured to deliver therapy to a patient based on identification of at least one vascular characteristic of the region of interest in which at least one portion of a blood vessel is located.

**[0025]** Further, in one or more embodiments of the method or system (e.g., image formation, image reconstruction, etc.), receiving pulse-echo data at each ultrasound transducer element of a plurality of ultrasound transducer elements from the region of interest in response to the delivered ultrasound energy may include using a discrete Fourier transform based filter bank for separation of pulse-echo data. For example, in one or more embodiments, the methods or systems herein may be configured to use a discrete Fourier transform based filter bank for separation of pulse-echo data.

**[0026]** Further, in one or more embodiments of the method or system, the one or more imaging waveforms may include a finite number of randomly selected single frequency components with each single frequency component being a carrier having a finite bandwidth specified by its duration and modulating pulse.

## BRIEF DESCRIPTION OF THE DRAWINGS

### [0027]

FIG. 1 is a block diagram depicting an exemplary ultrasound imaging system, with an optional therapy system.

FIG. 2 is a flow chart depicting an exemplary ultrasound imaging method, with optional diagnostics or therapy.

FIG. 3 is a flow chart depicting an exemplary ultrasound adaptive imaging method.

FIG. 4 is an illustration for use in describing the exemplary ultrasound adaptive imaging method of Figure 3 as related to vascular structures.

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FIG. 5 is an exemplary waveform synthesis algorithm for use in the ultrasound adaptive imaging method of Figure 3 as related to vascular structures.

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FIG. 6 is a block diagram of one exemplary embodiment that may be used for implementing an imaging system shown generally in Figure 1.

FIG. 7 is a diagram of one exemplary DFT receiver that may be used for implementation of an imaging system such as shown in Figure 3.

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FIG. 8 is a block diagram of another exemplary embodiment of an imaging system shown generally in Figure 1.

FIGS. 9 and 10 are illustrations for use in describing an exemplary filter designs. FIG. 11 provides an exemplary image of a blood vessel for use in describing one or more methods and/or systems shown generally herein as they relate to vascular diagnostics or vascular therapy.

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FIGS. 12-14 are illustrations for use in describing the extension of adaptive imaging to applications other than vascular applications.

FIG. 15 provides an illustration for implementing at least a portion of the image system with use of running DFT before beamforming, although running it post beamforming may also be possible.

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FIG. 16 provides an illustration for implementing image reconstruction that is applied in conjunction with post beamforming extraction of the SFPM data vector(s) after beamforming.

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FIGS. 17A-B provide an illustration of a single frequency five-focus pattern synthesis and an illustration of a five-focus pattern resulting from wavefront synthesis of five independent codes at the same five control points, respectively.

#### DETAILED DESCRIPTION OF EXEMPLARY EMBODIMENTS

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**[0028]** In the following detailed description of illustrative embodiments, reference is made to the accompanying figures of the drawing which form a part hereof, and in which are shown, by way of illustration, specific embodiments which may be practiced. It is to be understood that other embodiments may be utilized and structural changes may be made without departing from (e.g., still falling within) the scope of the disclosure presented hereby.

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**[0029]** Exemplary methods, apparatus, and systems shall be described with reference to Figures 1-14. It will be apparent to one skilled in the art that elements or processes (e.g., including steps thereof) from one embodiment may be used in combination with elements or processes of the other embodiments, and that the possible embodiments of such methods, apparatus, and systems using combinations of features set forth herein is not limited to the specific embodiments shown in the Figures and/or described herein. Further, it will be recognized that the embodiments described herein may include many elements that are not necessarily shown to scale. Still further, it will be recognized that timing of the processes and the size and shape of various elements herein may be modified but still fall within the scope of the present disclosure, although certain timings, one or more shapes and/or sizes, or types of elements, may be advantageous over others.

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**[0030]** FIG. 1 shows an exemplary ultrasound imaging system 10 including processing apparatus (block 12) (e.g., controller) and one or more ultrasound transducers, such as a transducer array that provides for transmission of pulses and reception of echoes (block 22). The processing apparatus (block 12) may be operably coupled to the one or more transducers (block 22) to facilitate imaging of an object of interest (e.g., capture of pulse-echo data from a region of interest) using the one or more transducers (block 22). Further, the processing apparatus (block 12) includes data storage (block 14). Data storage (block 14) allows for access to processing programs or routines (block 16) and one or more other types of data (block 18) that may be employed to carry out the exemplary imaging processes or methods (e.g., one which is shown generally in the block diagram of FIG. 2).

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**[0031]** For example, processing programs or routines (block 16) may include programs or routines for performing computational mathematics, matrix mathematics, compression algorithms (e.g., data compression algorithms), calibra-

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tion algorithms, image construction algorithms, inversion algorithms, signal processing algorithms, standardization algorithms, comparison algorithms, vector mathematics, or any other processing required to implement one or more embodiments as described herein (e.g., provide imaging, image reconstruction, etc.). Exemplary mathematical formulations/equations that may be used in the systems and methods described herein are more specifically described herein with reference to FIGS. 3-19.

**[0032]** Data (block 18) may include, for example, sampled pulse-echo information (e.g., sampled or collected using the one or more transducers (block 22)), data representative of measurements (e.g., measurements of structure in the region of interest, vascular properties or characteristics, etc.), results from one or more processing programs or routines employed according to the disclosure herein (e.g., reconstructed images of an object of interest, such as a blood vessel or regions around same), or any other data that may be necessary for carrying out the one or more processes or methods described herein.

**[0033]** In one or more embodiments, the system 10 may be implemented using one or more computer programs executed on programmable computers, such as computers that include, for example, processing capabilities (e.g., central processing units (CPUs), graphical processing units (GPUs)), data storage (e.g., volatile or non-volatile memory and/or storage elements), input devices, and output devices. Program code and/or logic described herein may be applied to input data to perform functionality described herein and generate desired output information (e.g., ultrasound images, reconstructed images, etc.). The output information may be applied, or otherwise used, as input to, or by, one or more other devices and/or processes as described herein (e.g., one or more therapy apparatus (block 20) such as a drug therapy apparatus, an ultrasound therapy apparatus, etc.).

**[0034]** The program(s) or routine(s) used to implement the processes described herein may be provided using any programmable language, e.g., a high level procedural and/or object orientated programming language that is suitable for communicating with a computer system. Any such programs may, for example, be stored on any suitable device, e.g., a storage media, readable by a general or special purpose program, computer or a processor apparatus for configuring and operating the computer (e.g., processor(s)) when the suitable device is read for performing the procedures described herein. In other words, at least in one embodiment, the system 10 may be implemented using a computer readable storage medium, configured with a computer program, where the storage medium so configured causes the computer to operate in a specific and predefined manner to perform functions described herein.

**[0035]** Likewise, the imaging system 10 may be configured at a remote site (e.g., an application server) that allows access by one or more users via a remote computer apparatus (e.g., via a web browser), and allows a user to employ the functionality according to the present disclosure (e.g., user accesses a graphical user interface associated with one or more programs to process data).

**[0036]** The processing apparatus (block 12), may be, for example, any fixed or mobile computer system (e.g., a personal computer or minicomputer, for example, with a CPU, GPU, etc.). The exact configuration of the computing apparatus is not limiting and essentially any device capable of providing suitable computing capabilities and control capabilities (e.g., control the imaging set up configuration and acquire data, such as pulse-echo data) may be used. Further, various peripheral devices, such as a computer display, mouse, keyboard, memory, printer, scanner, etc. are contemplated to be used in combination with the processing apparatus (block 12), such as for visualization of imaging results (e.g., display of images, display of therapy delivery in real time such as with use of high intensity focused ultrasound, etc.).

**[0037]** Further, in one or more embodiments, the output (e.g., an image, image data, an image data file, a digital file, a file in user-readable format, etc.) may be analyzed by a user, used by another machine that provides output based thereon, etc.

**[0038]** As described herein, a digital file may be any medium (e.g., volatile or non-volatile memory, a CD-ROM, magnetic recordable tape, etc.) containing digital bits (e.g., encoded in binary, trinary, etc.) that may be readable and/or writeable by processing apparatus (block 14) described herein.

**[0039]** Also, as described herein, a file in user-readable format may be any representation of data (e.g., ASCII text, binary numbers, hexadecimal numbers, decimal numbers, audio, graphical) presentable on any medium (e.g., paper, a display, sound waves, etc.) readable and/or understandable by a user.

**[0040]** Generally, the methods and systems as described herein may utilize algorithms implementing computational mathematics (e.g., matrix inversions, substitutions, Fourier transform techniques, etc.) to generate ultrasound images and/or reconstruct images described herein (e.g., from pulse-echo data).

**[0041]** In view of the above, it will be readily apparent that the functionality as described in one or more embodiments according to the present disclosure may be implemented in any manner as would be known to one skilled in the art. As such, the computer language, the computer system, or any other software/hardware which is to be used to implement the processes described herein shall not be limiting on the scope of the systems, processes or programs (e.g., the functionality provided by such systems, processes or programs) described herein.

**[0042]** One will recognize that a graphical user interface may be used in conjunction with the embodiments described herein. The user interface may provide various features allowing for user input thereto, change of input, importation or

exportation of files, or any other features that may be generally suitable for use with the processes described herein. For example, the user interface may allow default values to be used or may require entry of certain values, limits, threshold values, or other pertinent information. For example, such a user interface may allow a user to define control points (e.g., select points on a display panel, touchscreen, etc.), enter threshold values, perform therapy, use any of the features or functionality described herein, etc.

**[0043]** The methods described in this disclosure, including those attributed to the systems, or various constituent components, may be implemented, at least in part, in hardware, software, firmware, or any combination thereof. For example, various aspects of the techniques may be implemented within one or more processors, including one or more microprocessors, DSPs, ASICs, FPGAs, or any other equivalent integrated or discrete logic circuitry, as well as any combinations of such components, image processing devices, or other devices. The term "processor" or "processing circuitry" may generally refer to any of the foregoing logic circuitry, alone or in combination with other logic circuitry, or any other equivalent circuitry.

**[0044]** Such hardware, software, and/or firmware may be implemented within the same device or within separate devices to support the various operations and functions described in this disclosure. In addition, any of the described components may be implemented together or separately as discrete but interoperable logic devices. Depiction of different features, e.g., using block diagrams, etc., is intended to highlight different functional aspects and does not necessarily imply that such features must be realized by separate hardware or software components. Rather, functionality may be performed by separate hardware or software components, or integrated within common or separate hardware or software components.

**[0045]** When implemented in software, the functionality ascribed to the systems, devices and methods described in this disclosure may be embodied as instructions on a computer-readable medium such as RAM, ROM, NVRAM, EEPROM, FLASH memory, magnetic data storage media, optical data storage media, cloud storage, or the like. The instructions may be executed by one or more processors to support one or more aspects of the functionality described in this disclosure.

**[0046]** The imaging system 10 may further be used with, or may form a part of an optional therapy apparatus (block 20). For example, the therapy apparatus (block 20) may use the results of ultrasound imaging to provide one or more therapies. In one or more embodiments, the therapy apparatus (block 20) may be a non-invasive or invasive therapy apparatus such as a drug delivery apparatus or system (delivery of a drug to a particular location), a surgical apparatus or system (e.g., delivery of a stent to a particular position), an ablation apparatus or system (e.g., a high intensity focused ultrasound therapy apparatus or system), etc.

**[0047]** In one or more embodiments, the therapy apparatus (block 20) may be a separate system or apparatus that receives an output from the imaging system (e.g., image information) and delivers one or more therapies. In other embodiments, the therapy apparatus (block 20) may be integrated with the imaging system to perform the one or more therapies (e.g., a high intensity focused ultrasound system that uses dual mode ultrasound transducer(s) for diagnostics such as imaging, as well as for treatment, such as ablation). For example, in one or more embodiments, the therapy apparatus (block 20) may include one or more portions of a system such as described in PCT International Publication No. WO2009/002492 entitled "Image Guided Plaque Ablation," published 31 December 2008. For example, the ultrasound imaging described herein may be used for reducing vascular plaque non-invasively. For example, the ultrasound imaging described herein may be used to identify flow and vascular characteristics needed to non-invasively perform ablation of plaque as described in PCT International Publication No. WO2009/002492. Further, for example, one or more embodiments of the present disclosure may incorporate one or more features as described in U.S. Patent Application Publication No. US2012/0283564 A1 entitled "Vascular Characterization Using Ultrasound Imaging" published 8 November 2012 (e.g., including, for example, any image formation and/or reconstruction approaches described therein).

**[0048]** For example, the system may include a therapy system for non-invasively elevating the temperature of tissue by ultrasound energy waves including: at least one ultrasound delivery device adapted to deliver ultrasound energy waves to a focal point of targeted tissue; a temperature monitoring device for monitoring the temperature of targeted tissue at the focal point; and a controller for steering and controlling the ultrasound delivery device to deliver ultrasound energy waves at a focal point to elevate the temperature of targeted tissue to a desired temperature.

**[0049]** Further, for example, the therapy system may use one or more imaging systems described herein to produce an image of at least a portion of a mammalian body, e.g., such that the location of at least one vascular plaque in said image can be determined and to ascertain the location of the base of said vascular plaque. For example, ultrasound delivery device may ascertain one or more target locations at the base of the plaque. Still further one or more embodiments of the imaging system provided herein may be used in a method for elevating the temperature at a target location by an energy wave using an ultrasound therapy system (e.g., which may be the same ultrasound system (ultrasound transducers thereof) used for imaging). For example, the method may include delivering a beam of ultrasound energy waves from a source to the target location; monitoring the temperature of the target location; and stopping the delivering of the beam of ultrasound energy waves if a desired temperature at the target location has been reached.

**[0050]** Further, a method of preparing a plan for non-invasively elevating the temperature of tissue in a vessel wall

leading to regression of vascular plaques may include imaging at least a portion of a body to produce an image (e.g., using ultrasound imaging as described herein to image a vascular region); determining the location of at least one vascular plaque in said image; ascertaining the location of the base of said vascular plaque and one or more target locations at the base of the plaque (e.g., using the ultrasound generated image); and/or determining the parameters for delivering ultrasound energy waves from a source to a focal point for elevating the temperature of targeted tissue in the vessel wall to a desired temperature, sufficient for reducing or destroying vaso vasorum.

**[0051]** Further, for example, the ultrasound imaging described herein may be used to identify flow and vascular characteristics needed to perform invasive treatments of plaque (e.g., stent delivery, cardiac surgery, etc.)

**[0052]** Still further, in one or more embodiments, the therapy apparatus (block 20) may include one or more portions of a system such as described in U.S. Patent Application Publication No. US2013/0144165 A1, entitled "Dual Mode Ultrasound Transducer (DMUT) System and Method for Controlling Delivery of Ultrasound Therapy" published 6 June 2013. For example, the ultrasound imaging described herein may be performed with the same or similar transducer arrays described therein which can be used for both imaging (e.g., to monitor a therapy procedure), as well as for delivering therapy (e.g., to deliver high intensity focused ultrasound energy). For example, therapy may be delivered using the ultrasound transducer array, while the imaging modes using the same transducer array may be used to guide the therapeutic beam, assess thermal and mechanical tissue response to estimate doses of therapy (e.g., initial dose of therapy), monitor and characterize tissue response during therapy, and assess the state of the treated tissue at the completion of each exposure to the therapeutic ultrasound energy (e.g., real time monitoring between periods of therapy delivery).

**[0053]** For example, ultrasound imaging as described herein may be used to identify one or more vascular characteristics. An exemplary diagram of a blood vessel 50 is shown in Figure 11 to facilitate discussion of the use of imaging described herein. The blood vessel 50 shown in Figure 11 includes a vessel wall 52 having a plaque structure 54 formed on the interior of the vessel wall 52. The plaque architecture of the structure 54 may include, for example, a plaque base 56, a lipid core 58, and a fibrous or calcified cap 60. Blood 62 flows through the blood vessel 50 defined by the vessel wall 52.

**[0054]** One or more embodiments of methods and/or systems described herein may be used to identify one or more vascular characteristics, e.g., flow characteristics associated with the flow through the blood vessel 50, structural characteristics associated with the blood vessel 50, and/or hemodynamic characteristics. For example, flow characteristics may include flow velocity, volume flow, wall shear stress, wall shear rate, etc.

**[0055]** For example, structural characteristics may include determining boundaries of the vessel wall (e.g., outer and inner boundaries, such as in a coordinate system), thickness of the vessel wall, measurement of tissue properties within the vessel wall (e.g., stiffness of tissue, such as, for example, it relates to a diseased state), differentiation of plaque from vessel wall, differentiation of the various components of plaque (e.g., differentiation of base from lipid core, differentiation of base from fibrous cap, differentiation of lipid core from fibrous cap, etc.), etc. For example, in one or more embodiments, upon differentiation of the base from the fibrous cap of the plaque architecture, treatment may be provided to ablate the base to reduce further plaque buildup or growth or provide treatment according to PCT International Publication No. WO2009/002492.

**[0056]** Still further, for example, hemodynamic characteristics may include calculated hemodynamic measurements, such as, for example, arterial pressure, cardiac output, arterial compliance, pulse wave velocity, etc. At least in one embodiment, such hemodynamic measurements may be determined based on parameters relating to both tracking of the blood flow and tracking of vessel wall motion or displacement. As such, to obtain an accurate hemodynamic determination, the parameters or measurements relating to both tracking of the blood flow and tracking of vessel wall motion or displacement must be determined simultaneously, or within a periodic cycle in which both can be determined (e.g., determined effectively). For example, compliance of the vessel may be based on both volume flow which relates to tracking of blood flow and pressure within the vessel which can be determined by tracking vessel displacement.

**[0057]** In one or more embodiments, the ultrasound quantitative imaging system may be used for assessment of the disease state in atherosclerotic blood vessels. For example, the imaging may be used for the direct estimation of the strain fields in the vicinity of the vessel walls. Such methods may mitigate the deleterious effects of local deformations that could result in loss of correlation, and which may render the correlation-based speckle tracking approach useless in the vicinity of the vessel wall. Such deformations, depending on severity, could result in erroneous estimate in the velocity (and therefore strain) estimation or may even result in loss of accuracy.

**[0058]** The one or more ultrasound transducers (block 22) may be any apparatus (e.g., transmitting, receiving components, etc.) capable of delivering ultrasound pulses and sampling/collecting ultrasound echo energy contemplated to be used in ultrasound imaging systems and in combination with processing apparatus (block 12) of the system 10. As used herein, such transducers may include a transmitting portion, e.g., to deliver pulse energy, and a receiving portion, e.g., to sample/collect echo or reflected energy, which may or may not be the same portion. During the ultrasound imaging of a target (e.g., a blood vessel, such as a carotid artery, coronary artery, etc.), the one or more transducers (block 22) may be positioned relative to the target so as to be capable of delivering energy to the target resulting in

reflected energy (also known as the resultant pulse-echo or echo energy) and also sampling the echo energy.

**[0059]** The one or more transducers (block 22) may include multiple transducers position separately from one another or may be a transducer array. In one or more embodiments, various arrays may have one or more benefits over others. For example, in one or more embodiments, the transducer array may be a segmented concave transducer with multiple sub-apertures to insonify the vessel from multiple angles. This will allow for better definition of the vessel boundaries from more directions. At least one sub-aperture may be used in linear array or phased array mode for initial B-mode and strain imaging of the vessel. The driver of the transducer may be designed to drive the multiple sub-apertures with independent codes. Each sub-aperture may be a one-dimensional or two-dimensional array. Coded excitation may help improve both the data rates (e.g., provide higher frame rates) and echo quality (e.g., by reducing reverberations within the lumen). The receiver may be a multichannel receiver with beamforming and/or pulse compression for coded excitation.

**[0060]** For example, various arrays and operation thereof, are described in Ebbini et al., "Dual-Mode Ultrasound Phased Arrays for Image-Guided Surgery," *Ultrasound Imaging*, vol. 28, pp. 65-82 (2006); Ballard, et al., "Adaptive Transthoracic Refocusing of Dual-Mode Ultrasound Arrays," *IEEE Transactions on Biomedical Engineering*, vol. 57, no. 1, pp. 93-102 (Jan. 2010); Wan et al., "Imaging with Concave Large-Aperture Therapeutic Ultrasound Arrays Using Conventional Synthetic-Aperture Beamforming," *IEEE Transactions on Ultrasound, Ferroelectrics, and Frequency Control*, vol. 55, no. 8, pp. 1705-1718 (August 2008); and Y. Wan and E.S. Ebbini, "A Post-beamforming 2-D Pseudoinverse Filter for Coarsely Sampled Ultrasound Arrays," *IEEE Trans on Ultrasonics, Ferroelectrics, and Frequency Control*, vol. 56, no. 9, pp.1888-1902 (2009).

**[0061]** A flow chart of an exemplary method 30 using ultrasound imaging as described herein is depicted in FIG. 2. One will recognize that one or more of the blocks of functionality described herein may be carried out using one or more programs or routines, and/or any other components of an imaging system (e.g., the imaging system 10 of FIG. 1) and/or therapy system (e.g., the therapy apparatus 20 of FIG. 1).

**[0062]** Generally, the method 30 may include providing imaging of a region of interest (e.g., an ultrasound image of a region of interest using conventional ultrasound processes) (block 32). For example, the region of interest may be a region in a living subject (e.g., a human, an animal, etc.) such as a blood vessel, spinal region, brain region, kidney region, etc. For example, imaging may be performed using conventional synthetic aperture (SA) imaging, conventional B-mode imaging, M2D mode imaging (see, Liu and Ebbini, "Real-time 2D Temperature Imaging Using Ultrasound," *IEEE T-BME*, vol. 57, no. 1, pp. 12-16 (2010), etc. Further, for example, such imaging may be provided using other imaging technology such as magnetic resonance imaging (MRI), simultaneously or prior to the ultrasound scan, etc.

