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**(54) SYSTEMS AND METHODS FOR REDUCING NON-UNIFORM ROTATION DISTORTION IN
ULTRASOUND IMAGES**

SYSTEME UND VERFAHREN ZUR REDUZIERUNG VON UNGLEICHMÄSSIGER
ROTATIONSVERZERRUNG BEI ULTRASCHALLBILDERN

SYSTÈMES ET PROCÉDÉS DE RÉDUCTION DE DISTORSION DE ROTATION NON UNIFORME
DANS IMAGES ULTRASONORES

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DescriptionTECHNICAL FIELD

[0001] The present invention is directed to the area of imaging systems that are insertable into a patient and methods of making and using the imaging systems. The present invention is also directed to methods and imaging systems for reducing the effects of non-uniform rotation distortion in ultrasound images.

BACKGROUND

[0002] Ultrasound devices insertable into patients have proven diagnostic capabilities for a variety of diseases and disorders. For example, intravascular ultrasound ("IVUS") imaging systems have been used as an imaging modality for diagnosing blocked blood vessels and providing information to aid medical practitioners in selecting and placing stents and other devices to restore or increase blood flow. IVUS imaging systems have been used to diagnose atheromatous plaque build-up at particular locations within blood vessels. IVUS imaging systems can be used to determine the existence of an intravascular obstruction or stenosis, as well as the nature and degree of the obstruction or stenosis. IVUS imaging systems can be used to visualize segments of a vascular system that may be difficult to visualize using other intravascular imaging techniques, such as angiography, due to, for example, movement (e.g., a beating heart) or obstruction by one or more structures (e.g., one or more blood vessels not desired to be imaged). IVUS imaging systems can be used to monitor or assess ongoing intravascular treatments, such as angiography and stent placement in real (or almost real) time. Moreover, IVUS imaging systems can be used to monitor one or more heart chambers.

[0003] IVUS imaging systems have been developed to provide a diagnostic tool for visualizing a variety of diseases or disorders. An IVUS imaging system can include a control module (with a pulse generator, an image processor, and a monitor), a catheter, and one or more transducers disposed in the catheter. The transducer-containing catheter can be positioned in a lumen or cavity within, or in proximity to, a region to be imaged, such as a blood vessel wall or patient tissue in proximity to a blood vessel wall. The pulse generator in the control module generates electrical pulses that are delivered to the one or more transducers and transformed to acoustic pulses that are transmitted through patient tissue. Reflected pulses of the transmitted acoustic pulses are absorbed by the one or more transducers and transformed to electric pulses. The transformed electric pulses are delivered to the image processor and converted to an image displayable on the monitor. In many imaging systems the transducer rotates in order to image the entire vessel. Non-uniform rotation of the transducer may distort the images.

[0004] U.S. Patent No 6,267,727 discloses methods and apparatus for non-uniform rotation distortion detection for enhanced intravascular ultrasound imaging. In embodiments, a solution for addressing the problem of non-uniform rotation distortion in intravascular ultrasound imaging in systems which use mechanical scanning may be achieved. Correlation of received signals in an image vector from reverberating ultrasound in a bubbly liquid-flushed catheter may be utilized to determine non-uniform rotation of the transducer within the catheter. Alternatively, correlation of imaging vectors within a blood speckle region given a particular beamwidth of ultrasound energy from a transducer may be utilized to determine non-uniform rotation of the transducer.

[0005] U.S. Patent Application Publication No. 2007/0106155 discloses a system and method allegedly significantly reducing or substantially eliminating angular geometric distortions in devices designed for imaging and/or inspection of an interior portion or surface of a cavity. A series of processing steps or methods may be employed to eliminate Non-Uniform Rotational Distortion (NURD) in such devices, for example, unidirectional and bi-directional intravascular ultrasonic (IVUS) imaging systems. The system may include a processor and an electronic module which control operation of a transducer assembly provided at a distal end of a catheter assembly. The system invokes a first processing step or method to collect and store raw angle and line data, as well as one or more of second and third processing steps or methods which adjust for NURD experienced during backlash of a bi-directional imaging system and a fourth processing step or method which performs a line-to-line correlation function.

BRIEF SUMMARY

[0006] One embodiment is a method for generating an ultrasound image. The method including receiving an image frame comprising consecutive ultrasound scan lines obtained using a rotating ultrasound imaging arrangement and determining at least a first cross-correlation value and a second cross-correlation value for each of a plurality of the scan lines. For each individual scan line of the plurality of scan lines, the first cross-correlation value comprises a cross-correlation coefficient between a first subframe comprising a plurality of consecutive scan lines including the individual scan line and a second subframe comprising a plurality of scan lines shifted from the first subframe by a first integer value. The second correlation value comprising a cross-correlation coefficient between the first subframe and a third subframe comprising a plurality of scan lines shifted from the first subframe by a second integer value that is different

from the first integer value. The method further includes evaluating, individually for multiple scan lines of the plurality of scan lines, whether the scan line being evaluated exhibits non-uniform rotation distortion using at least one of the first and second correlation values for the scan line being evaluated. A correction for non-uniform rotation distortion is applied using at least one of the first and second correlation values for at least one of the plurality of scan lines. An ultrasound image is generated using at least the plurality of scan lines with the applied correction and the ultrasound image is displayed.

[0007] Another embodiment is a computer-readable medium having processor-executable instructions for generating an ultrasound image. The processor-executable instructions when installed onto a computing device enable the device to perform actions including receiving imaging data comprising consecutive ultrasound scan lines obtained using rotating ultrasound imaging arrangement; determining at least a first cross-correlation value and a second cross-correlation value for each of a plurality of the scan lines, wherein, for each individual scan line of the plurality of scan lines, the first cross-correlation value comprising a cross-correlation coefficient between a first subframe comprising a plurality of consecutive scan lines including the individual scan line and a second subframe comprising a plurality of scan lines shifted from the first subframe by a first integer value, the second correlation value comprising a cross-correlation coefficient between the first subframe and a third subframe comprising a plurality of scan lines shifted from the first subframe by a second integer value that is different from the first integer value; evaluating, individually for multiple scan lines of the plurality of scan lines, whether the scan line being evaluated exhibits non-uniform rotation distortion using at least one of the first and second correlation values for the scan line being evaluated; applying a correction for non-uniform rotation distortion using at least one of the first and second correlation values for at least one of the plurality of scan lines; generating an ultrasound image using at least the plurality of scan lines with the applied correction; and displaying the ultrasound image.

[0008] Yet another embodiment is a system for generating ultrasound images. The system includes a catheter and an ultrasound imaging core insertable into the catheter. The ultrasound imaging core includes at least one transducer and is configured and arranged for rotation of at least a portion of the ultrasound imaging core to provide a plurality of radial scan lines. The system also includes a processor that is coupleable to the ultrasound imaging core and is capable of executing processor-readable instructions that enable actions, including: receiving the plurality of scan lines obtained using the ultrasound imaging core; determining at least a first cross-correlation value and a second cross-correlation value for each of a plurality of the scan lines, wherein, for each individual scan line of the plurality of scan lines, the first cross-correlation value comprising a cross-correlation coefficient between a first subframe comprising a plurality of consecutive scan lines including the individual scan line and a second subframe comprising a plurality of scan lines shifted from the first subframe by a first integer value, the second correlation value comprising a cross-correlation coefficient between the first subframe and a third subframe comprising a plurality of scan lines shifted from the first subframe by a second integer value that is different from the first integer value; evaluating, individually for multiple scan lines of the plurality of scan lines, whether the scan line being evaluated exhibits non-uniform rotation distortion using at least one of the first and second correlation values for the scan line being evaluated; applying a correction for non-uniform rotation distortion using at least one of the first and second correlation values for at least one of the plurality of scan lines; generating an ultrasound image using at least the plurality of scan lines with the applied correction; and displaying the ultrasound image.

BRIEF DESCRIPTION OF THE DRAWINGS

[0009] Non-limiting and non-exhaustive embodiments of the present invention are described with reference to the following drawings. In the drawings, like reference numerals refer to like parts throughout the various figures unless otherwise specified.

[0010] For a better understanding of the present invention, reference will be made to the following Detailed Description, which is to be read in association with the accompanying drawings, wherein:

FIG. 1 is a schematic view of one embodiment of an ultrasound imaging system suitable for insertion into a patient, according to the invention;

FIG. 2 is a schematic side view of one embodiment of a catheter suitable for use with the ultrasound imaging system of FIG. 1, according to the invention;

FIG. 3 is a schematic longitudinal cross-sectional view of one embodiment of a distal end of the catheter of FIG. 2 with an imaging core disposed in a lumen defined in a sheath, according to the invention;

FIG. 4 is a schematic diagram illustrating spacing of scan lines;

FIG. 5 is a schematic block diagram illustrating one embodiment of a method for at least partially correcting for non-

uniform rotation distortion, according to the invention;

FIG. 6 is a graph of cross-correlation values and one embodiment of a scan line correction for a set of scan lines, according to the invention; and

FIG. 7 is a schematic block diagram illustrating one embodiment of a method for classifying the amount of correction to be applied to a set of imaging data.

DETAILED DESCRIPTION

[0011] The present invention is directed to the area of imaging systems that are insertable into a patient and methods of making and using the imaging systems. The present invention is also directed to methods and imaging systems for reducing the effects of non-uniform rotation distortion in ultrasound images.

[0012] The methods, systems, and devices described herein may be embodied in many different forms and should not be construed as limited to the embodiments set forth herein. Accordingly, the methods, systems, and devices described herein may take the form of an entirely hardware embodiment, an entirely software embodiment or an embodiment combining software and hardware aspects. The methods described herein can be performed using any type of computing device, such as a computer, that includes a processor or any combination of computing devices where each device performs at least part of the process.

[0013] Suitable computing devices typically include mass memory and typically include communication between devices. The mass memory illustrates a type of computer-readable media, namely computer storage media. Computer storage media may include volatile, nonvolatile, removable, and non-removable media implemented in any method or technology for storage of information, such as computer readable instructions, data structures, program modules, or other data. Examples of computer storage media include RAM, ROM, EEPROM, flash memory, or other memory technology, CD-ROM, digital versatile disks (DVD) or other optical storage, magnetic cassettes, magnetic tape, magnetic disk storage or other magnetic storage devices, or any other medium which can be used to store the desired information and which can be accessed by a computing device.

[0014] Methods of communication between devices or components of a system can include both wired and wireless (e.g., RF, optical, or infrared) communications methods and such methods provide another type of computer readable media; namely communication media. Communication media typically embodies computer-readable instructions, data structures, program modules, or other data in a modulated data signal such as a carrier wave, data signal, or other transport mechanism and include any information delivery media. The terms "modulated data signal," and "carrier-wave signal" includes a signal that has one or more of its characteristics set or changed in such a manner as to encode information, instructions, data, and the like, in the signal. By way of example, communication media includes wired media such as twisted pair, coaxial cable, fiber optics, wave guides, and other wired media and wireless media such as acoustic, RF, infrared, and other wireless media.

[0015] Suitable intravascular ultrasound ("IVUS") imaging systems include, but are not limited to, one or more transducers disposed on a distal end of a catheter configured and arranged for percutaneous insertion into a patient. Examples of IVUS imaging systems with catheters are found in, for example, U.S. Patents Nos. 7,246,959; 7,306,561; and 6,945,938; as well as U.S. Patent Application Publication Nos. 2006/0100522; 2006/0106320; 2006/0173350; 2006/0253028; 2007/0016054; and 2007/0038111.

[0016] Figure 1 illustrates schematically one embodiment of an IVUS imaging system 100. The IVUS imaging system 100 includes a catheter 102 that is coupleable to a control module 104. The control module 104 may include, for example, a processor 106, a pulse generator 108, a drive unit 110, and one or more displays 112. In at least some embodiments, the pulse generator 108 forms electric pulses that may be input to one or more transducers (312 in Figure 3) disposed in the catheter 102.

[0017] In at least some embodiments, mechanical energy from the drive unit 110 may be used to drive an imaging core (306 in Figure 3) disposed in the catheter 102. In at least some embodiments, electric signals transmitted from the one or more transducers (312 in Figure 3) may be input to the processor 106 for processing. In at least some embodiments, the processed electric signals from the one or more transducers (312 in Figure 3) can be displayed as one or more images on the one or more displays 112. For example, a scan converter can be used to map scan line samples (e.g., radial scan line samples, or the like) to a two-dimensional Cartesian grid to display the one or more images on the one or more displays 112.

[0018] In at least some embodiments, the processor 106 may also be used to control the functioning of one or more of the other components of the control module 104. For example, the processor 106 may be used to control at least one of the frequency or duration of the electrical pulses transmitted from the pulse generator 108, the rotation rate of the imaging core (306 in Figure 3) by the drive unit 110, the velocity or length of the pullback of the imaging core (306 in Figure 3) by the drive unit 110, or one or more properties of one or more images formed on the one or more displays 112.

[0019] Figure 2 is a schematic side view of one embodiment of the catheter 102 of the IVUS imaging system (100 in Figure 1). The catheter 102 includes an elongated member 202 and a hub 204. The elongated member 202 includes a proximal end 206 and a distal end 208. In Figure 2, the proximal end 206 of the elongated member 202 is coupled to the catheter hub 204 and the distal end 208 of the elongated member is configured and arranged for percutaneous insertion into a patient. Optionally, the catheter 102 may define at least one flush port, such as flush port 210. The flush port 210 may be defined in the hub 204. The hub 204 may be configured and arranged to couple to the control module (104 in Figure 1). In some embodiments, the elongated member 202 and the hub 204 are formed as a unitary body. In other embodiments, the elongated member 202 and the catheter hub 204 are formed separately and subsequently assembled together.