**[0063]** The method 30 may further perform adaptive ultrasound imaging using a plurality of control points defined within the region of interest (block 34) (e.g., to provide data for ultrasound image formation). In one or more embodiments, adaptive coded waveforms for application to ultrasound transducer elements of a transducer apparatus are designed to match the spectral content of the target or region of interest (e.g., a specular reflector like a blood vessel wall). Further, in one or more embodiments, the target or region of interest is defined by a set of appropriately selected control points. Such control points being used to define one or more performance criteria of the imaging system (e.g., signal-to-noise ratio, contrast ratio, etc.). For example, in one or more embodiments of the adaptive imaging, contrast ratio (CR) in the target region is incorporated as a measure for adjusting (e.g., increasing) bandwidth of the coded waveforms. Further, for example, in one or more embodiments of the adaptive imaging, signal-to-noise ratio (SNR) is incorporated as a measure for adjusting (e.g., improving) a spectral match between the coded waveforms at the frequency response of that target region (e.g., including the control points), for example, which may reduce the effective bandwidth (BW). Still further, in one or more embodiments of the adaptive imaging, a computationally efficient DFT-based filter bank (e.g., a pre-beamforming filter bank or a post-beamforming filter bank) may be used for analysis of pulse echo data received from the target region (e.g., including from the control points).

**[0064]** It will be recognized that the adaptive imaging described herein is distinctly different from the spread-spectrum approaches described, for example, in article, T. Misardis and J.A. Jensen, "Use of modulated excitation signals in medical ultrasound. Part I: basic concepts and expected benefits," *IEEE Trans. Ultrason., Ferroelect., Freq.Contr.*, vol. 52, no.2, pp. 177-191 (Feb. 2005) or in U.S. Patent Application Publication No. US2013/0123635 A1, to Wegner entitled "Spread Spectrum Coded Waveforms in Ultrasound Imaging." For example, such previously described spread spectrum approaches do not use waveform synthesis based on specific definition of control points within the target region of interest as described herein, do not provide an adaptive waveform code design that achieves specified contrast ratio and signal-to-noise ratio values within the region of interest as described herein (e.g., the adaptive imaging herein provides a time bandwidth (TBW) product that is adjustable and different control points in the region of interest compared to an open loop waveform design), and do not use running DFT-based detection and reconstruction components employed pre-beamforming and/or post-beamforming as part of the receiver chain.

**[0065]** Further, with reference to FIG 2, the adaptive imaging process (block 34) provides image data such that image formation and/or image reconstruction may be provided (block 36). Based upon such imaging, optional diagnostic and/or therapy processes may be performed (block 38) (e.g., HIFU processes, drug delivery, identification of diseased coronary structure, etc.).

5 [0066] A flow chart of an exemplary adaptive imaging method 80 is depicted in FIG. 3 and shall be described with reference thereto as well as to FIGS. 4-5. Generally, the method 80 includes providing a region of interest such as described with reference to FIG. 2 (e.g., an ultrasound image of a region of interest using conventional ultrasound imaging, such as conventional synthetic aperture (SA) imaging, conventional B-mode imaging, M2D mode imaging, etc.). For example, as shown in block 82, conventional/coded SA imaging may be used. With such imaging provided, a region of interest (ROI) is defined and control points (CPs) in the region of interest are defined (also shown in block 82). For example, such imaging may be provided using a transducer apparatus that includes a plurality of ultrasound transducer elements (e.g., such as shown generally in FIG. 1, wherein each of the plurality of ultrasound transducer elements being configured to deliver ultrasound energy to the region of interest in response to a waveform applied thereto). For example, block 82 more specifically describes the adaptive imaging starting from a conventional imaging process used to define the region of interest (ROI) and a set of control points (CPs) (e.g., which, in the context of vascular imaging, the CPs may be associated with the wall and lumen of a target vessel within the ROI).

10 [0067] Generally, for example, the control points defined in the region of interest correspond to identifiable portions therein. For example, at least a first portion of the control points may be associated with a first identifiable portion of the region of interest, a second portion of the control points may be associated with a second identifiable portion of the region of interest, and so forth. At least in one embodiment, the different portions of the control points correspond to identifiable portions of the region of interest that are distinct and/or different from each other portions therein. For example, as described herein, a first portion of the control points may be associated with a vessel wall of a vascular structure and the second portion of the control points may be associated with a lumen defined by at least a part of the vessel wall. Further, for example, a third portion of the control points may be associated with tissue about the vessel wall.

15 [0068] The selection of the CPs may be based on an initial hypothesis of the vessel wall location. This hypothesis may be formed based on conventional DMUA imaging or other a priori information, such as information from magnetic resonance imaging (MRI), diagnostic ultrasound imaging, intravascular ultrasound (IVUS) imaging, etc. For example, FIG. 4 illustrates the use of a DMUA 40 in imaging a cross-sectional view of a blood vessel wall 42 with assumed inner diameter 43 and outer diameter 44 (e.g., inner and outer diameters of 5.2 mm and 6.8 mm, respectively). The candidate CPs are shown as "Xs" and "Os" on a grid covering the lumen 45, vessel wall 42, and some of the surrounding tissues 46 around or about the vessel wall 42.

20 [0069] FIG. 4 also shows an array point spread function (psf) (e.g., discernible in gray scale as lighter at the center of the lumen 45 and having different shades outward therefrom) at a single frequency when focused at its geometric center. This classical psf illustrates the relatively high lateral resolution compared to the axial resolution in this single frequency (e.g., continuous wave (CW)) case. Broadband spectrum of the array excitation may improve the axial resolution.

25 [0070] Based on the hypothesized vessel wall geometry, a user can designate the CPs as vessel wall CPs (i.e., circles or Os), lumen CPs (Xs in lumen 45) or tissue CPs (Xs about the vessel wall 42). These candidate CPs and their designations can be modified based on adaptive imaging tests described herein. It is noted that the hypothesis does not limit the ability of image reconstruction algorithms to adaptively modify the wall geometry as a result of actual hypothesis testing based on multi-frequency echo data from the ROI.

30 [0071] With further reference to Figure 3, the adaptive imaging method 80, for example, using waveform synthesis, generates a waveform for each ultrasound transducer element of the plurality of ultrasound transducer elements used in the process (shown generally by arrow 85). For example, the waveform may be generated by selecting one or more imaging frequencies within a transducer apparatus bandwidth. Each of the one or more imaging frequencies may be associated with (e.g., be a carrier for) a pulse to be transmitted having a finite bandwidth within the transducer apparatus bandwidth.

35 [0072] Element frequency components (e.g., frequency component for each transducer element) are then generated for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element. In at least one embodiment, the transducer element frequency components are provided by generating one or more excitation vectors. For example, each excitation vector may be generated using field synthesis at a single frequency of the one or more imaging frequencies within the transducer apparatus bandwidth. The excitation vector generated includes an element frequency component corresponding to each ultrasound transducer element of the plurality of ultrasound transducer elements used for the adaptive process. In one or more embodiments, the term field synthesis refers to the use of single frequency component to produce a specified multiple focus pattern using a geometrically defined transducer array. For example, this may be achieved by solving an inverse problem that computes the complex excitation vector to the array elements. The complex elements of the excitation vector may define the magnitude and phase of the sinusoidal signals driving the array elements to realize the specified field pattern. This approach is, for example, described in Ebbini et al., "Multiple-focus ultrasound phased-array pattern synthesis: Optimal driving-signal distributions for hyperthermia", IEEE Transactions on Ultrasonics, Ferroelectrics, and Frequency Control, 36(5):540-548 (1989). The term waveform synthesis, at least in one or more embodiments herein used to provide imaging, refers to one or more processes of using an array driven by arbitrary waveforms to realize specific waveforms at specific control points with each synthesized waveform, in principle, completely independent of all the others. For

example, the actual level of independence or orthogonality between the waveforms depends on the available bandwidth and the selection of the control points (e.g., one cannot achieve two independent waveforms at two closely spaced waveforms when the spacing is smaller than the width of the point spread function of the array at that location). The synthesis algorithm defined in Fig. 5 is one exemplary approach to waveform synthesis.

**[0073]** In more detail with reference to FIG. 3, waveform generation 85 may be implemented by an algorithm that begins by selecting  $N_F$  frequencies from the available transducer apparatus bandwidth (block 84) (e.g., such frequencies or pulse carrier frequencies may be selected at random), or

i.e.,  $f_n \in [f_{min}, f_{max}]$ ,  $n = 1, 2, \dots, N_F$

**[0074]** Using a priori defined values of SNR and CR (e.g., desired SNR value, expected CR value as shown in block 86, for example, based on other information, such as other image data, knowledge of the target such as the type of target, etc.), each frequency component may be a carrier of a finite-bandwidth pulse (e.g., a raised cosine pulse) of duration  $T_n$ ; which defines the time-bandwidth (TBW product), where:

$T_n$ ,  $n = 1, 2, \dots, N_F$ .

**[0075]** The finite-bandwidth pulse of duration  $T_n$ ,

For each frequency component, a multiple-focus optimization problem may be solved using a synthesis algorithm which results in an excitation vector of the array elements,  $u(f_n)$ . For each array element,  $i$ , the component of the excitation vector,

$$\{u_i(f_n)\}_{i=1}^{N_e},$$

represents a frequency component  $f_n$ , of the coded waveform driving the transducer elements. Therefore, the waveform synthesis problem amounts to solving the multiple-focus synthesis problem at all frequencies of interest and combining their corresponding finite-bandwidth pulses (e.g., raised cosine waveforms) with appropriate weighting taking the system (e.g., transducer apparatus) bandwidth into account. One exemplary algorithm of such synthesis is provided in Algorithm 1 in Figure 5 provided with respect to vessel Wall CPs (e.g., control points on a vessel wall), Lumen CPs (e.g., control points in the lumen defined by a vessel wall), and Critical CPs (e.g., critical control points placed at certain locations, such as, for example, those locations where the transmit energy is to be minimized (e.g., ribs, etc.). For example, the wavefront synthesis approach described in at least one embodiment herein may employ a finite number of randomly selected single frequency components (e.g., carriers for pulses) within the transducer bandwidth. Each carrier, for example, has a finite bandwidth specified by its duration and modulating pulse, e.g., a raised cosine. The carrier phase and amplitude can be adjusted, in addition to the delay, to achieve a specified SNR and CR values for a given selection of CPs in the region of interest. This approach is distinct from other previously proposed waveform design methods by at least its adaptive nature and randomness of the carriers.

**[0076]** Once the waveform synthesis is completed, the element waveforms may be downloaded to a driver memory and used to drive the array of transducer elements in pulsed mode in substantially the same way as conventional ultrasound systems, except that different transducer elements of the array are driven by different waveforms. This may be performed without the need for any beamforming since beamforming is included in the selection of the CPs. Beamforming is included in the selection of CPs due to the fact that the waveform synthesis process, by producing specified waveforms at any CPs, automatically adjusts the delays, phase shifts, and amplitudes of the single-frequency components to achieve the necessary focusing at the CPs. For example, with reference to Figures 17A-B, take an example that includes five control points. A five focus wavefront may be used, with each of the five control points being associated with a desired waveform that was synthesized by a basis set of narrowband functions (e.g., almost like a single frequency waveform). Figure 17A illustrates the single frequency five-focus pattern synthesis, which is one step of the algorithm in Figure 5. The pattern in Figure 17B represents a five-focus pattern resulting from the wavefront synthesis of five independent codes at the same five control points.

**[0077]** In other words, after the waveform synthesis is completed, ultrasound energy is delivered in pulsed mode to the region of interest using the plurality of ultrasound transducer elements in response to waveforms generated for each of the plurality of ultrasound transducer elements. As shown in FIG. 3, a synthesized coded multi-focus pattern of ultrasound energy is provided (e.g., delivered or otherwise transmitted to) at the CPs. In the embodiment of a blood vessel as shown in FIG. 4, the multi-focus pattern of ultrasound energy is provided at the CPs around the vessel wall 42 and within the lumen 45.

**[0078]** In response to the delivery of ultrasound energy to the region of interest, pulse echo data is received at each ultrasound transducer element of a plurality of ultrasound transducer elements for use in generating an image based thereon. In other words, pulse-echo imaging is performed based on the pulse echo data received by the plurality of transducer elements (block 90). For example, various processes may be used to separate pulse echo components received from the control points associated with identifiable portions within the region of interest (e.g., pulse echo components received from the first portion of the control points associated with the first identifiable portion of the region

of interest may be separated from the received pulse echo data, pulse echo components received from the second portion of the control points associated with the second identifiable portion of the region of interest may be separated from the received pulse echo data, etc.)

**[0079]** For example, received pulse echo data may be beamformed in any suitable manner and filtering (e.g., pre-beamforming and/or post-beamforming) may be applied in any suitable manner to separate the pulse echo components from individual CPs (and their vicinities). Such pre-beamforming and/or post-beamforming may be DFT based beamforming. Further, for example, depending on  $N_f$  (i.e., the number of distinct frequencies used in synthesizing the driving waveforms), the received pulse echo data can be filtered using bandpass filters centered at  $f_n$  prior to beamforming. Further, for example, alternately, beamformed data can be processed by this type of filter bank. Regardless, any suitable processing may be used that provides the objective of estimating the spectral components of the echoes from each of the control points. Further, in one or more embodiments, pulse-compression techniques, such as inverse or matched filtering can be applied to at this stage. The energy of the echoes from the CPs can be used to compute a contrast ratio between identifiable portions in the region of interest (block 92). For example, a contrast ratio may be determined between the first and second identifiable portions based on the pulse echo components received from the first portion of the control points associated with the first identifiable portion (e.g., vessel wall) of the region of interest and the pulse echo components received from the second portion of the control points associated with the second identifiable portion (e.g., lumen) of the region of interest. Likewise, a contrast ratio may be determined between first and third identifiable portions based on the pulse echo components received from the first portion of the control points associated with the first identifiable portion (e.g., vessel wall) of the region of interest and the pulse echo components received from the second portion of the control points associated with the second identifiable portion (e.g., tissue about the vessel wall) of the region of interest.

**[0080]** For example, when contrast ratios for blood vessel structure,  $CR$  may be defined as:

$$CR = \frac{\sum_{k=1}^{N_W} E_k^W}{\sum_{k=1}^{N_L} E_k^L}$$

where  $E$  denotes the energy from a control point and the subscripts  $W$  and  $L$  denote wall and lumen, respectively.

**[0081]** Similarly, the energy of the echoes from the CPs and one or more reference portions of the region of interest can be used to compute a signal-to-noise ratio (block 96). For example, a signal-to-noise ratio may be determined based on pulse echo components received from a reference portion of the region of interest and pulse echo components received from the control points associated with one or more identifiable portions of the region of interest (e.g., control points associated with the first identifiable portion such as a vessel wall, control points associated with the second identifiable portion of the region of interest such as the lumen, etc.).

**[0082]** For example, signal-to-noise ratio for blood vessel structure,  $SNR$ , may be defined as:

$$SNR = \frac{\sum_{k=1}^{N_W} E_k^W + \sum_{k=1}^{N_L} E_k^L}{\sum_{k=1}^{N_R} E_k^R},$$

where the subscript  $R$  denotes a reference region which characterizes the noise, e.g. anechoic region.

**[0083]** As shown in FIG. 3, the waveform generated for one or more of the plurality of ultrasound transducer elements (e.g., generated using waveform synthesis of the block 88) may be modified based on at least one of the calculated contrast ratio and the signal-to-noise ratio (e.g., as shown by the decision blocks 92 and 96 along with respective loops via blocks 94 and 97). For example, the method 80 may compare at least a calculated signal-to-noise ratio to a threshold value and modify the waveform synthesis process for generating the waveform to be applied to the one or more plurality of ultrasound transducer elements based on the comparison. Likewise, for example, the method 80 may compare at least a calculated contrast ratio to a threshold value and modify the waveform synthesis process for generating the waveform to be applied to the one or more plurality of ultrasound transducer elements based on the comparison.

**[0084]** With further reference to FIG. 3, for example, the calculated  $CR$  and  $SNR$  quantities may be compared to specified threshold values  $\gamma_c$  and  $\gamma_s$  to decide the manner in which the frequency components of the transmit waveform for driving the plurality of ultrasound transducer elements should be modified. For example, if the calculated  $CR$  is below its threshold (block 92), the time-bandwidth (TBW) product may be increased (block 94) by increasing the gain at frequencies at the edge of the transducer passband (e.g., using a form of inverse filtering). If the calculated  $CR$  is not below its threshold (block 92), then the calculated  $SNR$  may be compared to its threshold (block 96). If the  $SNR$  is higher than the threshold (block 96), then the adaptive imaging procedure has converged and data may be acquired for image formation and reconstruction in the target region of interest (block 98). If the  $SNR$  is not higher than the threshold (block

96), then spectral matching between the transmit waveforms and the echo components is emphasized (block 97) (e.g., using a form of matched filtering). This amounts to reducing the TBW product. Therefore, the two tests (e.g., using calculated SNR and CR) produce two arms of balancing the spectral components of the transmit waveforms to maximize the contrast between the vessel wall and the lumen while maximizing the SNR from the whole region of interest.

5 **[0085]** In one or more embodiments, various actions may be taken to modify the waveform synthesis process. For example, such modifications may include adjusting gain at frequencies of the one or more frequencies located in more locations within the transducer apparatus bandwidth, adjusting one or more pulse parameters including at least one of pulse duration, pulse shape, pulse amplitude, and pulse phase to adjust time bandwidth product, etc.

10 **[0086]** Image formation is generally implemented using beamforming techniques which amount to back propagation in a homogeneous medium. This may also include an aberration correction that still produces an image of the reflectivity map of an inhomogeneous object. The adaptive imaging described herein may also perform image formation in the same sense as conventional image formation methods (e.g., producing an image of the reflectivity map of an object), but differs from these methods in that it modifies the transmit waveforms to maximize both SNR and CR in a given ROI.

15 **[0087]** This adaptive image formation may be followed by a reconstructive process that utilizes single-frequency components (e.g., extracted using a running DFT processor for each frequency). Any number of image reconstruction algorithms may be used. For example, the Born or Rytov algorithms can be used depending on the nature of the heterogeneity W.C. Chew, *Waves and Fields in Inhomogeneous Media*, Van Nostrand Reinhold, New York (1990). Further, a higher order distorted Born approximation can be used O. Haddadin and E.S. Ebbini, "Ultrasonic Focusing through Inhomogeneous Media by Application of the Inverse Scattering Problem," *J. Acoustical Society of America*, vol. 104, no. 1, pp. 313 - 325 (1990). For example, these algorithms may be implemented in matrix form and may best be implemented on a GPU or multi-core CPU. Further, for example, it can even be implemented on clusters in the cloud. In one or more embodiments, the matrix operators may be simplified and implemented in terms of the DFT.

20 **[0088]** Figures 15-16 show one or more embodiments usable for image reconstruction. Such embodiments are just examples, but a variety of similar scenarios can be achieved by proper synthesis of the coded wavefront to simplify the reconstruction operator. As shown therein, a plurality of transducer elements 600 are used to capture the pulse echo data and a running DFT computational block 602 at a frequency of interest for each receiving element may be used to extract single-frequency components from such pulse echo data. Beamforming may be applied, such as by a frequency-domain beamforming network 606 (e.g., DFT and beamforming may both be implemented on an FPGA). The interconnection network 604 may be implemented in software under program control using a programming language suitable for a multiple core GPU, e.g., CUDA or OpenCL. The interconnection network 604 may also be based on the use of physical memory for buffering running DFT outputs before beamforming. This physical memory may be realized inside an FPGA using distributed memory or block memory features available on many FPGA. Alternatively, interconnection network 604 may be implemented outside the FPGA with appropriate bus architecture and address control circuitry.

25 **[0089]** Image reconstruction 608 may be performed as described herein (e.g., to provide imaging of the scattering function or other quantitative property of the ROI). Further, an adaptive algorithm 610 may be used to provide enhanced image formation as described herein, for example, with reference to Figure 5. For example, to provide image reconstruction of scattering function or other quantitative property of the ROI (e.g., such as, speed of sound, attenuation, or reflection coefficients), the beamformed output 620 from the beamforming network 606 may be applied to an image reconstruction process as shown in Figure 16.

30 **[0090]** As shown in Figure 16, a matrix operator is pre-computed (see block 624) and used in solving inverse scattering problems 626 (see O. Haddadin and E.S. Ebbini, "Imaging Strongly Scattering Media Using Multiple-frequency Distorted Born Iterative Method," *IEEE Trans. UFFC*, vol. 5, no. 6, pp. 1485-1496, 1998). In the context of linear array imaging illustrated in Fig. 9, the running DFT (blocks 622) computes a SFPM vector that defines the receive data from one sub-aperture (associated with each image line). The distorted Born iterative method (DBIM) may be used to solve for the scattering function at every pixel using the pre-computed single-frequency operators associated with the sub-aperture associated with the given A-line.

35 **[0091]** The adaptive imaging approach described herein is not limited for use in imaging vascular structure. As indicated herein adaptive ultrasound has the potential to perform imaging and therapy in complex media using is a new paradigm which represents a unified approach to imaging and therapy using arbitrary waveform generation (e.g., as opposed to being hampered by the use of conventional CW or pulsed excitations on the therapy and imaging sides). In principle, given the target size and depth together with a general understanding of its surroundings (e.g. bone, ligaments, etc.) a DMUA with relatively small number of elements to produce high quality focusing (for imaging and therapy) within the target while avoiding the critical structures in the path of the beams may be designed. Therefore, lower back pain, stroke, cardiac ablation, renal denervation and any number of applications where precise ablation is sought can be exquisitely performed using this adaptive imaging described herein.

40 **[0092]** Such an approach can be extended to imaging more complex media such as shown in FIG. 12. FIG. 12 shows a DMUA 340 targeting of a liver tumor 342 in a transthoracic imaging/therapy scenario. Conventional synthetic aperture (SA) imaging as described in the article, Ebbini et al., "Dual-mode ultrasound phased arrays for image-guided surgery,"

Ultrasound Imaging, vol. 28, pp. 201-220 (2006), can be used to obtain an image of the medium suitable for adaptive refocusing as was illustrated in the article, Ballard, et al., "Adaptive transthoracic refocusing of dual-mode ultrasound arrays," IEEE Trans Biomed Eng, vol. 57, no. 1, pp. 93-1-2 (Jan 2010).