[0020] Figure 3 is a schematic perspective view of one embodiment of the distal end 208 of the elongated member 202 of the catheter 102. The elongated member 202 includes a sheath 302 with a longitudinal axis 303 and a lumen 304. An imaging core 306 is disposed in the lumen 304. The imaging core 306 includes an imaging device 308 coupled to a distal end of a driveshaft 310 that is rotatable either manually or using a computer-controlled drive mechanism. One or more transducers 312 may be mounted to the imaging device 308 and employed to transmit and receive acoustic signals. The sheath 302 may be formed from any flexible, biocompatible material suitable for insertion into a patient. Examples of suitable materials include, for example, polyethylene, polyurethane, plastic, spiral-cut stainless steel, nitinol hypotube, and the like or combinations thereof.

[0021] In a preferred embodiment (as shown in Figure 3), an array of transducers 312 are mounted to the imaging device 308. In alternate embodiments, a single transducer may be employed. Any suitable number of transducers 312 can be used. For example, there can be two, three, four, five, six, seven, eight, nine, ten, twelve, fifteen, sixteen, twenty, twenty-five, fifty, one hundred, five hundred, one thousand, or more transducers. As will be recognized, other numbers of transducers may also be used. When a plurality of transducers 312 are employed, the transducers 312 can be configured into any suitable arrangement including, for example, an annular arrangement, a rectangular arrangement, or the like.

[0022] The one or more transducers 312 may be formed from one or more known materials capable of transforming applied electrical pulses to pressure distortions on the surface of the one or more transducers 312, and vice versa. Examples of suitable materials include piezoelectric ceramic materials, piezocomposite materials, piezoelectric plastics, barium titanates, lead zirconate titanates, lead metaniobates, polyvinylidene fluorides, and the like. Other transducer technologies include composite materials, single-crystal composites, and semiconductor devices (e.g., capacitive micromachined ultrasound transducers ("cMUT"), piezoelectric micromachined ultrasound transducers ("pMUT"), or the like).

[0023] The pressure distortions on the surface of the one or more transducers 312 form acoustic pulses of a frequency based on the resonant frequencies of the one or more transducers 312. The resonant frequencies of the one or more transducers 312 may be affected by the size, shape, and material used to form the one or more transducers 312. The one or more transducers 312 may be formed in any shape suitable for positioning within the catheter 102 and for propagating acoustic pulses of a desired frequency in one or more selected directions. For example, transducers may be disc-shaped, block-shaped, rectangular-shaped, oval-shaped, and the like. The one or more transducers may be formed in the desired shape by any process including, for example, dicing, dice and fill, machining, microfabrication, and the like.

[0024] As an example, each of the one or more transducers 312 may include a layer of piezoelectric material sandwiched between a conductive acoustic lens and a conductive backing material formed from an acoustically absorbent material (e.g., an epoxy substrate with tungsten particles). During operation, the piezoelectric layer may be electrically excited by both the backing material and the acoustic lens to cause the emission of acoustic pulses.

[0025] The one or more transducers 312 can be used to form a radial cross-sectional image of a surrounding space. Thus, for example, when the one or more transducers 312 are disposed in the catheter 102 and inserted into a blood vessel of a patient, the one or more transducers 312 may be used to form an image of the walls of the blood vessel and tissue surrounding the blood vessel.

[0026] The imaging core 306 is rotated about the longitudinal axis 303 of the catheter 102. As the imaging core 306 rotates, the one or more transducers 312 emit acoustic signals in different radial directions (i.e., along different radial scan lines). For example, the one or more transducers 312 can emit acoustic signals at regular (or irregular) increments, such as 256 radial scan lines per revolution, or the like. It will be understood that other numbers of radial scan lines can be emitted per revolution, instead.

[0027] When an emitted acoustic pulse with sufficient energy encounters one or more medium boundaries, such as one or more tissue boundaries, a portion of the emitted acoustic pulse is reflected back to the emitting transducer as an echo pulse. Each echo pulse that reaches a transducer with sufficient energy to be detected is transformed to an electrical signal in the receiving transducer. The one or more transformed electrical signals are transmitted to the control module (104 in Figure 1) where the processor 106 processes the electrical-signal characteristics to form a displayable image of the imaged region based, at least in part, on a collection of information from each of the acoustic pulses transmitted and

the echo pulses received. In at least some embodiments, the rotation of the imaging core 306 is driven by the drive unit 110 disposed in the control module (104 in Figure 1). In alternate embodiments, the one or more transducers 312 are fixed in place and do not rotate. In which case, the driveshaft 310 may, instead, rotate a mirror that reflects acoustic signals to and from the fixed one or more transducers 312.

[0028] When the one or more transducers 312 are rotated about the longitudinal axis 303 of the catheter 102 emitting acoustic pulses, a plurality of images can be formed that collectively form a radial cross-sectional image (e.g., a tomographic image) of a portion of the region surrounding the one or more transducers 312, such as the walls of a blood vessel of interest and tissue surrounding the blood vessel. The radial cross-sectional image can, optionally, be displayed on one or more displays 112. The at least one of the imaging core 306 can be either manually rotated or rotated using a computer-controlled mechanism.

[0029] The imaging core 306 may also move longitudinally along the blood vessel within which the catheter 102 is inserted so that a plurality of cross-sectional images may be formed along a longitudinal length of the blood vessel. During an image procedure the one or more transducers 312 may be retracted (i.e., pulled back) along the longitudinal length of the catheter 102. The catheter 102 can include at least one telescoping section that can be retracted during pullback of the one or more transducers 312. In at least some embodiments, the drive unit 110 drives the pullback of the imaging core 306 within the catheter 102. The drive unit 110 pullback distance of the imaging core can be any suitable distance including, for example, at least 5 cm, 10 cm, 15 cm, 20 cm, 25 cm, or more. The entire catheter 102 can be retracted during an imaging procedure either with or without the imaging core 306 moving longitudinally independently of the catheter 102.

[0030] When the imaging core 306 is retracted while rotating, the images may collectively form a continuous spiral shape along a blood vessel. A stepper motor may, optionally, be used to pull back the imaging core 306. The stepper motor can pull back the imaging core 306 a short distance and stop long enough for the one or more transducers 306 to capture an image or series of images before pulling back the imaging core 306 another short distance and again capturing another image or series of images, and so on.

[0031] The quality of an image produced at different depths from the one or more transducers 312 may be affected by one or more factors including, for example, bandwidth, transducer focus, beam pattern, as well as the frequency of the acoustic pulse. The frequency of the acoustic pulse output from the one or more transducers 312 may also affect the penetration depth of the acoustic pulse output from the one or more transducers 312. In general, as the frequency of an acoustic pulse is lowered, the depth of the penetration of the acoustic pulse within patient tissue increases. In at least some embodiments, the IVUS imaging system 100 operates within a frequency range of 5 MHz to 100 MHz.

[0032] One or more conductors 314 can electrically couple the transducers 312 to the control module 104 (see e.g., Figure 1). In which case, the one or more conductors 314 may extend along a longitudinal length of the rotatable driveshaft 310.

[0033] The catheter 102 with one or more transducers 312 mounted to the distal end 208 of the imaging core 308 may be inserted percutaneously into a patient via an accessible blood vessel, such as the femoral artery, femoral vein, or jugular vein, at a site remote from the selected portion of the selected region, such as a blood vessel, to be imaged. The catheter 102 may then be advanced through the blood vessels of the patient to the selected imaging site, such as a portion of a selected blood vessel,

[0034] As indicated above, the transducer(s) or a mirror is typically rotated during operation. As the transducer(s) or mirror rotates, the transducer(s) is pulsed to emit acoustic energy. The transducer(s) then receives the reflected acoustic energy. During this reception period, the transducer(s) or mirror may be stationary or rotating. The received acoustic energy between two pulses can be referred to as a scan line. Each scan line typically includes a number of points that represent reception of the reflected acoustic energy over time and are generally correlated with depth. In at least some embodiments, the number of scan lines per revolution is at least 64, 100, 128, 200, 256, 300, 400, 500, 512, 1000, or 1028.

[0035] Ideally, the scan lines are spaced an equal distance apart. Equal spacing of the scan lines can be obtained by uniform rotation. If the rotation is non-uniform, then the spacing between the scan lines will also be non-uniform. Such non-uniformity can result in what is often referred to as non-uniform rotation distortion (NURD) and can produce distortion in the ultrasound image. Figure 4 schematically illustrates the concept of non-uniform rotation by graphing each scan line, $l_1, l_2, \dots, l_n$ versus rotational distance (x-axis). The y-axis corresponds to the sample points for each scan line. In Figure 4, scan lines l_1, l_2 , and l_3 are equally spaced apart indicating uniform rotation. In contrast, lines l_{i-1} and l_i are closer together, indicating that the rotational speed of the transducer(s) or mirror may have slowed. Lines l_i and l_{i+1} and lines l_{i+3} and l_{i+4} are further apart indicating that the rotational speed of the transducer(s) or mirror may have increased.

[0036] The scan lines and associated data can be examined and the presence of non-uniform rotation distortion can be observed and at least partially corrected. Although the correction of non-uniform rotation distortion is described herein in the context of ultrasound imaging, it will be understood that this correction can also be applied to other imaging techniques that utilize rotating imaging receivers, such as optical coherence tomography.

[0037] Figure 5 is a block diagram illustrating schematically one embodiment of a procedure for at least partially correcting non-uniform rotation distortion (NURD). The level of NURD around each scan line L in the image frame can

be calculated through cross-correlation values between image subframes. Image subframes are selected from the image frame (box 502). As an example, for each image frame $F(r,L)$ that includes L_T scan lines with each scan line containing r_T sample points, image subframes are selected with each subframe including a number Δ_L of consecutive scan lines distributed around, and including, a scan line, L , and a range $[r_1, r_2]$ of consecutive sample points from each scan line distributed around, and including, a sample point, r . It will be understood that the imaging data in the image frame can be the radio-frequency (RF) data directly from the transducer or data that has been at least partially processed (e.g., data with filtering, amplitude detection, log-compression or other non-linear mapping of amplitudes). The image frames can be averaged over consecutive acquisitions of ultrasound data.

[0038] The total number of scan lines, Δ_L , in a subframe can be two, three, four, five, six, seven, eight, nine, ten, eleven, twelve, or more. Preferably, the scan lines of the subframe are symmetrically selected about the particular scan line, L , which would result in Δ_L being an odd number (e.g., three, five, seven, nine, eleven, etc.)

[0039] The number of sample points per scan line in the range $[r_1, r_2]$ of the subframe is preferably at least one-eighth of the total number of sample points in the scan line and can be at least one-quarter, one-half, two-thirds, three-quarters, or even all of the sample points of the scan line. It will be understood that each scan line may have the same number of sample points or may have differing numbers of sample points.

[0040] In some embodiments, the level of NURD is estimated around each scan line in the image frame, therefore all scan lines in an image frame are selected for calculation. Alternatively, the level of NURD is estimated for only a portion of the scan lines (e.g., every other scan line or every third scan line), thus a subset of scan lines are selected for calculation.

[0041] The presence or absence of non-uniform rotation distortion (NURD) is then determined (box 504) for each selected scan line from the image frame. This determination includes calculating two or more cross-correlation values between nearby subframes for each selected line. In at least some embodiments, the subframe cross-correlation values are calculated between the subframe that includes the selected scan line and another subframe that may or may not includes that line.

[0042] Each subframe cross-correlation value is calculated between a subframe and another subframe that corresponds to the original subframe shifted by an integer number, δ_L , of scan lines. For a particular subframe, each calculated cross-correlation value is for a different value of δ_L . The integer number δ_L can be any suitable integer value such as one, two, three, four, five, six, seven, eight, or more and can be positive or negative.

[0043] One example of a cross-correlation value $C(L; \delta_L)$ is given by the following equation:

$$C(L; \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L'))$$

where In this instance, the cross-correlation values have been normalized. Alternatively, i) the cross-correlation values are not normalized, ii) the cross-correlation values are calculated without subtracting the mean values (e.g., $\bar{F}(L)$ and $\bar{F}(L + \delta_L)$), or iii) a combination of i) and ii).

[0044] These cross-correlation values are functions of both the lateral resolution of the imaging system and the rotation distortion. To separate the rotation distortion effects on the cross-correlation values from that of image revolution, the relative cross-correlation values, $CR(L; \delta_L)$, can be calculated by normalizing $C(L; \delta_L)$ with its average over the whole or a nearby portion of the image frame,

$$CR(L; \delta_L) = \frac{(2D+1) \cdot C(L; \delta_L)}{\sum_{L' = -D}^D C(L + L'; \delta_L)}$$

where $2D+1 < L_T$, the total number of scan lines in the frame or the selected portion of the frame.

[0045] As an example, the cross-correlation values $CR(L; 1)$ and $CR(L; 3)$ for each selected line can be calculated. Individual scan lines within an image frame can be identified as demonstrating non-uniform rotation distortion based on a selected threshold condition of the subframe cross-correlation values. As an example, a threshold condition could be

that non-uniform rotation distortion is indicated if one or more, or if a specific one, of the subframe cross-correlation values are outside of a threshold range. For example, it will be expected that image lines without non-uniform rotation distortion will have $CR(L;1) \cong 1$. Image lines with $CR(L;1)$ outside a threshold range around 1 will indicate the likely presence of non-uniform rotation distortion. For other cross-correlation values (e.g., $CR(L;3)$) the expected value will likely not be 1, but could be another number (for example, an average or median value for the imaging data). Any suitable threshold range and threshold values can be used and the threshold range may be asymmetrical or asymmetrical about the value of expected value (e.g., 1 for $CR(L;1)$). For example, the threshold range may be from $1-t$ to $1+t$ where t is any suitable value less than 1. The value t may be at least 0.05, 0.1, 0.15, 0.2, 0.25, or more.