**[0093]** In SA mode, the RF data from an image pixel at  $P(x_p, z_p)$  in a medium with uniform speed of sound,  $c$ , is computed by:

$$I(x_p, z_p) = \sum_{i=1}^{64} \sum_{j=1}^{64} A_i \cdot B_j \cdot s_{i,j} \left( \frac{R_{ip} + R_{jp}}{c} \right)$$

where  $A_i$  and  $B_j$  are, respectively, the transmit and receive apodization weights,  $R_{ip}$  and  $R_{jp}$  are, respectively, the distances from the transmitting and receiving elements to the image pixel  $P$ , and  $S_{i,j}(t)$  is the echo received by element  $j$  when transmitting with element  $i$ . Other imaging scenarios can be performed by specializing the image formation as described in the article, T. Misardis and J.A. Jensen, "Use of modulated excitation signals in medical ultrasound. Part I: basic concepts and expected benefits," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 52, no.2, pp. 177-191 (Feb. 2005).

**[0094]** SA imaging can be implemented in real time in an ultrasound imaging system. Furthermore, taking the directivity patterns into account can improve the contrast by rejecting echo data from low SNR pixels in the target region as described in the article, Y. Wan and E.S. Ebbini, "Imaging with concave large-aperture therapeutic ultrasound arrays as in conventional synthetic-aperture beamforming," IEEE Trans Ultrason Ferroelectr Freq Control, vol. 55, no. 8, pp. 1705-1718 (Aug 2008). For example, the pixel at  $(x_p, z_p)$  in FIG. 12 is shown outside the target tumor (darkest region) with lines from the centers of a pair of transmitting and receiving elements defining propagation delays for the SA imaging. The directivity functions for the transmit-receive pair are also shown. The product of the transmit-receive directivity patterns at pixel  $(x_p, z_p)$  for a given transmit-receive pair is a measure of the SNR. The SA beamforming can be modified to account for this variation in SNR resulting in an improved contrast at the expense of reducing the field of view of a concave array like the one shown in FIG. 12.

**[0095]** A heterogeneous medium with strong scatterers as shown in FIG. 12 can be approximately imaged using a real-time SA method. Alternatively, a tomographic reconstruction method can be employed, but these methods do not lend themselves to real-time implementation. The adaptive imaging algorithm shown and described herein can be applied with obvious modifications, primarily in the assignment of the CPs. For example, the CPs can be chosen to maximize the SNR within the "hypothesized tumor" or "target" region. This may be considered a generalization of our single-transmit focusing system described in the article, Ebbini et al., "Dual-mode ultrasound phased arrays for image-guided surgery," Ultrasound Imaging, vol. 28, pp. 201-220 (2006), and in earlier patent applications, such as U.S. Patent Application Publication No. US2013/0144165 A1, entitled "Dual Mode Ultrasound Transducer (DMUT) System and Method for Controlling Delivery of Ultrasound Therapy" published 6 June 2013. Additional critical points may be placed at the rib locations to minimize exposure to the ribs while maximizing the SNR at the target CPs.

**[0096]** Adaptive imaging can be used for imaging and targeting of complex structures for possible treatment of lower back pain in individuals not responding to medical treatment. Adaptive imaging will allow for maximizing the sensitivity and specificity to echoes from the soft disc tissues as shown in FIG. 13 while suppressing interference from the nearby bone structure. CPs associated with the disc region and echoes from the bone can be defined to perform the necessary optimization problem. In this application, it may be possible to image the nerve root associated with a given vertebra for targeting or avoidance as indicated by the appropriate protocol.

**[0097]** Adaptive imaging can also be applied in trans-skull imaging and targeting of brain structures, e.g. sonothrombolysis for acute ischemic stroke. The selection of the CPs will be to enhance the sensitivity and specificity of Doppler signals from the target (e.g., a clot) region. Other applications in the brain include deep brain stimulation and blood-brain barrier opening. FIG. 14A shows stroke imaging such as described in Lindsey et al., "Simultaneous bilateral real-time 3-d transcranial ultrasound imaging at 1 {MHz} through poor acoustic windows," Ultrasound in Medicine and Biology, vol. 39, no. 4, pp 721-734 (2013). The approach compromises on the aperture size (small aperture) and frequency of operation (low operating frequencies of 1.2 - 1.8 MHz). This results in an inevitably low contrast imaging system. Use of adaptive imaging as described herein capable of adjusting the spectral content of the imaging (and therapy) pulses based on real-time feedback to take advantage of more or all possible windows in space (e.g., by using larger apertures) and frequency (e.g., by utilizing all frequency bands with good transmission properties within the operating bandwidth of the DMUA).

**[0098]** By maximizing the time-bandwidth product of the imaging pulses within the target region while insuring maximum transmission through the skull, anatomically useful images may be produced. Only a crude outline of the vessels appears to currently be obtainable with the use of contrast-enhanced ultrasound (e.g., using Definity available from Lantheus Medical Imaging). For example, a DMUA capable of focusing at approximately 7 cm inside the brain from the temporal

side utilizing a window with skull thicknesses between 2 mm to 4 mm and operating in the frequency range of 0.6 MHz to 1.6 MHz may be designed. Using the arbitrary waveform generation capabilities of our driver, the SNR at the target may be maximized while maintaining the highest resolution possible.

5 [0099] The generation/transmission of ultrasound energy and the receipt/analysis of pulse-echo data may be provided using any ultrasound imaging system (e.g., the imaging system 10 of FIG. 1), although one or more imaging systems may be advantageous over others. In one or more embodiments, the waveform generation and pulse echo data acquisition may be performed by an imaging system 100 such as shown in Figures 6 and 7. For example, as shown in Figure 6, the imaging system 100 may be used to generate waveforms for driving a plurality of ultrasound transducer elements, as well as acquire and perform real-time processing of such acquired pulse echo data. The imaging system 100 may include an ultrasound scanner (e.g., a Verasonics Vantage (Verasonics, Redmond, WA)) loaded with one or more programs for generating waveforms for driving a plurality of ultrasound transducer elements and acquiring and perform real-time processing of acquired pulse echo data resulting from delivered ultrasound energy (e.g., to provide the adaptive algorithm described herein, to provide for high frame rate pulse-echo data collection, to perform therapy, etc.). The ultrasound scanner may include and/or be modified to include features such as chirp generation, waveform generation 10 such as the synthesis and adaptive algorithms described herein, image reconstruction as described herein, data collection, and data transfer capabilities.

15 [0100] Figures 6-7 (which may also implement the embodiments described with reference to Figures 15-16) provide one exemplary FPGA-GPU implementation for carrying out the adaptive algorithm described herein for image formation and image reconstruction as described herein. For example, in one or more embodiments, the implementation may include physical hardware, and FPGA, GPU, a CPU, and display. Generally, a running DFT 102 (e.g., a running DFT computational block at a frequency of interest for each receiving element) followed by a frequency-domain beamforming network 104 may be used in providing the functionality described herein (e.g., both of which may be implemented on the FPGA). Image reconstruction of the scattering function or other quantitative property of the ROI (e.g., block 106) may be performed after the single-frequency image formation (e.g., which may be performed on a graphical processing unit (GPU)). Alternatively (not shown), a DFT processor may be deployed after beamforming and before the reconstruction block. In this case, the DFT and the reconstruction block may be performed on a GPU. In general, all three stages are computational stages and can be implemented in FPGA, GPU, multi-core CPUs or any appropriate processing unit(s).

20 [0101] FPGA's are well suited for the generation of multiple arbitrary waveforms with exquisite timing precision. One exemplary and flexible solution for implementation of synthesis and generation is to provide a sufficiently deep memory for each channel with sufficient width (e.g., for accuracy). The depth of memory allows for controlling the time-bandwidth product (TBW) of the generated waveforms. The waveform synthesis can be performed on the CPU or the GPU, with the latter offering the advantage of parallelization. For example, the waveform synthesis approach described herein may be based on finite number of distinct, randomly-selected frequency components within the transducer bandwidth. A GPU can be programmed so that the synthesis described in FIG. 5 can be performed simultaneously on all frequency components to accelerate the adaptation.

25 [0102] As shown in the exemplary implementation embodiment of Figure 6, physical hardware of the system may be used to transmit pulses and collect pulse echo data. For example, an imaging array 110 may be controlled using a transmit/receive switch 112 to transmit pulses or receive pulse echo information. On the receive side, a multi-channel analog to digital (ADC) convertor 116 may be used to convert the transducer signal for receipt in channel circuitry 101 such that it may be operated upon by running DFT 102. transmit pulses or receive pulse echo information (e.g., the running DFT may include an implementation as shown in Figure 7). On the transmit side, a programmable multi-channel arbitrary waveform generator and digital to analog (DAC) convertor 120 may be used to generate waveforms for driving the transducer elements of the imaging array 110 to transmit pulses (e.g., the signal from the waveform generator 120 being applied to the transducer elements via an amplifier 114 and under control of switch 112). The programmable multi-channel arbitrary waveform generator and digital to analog (DAC) convertor 120 uses the adaptive algorithm 130 (e.g., such as that shown in Figure 5) to modify the waveforms being generated based on signal to noise ratio and contrast ratio (e.g., of control points) to enhance image formation (e.g., see block 104 which is generally representative of not only reconfigurable beamforming, but also provides image formation (e.g., formation of an image based on reflectivity; a reflectivity map image), and calculation of contrast ratio and signal to noise ratio as described herein.

30 [0103] Further, as shown in Figure 6, various other types of functionality may be implemented using the GPU and Cloud Computing together with the CPU-Display. For example, other image processing 107, such as image compounding (e.g., use of more than one single frequency image to provide a compounded image), Doppler processing (e.g., tracking small changes in the carrier), motion tracking (e.g., by evaluating the phase of the carrier), image analysis (e.g., separation of specular reflections from speckle components and recognition of structures like vessel walls), and feature extraction (e.g., identifying resonances that may reveal sub-resolution structures like layers of a vessel wall) may be performed.

35 [0104] Further, for example, other image processing 106, such as image reconstruction as described herein, quantitative imaging (e.g., speed of sound, attenuation, reflection coefficient from inverse scattering), motion tracking (e.g., in reconstructed image space, which is expected to have sharper demarcation between tissue structure due to its speckle-

free nature), image analysis (e.g., object identification and parameter estimation for computer-aided diagnostics), and feature extraction (e.g., lipid composition of a plaque within the vessel wall, calcification within the plaque, etc.) may be performed.

**[0105]** Still further, in one embodiment, high intensity focused ultrasound (HIFU) is also possible (e.g., for generating ultrasound for treatment or subtherapeutic mechanical and/or thermal effects). For example, a field-programmable gate array (FPGA) may be dedicated for a HIFU source and synchronized frame trigger generation. For example, the HIFU generator may be silenced while pulse-echo imaging is active.

**[0106]** In other words, in one or more embodiments, a system for imaging (e.g., vascular imaging) is provided herein that includes one or more ultrasound transducers (e.g., wherein the one or more transducers are configured to deliver ultrasound energy to a vascular region resulting in pulse-echo data therefrom) and processing apparatus (e.g., including one or more programs executable by one or more processors of the system to perform one or more functions thereof and as described herein, such as adaptive waveform generation, image formation, image reconstruction, etc.).

**[0107]** In other words, the processing apparatus (e.g., FPGA, GPU, CPU, Cloud computing, etc.) may be configured (e.g., operate under control of one or more programs) to, for example, allow definition of a region of interest (e.g., allow a user to define a region of interest in subject using ultrasound imaging), allow definition of a plurality of control points such as described herein, control waveform generation for driving a plurality of ultrasound transducer elements (e.g., of an array of elements), control delivery of ultrasound energy (e.g., in pulse mode) to the region of interest, control the capture of pulse-echo data from the region of interest (e.g., from the control points), separate pulse echo components received from one or more control points associated with corresponding identifiable portions of the region of interest; determining contrast ratios and signal-to-noise ratios for use in modifying the waveform generation, and controlling the modification of waveform generation based on one or more imaging performance characteristics, such as contrast ratio and signal-to-noise ratio.

**[0108]** Further, for example, processing apparatus may be configured to separate, from pulse echo data received, ultrasound energy corresponding to a single frequency and reconstructing an image representative of the more properties in the region of interest from the separated pulse echo data corresponding to a single frequency. Further, processing apparatus may be configured to separate, from the pulse echo data received, one or more additional portions thereof received corresponding to one or more additional single frequencies for use in reconstructing an image representative of one or more properties in the region of interest (e.g., such additional reconstructed images corresponding to multiple frequencies may be combined).

**[0109]** Still further, another exemplary ultrasound imaging system 500 which may be configured to implement adaptive imaging as described herein may be represented by the block diagram shown in FIG. 8. The system 500 may include transmitter apparatus 510 and receiver apparatus 540. For example, transmitter apparatus 510 may be configured to generate arbitrary waveforms (block 512) for driving each element of the transducer array 520 and to perform apodization of the waveform (e.g., changing the shape thereof) and/or and beamforming of the transmit waveforms to various degrees of focusing and steering (e.g., including the capability of providing no beamforming) (block 514). Such waveform generation is based on waveform synthesis and design 516 (e.g., such waveform generation for adaptive imaging is based on waveform synthesis algorithms designed for a particular application, such as vascular imaging).

**[0110]** For example, receiver apparatus 540 may be configured to receive pulse echo data from the plurality of transducer elements of the array 520 and perform pre-beamforming filtering (block 542), receive beamforming (block 544), and post-beamforming filtering (block 546). For example, the system 500 may be configured to perform various levels of beamforming of the received element pulse echo data, which assumed to be available in digital form through sampling and A/D conversion of the received waveforms. A reconfigurable receiver chain may allow for pre-beamforming filtering and post-beamforming filtering. Such beamforming filtering may be based on a beamforming filter design 548 for a particular application (e.g., such beamforming filter design for adaptive imaging may be based on algorithms designed for a particular application, such as vascular imaging). Further, transmit apodization and beamforming (block 514) and receive beamforming (block 544) for a particular application may be based on an aperture design 554 (e.g., an SA design, etc.).

**[0111]** A configured system 500 having such features may take advantage of various synthesis algorithms described below (e.g., the Ultrasound Imaging and Signal Processing Laboratory (UISPL) is believed to have successfully implemented a system that has nearly all the features assumed by the transmit-receive flow shown in FIG. 8). As such, existing ultrasound systems may be adapted to operate as described herein; for example, carry out algorithms described herein, such as with use of digital signal processing techniques (e.g., hardware and software).

**[0112]** The following subsections illustrate several aspects of the system architecture shown in FIG. 8. A brief description of an exemplary one-dimensional (1D) filter design usable with adaptive imaging described herein is given in Section A. A brief description of different exemplary approaches to coded excitation in ultrasound imaging which may be used with the other features described herein is provided in Section B. Such material is meant to provide an example of the operator design and coded excitation for the 1D case. Generalization to the 2D case, in the context of linear array imaging, is given in the article, Y. Wan and E.S. Ebbini, "A Post-beamforming 2-D Pseudoinverse Filter for Coarsely Sampled

Ultrasound Arrays," IEEE Trans on Ultrasonics, Ferroelectrics, and Frequency Control, vol. 56, no. 9, pp.1888-1902 (2009). Also, this formulation can be modified in a manner to allow for the use of coded waveforms and for the design of coded wavefronts, as illustrated in numerous publications, such as, E. Ebbini, "Optimal transversal filter bank for 3D real-time acoustical imaging," Signals, Systems and Computers, 1992. 1992 Conference Record of The Twenty-Sixth Asilomar Conference, vol.2, pp. 831-835 (1992); Ebbini et al., "A new svd-based optimal inverse filter design for ultrasonic applications," Ultrasonics Symposium, 1993. Proceedings, IEEE 1993, vol.2, pp. 1187-1190 (1993); Shen et al., "An optimal image operator design technique for coded excitation ultrasound imaging system," Ultrasonics Symposium, 1994. Proceedings., 1994 IEEE, vol. 3, pp. 1777-1781 (1994); J. Shen and E. Ebbini, "On the design of a transversal filter bank for parallel processing multiple image lines in real-time acoustic imaging," Acoustics, Speech, and Signal Processing, 1996. ICASSP-96. Conference Proceedings., 1996 IEEE International Conference, vol. 6, pp. 3109-3112 (1996); J. Shen and E.S. Ebbini, "Real-time 3d pulse-echo ultrasonic imaging with coded-excitation systems," Image Processing, 1996. Proceedings., International Conference, vol. 1, pp. 717-720 (1996); E. Ebbini and J. Shen, "Fundamental resolution limits of a coded-excitation system for real-time pulse-echo imaging," Ultrasonics Symposium, 1997. Proceedings, 1997IEEE, vol. 2, pp. 1539-1542 (1997); and E. S. Ebbini, "Region-adaptive motion tracking of speckle imagery," Proc. IEEE Int. Conference on Acoustics, Speech, and Signal Processing, pp. 2075-2078 (2000). Waveforms and wavefronts may be designed for nonlinear imaging using waveform and wavefront designs to create favorable conditions for enhancing the nonlinear response from the target region, e.g. with or without contrast agents.

Section A - One-Dimensional Pseudoinverse Filter Design

**[0113]** A 1D pseudoinverse filter was described in J. Shen and E. S. Ebbini, "A new coded-excitation ultrasound imaging system - part I: basic principles," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 43, no. 1, pp. 131-140 (1996) derived from a system model for a single A-line acquisition using a 1D linear array. A brief explanation of the filter design process is described herein, but defined on a Cartesian grid for the convenience of deriving the proposed 2-Dimensional Pseudoinverse Filter.

System Model

**[0114]** A uniform grid in the imaging field is defined as shown in FIG. 9 and assumes scatterers with random amplitude distribution at the grid points (e.g., a 1D linear array system model where the scattering is assumed to result from scatterers with random amplitudes on the Cartesian grid). The number of grid points within a range interval

$$[z_{min}, \tilde{z}_{max}]$$

in the axial direction,  $N$ , determines the axial sampling rate. Similarly, the number of grid points in the lateral direction (or the number of scan lines) within

$$[z_{min}, z_{max}],$$

$M$ , determines the lateral sampling rate. It is assumed that the grid spacing is small with respect to the correlation cell size of the imaging system in both directions. Note that the grid shown in FIG. 9 represents a subregion of an imaging volume for purposes of reconstructions. Scattering from outside this region must be accounted for by a simulation model for the received echo data.

**[0115]** Define  $s_{m,q}$  as the scatterer strength at grid location  $(m, q)$  ( $m \in [1, M], q \in [1, N]$ ),  $\zeta_m$  as a vector of size  $N_j \times 1$  containing amplitudes of scatterers along scan line  $m$  ( $N_j \gg N$ ). Let  $S$  be a vector containing all lines of scatterers in the imaging field ( $M_j \gg M$ ) as

$$S = [ \cdots \zeta_1^T \zeta_2^T \cdots \zeta_M^T \cdots ]^T,$$

where,  $T$  denotes matrix/vector transpose. Then the discretized version of the received echo for scan line  $m$  in the range interval  $[z_{min}, z_{max}]$  can be represented in vector form as  $f_m$  of size  $N \times 1$  and all the  $M$  scan lines can be grouped in  $F$  as follows:

$$F = [ f_1^T \quad f_2^T \quad \cdots \quad f_M^T ]^T$$

5 **[0116]** The impulse response of the system at a grid point is the echo from a single unit-strength scatterer positioned at that point. For illustration purposes, it is assumed that the point scatterer is at the center of the specified grid. Then, the generated pulse-echo impulse response at grid point  $q$  along line  $i$  is denoted as vector  $g_{i,q}$  of size  $N \times 1$  which contains the discretized samples in time-domain. The pulse-echo impulse responses at the grid points along line  $i$  can be grouped as

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$$G_i = [ \cdots \quad g_{i,1} \quad g_{i,2} \quad \cdots \quad g_{i,N} \quad \cdots ]$$

15 **[0117]** Assume  $G_0$  is the matrix containing the pulse-echo impulse responses from grid points along the line through the focus and  $\{G_{\pm i}\}_{i=1}^{\infty}$  are the matrices containing pulse-echo impulse responses from the grid points along the lines on right/left sides of focus. Typically,  $G_i = G_{-i}$  due to the symmetry of the linear array aperture or apodization. Based on the above notations and definitions, the received echo signal from one scan line is obtained by superposition, which can be represented in matrix form:

20

$$f_m = [ \cdots \quad G_{-i} \quad \cdots \quad G_{-1} \quad G_0 \quad G_1 \quad \cdots \quad G_i \quad \cdots ] S$$

25  $\underbrace{\hspace{15em}}_{\Psi}$

25

where,  $\Psi$  is the spatio-temporal impulse response of the system and each  $G_i$  represents the response in a given lateral direction. Therefore, for a single A-line, the sampled beamformer output  $f_m$  is related to the scatter distribution  $S$  by a discretized propagation operator (matrix)  $\Psi$ .

30

#### Filter Design

**[0118]** If AWGN noise is considered in the system, the system equation for a single A-line is

35

$$f_m = \Psi S + n$$

where,  $n$  contains the AWGN noise term. Thus a minimum-norm least-square estimate of the scatter distribution  $S$  can be obtained as

40

$$\hat{S} = \underbrace{\Psi^H (\Psi \Psi^H)^{\dagger}}_{PIO_{1D}} S$$

45

where, the superscripts  $H$ ,  $\dagger$  represent matrix Hermitian, and generalized inverse operators, respectively and the  $PIO_{1D}$  is defined as the 1-dimensional pseudoinverse operator (PIO).

50 **[0119]** A further reduction of computational complexity can be achieved by using the range-shift invariance (RSI) assumption as described in J. Shen and E. S. Ebbini, "A new coded-excitation ultrasound imaging system - part I: basic principles," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 43, no. 1, pp. 131-140 (1996); and J. Shen and E. S. Ebbini, "Filter-based coded-excitation system for high-speed ultrasonic imaging," IEEE Trans. Med. Imag., vol. 17, no. 6, pp. 923-934 (1998). The energy and the shape of the impulse responses in the matrices  $G_i$  are gradually changing along the axial direction. However, this change is moderate in the vicinity of the focus where one can establish computationally that the impulse responses can be approximated by the time-shifted versions of each other. With this assumption, the matrix  $G_i$  can be represented as Toeplitz. In addition, the array beam pattern justifies truncation of the impulse responses from grid points far away from the focus. This implies:

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$$g_{i,q} \rightarrow 0, q > N_f, N_f$$

5

is some finite value.

**[0120]** Using the shifted version of  $g_{i,c}$ , the pulse-echo impulse response at the focus, the RSI approximation version of  $G_i$  is a banded Toeplitz matrix of size  $N \times N$ :

10

$$G_i = \mathcal{T}(0, \dots, g_{i,c}(0), g_{i,c}(1), \dots, g_{i,c}(N_f), \dots, 0)$$

15

where  $N_f$  is the number of nonzero samples of the impulse response along the  $i$ th direction and  $\mathcal{T}$  stands for the operator of forming a Toeplitz matrix using a specified sequence. The Toeplitz structure allows diagonalization using DFT matrices:

$$G_i = F_N H_i F_N^{-1}$$

20

where,  $H_i$  is a diagonal matrix and  $F_N$  is a DFT matrix of size  $N$ :

25

$$F_N = \begin{pmatrix} 1 & 1 & \dots & 1 \\ 1 & W_N^{1 \cdot 1} & \dots & W_N^{1 \cdot (N-1)} \\ \vdots & \vdots & \ddots & \vdots \\ 1 & W_N^{(N-1) \cdot 1} & \dots & W_N^{(N-1) \cdot (N-1)} \end{pmatrix}$$

30

where  $W_N = e^{-j \frac{2\pi}{N}}$ . With this diagonalization, the  $PIO_{1D}$  becomes

35

$$PIO_{1D} = \left( PIOF_1 \quad PIOF_2 \quad \dots \quad PIOF_N \right)^T$$

40

where,  $PIOF_i = F_N Z_i F_N^{-1}$  is the  $i$ th filter for obtaining the scatterer distribution along  $i$ th lateral direction from received echo  $f_m$  and  $Z_i$  is a diagonal matrix with diagonal terms defined by

45

$$\{Z_i\}_{k,k} = \frac{H_{i\{k,k\}}}{\sum_{i=1}^N |H_{i\{k,k\}}|^2}$$

50

**[0121]** The above expression defines the  $PIO_{1D}$  filter bank in frequency domain. Thus, the estimate of the scatterer distribution is obtained by  $N$  filters:

55

$$\hat{s} = \left( PIOF_1 f_m \quad PIOF_2 f_m \quad \dots \quad PIOF_N f_m \right)^T$$

**[0122]** The RSI assumption followed by DFT operations allows complexity reduction from  $N \times N$  filters to  $N$  filters and

leads to the derivation of an illustrating expression of the  $PIO_{1D}$  filter as shown in the equation above for  $\{Z_{i,k,k'}\}$

**[0123]** This filter bank implementation allows parallel processing of echo data from multiple directions from a single beamforming operation. In principle, the filter bank could be designed to decouple echoes from different directions given the echoes from different directions are uncorrelated. Therefore, more efficiency in decoupling requires the operation in conjunction with multi-modal coded excitation, i.e. several distinct codes are transmitted simultaneously with single receive beamforming of echoes from the region of interest.

#### Section B - Coded Excitation

**[0124]** It is well known that in conventional pulse-echo ultrasound imaging, there is a trade-off between resolution and penetration under the limit of peak acoustic power. Narrower pulses will have wider bandwidth and better resolution, but suffer lower SNR for less penetration. Using coded waveforms as excitation enables elongated pulses for higher SNR.

#### Coded Waveforms.

**[0125]** Different coded excitation approaches have been proposed using different codes: PN sequences as described in J. Shen and E. S. Ebbini, "Filter-based coded-excitation system for high-speed ultrasonic imaging," IEEE Trans. Med. Imag., vol. 17, no. 6, pp. 923-934 (1998) and M. O'Donnell and Y. Wang, "Coded excitation for synthetic aperture ultrasound imaging," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 52, no. 2, pp. 171-176 (Feb. 2005); Golay codes as describe in R. Y. Chiao and X. Hao, "Coded excitation for diagnostic ultrasound: A system developer's perspective," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 52, no. 2, pp. 160-170 (Feb. 2005); and chirps as described in T. Misaridis and J. A. Jensen, "Use of modulated excitation signals in medical ultrasound, part I: basic concepts and expected benefits," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 52, no. 2, pp. 177-191 (Feb. 2005).

**[0126]** Coded waveforms can be categorized into 4 groups according to the ambiguity function as indicated in A. W. Rihaczek, "Radar waveform selection -a simplified approach," IEEE Trans. Aerosp. Electron. Syst., vol. AES-7, no. 6, pp. 1078-1086 (Nov. 1971).

1 - Constant-carrier pulse. This is the simplest form of the waveform that can be used and the form of a short duration of constant-carrier pulse is the excitation used in the conventional pulse-echo ultrasound imaging. This waveform allows for simple implementation or low complexity, good range resolution due to its large bandwidth, low sidelobe level with proper envelop and robustness to the frequency-dependent attenuation due to its short duration. Its disadvantage, lies in poor SNR resulting from lowest time-bandwidth (TBW) product possible: unity and high correlation in the imaging field.

2 - Pulse compression signals with thumbtack ambiguity function. These waveforms have time-bandwidth product larger than unity, thus they may produce higher SNR than constant-carrier pulse. Sets of orthogonal codes are used to reduce the correlation in the field. A problem with this type of waveforms is high sidelobe level after compression: average approximately  $1/TBW$ , although it is one type of waveform that achieves sharpest mainlobe peak. A special case in this family is complementary codes which are able to suppress sidelobe level by adding two or more transmitted sequences with equal-magnitude, opposite-sign sidelobes.

3 - Pulse compression signal with sheared ridge ambiguity function - linear chirp. Linear chirp is a special type of pulse compression signal because it has large time-bandwidth product as other pulse compression signals while it maintains low sidelobe level as the constant-carrier pulse. It is also robust to the frequency-dependent attenuation because the frequency shift mismatch can be translated to time shift, thus providing compression quality.

4 - Pulse trains. This type of waveform has the capability of suppressing sidelobe level, at the same time, achieving sharp mainlobe peaks.

**[0127]** One may select exciting waveforms not only based on the above classifications, but also they may be selected by iteratively calibrating/training the system, obtaining spatio-temporal codes capable of correcting the distortion in heterogeneous, lossy medium such as described in Montaldo et al., "Spatio-temporal coding in complex media for optimum beamforming: the iterative time-reversal approach," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 52, no. 2, pp. 220-230 (Feb. 2005); which manner of choosing coded waveform may cast light on optimum waveform design for specific applications/scenario.

## Receive Filter

**[0128]** A matched filter may be used as the receiving/compressing filter because it achieves the highest SNR at the peak of the compressed pulses. The highest possible SNR is proportional to the time-bandwidth of the transmitted waveforms. However, matched filters may not take system noise or clutter distribution into account, and as such, this type of filter may not balance performance parameters for optimum solutions of specific applications. On the other hand, a pseudoinverse filter may be used that has the capability of combining compression, decoupling, noise/clutter reduction and performance adjustment at the same time.

Section C - Pseudoinverse Filter Design with Coded Excitation.

**[0129]** One can use a linear chirp signal as an example of coded waveform and illustrate the design of 1D pseudoinverse Filter as receive filtering transmitted coded excitation. A linear chirp signal  $c(t)$  covering the frequency band of 0.5-1.5MHz may be transmitted as illustrated in FIGS. 10(a)-(d) (e.g., an illustration of the pseudoinverse compression filter frequency response designed for a Gaussian chirp transmit waveform). The effect of the regularization parameter,  $\beta$ , on the frequency response of the PIO is also shown.

**[0130]** The frequency response of the matched filter  $M(f)$  is  $C^*(f)$ , the complex conjugate of the Fourier transform of  $c(t)$ . The frequency response of the pseudoinverse filter,  $P(f)$ , is defined as

$$P(f) = \frac{C^*(f)}{S_s(f) + \beta S_n(f)},$$

where,  $S_s(f) = |C(f)|^2$  is the spectral density of the signal,  $S_n(f)$  is the spectral density of the noise and  $\beta$  is a regularization parameter for the noise term.

**[0131]** For illustration purpose, additive white Gaussian noise (AWGN) model is assumed. The above equation is basically the equation above for  $\{Z_{k,k}\}$  with noise model being considered. As shown in FIG. 10, the frequency response of the pseudoinverse filter changes with the value of  $\beta$ . Specifically, when the regularization parameter  $\beta$  is set equal to 0, the filter behaves as an inverse filter,  $1/C(f)$ , with widest bandwidth and highest noise floor. The pulse width in the time domain is inversely proportional to the bandwidth. Therefore, theoretically, the inverse filter obtains the highest axial resolution but with the lowest SNR. On the other extreme, when the regularization parameter  $\beta$  is large enough so that  $\beta S_n(f)$  dominates the denominator, the filter behaves as a matched filter as shown in FIG. 10(d). This solution maximizes the SNR, but may reduce the axial resolution (e.g., due to the reduced overall bandwidth of the system-matched filter cascade). The use of the pseudoinverse filter allows the shaping of the spectrum of the compressed received signal by regularized inversion of the system frequency response at frequencies where the SNR is sufficiently high. The appropriate value of  $\beta$  can be determined from the SNR of the system as a function of the frequency.

## D - Image Formation

**[0132]** Synthetic aperture imaging. Synthetic aperture (SA) imaging techniques, as described in K. Thomenius, "Evolution of ultrasound beamformers," IEEE Ultrason. Symp., pp. 1615-1622 (1996), may be used to obtain images with 2-way (i.e., transmit-and-receive) dynamic focusing. This may provide high quality images using conventional delay-and-sum beamforming. In this mode, the RF data from an image pixel at  $P(x_p, z_p)$  in a medium with uniform speed of sound,  $c$ , is computed by:

$$I(x_p, z_p) = \sum_{i=1}^{64} \sum_{j=1}^{64} A_i \cdot B_j \cdot s_{i,j} \left( \frac{R_{ip} + R_{jp}}{c} \right),$$

where  $A_i$  and  $B_j$  are, respectively, the transmit and receive apodization weights,  $R_{ip}$  and  $R_{jp}$  are, respectively, the distances from the transmitting and receiving elements to the image pixel  $P$ , and  $S_{ij}$  is the echo received by element  $j$  when transmitting with element  $i$ . Other imaging scenarios can be performed by specializing the image formation as described, for example, in T. Misaridis and J. A. Jensen, "Use of modulated excitation signals in medical ultrasound. part I: basic concepts and expected benefits," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 52, no. 2, pp. 177-191 (Feb. 2005). In the context of SA imaging, adaptive imaging may be performed by using distinct arbitrary waveforms on each

element on transmit and pre-beamforming signal separation using the running DFT. The signal components obtained at the outputs of the running DFTs may be used in image-formation and compounding to allow for the evaluation of the performance measures (e.g., SNR and CR) with respect to the identified CPs. The signal may also be used in image reconstruction upon the convergence of the adaptive imaging algorithms.

5 **[0133]** Linear Array Imaging: Linear array imaging is widely used in pulse-echo medical ultrasound due to its simplicity and usefulness in many applications, e.g., vascular imaging, breast imaging, etc. It can be described with reference to Figure 9 which shows a linear array and an imaging beam used to acquire one image line on a rectilinear grid in the axial and lateral directions. The pulse-echo data attributed to this image line may be obtained by using one transmit beam and employing dynamic receive focusing to maximize the field of view (FOV). In the context of linear array imaging, adaptive imaging may be performed by using arbitrary waveform generation on the transmitter side and post-beamforming separation of the echo components (e.g., using the running DFT) before compounding and/or performing image reconstruction of tissue properties.

10 **[0134]** Other Image Formation Methods: Conventional modern scanners employ other types of image formation models, e.g., phased array, convex, steered linear, etc. In each case, the adaptive imaging approach described herein may be applied as appropriate for the particulars of the transmit-receive methods used. The principles are the substantially same.

E - Assessment of Imaging Performance

20 **[0135]** Spatial resolution. For wire target images, the 6-dB width and length of the envelope may be used to measure the lateral and axial resolution, respectively. For quality assurance and scatterer phantoms the speckle correlation cell size as described in R. F. Wagner, M. F. Insana, and S. W. Smith, "Fundamental correlation lengths of coherent speckle in medical ultrasonic images," IEEE Trans. Ultrason., Ferroelect., Freq. Contr., vol. 35, no. 1, pp. 34-44 (Jan. 1988) may be used. Uniform speckle regions from the test object area may be identified to compute the average speckle correlation cell size in the axial and lateral directions as follows:

25

$$S_{cx} = \int_{-X}^X \frac{C_I(x, 0)}{C_I(0, 0)} dx \quad S_{cz} = \int_{-Z}^Z \frac{C_I(0, z)}{C_I(0, 0)} dz$$

30

where  $S_{cx}$  and  $S_{cz}$  are, respectively, the lateral and axial cell size values and  $C_I(x,z)$  is the 2D intensity autocovariance function. The integration limits X and Z may be chosen to be large enough to allow the magnitude of the autocovariance to drop to negligible levels. The integrals may be evaluated numerically in Cartesian coordinates using the trapezoidal rule to obtain the speckle cell size in the axial and lateral directions.

35 **[0136]** Contrast. The contrast ratio (CR) is defined as following:

40

$$CR = 10 \log_{10} \left[ \frac{\bar{I}_2}{\bar{I}_1} \right]$$

where  $\bar{I}_2$  and  $\bar{I}_1$  are the average intensities in the region of interest (e.g. cyst) and a reference region, respectively. This definition of the CR may be acceptable and applicable in imaging quality assurance phantom. For purposes of at least one embodiment of adaptive imaging, a definition of CR related to the selection of CPs (e.g. in the wall and lumen of a blood vessel) is shown herein in the description with reference to Figure 3.

45 **[0137]** The SNR is typically computed from speckle statistics. Specifically, the envelope of the echo signal in a uniform speckle region follows Rayleigh statistics. The SNR is typically obtained from the ratio of the mean and the standard deviation in a uniform region. The SNR can also be evaluated by computing a ratio between the energies in the ROI and a reference region identified with noise. Both of these approaches to the computation of SNR may be useful in adaptive imaging.

55 **Claims**

1. An ultrasound imaging method (30; 80) comprising:

providing a region of interest (ROI) in a subject;  
defining a plurality of control points (CPs) within the region of interest (ROI), wherein at least a first portion of the control points (CPs) are associated with a first identifiable portion of the region of interest (ROI) and a second portion of the control points (CPs) are associated with a second identifiable portion of the region of interest (ROI) that is different than the first identifiable portion;  
providing a transducer apparatus (22) comprising a plurality of ultrasound transducer elements, wherein each of the plurality of ultrasound transducer elements is configured to deliver ultrasound energy to the region of interest (ROI) in response to a waveform applied thereto;  
generating a waveform for each ultrasound transducer element of the plurality of ultrasound transducer elements, wherein generating the waveform comprises:

selecting one or more imaging frequencies within a transducer apparatus bandwidth, each of the one or more imaging frequencies being a carrier of a pulse to be transmitted having a finite bandwidth within the transducer bandwidth and having a time duration; and  
generating element frequency components for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element;

delivering ultrasound energy in pulse mode to the region of interest using the plurality of ultrasound transducer elements in response to waveforms generated for each of the plurality of ultrasound transducer elements;  
receiving pulse-echo data at each ultrasound transducer element of a plurality of ultrasound transducer elements from the region of interest (ROI) in response to the delivered ultrasound energy to generate an image based thereon;  
separating pulse-echo components received from at least one of the first portion of the control points associated with the first identifiable portion of the region of interest and received from the second portion of the control points associated with the second identifiable portion of the region of interest;  
determining at least one of a contrast ratio (CR) between the first and second identifiable portions based on the pulse-echo components received from the first portion of the control points (CPs) associated with the first identifiable portion of the region of interest (ROI) and the pulse-echo components received from the second portion of the control points (CPs) associated with the second identifiable portion of the region of interest (ROI) and a signal to noise ratio (SNR) based on pulse-echo components received from a reference portion of the region of interest (ROI) and pulse-echo components received from at least one of the first portion of the control points (CPs) and the second portion of the control points (CPs); and  
modifying the waveform generated for one or more of the plurality of ultrasound transducer elements based on at least one of a comparison of the contrast ratio (CR) determined between the first and second identifiable portions to a threshold value and a comparison of the signal to noise ratio (SNR) to a threshold value, wherein modifying the waveform generated for one or more of the plurality of ultrasound transducer elements comprises at least one of adjusting gain at frequencies of the one or more frequencies located at one or more locations within the transducer apparatus bandwidth, and adjusting one or more pulse parameters including at least one of pulse duration, pulse shape, pulse amplitude, and pulse phase to adjust time-bandwidth product to maximize at least one of contrast ratio (CR) between the first and second identifiable portions of the region of interest (ROI) and a signal to noise ratio (SNR) from the region of interest (ROI).

**2.** A system for ultrasound imaging (10), comprising:

a transducer apparatus (22) comprising a plurality of ultrasound transducer elements, wherein each of the plurality of ultrasound transducer elements is configured to deliver ultrasound energy to a region of interest (ROI) in response to a waveform applied thereto resulting in pulse-echo data therefrom; and  
means for providing a region of interest (ROI) in a subject configured to define a plurality of control points (CPs) within the region of interest (ROI), wherein at least a first portion of the control points (CPs) are associated with a first identifiable portion of the region of interest (ROI) and a second portion of the control points (CPs) are associated with a second identifiable portion of the region of interest (ROI) that is different than the first identifiable portion;  
means for generating a waveform for each ultrasound transducer element of the plurality of ultrasound transducer elements, wherein the waveform generation means comprises:

means for selecting one or more imaging frequencies within a transducer apparatus bandwidth, each of the one or more imaging frequencies being a carrier of a pulse to be transmitted having a finite bandwidth within the transducer apparatus bandwidth and having a time duration; and

means for generating element frequency components for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element;

5 means for controlling delivery of ultrasound energy in pulse mode to the region of interest (ROI) using the plurality of ultrasound transducer elements in response to waveforms generated for each of the plurality of ultrasound transducer elements;

means for controlling capture of pulse-echo data at each ultrasound transducer element of a plurality of ultrasound transducer elements from the region of interest in response to the delivered ultrasound energy to generate an image based thereon;

10 means for separating pulse-echo components received from at least one of the first portion of the control points (CPs) associated with the first identifiable portion of the region of interest (ROI) and received from the second portion of the control points (CPs) associated with the second identifiable portion of the region of interest (ROI);

15 means for determining at least one of a contrast ratio (CR) between the first and second identifiable portions based on the pulse-echo components received from the first portion of the control points (CPs) associated with the first identifiable portion of the region of interest (ROI) and the pulse-echo components received from the second portion of the control points (CPs) associated with the second identifiable portion of the region of interest (ROI) and a signal to noise ratio (SNR) based on pulse-echo components received from a reference portion of the region of interest (ROI) and pulse-echo components received from at least one of the first portion of the control points (CPs) and the second portion of the control points (CPs); and

20 means for modifying the waveform generated for one or more of the plurality of ultrasound transducer elements based on at least one of a comparison of the contrast ratio (CR) determined between the first and second identifiable portions to a threshold value and a comparison of the signal to noise ratio (SNR) to a threshold value, wherein modifying the waveform generated for one or more of the plurality of ultrasound transducer elements comprises at least one of adjusting gain at frequencies of the one or more frequencies located at one  
25 or more locations within the transducer apparatus bandwidth, and adjusting one or more pulse parameters including at least one of pulse duration, pulse shape, pulse amplitude, and pulse phase to adjust time-bandwidth product to maximize at least one of contrast ratio (CR) between the first and second identifiable portions of the region of interest (ROI) and a signal to noise ratio (SNR) from the region of interest (ROI).

30 **3.** The method or system of any of claims 1 to 2, wherein the first portion of the control points (CPs) are associated with a vessel wall of a vascular structure of the subject and the second portion of the control points (CPs) are associated with a lumen defined at least in part by the vessel wall.

35 **4.** The method or system of claim 3, wherein the plurality of control points (CPs) within the region of interest further comprise a third portion of the control points (CPs) associated with tissue (46) surrounding the vessel wall of the vascular structure, wherein pulse-echo components received from the third portion of the control points (CPs) associated with the tissue are separated from the pulse-echo components received from other portions of the control points (CPs), and further wherein, at least a contrast ratio (CR) between the tissue and at least one of the vessel wall (42) or lumen (45) is determined for use in modifying the waveform generated for one or more of the plurality  
40 of ultrasound transducer elements.

**5.** The method or system of any of claims 1 to 4, wherein the method further comprises or the system is configured for:

45 separating, from the pulse echo data received, at least a portion thereof received at each ultrasound transducer element from the region of interest in response to the delivered ultrasound energy corresponding to a single frequency of the one or more image frequencies; and

reconstructing an image representative of one or more properties in the region of interest from the separated pulse-echo data corresponding to the single frequency of the one or more image frequencies.

50 **6.** The system of any of claims 2 to 5, wherein the system is configured to deliver therapy to a patient based on identification of at least one vascular characteristic of the region of interest in which at least one portion of a blood vessel is located.

55 **7.** The method or system of any of claims 1 to 6, wherein generating element frequency components for each of the one or more imaging frequencies to form at least a part of the waveform to be applied to the ultrasound transducer element comprises generating one or more excitation vectors, and further wherein generating the one or more excitation vectors comprises generating each excitation vector using field synthesis at a single frequency of the one or more imaging frequencies within the transducer bandwidth.