[0046] Figure 6 is a graph of $CR(L;1)$ 602 and $CR(L;3)$ 604 for one set of data. Also illustrated are threshold values 606. Values of $CR(L;1)$ outside this range may be considered to indicate non-uniform rotation distortion. Alternative threshold values 606a are also illustrated. In some embodiments, one cross-correlation value (e.g. $CR(L;1)$) is used to determine the likelihood of non-uniform rotation distortion and a second cross-correlation value (e.g., $CR(L;3)$) is used to confirm that determination.

[0047] In at least some embodiments, only portions of the image frame that are determined to likely demonstrate non-uniform rotation distortion will be corrected. In other embodiments, those portions, as well as adjacent portions of the data, will be corrected. In yet other embodiments, all of the image frame will be corrected.

[0048] In some embodiments, the portion of the image frame that will be corrected can depend on the relative amount of non-uniform rotation distortion (NURD) identified within the image frame. Figure 7 illustrates in a block diagram one embodiment of a procedure for determining which portions of the image frame will be corrected. A NURD classifier 702 evaluates the cross-correlation values for the image frames. If there is little or no NURD present in the image frame, then no NURD correction is applied (box 704). If it is determined that NURD is likely present in a limited region or regions of frame, the NURD correction is applied to those regions (and optionally to adjacent regions) (box 706). If there is extensive NURD in the image frame, then NURD correction is applied to the entire set of frame (box 708). It will be understood that the thresholds between the three conditions (e.g., the threshold between when no NURD correction is applied and when NURD correction is applied regionally, or the threshold between when regional NURD correction is applied and when global NURD correction is applied) can be selected to be any suitable values and may depend on the imaging application or setting or may be set by a user.

[0049] Returning to Figure 5, a correction for one or more regions or, in some embodiments, for the entire image frame can be determined (box 506). Figure 6 illustrates a scan line correction 608 that is applied to only some scan lines. A correction can be calculated for each scan line to be corrected. The correction may be a line spacing correction that interpolates a corrected scan line from lines adjacent the scan line to be corrected. Alternatively, the correction may include a determination of the actual coordinates of one or more of the scan lines.

[0050] One example of a scan line correction, $s(L)$, for a scan line, L , has the following form:

$$\begin{aligned} s(L) &= k/CR(L;1) && \text{when } CR(L;1) \leq 1; \\ s(L) &= k/2 && \text{when } CR(L;1) > 1 \text{ and } C_s \leq 0; \\ s(L) &= k/2/(1+C_s) && \text{when } CR(L;1) > 1 \text{ and } C_s > 0, \text{ where} \\ &&& k \text{ is a scaling constant;} \end{aligned}$$

$C_s = (C_{3\text{thresh}} - CR(L;3))/(CR(L;3) - CR(L;1))$ where $C_{3\text{thresh}}$ is a threshold level selected for $CR(L;3)$. For example, $C_{3\text{thresh}}$ can be 1.10, 1.05, 1.00, or 0.95.

[0051] The scaling constant k can be one or may be selected for normalization with respect to the entire set of imaging data or may be selected for normalization with respect to only a portion of the imaging data including the scan line, L . In some embodiments, the scaling constant, k , may be different for each scan line and vary based on the degree to which one or more of the cross-correlation values for that scan line are outside of the threshold range.

[0052] For a smother frame to frame transition, $s(L)$ can be smoothed over consecutive image frames. For example, for frame n with scan line correction $s_n(L)$, the smoothed correction for frame n becomes,

$$s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha) s_n(L), \text{ where } \alpha < 1 \text{ is a weighting constant,}$$

[0053] In a more general form,

$$s'_n(L) = \sum_{n'=-\Delta_1}^{\Delta_2} \alpha_{n'} s_{n+n'}(L), \text{ where } \sum_{n=-\Delta_1}^{\Delta_2} \alpha_n = 1 \text{ and } \Delta_1 \text{ and } \Delta_2 \text{ are integers and can be the same or different.}$$

[0054] In another embodiment, a modified scan line correction, $s_T(L)$, can be determined for all or some of the scan lines. The modified scan line correction can include the scan line correction, $s(L)$, and a global scan line correction, $s_g(L)$, that are combined in a weighed arrangement.

[0055] As an example,

$s_T(L) = \beta s(L) + (1-\beta)s_g(L)$, where $s(L)$ is calculated as described above;

$S_g(L) = k_g/C(L;1)$ when $G(L;1) \leq 1$;

$s_g(L) = k_g/2$ when $C(L;1) > 1$ and $C_s \leq 0$;

$s_g(L) = k_g/2/(1+C_s)$ when $C(L;1) > 1$ and $C_s > 0$, where k_g is a scaling constant; and

β is a weighting constant that is between 0 and 1.

[0056] The scan line correction $s(L)$ (or $s'(L)$ or $s_T(L)$) can be made to each scan line that is to be corrected (box 508) to give a corrected scan lines/frames (box 510). In some embodiments, the scan line correction, $s(L)$ (or $s'(L)$ or $s_T(L)$), can be applied to each scan line for which NURD is likely determined. In other embodiments, the scan line correction, $s(L)$ (or $s'(L)$ or $s_T(L)$), is applied to every scan line.

[0057] The corrected scan lines can then be processed using any known processing method to yield one or more images (e.g., ultrasound images). The corrections to the scan lines should improve the quality of the images.

[0058] It will be understood that each block of the block diagram illustrations, and combinations of blocks in the block diagram illustrations, as well as any portion of the systems and methods disclosed herein, can be implemented by computer program instructions. These program instructions may be provided to a processor to produce a machine, such that the instructions, which execute on the processor, create means for implementing the actions specified in the block diagram block or blocks or described for the systems and methods disclosed herein. The computer program instructions may be executed by a processor to cause a series of operational steps to be performed by the processor to produce a computer implemented process. The computer program instructions may also cause at least some of the operational steps to be performed in parallel. Moreover, some of the steps may also be performed across more than one processor, such as might arise in a multi-processor computer system. In addition, one or more processes may also be performed concurrently with other processes, or even in a different sequence than illustrated without departing from the scope or spirit of the invention.

[0059] The computer program instructions can be stored on any suitable computer-readable medium including, but not limited to, RAM, ROM, EEPROM, flash memory or other memory technology, CD-ROM, digital versatile disks (DVD) or other optical storage, magnetic cassettes, magnetic tape, magnetic disk storage or other magnetic storage devices, or any other medium which can be used to store the desired information and which can be accessed by a computing device.

[0060] The above specification, examples and data provide a description of the manufacture and use of the composition of the invention. Many embodiments of the invention can be made without departing from the scope of the invention defined in the claims.

Claims

1. A method for generating an ultrasound image, the method comprising:

receiving an image frame comprising consecutive ultrasound scan lines ($l_1, l_2, \dots, l_n$) obtained using a rotating ultrasound imaging arrangement;

determining at least a first cross-correlation value and a second cross-correlation value for each of a plurality of the scan lines ($l_1, l_2, \dots, l_n$);

evaluating, individually for multiple scan lines of the plurality of scan lines ($l_1, l_2, \dots, l_n$), whether the scan line being evaluated exhibits non-uniform rotation distortion using at least one of the first and second correlation values for the scan line being evaluated;

applying a correction for non-uniform rotation distortion using at least one of the first and second correlation values for at least one of the plurality of scan lines ($l_1, l_2, \dots, l_n$);

generating an ultrasound image using at least the plurality of scan lines ($l_1, l_2, \dots, l_n$) with the applied correction; and displaying the ultrasound image,

characterized in that

for each individual scan line of the plurality of scan lines ($l_1, l_2, \dots, l_n$), the first cross-correlation value comprising a cross-correlation coefficient between a first subframe comprising a plurality of consecutive scan lines including the individual scan line and a second subframe comprising a plurality of scan lines shifted from the first subframe by a first integer value, the second correlation value comprising a cross-correlation coefficient between the first subframe and a third subframe comprising a plurality of scan lines shifted from the first subframe by a second integer value that is different from the first integer value.

2. The method of claim 1, wherein the first cross-correlation value and the second cross correlation value are normalized.
3. The method of claim 1, wherein the first integer value is one, and optionally the second integer value is two.

4. The method of claim 1, wherein, for the image frame $F(r,L)$ where L is a scan line in the imaging frame and r is a sample point of the scan line, the first subframe includes Δ_L scan lines around a particular scan line L and sample points in the range of $[r_1, r_2]$ and the first cross-correlation value is $C(L, \delta_L)$, wherein δ_L is the first integer value and to be used for determining the first cross-correlation value, and

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wherein } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L')).$$

5. The method of claim 1, wherein, for the image frame $F(r,L)$ where L is a scan line in the imaging frame and r is a sample point of the scan line, the first subframe includes Δ_L scan lines around a particular scan line L and sample points in the range of $[r_1, r_2]$ and the first cross-correlation value is $CR(L, \delta_L)$ wherein δ_L is the first integer value and to be used for determining the first cross-correlation value, and $CR(L, \delta_L)$ is a normalized multiple line average of $C(L, \delta_L)$ around the line L , wherein

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wherein } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L')).$$

6. The method of claim 5, wherein the first cross-correlation value is $CR(L, 1)$ and the second cross-correlation value is $CR(L, 3)$, wherein optionally the correction for non-uniform rotation for a scan line L is:

$$\begin{aligned} s(L) &= k/CR(L, 1) && \text{when } CR(L, 1) \leq 1; \\ s(L) &= k/2 && \text{when } CR(L, 1) > 1 \text{ and } C_s \leq 0; \\ s(L) &= k/2/(1 + C_s) && \text{when } CR(L, 1) > 1 \text{ and } C_s > 0; \end{aligned}$$

wherein k is a scaling constant; and

$C_s = (C_{3\text{thresh}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L, 3)$,

or

wherein the correction for non-uniform rotation for scan line L in an n -th image frame is $s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha)s_n(L)$, where $\alpha < 1$, is a weighting constant and an unsmoothed scan line correction $s_n(L)$, defined in the n -th image frame, is

$$\begin{aligned} s_n(L) &= k/CR(L,1) && \text{when } CR(L,1) \leq 1; \\ s_n(L) &= k/2 && \text{when } CR(L,1) > 1 \text{ and } C_s \leq 0; \\ s_n(L) &= k/2/(1+C_s) && \text{when } CR(L,1) > 1 \text{ and } C_s > 0; \end{aligned}$$

wherein k is a scaling constant; and

$C_s = (C_{3\text{thresh}} - CR(L,3))/(CR(L,3) - CR(L,1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L,3)$,
or

wherein the correction for non-uniform rotation for scan line L in an n-th image frame is $s'_n(L) = \sum_{n'=-\Delta_1}^{\Delta_2} \alpha_{n'} s_{n+n'}(L)$,

wherein $\sum_{n=\Delta_1}^{\Delta_2} \alpha_n = 1$ and Δ_1 and Δ_2 are integers and can be the same or different, and an unsmoothed scan line correction $s_n(L)$, defined in the n-th image frame, is

$$\begin{aligned} s_n(L) &= k/CR(L,1) && \text{when } CR(L,1) \leq 1; \\ s_n(L) &= k/2 && \text{when } CR(L,1) > 1 \text{ and } C_s \leq 0; \\ s_n(L) &= k/2/(1+C_s) && \text{when } CR(L,1) > 1 \text{ and } C_s > 0; \end{aligned}$$

wherein k is a scaling constant; and

$C_s = (C_{3\text{thresh}} - CR(L,3))/(CR(L,3) - CR(L,1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L,3)$,
or

wherein the correction for non-uniform rotation for scan line 1 is:

$$s_T(L) = \beta s(L) + (1-\beta)s_g(L),$$

wherein

$$\begin{aligned} s(L) &= k/CR(L,1) && \text{when } CR(L,1) \leq 1; \\ s(L) &= k/2 && \text{when } CR(L,1) > 1 \text{ and } C_s \leq 0; \\ s(L) &= k/2/(1+C_s) && \text{when } CR(L,1) > 1 \text{ and } C_s > 0; \end{aligned}$$

k is a scaling constant;

$C_s = (C_{3\text{thresh}} - CR(L,3))/(CR(L,3) - CR(L,1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L,3)$;

$$\begin{aligned} s_g(L) &= k_g/C(L,1) && \text{when } C(L,1) \leq 1; \\ s_g(L) &= k_g/2 && \text{when } C(L,1) > 1 \text{ and } C_s \leq 0; \\ s_g(L) &= k_g/2/(1+C_s) && \text{when } C(L,1) > 1 \text{ and } C_s > 0; \end{aligned}$$

k_g is a scaling constant, e.g. 1; and

β is a weighting constant that is between 0 and 1.

7. A computer-readable medium having processor-executable instructions for generating an ultrasound image, the processor-executable instructions when installed onto a computing device enable the device to perform actions, comprising:

receiving imaging data comprises consecutive ultrasound scan lines ($l_1, l_2, \dots, l_n$) obtained using a rotating ultrasound imaging arrangement;

determining at least a first cross-correlation value and a second cross-correlation value for each of a plurality of the scan lines ($l_1, l_2, \dots, l_n$);

evaluating, individually for multiple scan lines of the plurality of scan lines ($l_1, l_2, \dots, l_n$), whether the scan line being evaluated exhibits non-uniform rotation distortion using at least one of the first and second correlation values for the scan line being evaluated;

applying a correction for non-uniform rotation distortion using at least one of the first and second correlation values for at least one of the plurality of scan lines ($l_1, l_2, \dots, l_n$);
generating an ultrasound image using at least the plurality of scan lines with the applied correction; and
displaying the ultrasound image,

characterized in that

for each individual scan line of the plurality of scan lines ($l_1, l_2, \dots, l_n$), the first cross-correlation value comprising a cross-correlation coefficient between a first subframe comprising a plurality of consecutive scan lines including the individual scan line and a second subframe comprising a plurality of scan lines shifted from the first subframe by a first integer value, the second correlation value comprising a cross-correlation coefficient between the first subframe and a third subframe comprising a plurality of scan lines shifted from the first subframe by a second integer value that is different from the first integer value.

8. The computer-readable medium of claim 7 wherein, for the image frame $F(r, L)$ where L is a scan line in the imaging frame and r is a sample point of the scan line, the first subframe includes Δ_L scan lines around a particular scan line L and sample points in the range of $[r_1, r_2]$ and the first cross-correlation value is $CR(L, \delta_L)$, wherein δ_L is the first integer value and to be used for determining the first cross-correlation value, and $CR(L, \delta_L)$ is a normalized multiple line average of $C(L, \delta_L)$ around the line L , wherein

$$C(L, \delta_L) = \frac{\sum_{L'=(\Delta_L-1)/2}^{(\Delta_L+1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L') - \bar{F}(L)) \cdot (F(r, L+\delta_L+L') - \bar{F}(L+\delta_L))}{\sqrt{\sum_{L'=(\Delta_L-1)/2}^{(\Delta_L+1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L'=(\Delta_L-1)/2}^{(\Delta_L+1)/2} \sum_{r=r_1}^{r_2} (F(r, L+\delta_L+L') - \bar{F}(L+\delta_L))^2}}$$

$$\text{wherein } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L'=(\Delta_L-1)/2}^{(\Delta_L+1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L')).$$

9. The computer-readable medium of claim 8, wherein the first cross-correlation value is $CR(L, 1)$ and the second cross-correlation value is $CR(L, 3)$.

10. The computer-readable medium of claim 9, wherein the correction for non-uniform rotation for a scan line l is:

$$\begin{aligned} s(L) &= k/CR(L, 1) && \text{when } CR(L, 1) \leq 1; \\ s(L) &= k/2 && \text{when } CR(L, 1) > 1 \text{ and } C_s \leq 0; \\ s(L) &= k/2/(1 + C_s) && \text{when } CR(L, 1) > 1 \text{ and } C_s > 0; \end{aligned}$$

wherein k is a scaling constant; and

$C_s = (C_{3\text{thresh}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L, 3)$.

11. The computer-readable medium of claim 9, wherein the correction for non-uniform rotation for scan line L in an n -th image frame is $s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha)s_n(L)$, wherein $\alpha < 1$ is a weighting constant and an unsmoothed scan line correction $s_n(L)$, defined in the n -th image frame, is

$$\begin{aligned} s_n(L) &= k/CR(L, 1) && \text{when } CR(L, 1) \leq 1; \\ s_n(L) &= k/2 && \text{when } CR(L, 1) > 1 \text{ and } C_s \leq 0; \\ s_n(L) &= k/2/(1 + C_s) && \text{when } CR(L, 1) > 1 \text{ and } C_s > 0; \end{aligned}$$

wherein k is a scaling constant; and

$C_s = (C_{3\text{thresh}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L, 3)$.

12. The computer-readable medium of claim 9, wherein the correction for non-uniform rotation for scan line L in an n -

th image frame is $s'_n(L) = \sum_{n'=\Delta_1}^{\Delta_2} \alpha_{n'} s_{n+n'}(L)$, wherein $\sum_{n=\Delta_1}^{\Delta_2} \alpha_n = 1$ and Δ_1 and Δ_2 are integers and can be the same or different, and an unsmoothed scan line correction $s_n(L)$, defined in the n-th image frame, is

$$\begin{aligned} s_n(L) &= k/CR(L,1) && \text{when } CR(L,1) \leq 1; \\ s_n(L) &= k/2 && \text{when } CR(L,1) > 1 \text{ and } C_s \leq 0; \\ s_n(L) &= k/2/(1+C_s) && \text{when } CR(L,1) > 1 \text{ and } C_s > 0; \end{aligned}$$

wherein k is a scaling constant; and

$C_s = (C_{3\text{thresh}} - CR(L,3))/(CR(L,3) - CR(L,1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L,3)$.

13. The computer-readable medium of claim 9, wherein the correction for non-uniform rotation for scan line l is:

$$s_T(L) = \beta s(L) + (1-\beta)s_g(L),$$

wherein,

$$\begin{aligned} s(L) &= k/CR(L,1) && \text{when } CR(L,1) \leq 1; \\ s(L) &= k/2 && \text{when } CR(L,1) > 1 \text{ and } C_s \leq 0; \\ s(L) &= k/2/(1+C_s) && \text{when } CR(L,1) > 1 \text{ and } C_s > 0, \end{aligned}$$

k is a scaling constant;

$C_s = (C_{3\text{thresh}} - CR(L,3))/(CR(L,3) - CR(L,1))$ wherein $C_{3\text{thresh}}$ is a threshold level selected for $CR(L,3)$;

$$\begin{aligned} s_g(L) &= k_g/C(L;1) && \text{when } C(L;1) \leq 1; \\ s_g(L) &= k_g/2 && \text{when } C(L;1) > 1 \text{ and } C_s \leq 0; \\ s_g(L) &= k_g/2/(1+C_s) && \text{when } C(L;1) > 1 \text{ and } C_s > 0; \end{aligned}$$

k_g is a scaling constant, e.g. 1; and

β is a weighting constant that is between 0 and 1.

14. A system (100) for generating ultrasound images, comprising:

a catheter (102);

an ultrasound imaging core (306) insertable into the catheter (102), the ultrasound imaging core (306) comprising at least one transducer (312) and configured and arranged for rotation of at least a portion of the ultrasound imaging core (306) to provide a plurality of radial scan lines ($l_1, l_2, \dots, l_n$);

a processor (106), coupleable to the ultrasound imaging core (306), for executing processor-readable instructions that enable actions, including:

receiving the plurality of scan lines ($l_1, l_2, \dots, l_n$) obtained using the ultrasound imaging core (306);

determining at least a first cross-correlation value and a second cross-correlation value for each of a plurality of the scan lines ($l_1, l_2, \dots, l_n$);

evaluating, individually for multiple scan lines of the plurality of scan lines ($l_1, l_2, \dots, l_n$), whether the scan line being evaluated exhibits non-uniform rotation distortion using at least one of the first and second correlation values for the scan line being evaluated;

applying a correction for non-uniform rotation distortion using at least one of the first and second correlation values for at least one of the plurality of scan lines ($l_1, l_2, \dots, l_n$);

generating an ultrasound image using at least the plurality of scan lines ($l_1, l_2, \dots, l_n$) with the applied correction; and

displaying the ultrasound image,

characterized in that

for each individual scan line of the plurality of scan lines ($l_1, l_2, \dots, l_n$), the first cross-correlation value

comprising a cross-correlation coefficient between a first subframe comprising a plurality of consecutive scan lines including the individual scan line and a second subframe comprising a plurality of scan lines shifted from the first subframe by a first integer value, the second correlation value comprising a cross-correlation coefficient between the first subframe and a third subframe comprising a plurality of scan lines (l₁, l₂, ..., l_n) shifted from the first subframe by a second integer value that is different from the first integer value.

15. The system of claim 14, wherein, for the image frame F(r,L) where L is a scan line in the imaging frame and r is a sample point of the scan line, the first subframe includes Δ_L scan lines around a particular scan line L and sample points in the range of [r₁, r₂] and the first cross-correlation value is CR(L, δ_L), wherein δ_L is the first integer value and to be used for determining the first cross-correlation value, and CR(L, δ_L) is a normalized multiple line average of C(L, δ_L) around the line L, wherein

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wherein } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L'))$$

Patentansprüche

1. Verfahren zum Erzeugen eines Ultraschallbilds, wobei das Verfahren aufweist:

Empfangen eines Bildrahmens, der aufeinanderfolgende Ultraschallabtastzeilen (l₁, l₂, ..., l_n) aufweist, die mittels einer rotierenden Ultraschallabbildungsanordnung erhalten werden;

Bestimmen mindestens eines ersten Kreuzkorrelationswerts und eines zweiten Kreuzkorrelationswerts für jede einer Vielzahl der Abtastzeilen (l₁, l₂, ..., l_n);

einzelnes Beurteilen für mehrere Abtastzeilen der Vielzahl der Abtastzeilen (l₁, l₂, ..., l_n), ob die Abtastzeile, die beurteilt wird, eine ungleichmäßige Rotationsverzerrung aufweist, unter Verwendung von mindestens einem der ersten und zweiten Korrelationswerte für die Abtastzeile, die beurteilt wird;

Anwenden einer Korrektur für die ungleichmäßige Rotationsverzerrung unter Verwendung von mindestens einem der ersten und zweiten Korrelationswerte für mindestens eine der Vielzahl der Abtastzeilen (l₁, l₂, ..., l_n);

Erzeugen eines Ultraschallbilds unter Verwendung mindestens der Vielzahl der Abtastzeilen (l₁, l₂, ..., l_n) mit der angewendeten Korrektur; und

Anzeigen des Ultraschallbilds,

dadurch gekennzeichnet, dass

für jede einzelne Abtastzeile der Vielzahl der Abtastzeilen (l₁, l₂, ..., l_n), der erste Kreuzkorrelationswert einen Kreuzkorrelationskoeffizienten zwischen einem ersten Teilrahmen, der eine Vielzahl von aufeinanderfolgenden Abtastzeilen einschließlich der einzelnen Abtastzeile aufweist, und einem zweiten Teilrahmen aufweist, der eine Vielzahl von Abtastzeilen aufweist, die vom ersten Teilrahmen um einen ersten ganzzahligen Wert verschoben sind, und der zweite Korrelationswert einen Kreuzkorrelationskoeffizienten zwischen dem ersten Teilrahmen und einem dritten Teilrahmen aufweist, der eine Vielzahl von Abtastzeilen aufweist, die vom ersten Teilrahmen um einen zweiten ganzzahligen Wert verschoben sind, der sich vom ersten ganzzahligen Wert unterscheidet.

2. Verfahren nach Anspruch 1, wobei der erste Kreuzkorrelationswert und der zweite Kreuzkorrelationswert normiert werden.

3. Verfahren nach Anspruch 1, wobei der erste ganzzahlige Wert eins ist, und optional der zweite ganzzahlige Wert zwei ist.

4. Verfahren nach Anspruch 1,

wobei für den Bildrahmen $F(r, L)$, wobei L eine Abtastzeile im Abbildungsrahmen ist und r ein Abtastpunkt der Abtastzeile ist, der erste Teilrahmen Δ_L Abtastzeilen um eine bestimmte Abtastzeile L und Abtastpunkte im Bereich von $[r_1, r_2]$ umfasst und der erste Kreuzkorrelationswert $C(L, \delta_L)$ ist, wobei δ_L der erste ganzzahlige Wert ist und zum Bestimmen des ersten Kreuzkorrelationswerts verwendet werden soll, und

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wobei } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L')) .$$

5. Verfahren nach Anspruch 1,

wobei für den Bildrahmen $F(r, L)$, wobei L eine Abtastzeile im Abbildungsrahmen ist und r ein Abtastpunkt der Abtastzeile ist, der erste Teilrahmen Δ_L Abtastzeilen um eine bestimmte Abtastzeile L und Abtastpunkte im Bereich von $[r_1, r_2]$ umfasst und der erste Kreuzkorrelationswert $CR(L, \delta_L)$ ist, wobei δ_L der erste ganzzahlige Wert ist und zum Bestimmen des ersten Kreuzkorrelationswerts verwendet werden soll, und $CR(L, \delta_L)$ ein normierter Mittelwert von mehreren Zeilen von $C(L, \delta_L)$ um die Zeile L ist, wobei

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wobei } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L')) .$$

6. Verfahren nach Anspruch 5, wobei der erste Kreuzkorrelationswert $CR(L, 1)$ ist und der zweite Kreuzkorrelationswert $CR(L, 3)$ ist,

wobei optional die Korrektur für eine ungleichmäßige Rotation für eine Abtastzeile 1 ist:

$$\begin{aligned} s(L) &= k/CR(L, 1) && \text{wenn } CR(L, 1) \leq 1; \\ s(L) &= k/2 && \text{wenn } CR(L, 1) > 1 \text{ und } C_s \leq 0; \\ s(L) &= k/2/(1 + C_s) && \text{wenn } CR(L, 1) > 1 \text{ und } C_s > 0; \end{aligned}$$

wobei k eine Skalierungskonstante ist; und

$C_s = (C_{3_{\text{thresh}}} \cdot CR(L, 3)) / (CR(L, 3) - CR(L, 1))$, wobei $C_{3_{\text{thresh}}}$ ein für $CR(L, 3)$ gewählter Schwellenwertpegel ist, oder

wobei die Korrektur für eine ungleichmäßige Rotation für die Abtastzeile L in einem n -ten Bildrahmen $s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha) s_n(L)$ ist, wobei $\alpha < 1$ eine Gewichtungskonstante ist und eine nicht geglättete Abtastzeilenkorrektur $s_n(L)$, die im n -ten Bildrahmen definiert ist, ist

$$\begin{aligned} s_n(L) &= k/CR(L, 1) && \text{wenn } CR(L, 1) \leq 1; \\ s_n(L) &= k/2 && \text{wenn } CR(L, 1) > 1 \text{ und } C_s \leq 0; \\ s_n(L) &= k/2/(1 + C_s) && \text{wenn } CR(L, 1) > 1 \text{ und } C_s > 0; \end{aligned}$$

wobei k eine Skalierungskonstante ist; und

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$, wobei $C_{3_{\text{thresh}}}$ ein für CR(L,3) gewählter Schwellenwertpegel ist, oder

wobei die Korrektur für eine ungleichmäßige Rotation für die Abtastzeile L in einem n-ten Bildrahmen