8. The method or system of claim 7, wherein the excitation vector generated comprises an element frequency component corresponding to each ultrasound transducer element of the plurality of ultrasound transducer elements.
9. The system of any of claims 2 to 8, wherein the system is configured to deliver therapy to a patient based on identification of at least one vascular characteristic of the region of interest (ROI) in which at least one portion of a blood vessel is located.
10. The system of claim 9, wherein using ultrasonic energy to deliver therapy comprises using the transducer apparatus to deliver ultrasound energy and receive pulse-echo data and to generate ultrasonic energy to deliver therapy.
11. The method or system of any of claims 1 to 10, wherein receiving pulse-echo data at each ultrasound transducer element of a plurality of ultrasound transducer elements from the region of interest in response to the delivered ultrasound energy comprises using a discrete Fourier transform based filter bank for separation of pulse-echo data.
12. The method or system of any of claims 1 to 11, wherein the one or more imaging waveforms comprise a finite number of randomly selected single frequency components, each single frequency component being a carrier having a finite bandwidth specified by its duration and modulating pulse.

## Patentansprüche

1. Ein Ultraschall-Bildgebungsverfahren (30; 80), umfassend:

Bestimmen eines Untersuchungsbereichs (ROI) in einem Subjekt;  
 Definieren von mehreren Kontrollpunkten (CP) innerhalb des Untersuchungsbereichs (ROI), wobei wenigstens ein erster Anteil der Kontrollpunkte (CP) zu einem ersten identifizierbaren Teil des Einflussbereichs (ROI) und ein zweiter Anteil der Kontrollpunkte (CP) zu einem zweiten identifizierbaren Teil des Untersuchungsbereichs (ROI), der zu dem ersten identifizierbaren Anteil unterschiedlich ist, zugehörig sind;  
 Vorsehen einer Sonde bzw. Transducervorrichtung (22), umfassend mehrere Ultraschall-Transducerelemente, wobei jedes der mehreren Ultraschall-Transducerelemente derart ausgestaltet ist, dass als Antwort auf eine daran angelegte Wellenform Ultraschallenergie zu dem Untersuchungsbereich (ROI) gesendet wird;  
 Erzeugen einer Wellenform für ein jedes Ultraschall-Transducerelement der mehreren Ultraschall-Transducerelemente, wobei die Erzeugung der Wellenform das Folgende umfasst:

Auswählen von einer oder mehreren Bildgebungsfrequenzen innerhalb der Bandbreite der Transducervorrichtung, wobei jede der einen oder mehreren Bildgebungsfrequenzen ein Träger für einen zu übermittelnden Impuls mit einer finiten Bandbreite innerhalb der Transducerbandbreite und mit einer bestimmten Zeitdauer ist; und  
 Erzeugen von Frequenzkomponenten eines Elements für jede der einen oder mehreren Bildgebungsfrequenzen, um wenigstens einen Teil der an das Ultraschall-Transducerelement anzulegenden Wellenform auszubilden;

Senden von Ultraschallenergie in einem Impulsmodus zu dem Untersuchungsbereich unter Verwendung der mehreren Ultraschall-Transducerelemente als Antwort auf die für jedes der mehreren Ultraschall-Transducerelemente erzeugten Wellenformen;

Empfangen von Puls-Echo-Daten des Untersuchungsbereichs (ROI) als Antwort auf die gesendete Ultraschallenergie an jedem der Ultraschall-Transducerelemente der mehreren Ultraschall-Transducerelemente, um ein drauf basiertes Abbild zu erzeugen;

Trennen von Puls-Echo-Komponenten, die wenigstens von dem ersten Anteil der Kontrollpunkte, die zu dem ersten identifizierbaren Teil des Untersuchungsbereichs zugehörig sind, oder dem zweiten Anteil der Kontrollpunkte, die zu dem zweiten identifizierbaren Teil des Untersuchungsbereichs zugehörig sind, empfangen worden sind;

Bestimmen von wenigstens einem Verhältnis, ausgewählt aus einem Kontrastverhältnis (CR) zwischen den ersten und zweiten identifizierbaren Teilen basierend auf den Puls-Echo-Komponenten, die von dem ersten Anteil der Kontrollpunkte (CP), die zu dem ersten identifizierbaren Teil des Untersuchungsbereichs (ROI) zugehörig sind, empfangen worden sind, und den Puls-Echo-Komponenten, die von dem zweiten Anteil der Kontrollpunkte (CP), die zu dem zweiten identifizierbaren Teil des Untersuchungsbereichs (ROI) zugehörig sind, empfangen worden sind, und einem Signal-Rausch-verhältnis (SNR), basierend auf den Puls-Echo-Kompo-

nenten, die von einem Referenz-Anteil des Untersuchungsbereichs (ROI) empfangen worden sind, und den Puls-Echo-Komponenten, die von wenigstens einem Teil, ausgewählt aus dem ersten Anteil der Kontrollpunkte (CP) und dem zweiten Anteil der Kontrollpunkte (CP), empfangen worden sind; und  
 Modifizieren der für ein oder mehrere der mehreren Ultraschall-Transducerelemente erzeugten Wellenform, basierend auf wenigstem einem Vergleich des Kontrastverhältnisses (CR), bestimmt zwischen dem ersten und zweiten identifizierbaren Teilen, mit einem Schwellenwert und einem Vergleich des Signal-Rausch-Verhältnisses (SNR) mit einem Schwellenwert, wobei das Modifizieren der für ein oder mehrere der mehreren Ultraschall-Transducerelemente erzeugten Wellenform wenigstens eines der Folgenden umfasst: Anpassen der Verstärkung der Frequenzen der einen oder mehreren Frequenzen, die an einem oder mehreren Orten innerhalb der Bandbreite der Transducervorrichtung angeordnet sind, und Anpassen eines oder mehrerer Impuls-Parameter, einschließlich wenigstens einem, ausgewählt aus Impulsdauer, Impulsform, Impulsamplitude und Impulsphase, um das Zeit-Bandbreite-Produkt für die Maximierung wenigstens des Kontrastverhältnisses (CR) zwischen dem ersten und dem zweiten identifizierbaren Bereich des Untersuchungsbereichs (ROI) und einem Signal-Rausch-Verhältnis (SNR) aus dem Untersuchungsbereich (ROI) anzupassen.

## 2. Ein System zur Ultraschall-Bildgebung (10), umfassend:

eine Transducervorrichtung (22), umfassend mehrere Ultraschall-Transducerelemente, wobei jedes der mehreren Ultraschall-Transducerelemente derart ausgestaltet ist, dass als Antwort auf eine daran angelegte Wellenform Ultraschallenergie zu einem Untersuchungsbereich (ROI) gesendet wird, wobei daraus Puls-Echo-Daten gewonnen werden; und

Mittel zum Bestimmen eines Untersuchungsbereichs (ROI) in einem Subjekt, wobei dieses derart ausgestaltet ist, dass mehrere Kontrollpunkte (CP) innerhalb des Untersuchungsbereichs (ROI) definiert sind, wobei wenigstens ein erster Anteil der Kontrollpunkte (CP) zu einem ersten identifizierbaren Teil des Untersuchungsbereichs (ROI) und ein zweiter Anteil der Kontrollpunkte (CP) zu einem zweiten identifizierbaren Teil des Untersuchungsbereichs (ROI), der zu dem ersten identifizierbaren Anteil unterschiedlich ist, zugehörig sind; Mittel zum Erzeugen einer Wellenform für ein jedes Ultraschall-Transducerelement der mehreren Ultraschall-Transducerelemente, wobei das Mittel zur Erzeugung der Wellenform das Folgende umfasst:

Mittel zum Auswählen von einer oder mehreren Bildgebungsfrequenzen innerhalb der Bandbreite der Transducervorrichtung, wobei jede der einen oder mehreren Bildgebungsfrequenzen ein Träger für einen zu übermittelnden Impuls mit einer finiten Bandbreite innerhalb der Bandbreite der Transducervorrichtung und mit einer bestimmten Zeitdauer ist; und

Mittel zum Erzeugen von Elementfrequenzkomponenten für eine der einen oder mehreren Bildgebungsfrequenzen, um wenigstens einen Teil der an das Ultraschall-Transducerelement anzulegenden Wellenform auszubilden;

Mittel zum Steuern des Sendens von Ultraschallenergie in einem Impulsmodus zu dem Untersuchungsbereich (ROI) unter Verwendung der mehreren Ultraschall-Transducerelemente als Antwort auf die für jedes der mehreren Ultraschall-Transducerelemente erzeugten Wellenformen;

Mittel zum Steuern des Empfangs von Puls-Echo-Daten des Untersuchungsbereichs an jedem der Ultraschall-Transducerelemente der mehreren Ultraschall-Transducerelemente als Antwort auf die gesendete Ultraschallenergie, um ein drauf basiertes Bild zu erzeugen;

Mittel zum Trennen von Puls-Echo-Komponenten, die von wenigstens einem Anteil von Kontrollpunkten empfangen worden sind, ausgewählt aus dem ersten Anteil der Kontrollpunkte (CP), die zu dem ersten identifizierbaren Teil des Untersuchungsbereichs (ROI) zugehörig sind, und dem zweiten Anteil der Kontrollpunkte (CP), die zu dem zweiten identifizierbaren Teil des Untersuchungsbereichs (ROI) zugehörig sind;

Mittel zum Bestimmen von wenigstens einem Verhältnis, ausgewählt aus dem Kontrastverhältnis (CR) zwischen den ersten und zweiten identifizierbaren Teilen basierend auf den Puls-Echo-Komponenten, die von dem ersten Anteil der Kontrollpunkte (CP), die zu dem ersten identifizierbaren Teil des Untersuchungsbereichs (ROI) zugehörig sind, erhalten worden sind, und den Puls-Echo-Komponenten, die von dem ersten Anteil der Kontrollpunkte (CP), die zu dem zweiten identifizierbaren Teil des Untersuchungsbereichs (ROI) zugehörig sind, erhalten worden sind, und einem Signal-Rausch-Verhältnis (SNR), basierend auf Puls-Echo-Komponenten, die von einem Referenz-Anteil des Untersuchungsbereichs (ROI) empfangen worden sind, und Puls-Echo-Komponenten, die von wenigstens einem Teil, ausgewählt aus dem ersten Anteil der Kontrollpunkte (CP) und dem zweiten Anteil der Kontrollpunkte (CP), empfangen worden sind; und

Mittel zum Modifizieren der für ein oder mehrere der mehreren Ultraschall-Transducerelemente erzeugten Wellenform, basierend auf wenigstem einem Vergleich des Kontrastverhältnisses (CR), bestimmt zwischen

dem ersten und zweiten identifizierbaren Teilen, mit einem Schwellenwert und einem Vergleich des Signal-Rausch-Verhältnisses (SNR) mit einem Schwellenwert, wobei das Modifizieren der für ein oder mehrere der mehreren Ultraschall-Transducerelemente erzeugten Wellenform wenigstens eines der folgenden umfasst: Anpassen der Verstärkung der Frequenzen der einen oder mehreren Frequenzen, die an einem oder mehreren Orten innerhalb der Bandbreite der Transducervorrichtung angeordnet sind, und Anpassen eines oder mehrerer Impuls-Parameter, einschließlich wenigstens einem, ausgewählt aus Pulsdauer, Impulsform, Impulsamplitude und Impulsphase, um das Zeit-Bandbreite-Produkt für die Maximierung wenigstens des Kontrastverhältnisses (CR) zwischen dem ersten und dem zweiten identifizierbaren Bereich des Untersuchungsbereichs (ROI) und einem Signal-Rausch-Verhältnis (SNR) aus dem Untersuchungsbereich (ROI) anzupassen.

3. Das Verfahren oder System gemäß einem der Ansprüche 1 bis 2, wobei der erste Anteil der Kontrollpunkte (CP) zu einer Gefäßwand einer vaskulären Struktur des Subjekts zugehörig ist und der zweite Anteil der Kontrollpunkte (CP) zu einem Lumen zugehörig ist, das wenigstens zum Teil durch die Gefäßwand definiert bzw. begrenzt ist.

4. Das Verfahren oder System gemäß Anspruch 3, wobei die mehreren Kontrollpunkte (CP) innerhalb des Untersuchungsbereichs ferner einen Anteil an Kontrollpunkten (CP) umfasst, welche zu dem die Gefäßwand umgebenden Gewebe (46) der vaskulären Struktur zugehörig sind, wobei die von dem dritten Anteil der Kontrollpunkte (CP) empfangenen Puls-Echo-Komponenten, die zu dem Gewebe zugehörig sind, von den von den anderen Anteilen der Kontrollpunkte (CP) empfangenen Puls-Echo-Komponenten getrennt werden bzw. sind, und wobei ferner wenigstens ein Kontrastverhältnis (CR) zwischen dem Gewebe und wenigstens einer Struktur, ausgewählt aus der Gefäßwand (42) oder dem Lumen (45), zur Verwendung der Modifizierung der für eine oder mehrere der mehreren Ultraschall-Transducerelemente erzeugten Wellenformen bestimmt wird bzw. ist.

5. Das Verfahren oder System gemäß einem der Ansprüche 1 bis 4, wobei das Verfahren ferner das Folgende umfasst oder das System folgendermaßen ausgestaltet ist:

Trennen wenigstens eines Anteils der empfangenen Puls-Echo-Daten, die als Antwort auf die gesendete Ultraschallenergie, die einer einzelnen Frequenz der einen oder mehreren Bildfrequenzen entspricht, bei jedem Ultraschall-Transducerelement aus dem Untersuchungsbereich empfangen worden ist; und Wiederherstellen eines für eine oder mehrere Eigenschaften in dem Untersuchungsbereich repräsentativen Abbildes aus den getrennten Puls-Echo-Daten, die der einzelnen Frequenz der einen oder mehreren Bildfrequenzen entsprechen.

6. Das System gemäß einem der Ansprüche 2 bis 5, wobei das System derart ausgestaltet ist, dass es eine Therapie für einen Patienten basierend auf der Identifizierung wenigstens einer vaskulären Eigenschaft des Untersuchungsbereichs, in welchem ein Anteil eines Blutgefäßes angeordnet ist, liefert.

7. Das Verfahren oder System gemäß einem der Ansprüche 1 bis 6, wobei die Erzeugung der Elementfrequenzkomponenten für jede der einen oder mehreren Bildfrequenzen zur Ausbildung wenigstens eines Teils der Wellenform, welche an das Ultraschall-Transducerelement angelegt wird, die Erzeugung einer oder mehrerer Ansteuerungsvektoren umfasst, und wobei ferner das Erzeugen der einen oder mehreren Ansteuerungsvektoren die Erzeugung eines jeden Ansteuerungsvektors unter Verwendung einer Feldanalyse bei einer einzelnen Frequenz der einen oder mehreren Bildfrequenzen innerhalb der Transducerbandbreite umfasst.

8. Das Verfahren oder System gemäß Anspruch 7, wobei der erzeugte Ansteuerungsvektor eine Elementfrequenzkomponente umfasst, welche einem jeden Ultraschall-Transducerelement der Mehrzahl an Ultraschall-Transducerelementen entspricht.

9. Das System gemäß einem der Ansprüche 2 bis 8, wobei das System derart ausgestaltet ist, dass es einem Patienten auf Basis der Identifizierung wenigstens einer vaskulären Eigenschaft des Untersuchungsbereichs (ROI), in welchem wenigstens ein Teil eines Blutgefäßes angeordnet ist, eine Therapie liefert.

10. Das System gemäß Anspruch 9, wobei die Verwendung von Ultraschallenergie zur Lieferung einer Therapie die Verwendung der Transducervorrichtung umfasst, um Ultraschallenergie zu senden, Puls-Echo-Daten zu empfangen und Ultraschallenergie zur Lieferung der Therapie zu erzeugen.

11. Das Verfahren oder System gemäß einem der Ansprüche 1 bis 10, wobei das Empfangen von Puls-Echo-Daten als Antwort auf die abgegebene Ultraschallenergie an jedem Ultraschall-Transducerelement der Mehrheit der Ul-

trascall-Transducerelemente aus dem Untersuchungsbereich die Anwendung einer Filterbank basierend auf einer diskreten Fourier-Transformation zur Trennung der Puls-Echo-Daten umfasst.

- 5 12. Das Verfahren oder System gemäß einem der Ansprüche 1 bis 11, wobei die eine oder mehreren Bildgebungs-Wellenformen eine finite Anzahl von wahlweise ausgewählten Einzelfrequenzkomponenten umfasst, wobei jede Einzelfrequenzkomponente einen Träger mit einer finiten Bandbreite aufweist, welche durch ihre Dauer und ihren Modulationsimpuls gekennzeichnet ist.

10 **Revendications**

1. Procédé d'imagerie par ultrasons (30 ; 80) comprenant :

fournir une région d'intérêt (ROI) chez un sujet ;  
 15 définir une pluralité de points de contrôle (CP) à l'intérieur de la région d'intérêt (ROI), au moins une première partie des points de contrôle (CP) étant associée à une première partie identifiable de la région d'intérêt (ROI) et une deuxième partie des points de contrôle (CP) étant associée à une seconde partie identifiable de la région d'intérêt (ROI) qui est différente de la première partie identifiable ;  
 20 fournir un appareil de transducteur (22) comprenant une pluralité d'éléments transducteurs à ultrasons, chacun parmi la pluralité d'éléments transducteurs à ultrasons étant configuré pour délivrer de l'énergie ultrasonore à la région d'intérêt (ROI) en réponse à une forme d'onde appliquée à celui-ci ;  
 générer une forme d'onde pour chaque élément transducteur à ultrasons parmi la pluralité d'éléments transducteurs à ultrasons, générer la forme d'onde comprenant :

25 sélectionner une ou plusieurs fréquences d'imagerie à l'intérieur d'une largeur de bande d'appareil de transducteur, la ou chacune des fréquences d'imagerie étant une porteuse d'une impulsion à transmettre ayant une largeur de bande finie à l'intérieur de la largeur de bande de transducteur et ayant une durée ; et  
 générer des composantes de fréquence d'élément pour la ou chacune des fréquences d'imagerie pour former au moins une partie de la forme d'onde à appliquer à l'élément transducteur à ultrasons ;

30 délivrer de l'énergie ultrasonore dans un mode à impulsions à la région d'intérêt à l'aide de la pluralité d'éléments transducteurs à ultrasons en réponse à des formes d'onde générées pour chacun parmi la pluralité d'éléments transducteurs à ultrasons ;

35 recevoir des données d'écho d'impulsion, à chaque élément transducteur à ultrasons parmi une pluralité d'éléments transducteurs à ultrasons, à partir de la région d'intérêt (ROI) en réponse à l'énergie ultrasonore délivrée, pour générer une image sur la base de celles-ci ;

séparer des composantes d'écho d'impulsion reçues en provenance d'au moins une parmi la première partie des points de contrôle associée à la première partie identifiable de la région d'intérêt et la deuxième partie des points de contrôle associée à la seconde partie identifiable de la région d'intérêt ;

40 déterminer au moins un parmi un rapport de contraste (CR) entre les première et seconde parties identifiées sur la base des composantes d'écho d'impulsion reçues en provenance de la première partie des points de contrôle (CP) associée à la première partie identifiable de la région d'intérêt (ROI) et des composantes d'écho d'impulsion reçues en provenance de la deuxième partie des points de contrôle (CP) associée à la seconde partie identifiable de la région d'intérêt (ROI), et un rapport signal sur bruit (SNR) sur la base des composantes d'écho d'impulsion reçues en provenance d'une partie de référence de la région d'intérêt (ROI) et des composantes d'écho d'impulsion reçues en provenance d'au moins une parmi la première partie des points de contrôle (CP) et la deuxième partie des points de contrôle (CP) ; et

45 modifier la forme d'onde générée pour un ou plusieurs parmi la pluralité d'éléments transducteurs à ultrasons sur la base d'au moins une parmi une comparaison du rapport de contraste (CR) déterminé entre les première et seconde parties identifiées à une valeur de seuil et une comparaison du rapport signal sur bruit (SNR) à une valeur de seuil, modifier la forme d'onde générée pour un ou plusieurs parmi la pluralité d'éléments transducteurs à ultrasons comprenant au moins un parmi ajuster un gain à des fréquences parmi la ou les fréquences situées à un ou plusieurs emplacements à l'intérieur de la largeur de bande d'appareil de transducteur, et ajuster un ou plusieurs paramètres d'impulsion comprenant au moins une parmi une durée d'impulsion, une forme d'impulsion, une amplitude d'impulsion et une phase d'impulsion, pour ajuster un produit temps/largeur de bande afin de rendre maximal au moins un parmi le rapport de contraste (CR) entre les première et seconde parties identifiées de la région d'intérêt (ROI) et un rapport signal sur bruit (SNR) à partir de la région d'intérêt (ROI).

## 2. Système d'imagerie par ultrasons (10), comprenant :

un appareil de transducteur (22) comprenant une pluralité d'éléments transducteurs à ultrasons, chacun parmi la pluralité d'éléments transducteurs à ultrasons étant configuré pour délivrer de l'énergie ultrasonore à une région d'intérêt (ROI) en réponse à une forme d'onde appliquée à celui-ci résultant de données d'écho d'impulsion provenant de celle-ci ; et

des moyens pour fournir une région d'intérêt (ROI) chez un sujet, configurés pour définir une pluralité de points de contrôle (CP) à l'intérieur de la région d'intérêt (ROI), au moins une première partie des points de contrôle (CP) étant associée à une première partie identifiable de la région d'intérêt (ROI) et une deuxième partie des points de contrôle (CP) étant associée à une seconde partie identifiable de la région d'intérêt (ROI) qui est différente de la première partie identifiable ;

des moyens pour générer une forme d'onde pour chaque élément transducteur à ultrasons parmi la pluralité d'éléments transducteurs à ultrasons, les moyens de génération de forme d'onde comprenant :

des moyens pour sélectionner une ou plusieurs fréquences d'imagerie à l'intérieur d'une largeur de bande d'appareil de transducteur, la ou chacune des fréquences d'imagerie étant une porteuse d'une impulsion à transmettre ayant une largeur de bande finie à l'intérieur de la largeur de bande d'appareil de transducteur et ayant une durée ; et

des moyens pour générer des composantes de fréquence d'élément pour la ou chacune des fréquences d'imagerie pour former au moins une partie de la forme d'onde à appliquer à l'élément transducteur à ultrasons ;

des moyens pour commander la distribution d'énergie ultrasonore dans un mode à impulsion à la région d'intérêt (ROI) à l'aide de la pluralité d'éléments transducteurs à ultrasons en réponse à des formes d'onde générées pour chacun parmi la pluralité d'éléments transducteurs à ultrasons ;

des moyens pour commander la capture de données d'écho d'impulsion à chaque élément transducteur à ultrasons parmi une pluralité d'éléments transducteurs à ultrasons, provenant de la région d'intérêt en réponse à l'énergie ultrasonore délivrée, pour générer une image sur la base de celles-ci ;

des moyens pour séparer des composantes d'écho d'impulsion reçues en provenance d'au moins une parmi la première partie des points de contrôle (CP) associée à la première partie identifiable de la région d'intérêt (ROI) et la deuxième partie des points de contrôle (CP) associée à la seconde partie identifiable de la région d'intérêt (ROI) ;

des moyens pour déterminer au moins un parmi un rapport de contraste (CR) entre les première et seconde parties identifiables, sur la base des composantes d'écho d'impulsion reçues en provenance de la première partie des points de contrôle (CP) associée à la première partie identifiable de la région d'intérêt (ROI) et des composantes d'écho d'impulsion reçues en provenance de la deuxième partie des points de contrôle (CP) associée à la seconde partie identifiable de la région d'intérêt (ROI), et un rapport signal sur bruit (SNR) sur la base des composantes d'écho d'impulsion reçues en provenance d'une partie de référence de la région d'intérêt (ROI) et des composantes d'écho d'impulsion reçues en provenance d'au moins une parmi la première partie des points de contrôle (CP) et la deuxième partie des points de contrôle (CP) ; et

des moyens pour modifier la forme d'onde générée pour un ou plusieurs parmi la pluralité d'éléments transducteurs à ultrasons sur la base d'au moins une parmi une comparaison du rapport de contraste (CR) déterminé entre les première et seconde parties identifiables à une valeur de seuil et une comparaison du rapport signal sur bruit (SNR) à une valeur de seuil, modifier la forme d'onde générée pour un ou plusieurs parmi la pluralité d'éléments transducteurs à ultrasons comprenant au moins un parmi ajuster un gain à des fréquences parmi la ou les fréquences situées à un ou plusieurs emplacements à l'intérieur de la largeur de bande d'appareil de transducteur, et ajuster un ou plusieurs paramètres d'impulsion comprenant au moins une parmi une durée d'impulsion, une forme d'impulsion, une amplitude d'impulsion et une phase d'impulsion, pour ajuster un produit temps/largeur de bande afin de rendre maximal au moins un parmi le rapport de contraste (CR) entre les première et seconde parties identifiables de la région d'intérêt (ROI) et un rapport signal sur bruit (SNR) à partir de la région d'intérêt (ROI).

3. Procédé ou système selon l'une quelconque des revendications 1 à 2, dans lequel la première partie des points de contrôle (CP) est associée à une paroi de vaisseau d'une structure vasculaire du sujet et la deuxième partie des points de contrôle (CP) est associée à une lumière définie au moins en partie par la paroi de vaisseau.

4. Procédé selon la revendication 3, dans lequel la pluralité de points de contrôle (CP) à l'intérieur de la région d'intérêt comprennent en outre une troisième partie des points de contrôle (CP) associée à un tissu (46) entourant la paroi

de vaisseau de la structure vasculaire, des composantes d'écho d'impulsion reçues en provenance de la troisième partie des points de contrôle (CP) associée au tissu étant séparées des composantes d'écho d'impulsion reçues en provenance d'autres parties des points de contrôle (CP) et, en outre, au moins un rapport de contraste (CR) entre le tissu et au moins une parmi la paroi de vaisseau (42) et la lumière (45) étant déterminé pour une utilisation dans la modification de la forme d'onde générée pour un ou plusieurs parmi la pluralité d'éléments transducteurs à ultrasons.

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5. Procédé ou système selon l'une quelconque des revendications 1 à 4, dans lequel le procédé comprend en outre ou le système est configuré pour :

séparer, à partir des données d'écho d'impulsion reçues, au moins une partie de celles-ci reçue à chaque élément transducteur à ultrasons en provenance de la région d'intérêt en réponse à l'énergie ultrasonore délivrée correspondant à une fréquence individuelle parmi la ou les fréquences d'imagerie ; et reconstruire une image représentative d'une ou de plusieurs propriétés dans la région d'intérêt à partir des données d'écho d'impulsion séparées correspondant à la fréquence individuelle parmi la ou les fréquences d'imagerie.

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6. Système selon l'une quelconque des revendications 2 à 5, dans lequel le système est configuré pour administrer une thérapie à un patient sur la base d'une identification d'au moins une caractéristique vasculaire de la région d'intérêt dans laquelle au moins une partie d'un vaisseau sanguin est située.

- 25
7. Procédé ou système selon l'une quelconque des revendications 1 à 6, dans lequel générer des composantes de fréquence d'élément pour la ou chacune des fréquences d'imagerie pour former au moins une partie de la forme d'onde à appliquer à l'élément transducteur à ultrasons comprend générer un ou plusieurs vecteurs d'excitation et, en outre, générer le ou les vecteurs d'excitation comprend générer chaque vecteur d'excitation à l'aide d'une synthèse de champ à une fréquence individuelle parmi la ou les fréquences d'imagerie à l'intérieur de la largeur de bande de transducteur.

- 30
8. Procédé ou système selon la revendication 7, dans lequel le vecteur d'excitation généré comprend une composante de fréquence d'élément correspondant à chaque élément transducteur à ultrasons parmi la pluralité d'éléments transducteurs à ultrasons.

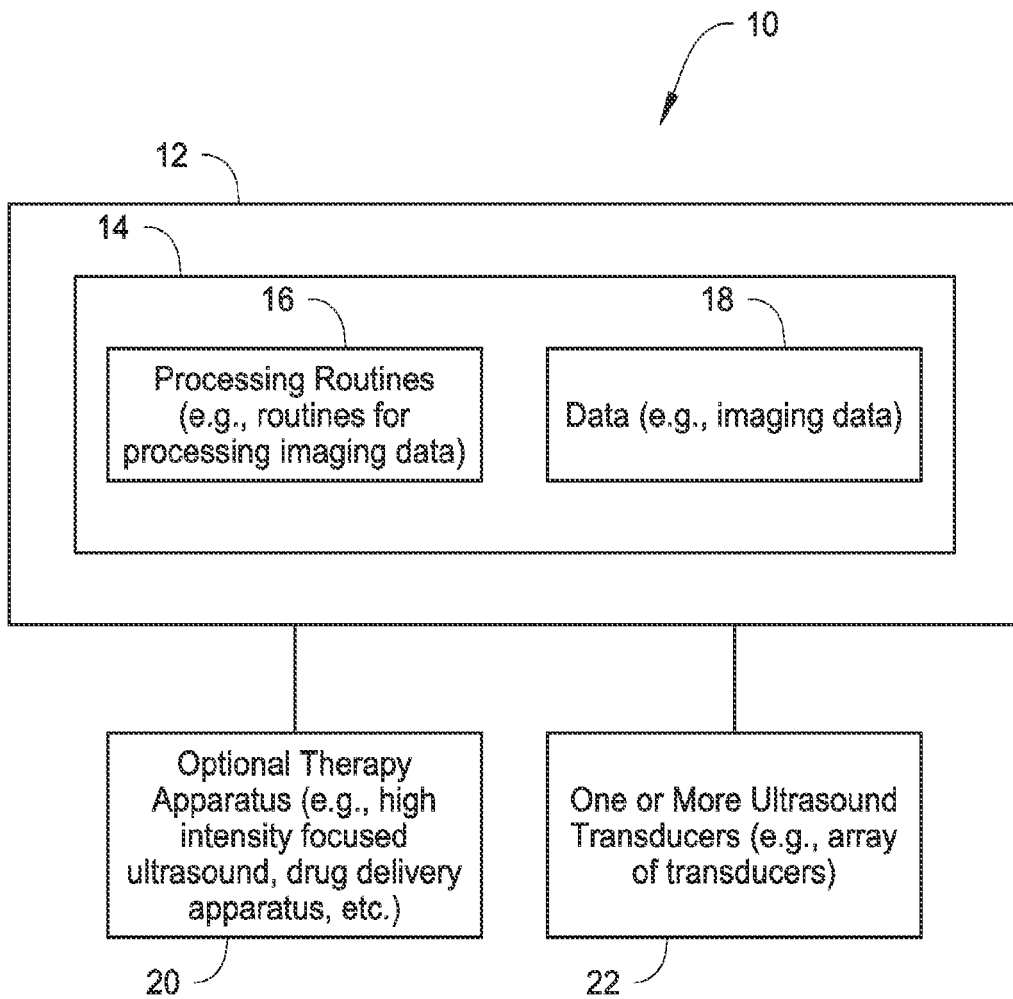
- 35
9. Système selon l'une quelconque des revendications 2 à 8, dans lequel le système est configuré pour administrer une thérapie à un patient sur la base d'une identification d'au moins une caractéristique vasculaire de la région d'intérêt (ROI) dans laquelle au moins une partie d'un vaisseau sanguin est située.

- 40
10. Système selon la revendication 9, dans lequel utiliser de l'énergie ultrasonore pour administrer une thérapie comprend utiliser l'appareil de transducteur pour délivrer de l'énergie ultrasonore et recevoir des données d'écho d'impulsion, et pour générer de l'énergie ultrasonore pour administrer une thérapie.

- 45
11. Procédé ou système selon l'une quelconque des revendications 1 à 10, dans lequel recevoir des données d'écho d'impulsion, à chaque élément transducteur à ultrasons parmi une pluralité d'éléments transducteurs à ultrasons, en provenance de la région d'intérêt en réponse à l'énergie ultrasonore délivrée, comprend utiliser un banc de filtres basés sur la transformée de Fourier discrète pour la séparation de données d'écho d'impulsion.

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12. Procédé ou système selon l'une quelconque des revendications 1 à 11, dans lequel la ou les formes d'onde d'imagerie comprennent un nombre fini de composantes de fréquence individuelles sélectionnées de manière aléatoire, chaque composante de fréquence individuelle étant une porteuse ayant une largeur de bande finie spécifiée par sa durée et son impulsion de modulation.

*Fig. 1*



*Fig. 2*

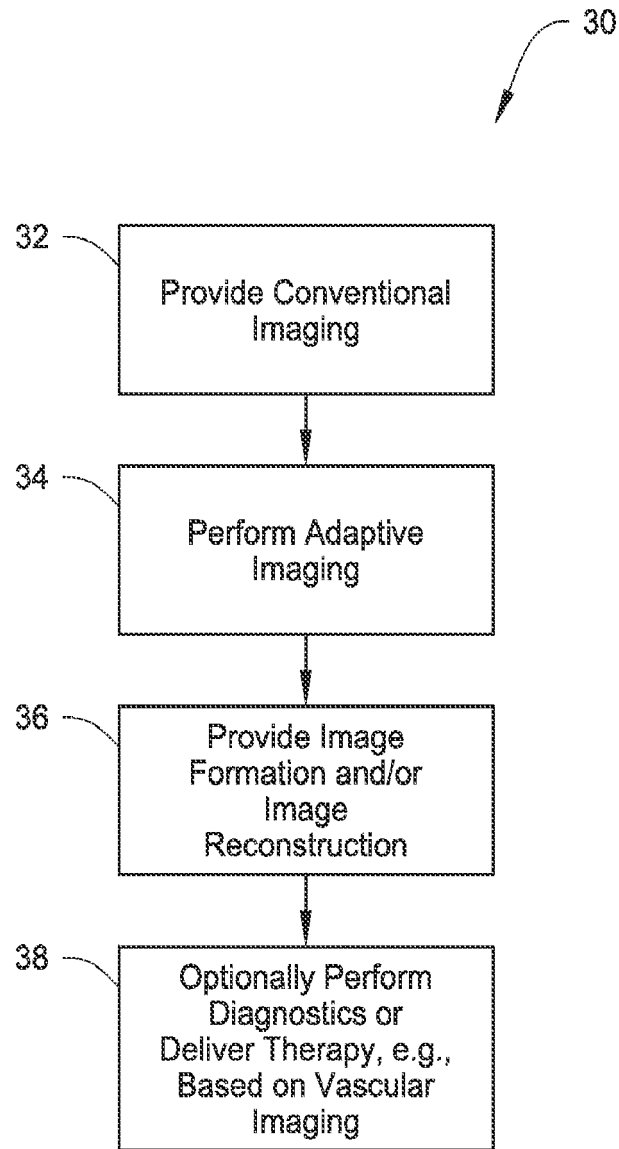
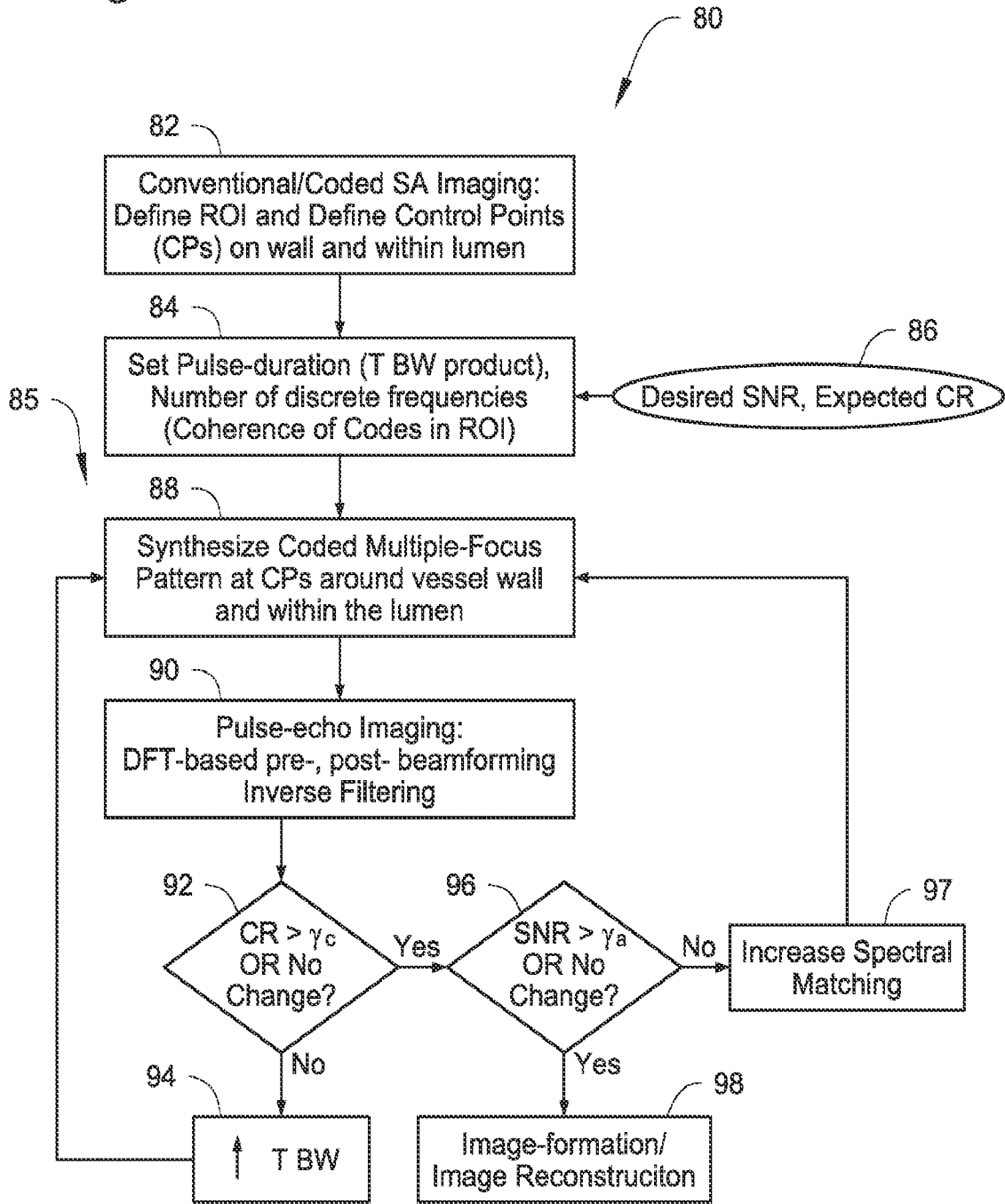
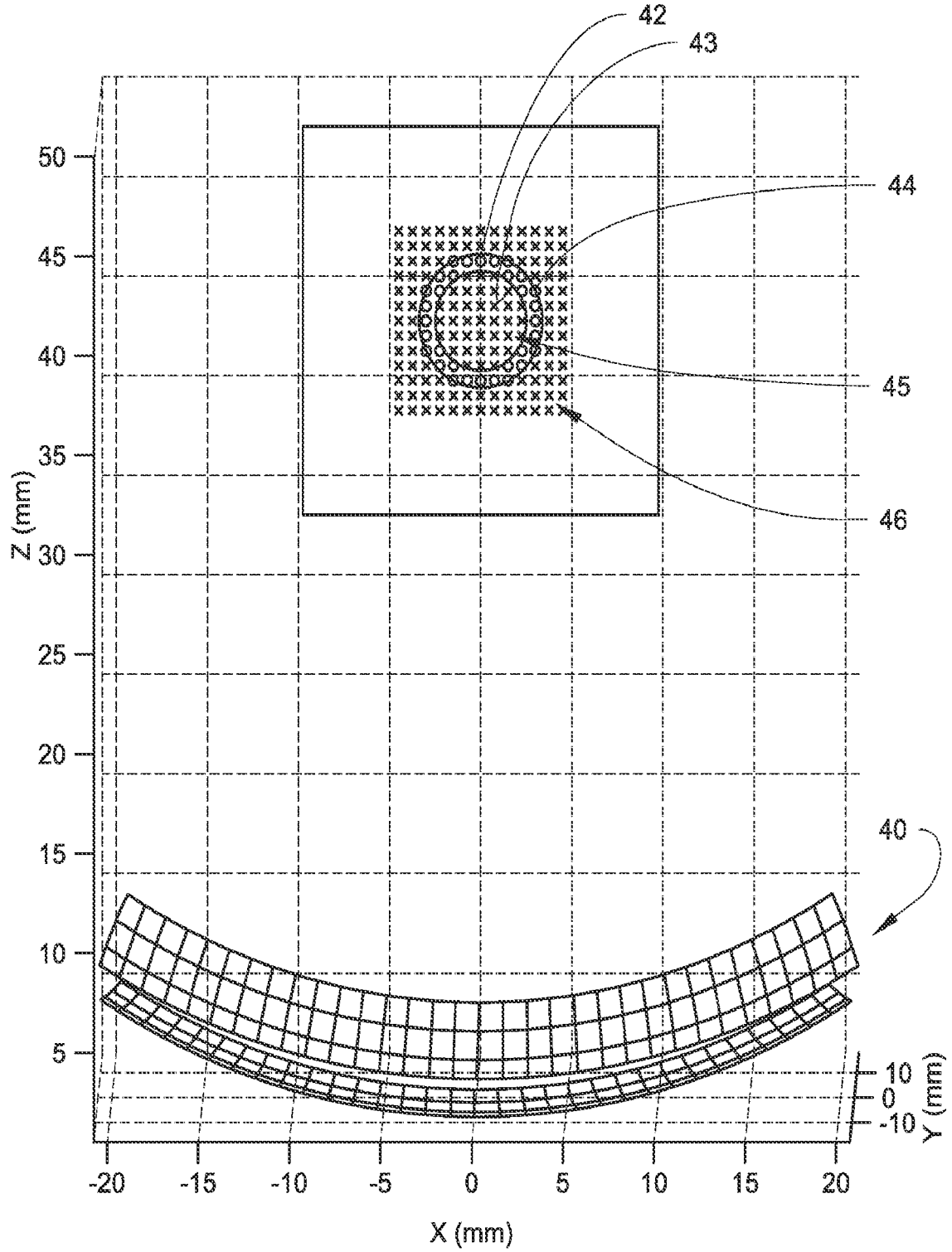


Fig. 3



Remarks: 1. CR Energy on wall CPs/Energy in Lumen CPs; 2. SNR Int Gain at all CPs (ref linear chirp); 3. Increasing spectral matching decreases BW;

Fig. 4



## Fig. 5

## Algorithm 1 Optimal Synthesis of Multiple-focus, Multiple-frequency Transmit-receive Patterns

Element waveforms  $u_n(t) = 0 \quad \forall n = 1, 2, \dots, N$  ▷  $N$  number of elements  
 Wall CPs  $\rightarrow H_W(f)$  ▷ Size  $M_W \times N$   
 Lumen CPs  $\rightarrow H_L(f)$  ▷ Size  $M_L \times N$   
 Critical CPs  $\rightarrow H_C(f)$  ▷ Size  $M_C \times N$

1: for all  $i = 1, \dots, N_F$  do  
 2: procedure SOLVE OPTIMIZATION PROBLEM ( $H_W(f_i), H_L(f_i), H_C(f_i), u_{opt}(f_i)$ )  
 3:  $H_T = \begin{bmatrix} H_W \\ H_L \end{bmatrix}$  and  $H_C = H_C$   
 4:  $W_T = H_T^H H_T$ ,  $W_C = (H_C^H H_C + \gamma C D)$ ,  $\gamma C > 0$  (small)

$$u_{opt}^{(i)} = W_C^{-1} H_T^H (H_T W_C^{-1} H_T^H)^{\dagger} p_T$$

Or Generalized Eigenvalue:

$$\text{Choose } u_{opt} \text{ such that } \lambda_{max}(W_T, W_C) = \sup_{u \neq 0} \frac{u^H W_T u}{u^H W_C u}$$

Solution through Generalized Eigenvalue Decomposition

$$\lambda_{max} = \max \{ \lambda \mid \det(\lambda W_C - W_T) = 0 \}$$

Other optimization criteria can be applied, e.g. constant modulus or weighted solutions. These solutions can be generated separately or in parallel.