$s'_n(L) = \sum_{n'=-\Delta_1}^{\Delta_2} \alpha_{n'} s_{n+n'}(L)$ ist, wobei $\sum_{n=\Delta_1}^{\Delta_2} \alpha_n = 1$ und Δ_1 und Δ_2 ganze Zahlen sind und dieselben sein oder sich unterscheiden können, und eine nicht geglättete Abtastzeilenkorrektur $s_n(L)$, die im n-ten Bildrahmen definiert ist, ist

$$\begin{aligned} s_n(L) &= k/CR(L,1) && \text{wenn } CR(L,1) \leq 1; \\ s_n(L) &= k/2 && \text{wenn } CR(L,1) > 1 \text{ und } C_s \leq 0; \\ s_n(L) &= k/2/(1 + C_s) && \text{wenn } CR(L,1) > 1 \text{ und } C_s > 0; \end{aligned}$$

wobei k eine Skalierungskonstante ist; und

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$, wobei $C_{3_{\text{thresh}}}$ ein für CR(L,3) gewählter Schwellenwertpegel ist, oder

wobei die Korrektur für eine ungleichmäßige Rotation für die Abtastzeile L ist:

$$s_T(L) = \beta s(L) + (1-\beta)s_g(L),$$

wobei

$$\begin{aligned} s(L) &= k/CR(L,1) && \text{wenn } CR(L,1) \leq 1; \\ s(L) &= k/2 && \text{wenn } CR(L,1) > 1 \text{ und } C_s \leq 0; \\ s(L) &= k/2/(1 + C_s) && \text{wenn } CR(L,1) > 1 \text{ und } C_s > 0; \end{aligned}$$

k eine Skalierungskonstante ist;

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$, wobei $C_{3_{\text{thresh}}}$ ein für CR(L,3) gewählter Schwellenwertpegel ist;

$$\begin{aligned} sg(L) &= k_g/C(L,1) && \text{wenn } C(L,1) \leq 1; \\ sg(L) &= k_g/2 && \text{wenn } C(L,1) > 1 \text{ und } C_s \leq 0; \\ sg(L) &= k_g/2/(1 + C_s) && \text{wenn } C(L,1) > 1 \text{ und } C_s > 0; \end{aligned}$$

k_g eine Skalierungskonstante wie z.B. 1 ist; und

β eine Gewichtungskonstante ist, die zwischen 0 und 1 liegt.

7. Computerlesbares Medium, das prozessorausführbare Befehle zum Erzeugen eines Ultraschallbilds aufweist, wobei die prozessorausführbaren Befehle, wenn sie in einer Computervorrichtung installiert sind, es der Vorrichtung ermöglichen, Aktionen auszuführen, die aufweisen:

Empfangen von Abbildungsdaten, die aufeinanderfolgende Ultraschallabtastzeilen ($l_1, l_2, \dots, l_n$) aufweisen, die mittels einer rotierenden Ultraschallabbildungsanordnung erhalten werden;

Bestimmen mindestens eines ersten Kreuzkorrelationswerts und eines zweiten Kreuzkorrelationswerts für jede einer Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$);

Einzelnes Beurteilen für mehrere Abtastzeilen der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$), ob die Abtastzeile, die beurteilt wird, eine ungleichmäßige Rotationsverzerrung aufweist, unter Verwendung von mindestens einem der ersten und zweiten Korrelationswerte für die Abtastzeile, die beurteilt wird;

Anwenden einer Korrektur für die ungleichmäßige Rotationsverzerrung unter Verwendung von mindestens einem der ersten und zweiten Korrelationswerte für mindestens eine der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$);

Erzeugen eines Ultraschallbilds unter Verwendung mindestens der Vielzahl der Abtastzeilen mit der angewendeten Korrektur; und

Anzeigen des Ultraschallbilds,

dadurch gekennzeichnet, dass

für jede einzelne Abtastzeile der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$), der erste Kreuzkorrelationswert einen

Kreuzkorrelationskoeffizienten zwischen einem ersten Teilrahmen, der eine Vielzahl von aufeinanderfolgenden Abtastzeilen einschließlich der einzelnen Abtastzeile aufweist, und einem zweiten Teilrahmen aufweist, der eine Vielzahl von Abtastzeilen aufweist, die vom ersten Teilrahmen um einen ersten ganzzahligen Wert verschoben sind, und der zweite Korrelationswert einen Kreuzkorrelationskoeffizienten zwischen dem ersten Teilrahmen und einem dritten Teilrahmen aufweist, der eine Vielzahl von Abtastzeilen aufweist, die vom ersten Teilrahmen um einen zweiten ganzzahligen Wert verschoben sind, der sich vom ersten ganzzahligen Wert unterscheidet.

8. Computerlesbares Medium nach Anspruch 7, wobei für den Bildrahmen $F(r, L)$, wobei L eine Abtastzeile im Abbildungsrahmen ist und r ein Abtastpunkt der Abtastzeile ist, der erste Teilrahmen Δ_L Abtastzeilen um eine bestimmte Abtastzeile L und Abtastpunkte im Bereich von $[r_1, r_2]$ umfasst und der erste Kreuzkorrelationswert $CR(L, \delta_L)$ ist, wobei δ_L der erste ganzzahlige Wert ist und zum Bestimmen des ersten Kreuzkorrelationswerts verwendet werden soll, und $CR(L, \delta_L)$ ein normierter Mittelwert von mehreren Zeilen ist $C(L, \delta_L)$ um die Zeile L ist, wobei

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wobei } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L'))$$

9. Computerlesbares Medium nach Anspruch 8, wobei der erste Kreuzkorrelationswert $CR(L, 1)$ ist und der zweite Kreuzkorrelationswert $CR(L, 3)$ ist.

10. Computerlesbares Medium nach Anspruch 9, wobei die Korrektur für eine ungleichmäßige Rotation für eine Abtastzeile 1 ist:

$$\begin{aligned} s(L) &= k/CR(L, 1) && \text{wenn } CR(L, 1) \leq 1; \\ s(L) &= k/2 && \text{wenn } CR(L, 1) > 1 \text{ und } C_s \leq 0; \\ s(L) &= k/2/(1 + C_s) && \text{wenn } CR(L, 1) > 1 \text{ und } C_s > 0; \end{aligned}$$

wobei k eine Skalierungskonstante ist; und

$C_s = (C_{3_{\text{thresh}}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$, wobei $C_{3_{\text{thresh}}}$ ein für $CR(L, 3)$ gewählter Schwellenwertpegel ist.

11. Computerlesbares Medium nach Anspruch 9, wobei die Korrektur für eine ungleichmäßige Rotation für die Abtastzeile L in einem n -ten Bildrahmen $s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha)s_n(L)$ ist, wobei $\alpha < 1$ eine Gewichtungskonstante ist, und eine nicht geglättete Abtastzeilenkorrektur $s_n(L)$, die im n -ten Bildrahmen definiert ist, ist

$$\begin{aligned} s_n(L) &= k/CR(L, 1) && \text{wenn } CR(L, 1) \leq 1; \\ s_n(L) &= k/2 && \text{wenn } CR(L, 1) > 1 \text{ und } C_s \leq 0; \\ s_n(L) &= k/2/(1 + C_s) && \text{wenn } CR(L, 1) > 1 \text{ und } C_s > 0; \end{aligned}$$

wobei k eine Skalierungskonstante ist; und

$C_s = (C_{3_{\text{thresh}}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$ wobei $C_{3_{\text{thresh}}}$ ein für $CR(L, 3)$ gewählter Schwellenwertpegel ist.

12. Computerlesbares Medium nach Anspruch 9, wobei die Korrektur für eine ungleichmäßige Rotation für die Abtastzeile L in einem n -ten Bildrahmen $s'_n(L) = \sum_{n' = -\Delta_1}^{\Delta_2} \alpha_{n'} s_{n+n'}(L)$ ist, wobei $\sum_{n = \Delta_1}^{\Delta_2} \alpha_n = 1$ und Δ_1 und Δ_2 ganze Zahlen sind und dieselben sein oder sich unterscheiden können, und eine nicht geglättete Abtastzeilenkorrektur $s_n(L)$, die im n -ten Bildrahmen definiert ist, ist

$$\begin{aligned}
s_n(L) &= k/CR(L,1) && \text{wenn } CR(L,1) \leq 1; \\
s_n(L) &= k/2 && \text{wenn } CR(L,1) > 1 \text{ und } C_s \leq 0; \\
s_n(L) &= k/2/(1 + C_s) && \text{wenn } CR(L,1) > 1 \text{ und } C_s > 0;
\end{aligned}$$

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wobei k eine Skalierungskonstante ist; und

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$ wobei $C_{3_{\text{thresh}}}$ ein für CR(L,3) gewählter Schwellenwertpegel ist.

- 10 **13.** Computerlesbares Medium nach Anspruch 9, wobei die Korrektur für eine ungleichmäßige Rotation für die Abtastzeile L ist:

$$s_T(L) = \beta s(L) + (1-\beta)s_g(L),$$

15

wobei

$$\begin{aligned}
s(L) &= k/CR(L,1) && \text{wenn } CR(L,1) \leq 1; \\
s(L) &= k/2 && \text{wenn } CR(L,1) > 1 \text{ und } C_s \leq 0; \\
s(L) &= k/2/(1 + C_s) && \text{wenn } CR(L,1) > 1 \text{ und } C_s > 0;
\end{aligned}$$

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k eine Skalierungskonstante ist;

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$, wobei $C_{3_{\text{thresh}}}$ ein für CR(L,3) gewählter Schwellenwertpegel ist;

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$$\begin{aligned}
s_g(L) &= k_g/C(L,1) && \text{wenn } C(L,1) \leq 1; \\
s_g(L) &= k_g/2 && \text{wenn } C(L,1) > 1 \text{ und } C_s \leq 0; \\
s_g(L) &= k_g/2/(1 + C_s) && \text{wenn } C(L,1) > 1 \text{ und } C_s > 0;
\end{aligned}$$

30

k_g eine Skalierungskonstante wie z.B. 1 ist; und

β eine Gewichtungskonstante ist, die zwischen 0 und 1 liegt.

- 14.** System (100) zum Erzeugen von Ultraschallbildern, das aufweist:

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einen Katheter (102);

einen Ultraschallabbildungskern (306), der in den Katheter (102) einsetzbar ist, wobei der Ultraschallabbildungskern (306) mindestens einen Transducer (312) aufweist und

zur Rotation von mindestens einem Abschnitt des Ultraschallabbildungskerns (306) konfiguriert und eingerichtet ist, um eine Vielzahl von radialen Abtastzeilen ($l_1, l_2, \dots,$

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l_n) bereitzustellen;

einen Prozessor (106), der mit dem Ultraschallabbildungskern (306) koppelbar ist, zum Ausführen von prozessorlesbaren Befehlen, die Aktionen ermöglichen, die umfassen:

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Empfangen der Vielzahl von Abtastzeilen ($l_1, l_2, \dots, l_n$), die mittels des Ultraschallabbildungskerns (306) erhalten werden;

Bestimmen mindestens eines ersten Kreuzkorrelationswerts und eines zweiten Kreuzkorrelationswerts für jede einer Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$);

Einzelnes Beurteilen für mehrere Abtastzeilen der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$), ob die Abtastzeile, die beurteilt wird, eine ungleichmäßige Rotationsverzerrung aufweist, unter Verwendung von mindestens einem der ersten und zweiten Korrelationswerte für die Abtastzeile, die beurteilt wird;

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Anwenden einer Korrektur für die ungleichmäßige Rotationsverzerrung unter Verwendung von mindestens einem der ersten und zweiten Korrelationswerte für mindestens eine der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$);

Erzeugen eines Ultraschallbilds unter Verwendung mindestens der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$) mit der angewendeten Korrektur; und

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Anzeigen des Ultraschallbilds,

dadurch gekennzeichnet, dass

für jede einzelne Abtastzeile der Vielzahl der Abtastzeilen ($l_1, l_2, \dots, l_n$), der erste Kreuzkorrelationswert einen Kreuzkorrelationskoeffizienten zwischen einem ersten Teilrahmen, der eine Vielzahl von aufeinanderfolgenden Abtastzeilen einschließlich der einzelnen Abtastzeile aufweist, und einem zweiten Teilrahmen aufweist, der eine Vielzahl von Abtastzeilen aufweist, die vom ersten Teilrahmen um einen ersten ganzzahligen Wert verschoben sind, und der zweite Korrelationswert einen Kreuzkorrelationskoeffizienten zwischen dem ersten Teilrahmen und einem dritten Teilrahmen aufweist, der eine Vielzahl von Abtastzeilen ($l_1, l_2, \dots, l_n$) aufweist, die vom ersten Teilrahmen um einen zweiten ganzzahligen Wert verschoben sind, der sich vom ersten ganzzahligen Wert unterscheidet.

15. System nach Anspruch 14, wobei für den Bildrahmen $F(r, L)$, wobei L eine Abtastzeile im Abbildungsrahmen ist und r ein Abtastpunkt der Abtastzeile ist, der erste Teilrahmen Δ_L Abtastzeilen um eine bestimmte Abtastzeile L und Abtastpunkte im Bereich von $[r_1, r_2]$ umfasst und der erste Kreuzkorrelationswert $CR(L, \delta_L)$ ist, wobei δ_L der erste ganzzahlige Wert ist und zum Bestimmen des ersten Kreuzkorrelationswerts verwendet werden soll, und $CR(L, \delta_L)$ ein normierter Mittelwert von mehreren Zeilen von $C(L, \delta_L)$ um die Zeile L ist, wobei

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{wobei } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1)/2}^{(\Delta_L - 1)/2} \sum_{r=r_1}^{r_2} (F(r, L + L')) .$$

Revendications

1. Procédé de génération d'une image ultrasonore, ledit procédé comprenant :

la réception d'une image comprenant des lignes de balayage ultrasonore consécutives ($l_1, l_2, \dots, l_n$) obtenues à l'aide d'un agencement d'imagerie ultrasonore rotatif ;

la détermination d'au moins une première valeur de corrélation croisée et d'une deuxième valeur de corrélation croisée pour chaque ligne d'une pluralité des lignes de balayage ($l_1, l_2, \dots, l_n$) ;

l'évaluation individuelle pour plusieurs lignes de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$), si la ligne de balayage évaluée présente une distorsion de rotation non uniforme, en recourant à la première et/ou à la deuxième valeurs de corrélation pour la ligne de balayage évaluée ;

l'application d'une correction de la distorsion de rotation non uniforme en recourant à la première et/ou à la deuxième valeurs de corrélation pour au moins une ligne de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) ;

la génération d'une image ultrasonore en recourant au moins à la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) ayant la correction appliquée ; et

l'affichage de l'image ultrasonore,

caractérisé

en ce que pour chaque ligne de balayage individuelle de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$), la première valeur de corrélation croisée comprend un coefficient de corrélation croisée entre une première sous-image comprenant une pluralité de lignes de balayage consécutives incluant la ligne de balayage individuelle et une deuxième sous-image comprenant une pluralité de lignes de balayage décalées de la première sous-image par une première valeur entière, la deuxième valeur de corrélation comprend un coefficient de corrélation croisée entre la première sous-image et une troisième sous-image comprenant une pluralité de lignes de balayage décalées de la première sous-image par une deuxième valeur entière différente de la première valeur entière.

2. Procédé selon la revendication 1, où la première valeur de corrélation croisée et la deuxième valeur de corrélation croisée sont normalisées.

3. Procédé selon la revendication 1, où la première valeur entière est un, et facultativement la deuxième valeur entière

est deux.

4. Procédé selon la revendication 1,

où, pour l'image $F(r, L)$ où L est une ligne de balayage dans la trame d'image et r un point d'échantillonnage de la ligne de balayage, la première sous-image inclut Δ_L lignes de balayage autour d'une ligne de balayage L particulière et des points d'échantillonnage dans une plage $[r_1, r_2]$, et la première valeur de corrélation croisée est $C(L, \delta_L)$, δ_L étant la première valeur entière à utiliser pour déterminer la première valeur de corrélation croisée, et

$$C(L, \delta_L) = \frac{\sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L') - \bar{F}(L)) \cdot (F(r, L+\delta_L+L') - \bar{F}(L+\delta_L))}{\sqrt{\sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+\delta_L+L') - \bar{F}(L+\delta_L))^2}}$$

$$\text{où } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L')).$$

5. Procédé selon la revendication 1,

où, pour l'image $F(r, L)$ où L est une ligne de balayage dans la trame d'imagerie et r un point d'échantillonnage de la ligne de balayage, la première sous-image inclut Δ_L lignes de balayage autour d'une ligne de balayage L particulière et des points d'échantillonnage dans une plage de $[r_1, r_2]$, et la première valeur de corrélation croisée est $CR(L, \delta_L)$, δ_L étant la première valeur entière à utiliser pour déterminer la première valeur de corrélation croisée, et $CR(L, \delta_L)$ une moyenne normalisée de plusieurs lignes de $C(L, \delta_L)$ autour de la ligne L , où

$$C(L, \delta_L) = \frac{\sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L') - \bar{F}(L)) \cdot (F(r, L+\delta_L+L') - \bar{F}(L+\delta_L))}{\sqrt{\sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+\delta_L+L') - \bar{F}(L+\delta_L))^2}}$$

$$\text{où } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L'=-\Delta_L/2}^{(\Delta_L-1)/2} \sum_{r=r_1}^{r_2} (F(r, L+L')).$$

6. Procédé selon la revendication 5, où la première valeur de corrélation croisée est $CR(L, 1)$ et la deuxième valeur de corrélation croisée est $CR(L, 3)$,

où facultativement la correction pour rotation non uniforme pour une ligne de balayage 1 est :

$$\begin{aligned} s(L) &= k/CR(L, 1) && \text{si } CR(L, 1) \leq 1 ; \\ s(L) &= k/2 && \text{si } CR(L, 1) > 1 \text{ et } C_s \leq 0 ; \\ s(L) &= k/2/(1 + C_s) && \text{si } CR(L, 1) > 1 \text{ et } C_s > 0 ; \end{aligned}$$

k étant une constante scalaire ; et

$C_s = (C_{3\text{thresh}} \cdot CR(L, 3)) / (CR(L, 3) - CR(L, 1))$, $C_{3\text{thresh}}$ étant un niveau seuil retenu pour $CR(L, 3)$,

ou bien

où la correction pour rotation non uniforme pour la ligne de balayage L dans une $n^{\text{ième}}$ image est

$s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha) s_n(L)$, où α est < 1 , est une constante de pondération et où une correction de ligne de balayage non lissée $s_n(L)$, définie dans la $n^{\text{ième}}$ image, est

$$s_n(L) = k/CR(L, 1) \quad \text{si } CR(L, 1) \leq 1 ;$$

(suite)

$$s_n(L) = k/2 \quad \text{si } CR(L,1) > 1 \text{ et } C_s \leq 0 ;$$

$$s_n(L) = k/2/(1 + C_s) \quad \text{si } CR(L,1) > 1 \text{ et } C_s > 0 ;$$

5

k étant une constante scalaire ; et

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$, $C_{3_{\text{thresh}}}$ étant un niveau seuil retenu pour $CR(L,3)$,
ou bien

10 où la correction pour rotation non uniforme pour la ligne de balayage L dans une n^{ième} image est $s'_n(L) = \sum_{n'=-\Delta_2}^{\Delta_1} \alpha_{n'} s_{n+n'}(L)$, où $\sum_{n'=-\Delta_2}^{\Delta_1} \alpha_{n'} = 1$ et Δ_1 et Δ_2 sont entiers et peuvent être identiques ou différents, et une correction de ligne de balayage non lissée $s_n(L)$, définie dans la n^{ième} image, est

15

$$s_n(L) = k/CR(L, 1) \quad \text{si } CR(L,1) \leq 1 ;$$

$$s_n(L) = k/2 \quad \text{si } CR(L,1) > 1 \text{ et } C_s \leq 0 ;$$

$$s_n(L) = k/2/(1 + C_s) \quad \text{si } CR(L,1) > 1 \text{ et } C_s > 0 ;$$

20

k étant une constante scalaire ; et

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L,1))$, $C_{3_{\text{thresh}}}$ étant un niveau seuil retenu pour $CR(L,3)$,
ou bien

où la correction pour rotation non uniforme pour la ligne de balayage L est :

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$$s_T(L) \beta s(L) + (1-\beta)s_g(L),$$

où

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$$s(L) = k/CR(L, 1) \quad \text{si } CR(L,1) \leq 1 ;$$

$$s(L) = k/2 \quad \text{si } CR(L,1) > 1 \text{ et } C_s \leq 0 ;$$

$$s(L) = k/2/(1 + C_s) \quad \text{si } CR(L,1) > 1 \text{ et } C_s > 0 ;$$

35

k étant une constante scalaire ;

$C_s = (C_{3_{\text{thresh}}} - CR(L,3))/(CR(L,3) - CR(L, 1))$, $C_{3_{\text{thresh}}}$ étant un niveau seuil retenu pour $CR(L,3)$;

40

$$s_g(L) = k_g/C(L ; 1) \quad \text{si } C(L ; 1) \leq 1 ;$$

$$s_g(L) = k_g/2 \quad \text{si } C(L ; 1) > 1 \text{ et } C_s \leq 0 ;$$

$$s_g(L) = k_g/2/(1 + C_s) \quad \text{si } C(L ; 1) > 1 \text{ et } C_s > 0 ;$$

k_g étant une constante scalaire, p. ex. 1 ; et

β étant une constante de pondération entre 0 et 1.

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7. Support lisible par ordinateur, comportant des instructions exécutables par un processeur pour la génération d'une image ultrasonore, lesdites instructions exécutables par un processeur étant installées sur un dispositif de calcul permettant l'exécution d'actions par le dispositif, comprenant :

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la réception de données d'imagerie comprenant des lignes de balayage ultrasonore consécutives ($l_1, l_2, \dots, l_n$) obtenues à l'aide d'un agencement d'imagerie ultrasonore rotatif ;

la détermination d'au moins une première valeur de corrélation croisée et d'une deuxième valeur de corrélation croisée pour chaque ligne d'une pluralité des lignes de balayage ($l_1, l_2, \dots, l_n$) ;

l'évaluation individuelle pour plusieurs lignes de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$), si la ligne de balayage évaluée présente une distorsion de rotation non uniforme, en recourant à la première et/ou à la deuxième valeurs de corrélation pour la ligne de balayage évaluée ;

55

l'application d'une correction pour distorsion de rotation non uniforme en recourant à la première et/ou à la deuxième valeurs de corrélation pour au moins une ligne de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) ;

la génération d'une image ultrasonore en recourant au moins à la pluralité de lignes de balayage ayant la

correction appliquée ; et
l'affichage de l'image ultrasonore,
caractérisé

en ce que pour chaque ligne de balayage individuelle de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$), la première valeur de corrélation croisée comprend un coefficient de corrélation croisée entre une première sous-image comprenant une pluralité de lignes de balayage consécutives incluant la ligne de balayage individuelle et une deuxième sous-image comprenant une pluralité de lignes de balayage décalées de la première sous-image par une première valeur entière, la deuxième valeur de corrélation comprend un coefficient de corrélation croisée entre la première sous-image et une troisième sous-image comprenant une pluralité de lignes de balayage décalées de la première sous-image par une deuxième valeur entière différente de la première valeur entière.

8. Support lisible par ordinateur selon la revendication 7 où, pour l'image $F(r, L)$ où L est une ligne de balayage dans la trame d'imagerie et r un point d'échantillonnage de la ligne de balayage, la première sous-image inclut Δ_L lignes de balayage autour d'une ligne de balayage L particulière et des points d'échantillonnage dans une plage $[r_1, r_2]$, et la première valeur de corrélation croisée est $CR(L, \delta_L)$, δ_L étant la première valeur entière à utiliser pour déterminer la première valeur de corrélation croisée, et $CR(L, \delta_L)$ une moyenne normalisée de plusieurs lignes de $C(L, \delta_L)$ autour de la ligne L , où

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{où } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L')) .$$

9. Support lisible par ordinateur selon la revendication 8, où la première valeur de corrélation croisée est $CR(L, 1)$ et la deuxième valeur de corrélation croisée est $CR(L, 3)$.
10. Support lisible par ordinateur selon la revendication 9, où la correction pour rotation non uniforme pour une ligne de balayage 1 est :

$$\begin{aligned} s(L) &= k / CR(L, 1) & \text{si } CR(L, 1) \leq 1 ; \\ s(L) &= k / 2 & \text{si } CR(L, 1) > 1 \text{ et } C_s \leq 0 ; \\ s(L) &= k / 2 / (1 + C_s) & \text{si } CR(L, 1) > 1 \text{ et } C_s > 0 ; \end{aligned}$$

k étant une constante scalaire ; et

$C_s = (C_{3_{\text{thresh}}} - CR(L, 3)) / (CR(L, 3) - CR(L, 1))$, $C_{3_{\text{thresh}}}$ étant un niveau seuil retenu pour $CR(L, 3)$.

11. Support lisible par ordinateur selon la revendication 9, où la correction pour rotation non uniforme pour la ligne de balayage L dans une $n^{\text{ième}}$ image est $s'_n(L) = \alpha s_{n-1}(L) + (1 - \alpha) s_n(L)$, où $\alpha < 1$ est une constante de pondération et où une correction de ligne de balayage non lissée $s_n(L)$, définie dans la $n^{\text{ième}}$ image, est

$$\begin{aligned} s_n(L) &= k / CR(L, 1) & \text{si } CR(L, 1) \leq 1 ; \\ s_n(L) &= k / 2 & \text{si } CR(L, 1) > 1 \text{ et } C_s \leq 0 ; \\ s_n(L) &= k / 2 / (1 + C_s) & \text{si } CR(L, 1) > 1 \text{ et } C_s > 0 ; \end{aligned}$$

k étant une constante scalaire ; et

$C_s = (C_{3_{\text{thresh}}} - CR(L, 3)) / (CR(L, 3) - CR(L, 1))$, $C_{3_{\text{thresh}}}$ étant un niveau seuil retenu pour $CR(L, 3)$.