6: end procedure

7: for all  $N$  DMUA elements  $n = 1, 2, \dots, N$  do

$$u_n(t) = u_n(t) + \Re \left\{ u_{opt_n}^*(f_i) e^{j2\pi f_i t} g(t) \right\}$$

8: end for

9: end for

▷  $g(t)$ , e.g. raised cosine

Fig. 6

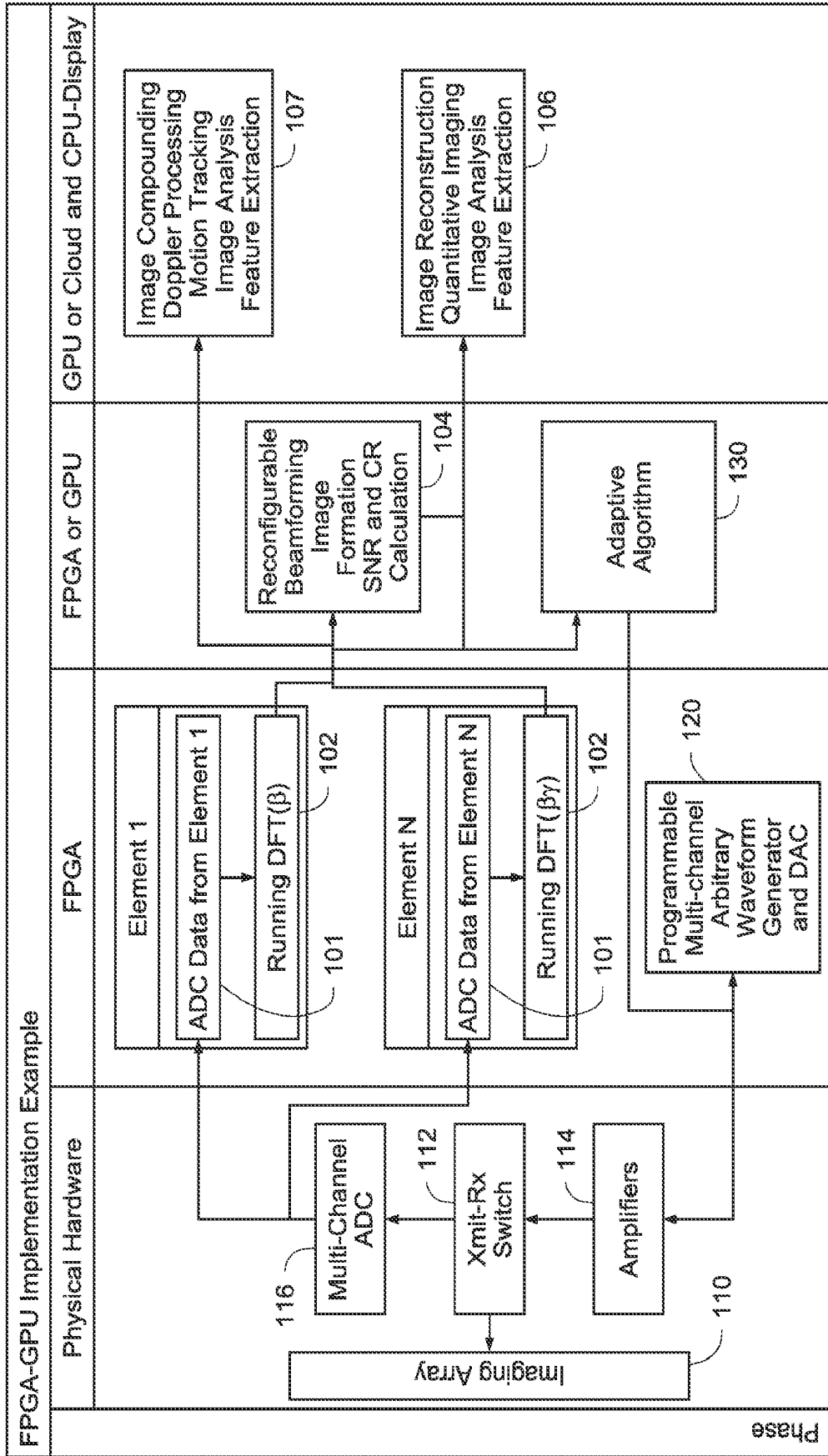


Fig. 7

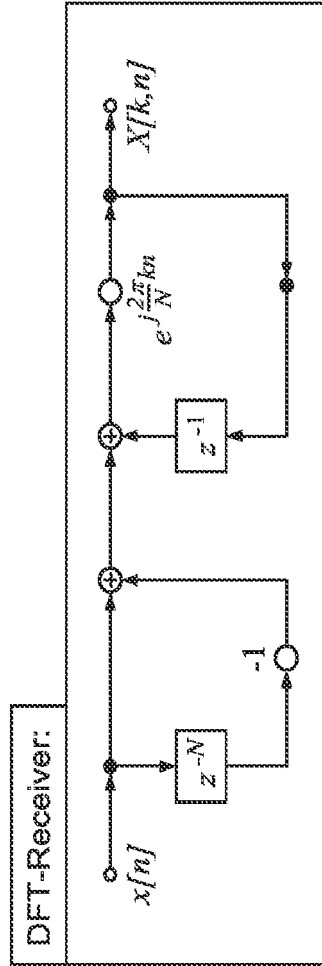


Fig. 8

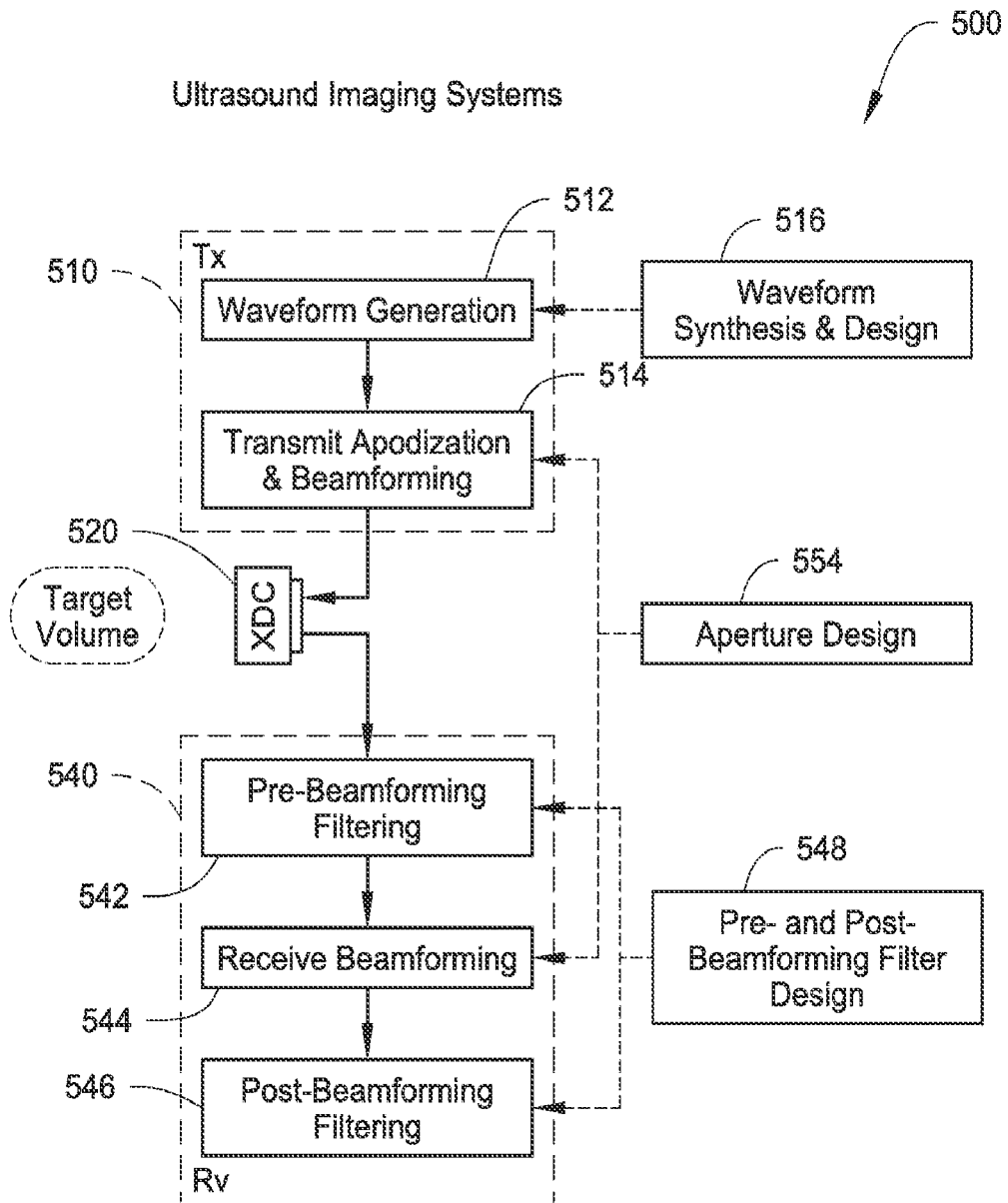


Fig. 9

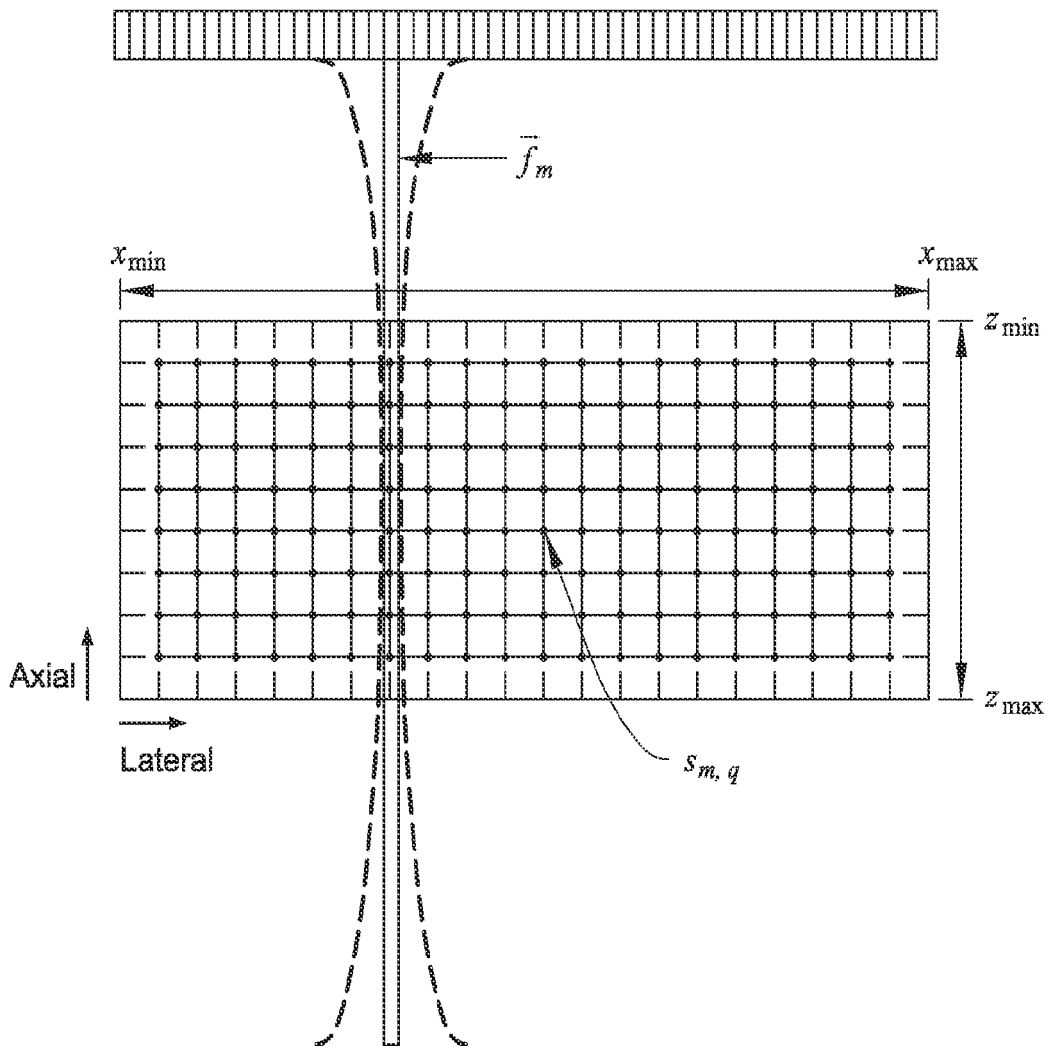
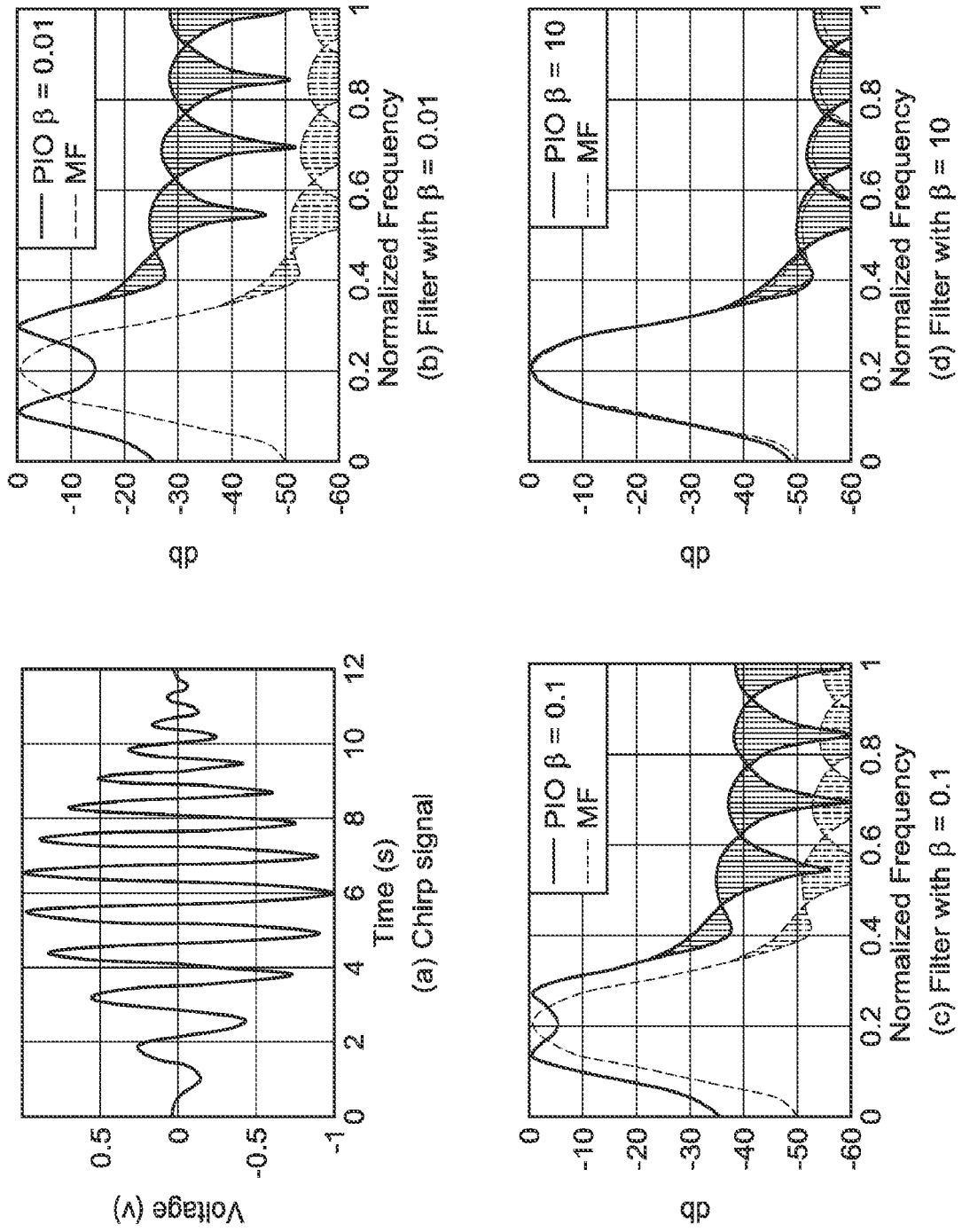


Fig. 10



*Fig. 11*

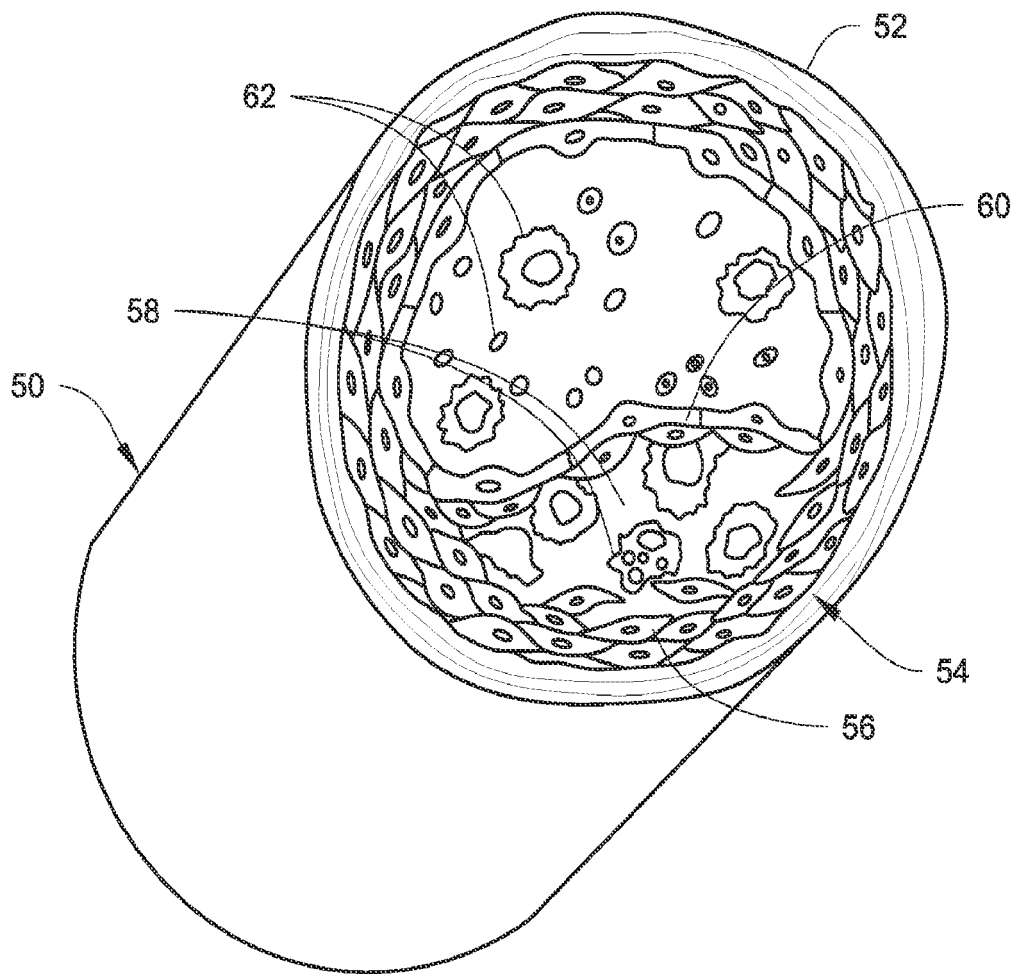
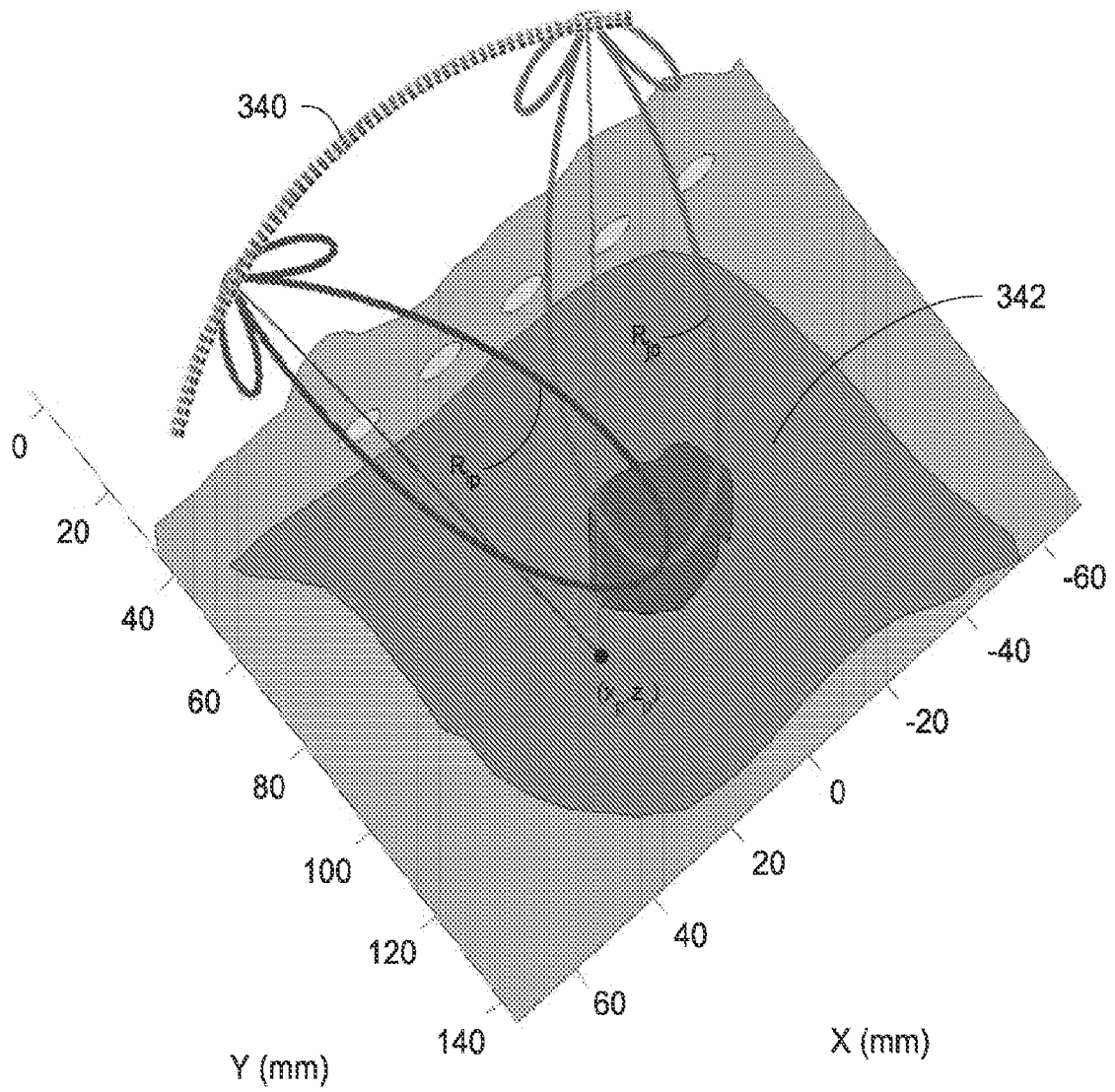