12. Support lisible par ordinateur selon la revendication 9, où la correction pour rotation non uniforme pour la ligne de balayage L dans une n^{ième} image est $s_n'(L) = \sum_{m=-\Delta_1}^{\Delta_2} \alpha_m' s_{n+m'}(L)$, où $\sum_{m=-\Delta_1}^{\Delta_2} \alpha_m = 1$ et Δ_1 et Δ_2 sont entiers et peuvent être identiques ou différents, et où une correction de ligne de balayage $s_n(L)$, définie dans la n^{ième} image, est

$$\begin{aligned} s_n(L) &= k/CR(L, 1) && \text{si } CR(L, 1) \leq 1 ; \\ s_n(L) &= k/2 && \text{si } CR(L, 1) > 1 \text{ et } C_s \leq 0 ; \\ s_n(L) &= k/2/(1 + C_s) && \text{si } CR(L, 1) > 1 \text{ et } C_s > 0 ; \end{aligned}$$

k étant une constante scalaire ; et

$C_s = (C_{3\text{thresh}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$, $C_{3\text{thresh}}$ étant un niveau seuil retenu pour $CR(L, 3)$.

13. Support lisible par ordinateur selon la revendication 9, où la correction pour rotation non uniforme pour la ligne de balayage L est :

$$s_T(L) = \beta s(L) + (1 - \beta) s_g(L),$$

où

$$\begin{aligned} s(L) &= k/CR(L, 1) && \text{si } CR(L, 1) \leq 1 ; \\ s(L) &= k/2 && \text{si } CR(L, 1) > 1 \text{ et } C_s \leq 0 ; \\ s(L) &= k/2/(1 + C_s) && \text{si } CR(L, 1) > 1 \text{ et } C_s > 0 ; \end{aligned}$$

k étant une constante scalaire ;

$C_s = (C_{3\text{thresh}} - CR(L, 3))/(CR(L, 3) - CR(L, 1))$, $C_{3\text{thresh}}$ étant un niveau seuil retenu pour $CR(L, 3)$;

$$\begin{aligned} s_g(L) &= k_g/C(L ; 1) && \text{si } C(L ; 1) \leq 1 ; \\ s_g(L) &= k_g/2 && \text{si } C(L ; 1) > 1 \text{ et } C_s \leq 0 ; \\ s_g(L) &= k_g/2/(1 + C_s) && \text{si } C(L ; 1) > 1 \text{ et } C_s > 0 ; \end{aligned}$$

k_g étant une constante scalaire, p. ex. 1 ; et

β étant une constante de pondération entre 0 et 1.

14. Système (100) pour la génération d'images ultrasonores, comprenant :

un cathéter (102) ;

un noyau d'imagerie ultrasonore (306) insérable dans le cathéter (102), ledit noyau d'imagerie ultrasonore (306) comprenant au moins un transducteur (312) et étant prévu et disposé pour permettre la rotation d'au moins une partie du noyau d'imagerie ultrasonore (306) afin de couvrir une pluralité de lignes de balayage radiales ($l_1, l_2, \dots, l_n$) ;

un processeur (106) pouvant être relié au noyau d'imagerie ultrasonore (306) pour l'exécution d'instructions lisibles par processeur déclenchant des actions, incluant :

la réception de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) obtenues au moyen du noyau d'imagerie ultrasonore (306) ;

la détermination d'au moins une première valeur de corrélation croisée et d'une deuxième valeur de corrélation croisée pour chaque ligne d'une pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) ;

l'évaluation individuelle pour plusieurs lignes de balayage de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$), si la ligne de balayage évaluée présente une distorsion de rotation non uniforme, en recourant à la première et/ou à la deuxième valeurs de corrélation pour la ligne de balayage évaluée ;

l'application d'une correction de la distorsion de rotation non uniforme en recourant à la première et/ou à la deuxième valeurs de corrélation pour au moins une ligne de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) ;

la génération d'une image ultrasonore en recourant au moins à la pluralité de lignes de balayage ($l_1, l_2, \dots$,

l_n) ayant la correction appliquée ; et
l'affichage de l'image ultrasonore,
caractérisé

en ce que pour chaque ligne de balayage individuelle de la pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$), la première valeur de corrélation croisée comprend un coefficient de corrélation croisée entre une première sous-image comprenant une pluralité de lignes de balayage consécutives incluant la ligne de balayage individuelle et une deuxième sous-image comprenant une pluralité de lignes de balayage décalées de la première sous-image par une première valeur entière, la deuxième valeur de corrélation comprend un coefficient de corrélation croisée entre la première sous-image et une troisième sous-image comprenant une pluralité de lignes de balayage ($l_1, l_2, \dots, l_n$) décalées de la première sous-image par une deuxième valeur entière différente de la première valeur entière.

15. Système selon la revendication 14, où, pour l'image $F(r, L)$ où L est une ligne de balayage dans la trame d'imagerie et r un point d'échantillonnage de la ligne de balayage, la première sous-image inclut Δ_L lignes de balayage autour d'une ligne de balayage L particulière et des points d'échantillonnage dans une plage $[r_1, r_2]$, et la première valeur de corrélation croisée est $CR(L, \delta_L)$, δ_L étant la première valeur entière à utiliser pour déterminer la première valeur de corrélation croisée, et $CR(L, \delta_L)$ une moyenne normalisée de plusieurs lignes de $C(L, \delta_L)$ autour de la ligne L , où

$$C(L, \delta_L) = \frac{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L)) \cdot (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))}{\sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L') - \bar{F}(L))^2} \cdot \sqrt{\sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + \delta_L + L') - \bar{F}(L + \delta_L))^2}}$$

$$\text{où } \bar{F}(L) = \frac{1}{\Delta_L \cdot (r_2 - r_1)} \cdot \sum_{L' = -(\Delta_L - 1) / 2}^{(\Delta_L - 1) / 2} \sum_{r = r_1}^{r_2} (F(r, L + L')) .$$

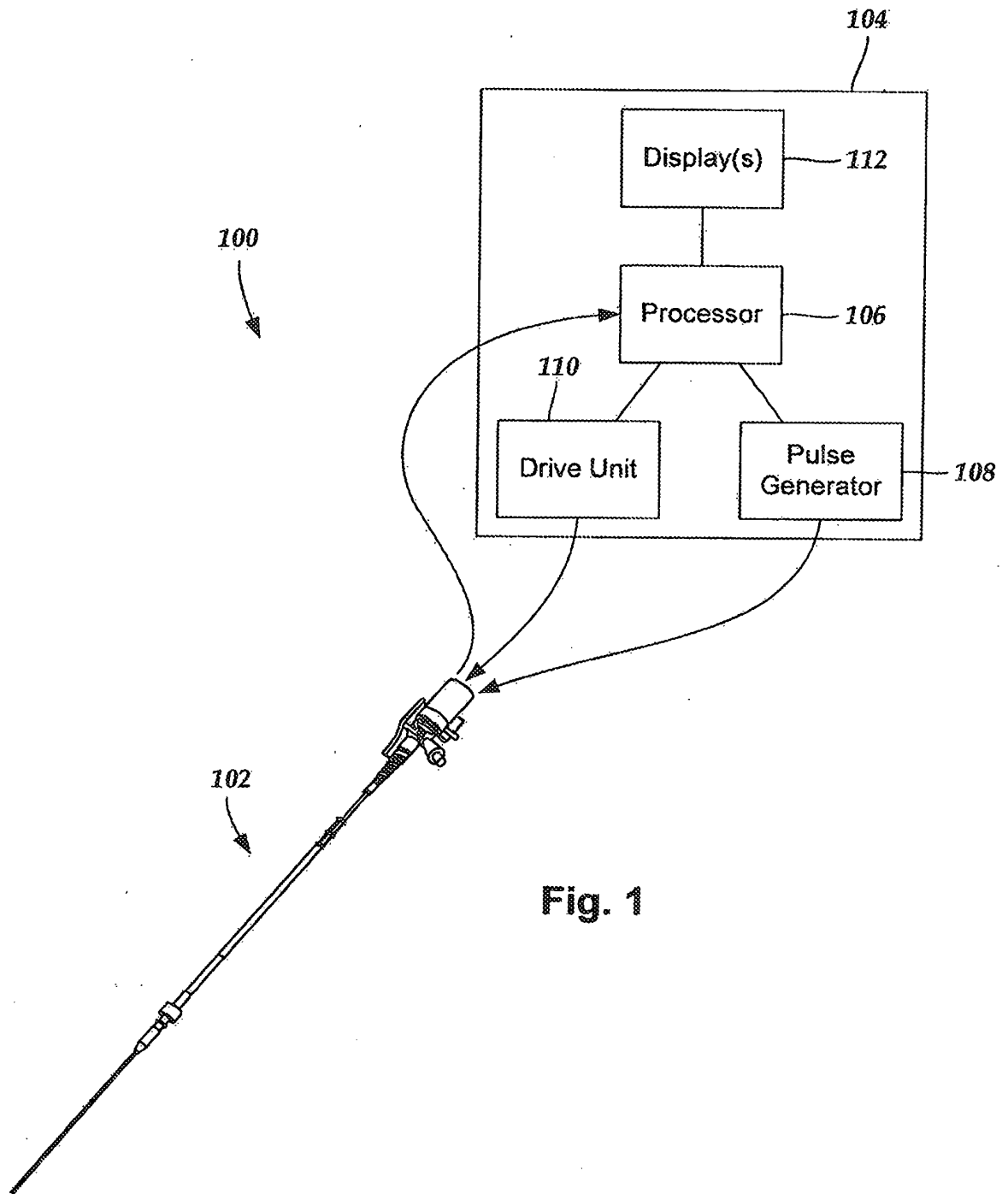


Fig. 1

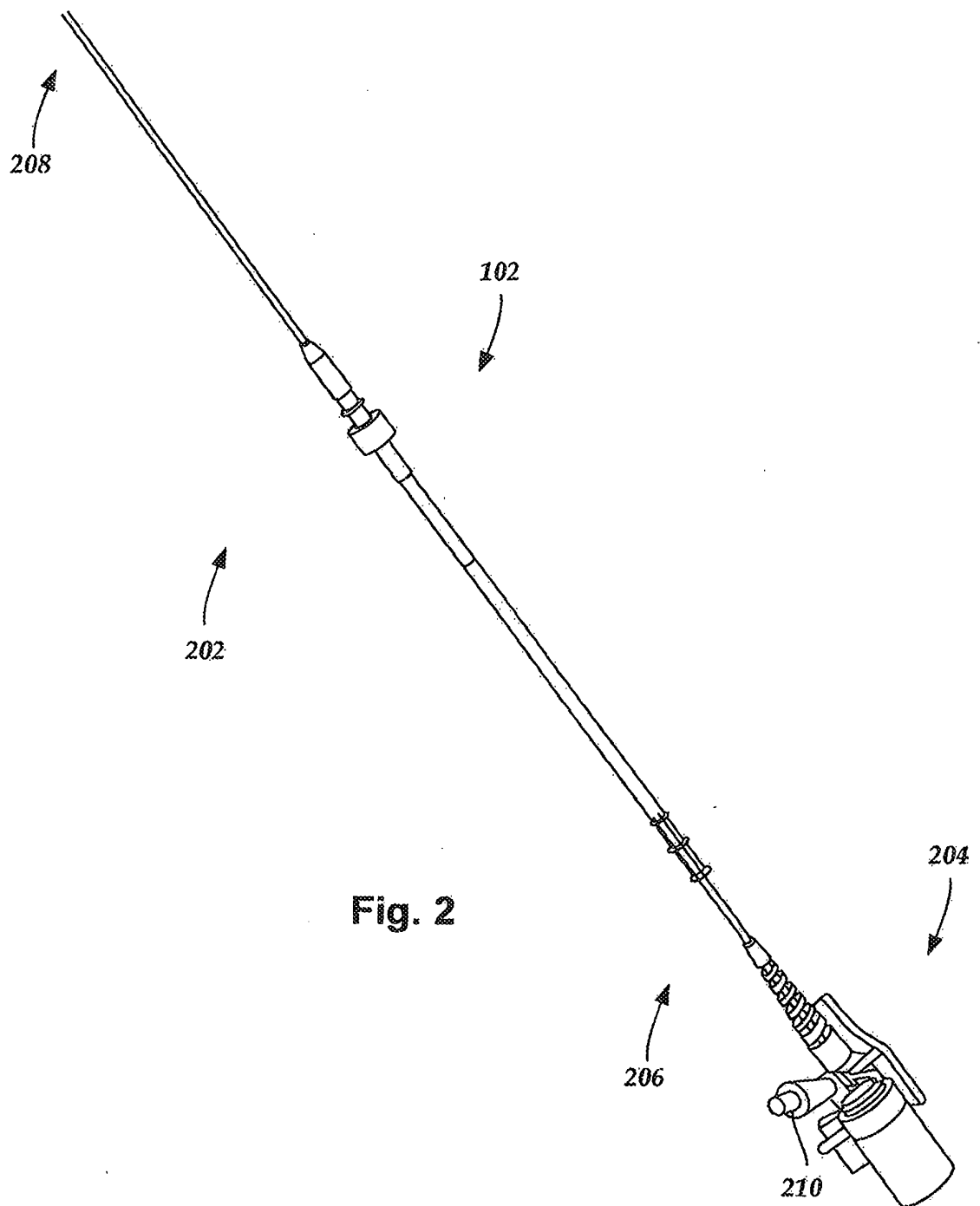


Fig. 2

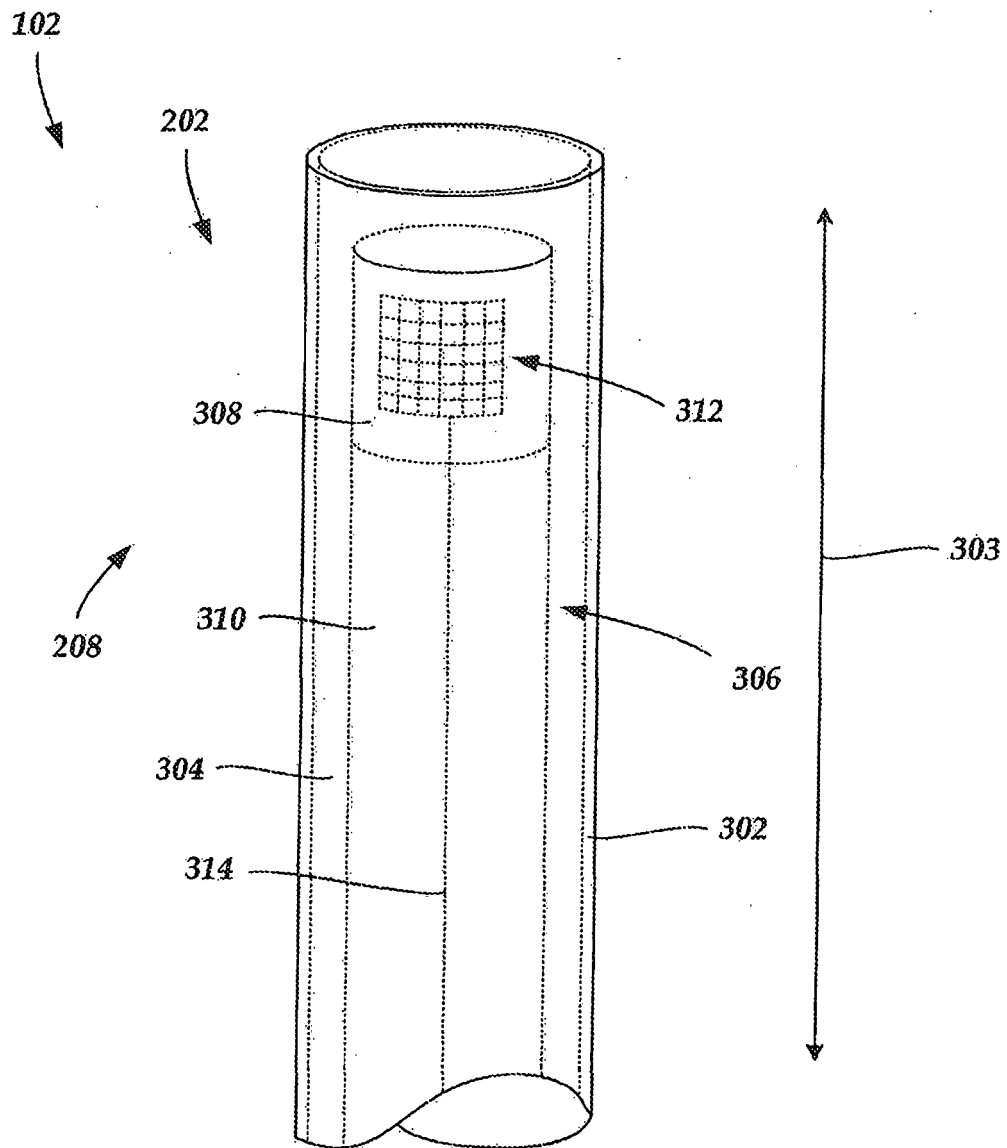


Fig. 3

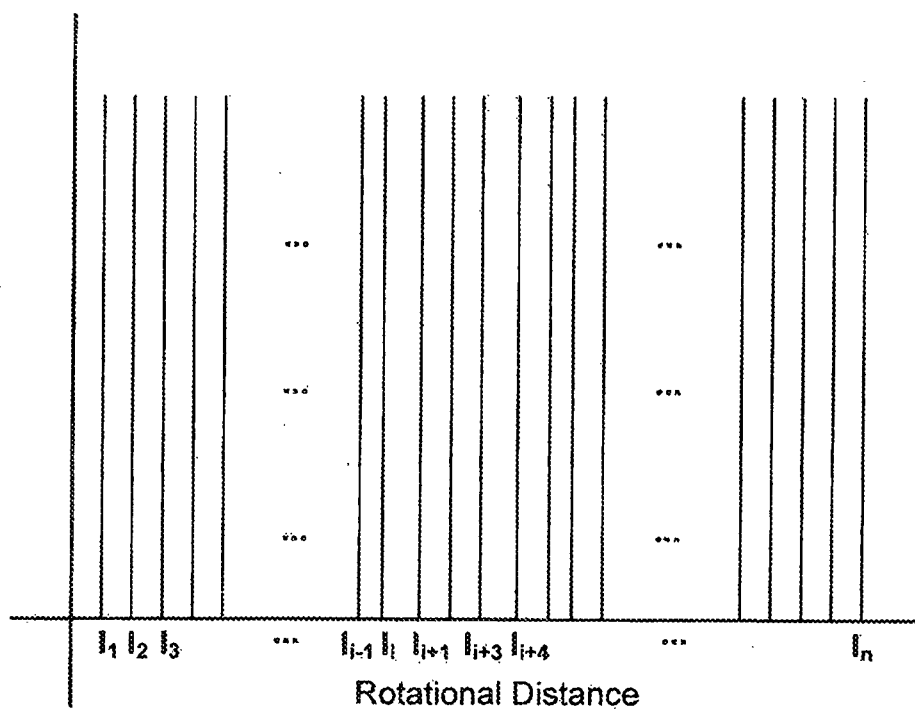


Fig. 4

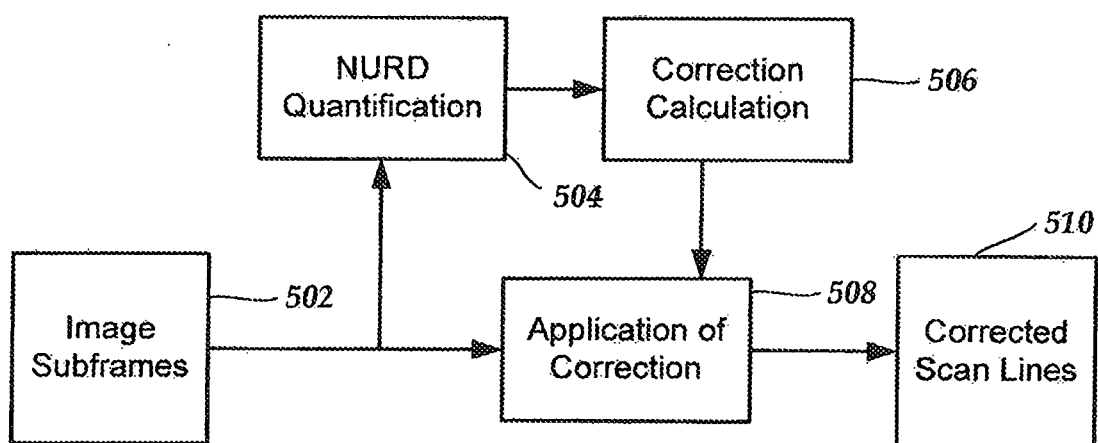


Fig. 5

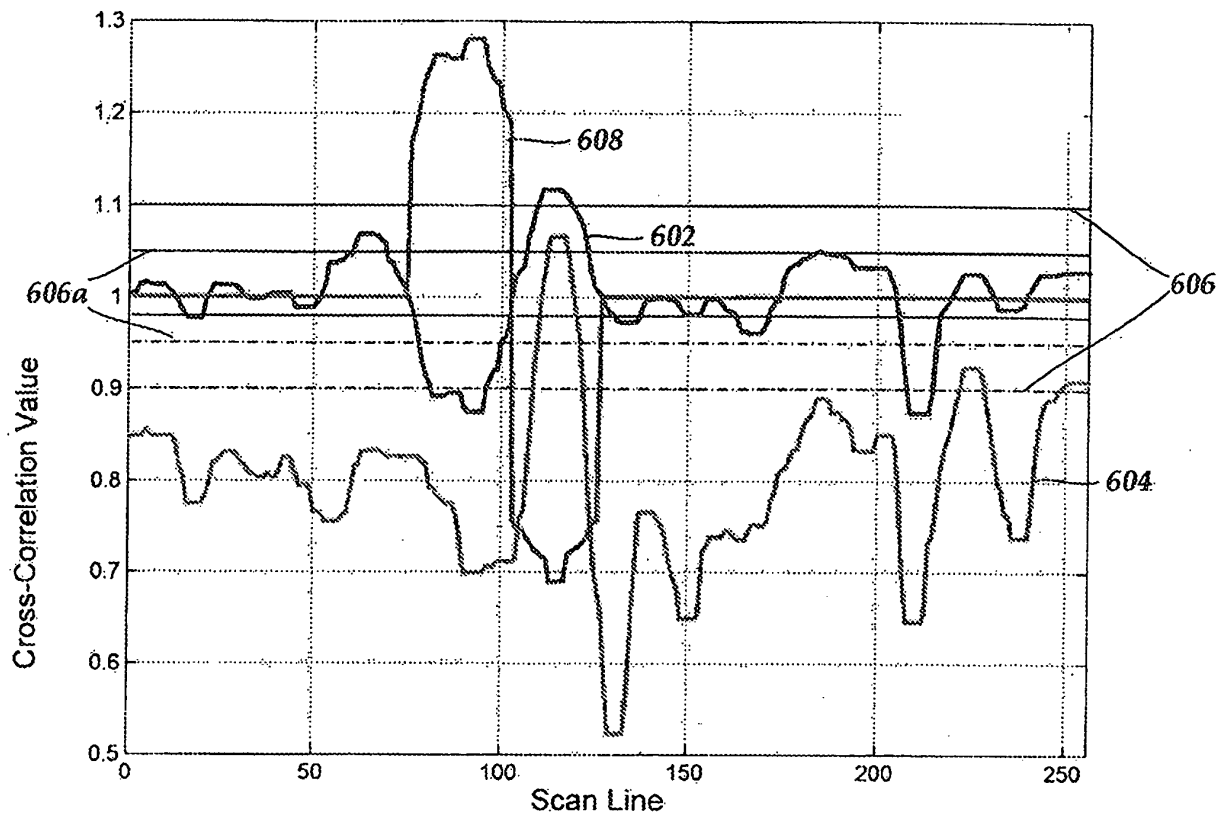


Fig. 6

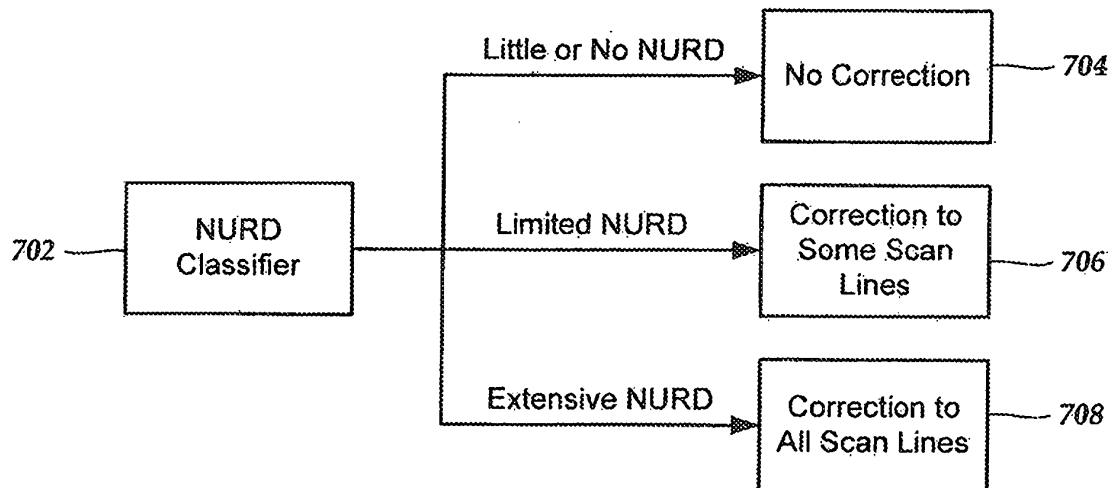


Fig. 7

REFERENCES CITED IN THE DESCRIPTION

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专利名称(译)	用于减少超声图像中的非均匀旋转失真的系统和方法		
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外部链接	Espacenet		

摘要(译)

一种用于产生超声图像的方法包括接收包括使用旋转超声成像装置获得的连续超声扫描线的图像帧，并且为多个扫描线中的每一个确定至少第一互相关值和第二互相关值。。对于多条扫描线中的每条单独扫描线，第一互相关值包括第一子帧与第二子帧之间的互相关系数，第一子帧包括多条连续扫描线，所述多条连续扫描线包括单独扫描线，第二子帧包括多条扫描线从第一个子帧移位第一个整数值。第二相关值包括之间的互相关系数第一子帧和第三子帧包括从第一子帧移位与第一整数值不同的第二整数值的多条扫描线。该方法还包括：对于多条扫描线的多条扫描线，分别评估被评估的扫描线是否使用被评估的扫描线的第一和第二相关值中的至少一个来表现出非均匀的旋转失真，A校正对于非均匀旋转，使用多个扫描线中的至少一个扫描线中的至少一个第一和第二相关值来施加非均匀旋转失真。利用所施加的校正和超声图像至少使用多条扫描线生成超声图像显示。

$$C(L, \delta) = \frac{\sum_{L=(L_1-1)/2}^{(L_1-1)/2} \sum_{l=1}^L (F(r, L+l) - \bar{F}(L)) (F(r, L+\delta_l+l) - \bar{F}(L+\delta_l))}{\sqrt{\sum_{L=(L_1-1)/2}^{(L_1-1)/2} \sum_{l=1}^L (F(r, L+l) - \bar{F}(L))^2} \sqrt{\sum_{L=(L_1-1)/2}^{(L_1-1)/2} \sum_{l=1}^L (F(r, L+\delta_l+l) - \bar{F}(L+\delta_l))^2}}$$