Fig. 12



*Fig. 13*

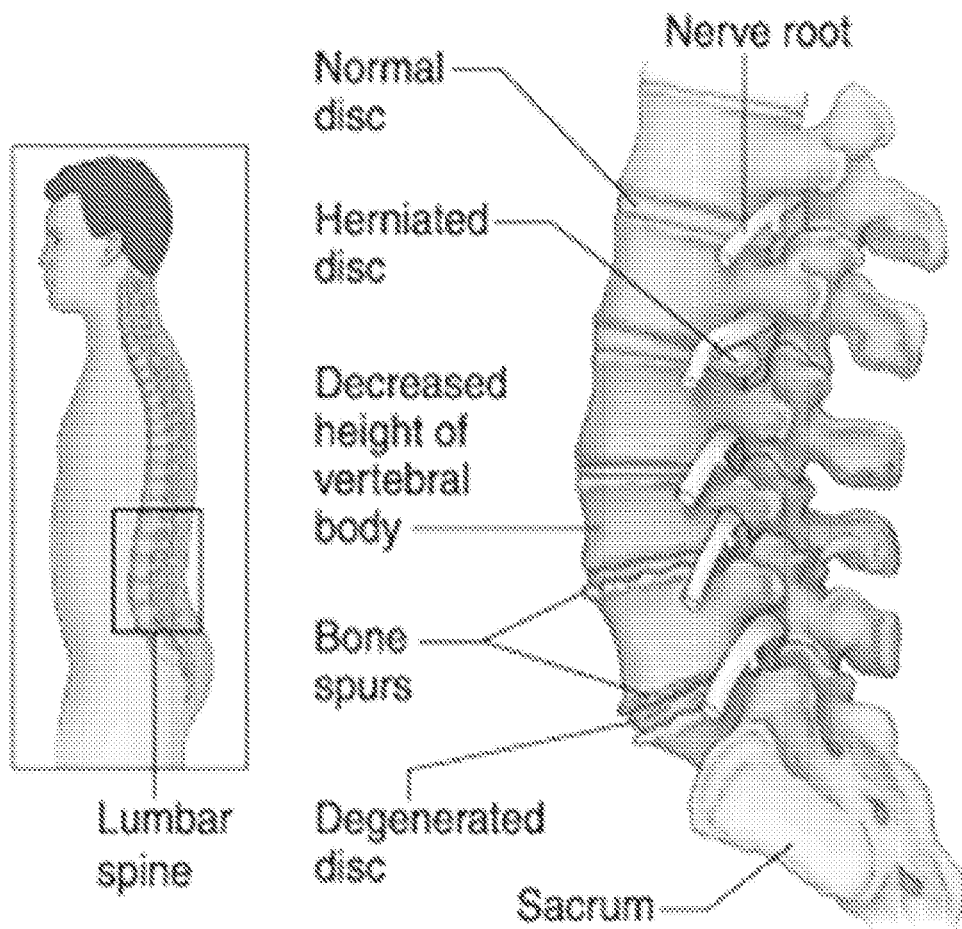


Fig. 14

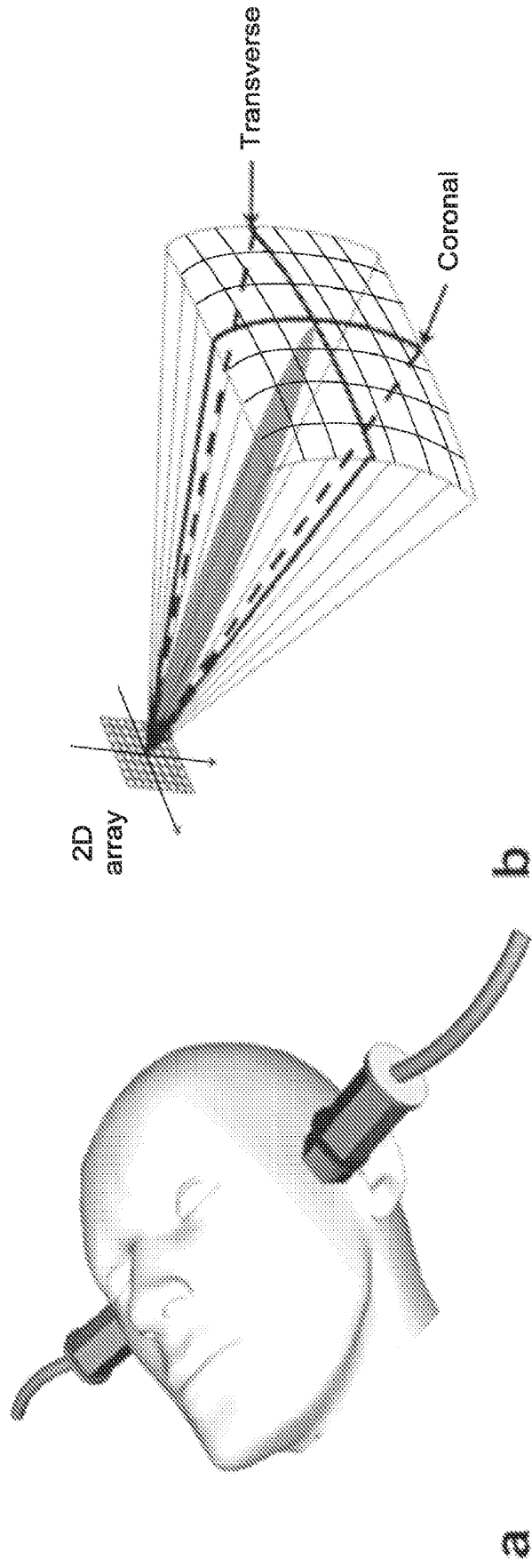
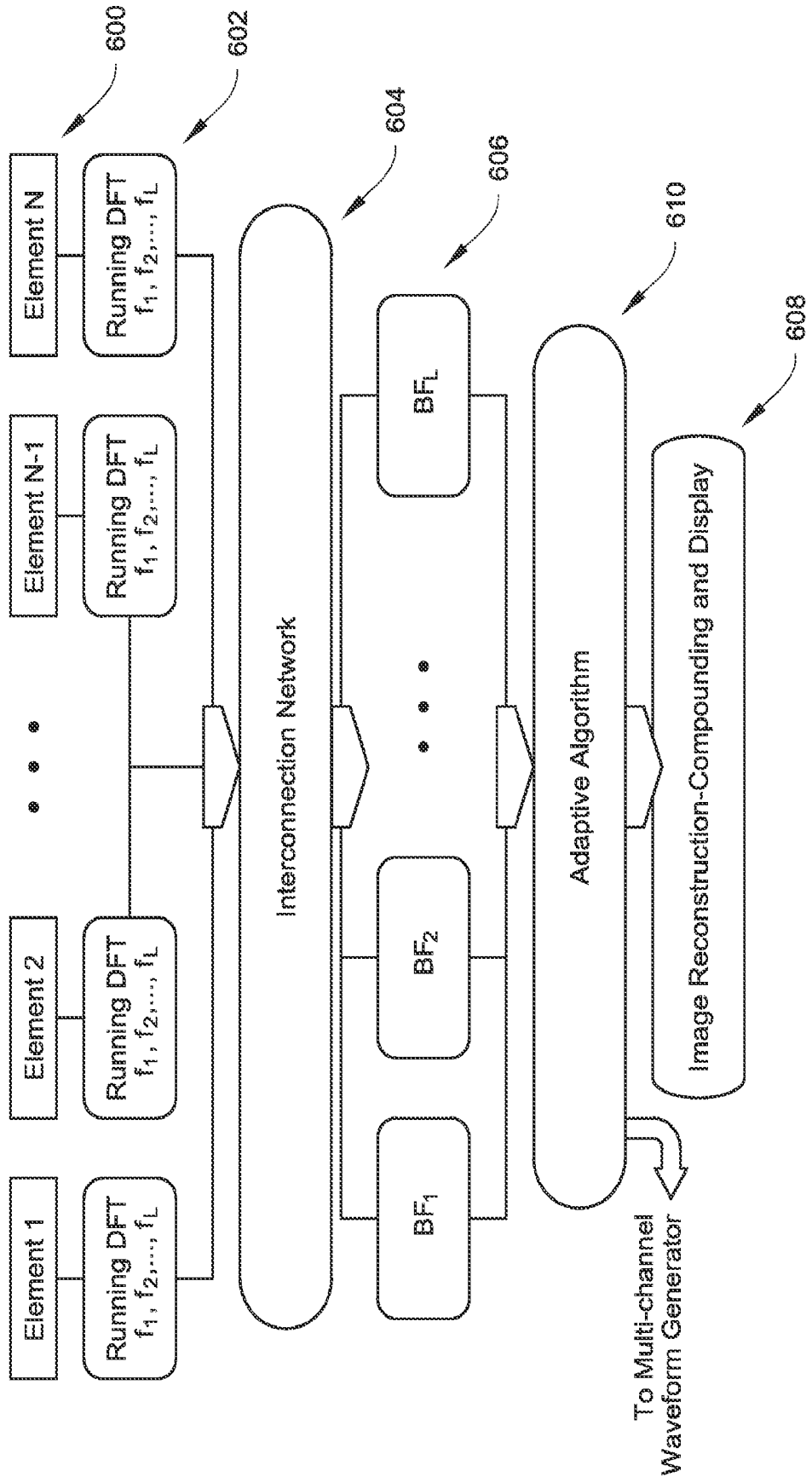


Fig. 15



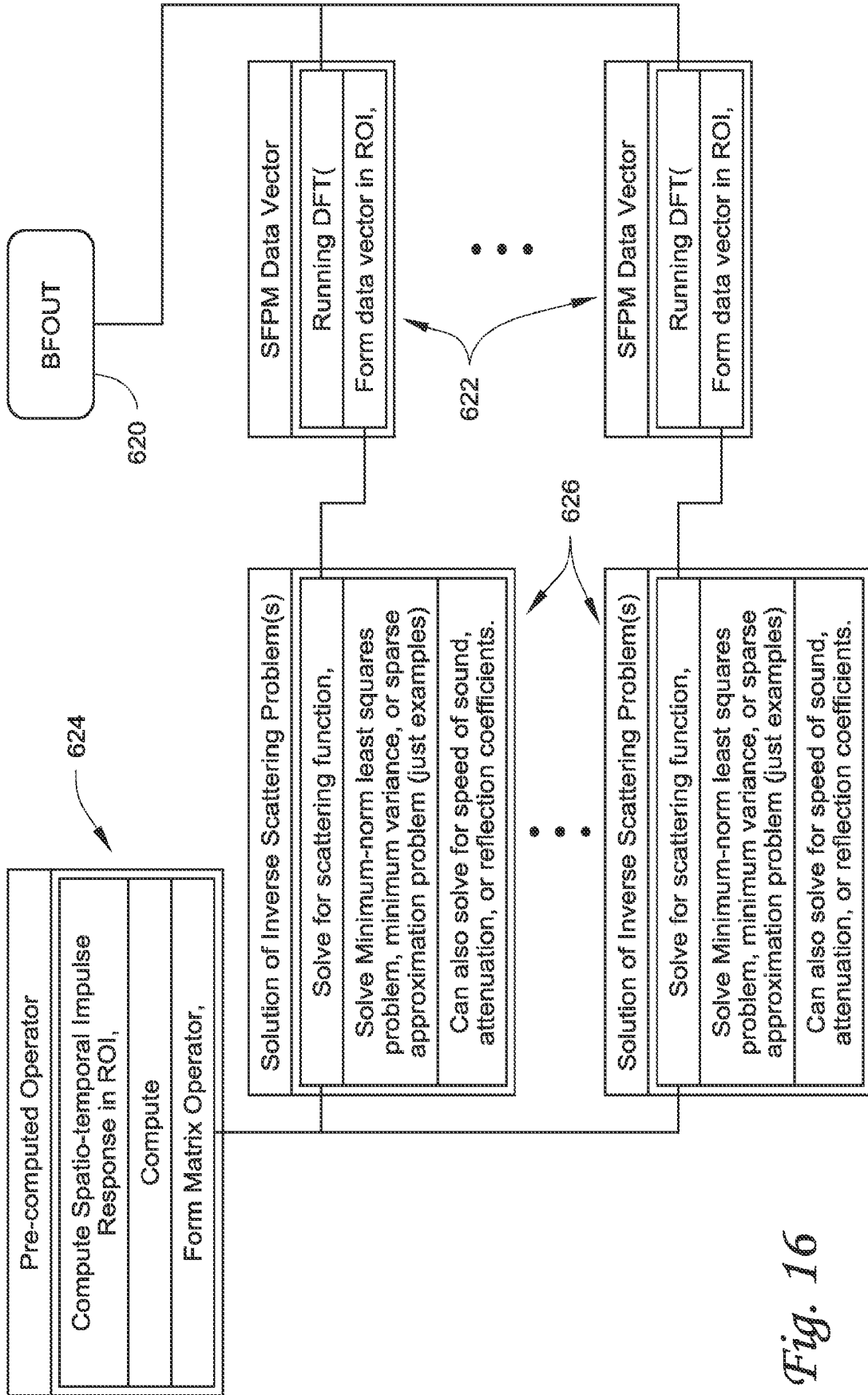
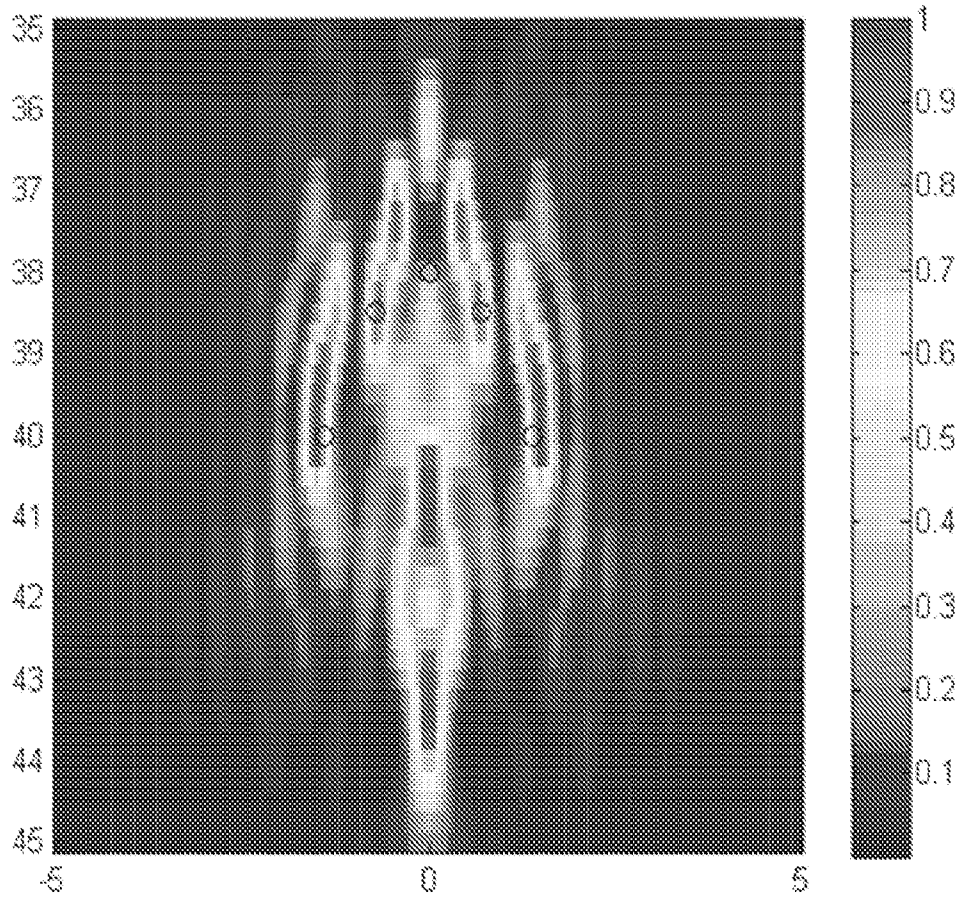
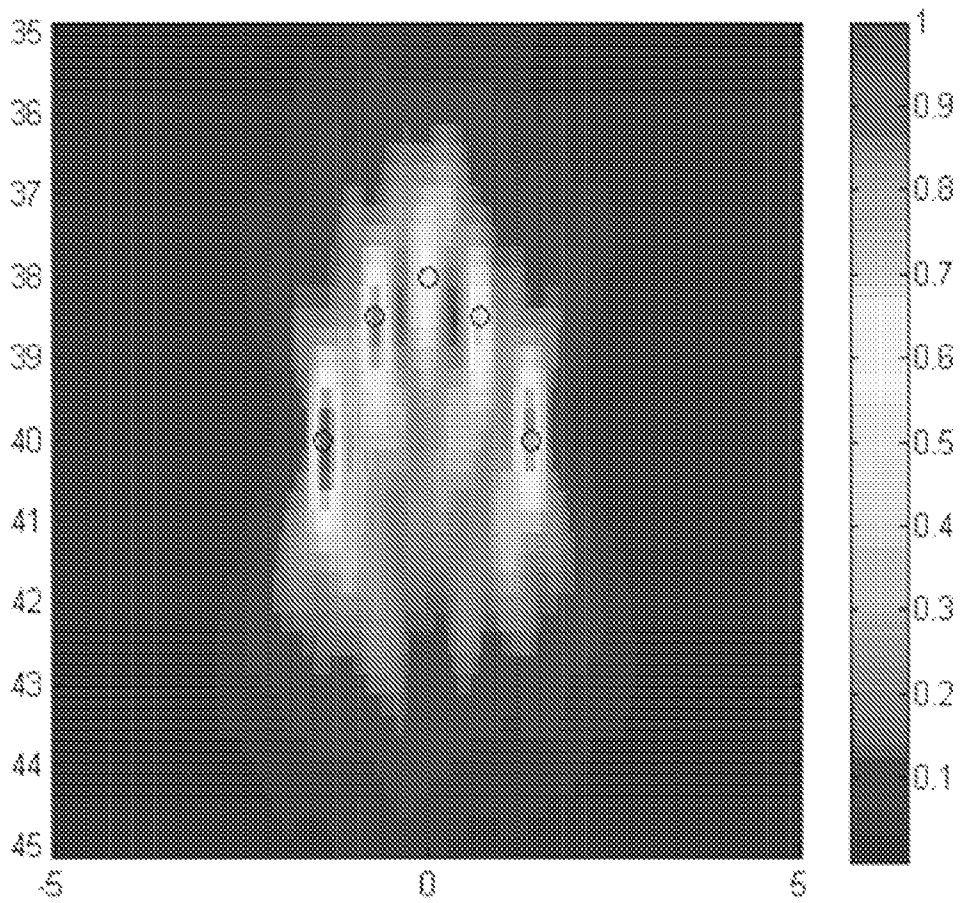


Fig. 16

*Fig. 17A*



*Fig. 17B*



## REFERENCES CITED IN THE DESCRIPTION

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专利名称(译)	使用多个频率波形的超声图像的形成和/或重建		
公开(公告)号	<a href="#">EP3025166B1</a>	公开(公告)日	2020-06-17
申请号	EP2014750404	申请日	2014-07-21
[标]申请(专利权)人(译)	明尼苏达大学		
申请(专利权)人(译)	明尼苏达大学校董会		
当前申请(专利权)人(译)	明尼苏达大学校董会		
[标]发明人	EBBINI EMAD S LIU DALONG CASPER ANDREW J		
发明人	EBBINI, EMAD S. LIU, DALONG CASPER, ANDREW J.		
IPC分类号	G01S15/89 G01S7/52 G10K11/34 A61B8/14		
CPC分类号	A61B8/14 A61B8/4438 G01S7/5202 G01S7/52046 G01S15/8915 G01S15/8952 G01S15/8959 G01S15/8997 A61B8/0891 A61B8/5207 A61N7/00		
代理机构(译)	LATZEL , KLAUS		
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摘要(译)

超声自适应成像方法和/或系统提供了波形生成的修改以驱动多个换能器元件。该修改可以基于相对于感兴趣区域中的控制点所确定的对比度或信噪比中的至少一个。此外，可以响应于所传送的超声能量对应于一个或多个图像频率的单个频率，从接收的脉冲回波数据中，将每个超声换能器元件处接收的至少一部分从感兴趣区域中分离出来，从而执行图像重建。在换能器设备带宽内。从与一个或多个图像频率的单个频率相对应的分离的脉冲回波数据重构的图像可以单独使用，也可以与类似的图像数据组合使用（例如，以提供代表感兴趣区域中一个或多个属性的图像）。

$$\{w_i(f, \tau)\}_{i=1}^{N_s}$$