

analysis of the detrended raw reference signal, identify a frequency band of interest associated with the spontaneous hemodynamic oscillations, and perform an inverse fast Fourier transform within the frequency band of interest to generate a reference signal indicative of blood volume oscillations at a selected spontaneous hemodynamic oscillation. For each sample of the reference signal at a predetermined point in time, the controller multiplies the sample by each pixel of a frame at the same predetermined point in time to generate a three-dimensional coordinate matrix including a plurality of correlation matrix frames at each predetermined point in time. The controller adds the plurality of correlation matrix frames at each predetermined point in time to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation to assess the viability of the tissue in the predetermined area.

17 Claims, 7 Drawing Sheets

(56)

References Cited

U.S. PATENT DOCUMENTS

2010/0210931 A1	8/2010	Cuccia et al.
2013/0237860 A1	9/2013	Ince

OTHER PUBLICATIONS

Pichette et al., "Intraoperative video-rate hemodynamic response assessment in human cortex using snapshot hyperspectral optical imaging", *Neurophotonics*, 3(4) (2016), ten (10) pages.

Ryan C., et al., "Objective Estimates of the Probability of Death from Burn Injuries", *New England Journal of Medicine* 1998:338:362-6.

Orgill D., "Excision and Skin Grafting of Thermal Burns", *New England Journal of Medicine* Feb. 26, 2009;360(9):893-901.

Jaskille AD et al., Critical Review of Burn Depth Assessment Techniques: Part . Historical Review, *Journal of Burn Care & Research*, Nov./Dec. 2009, 937-947.

O'Reilly TJ et al., "Laser Doppler Flowmetry Evaluation of Burn Wound Depth", *Journal of Burn Care Rehabilitation*, 1989; 10:1-6.

Atilas L. et al., "Laser Doppler Flowmetry in Burn Wounds", *Journal of Burn Care Rehabilitation*, 1995, 16:388-393.

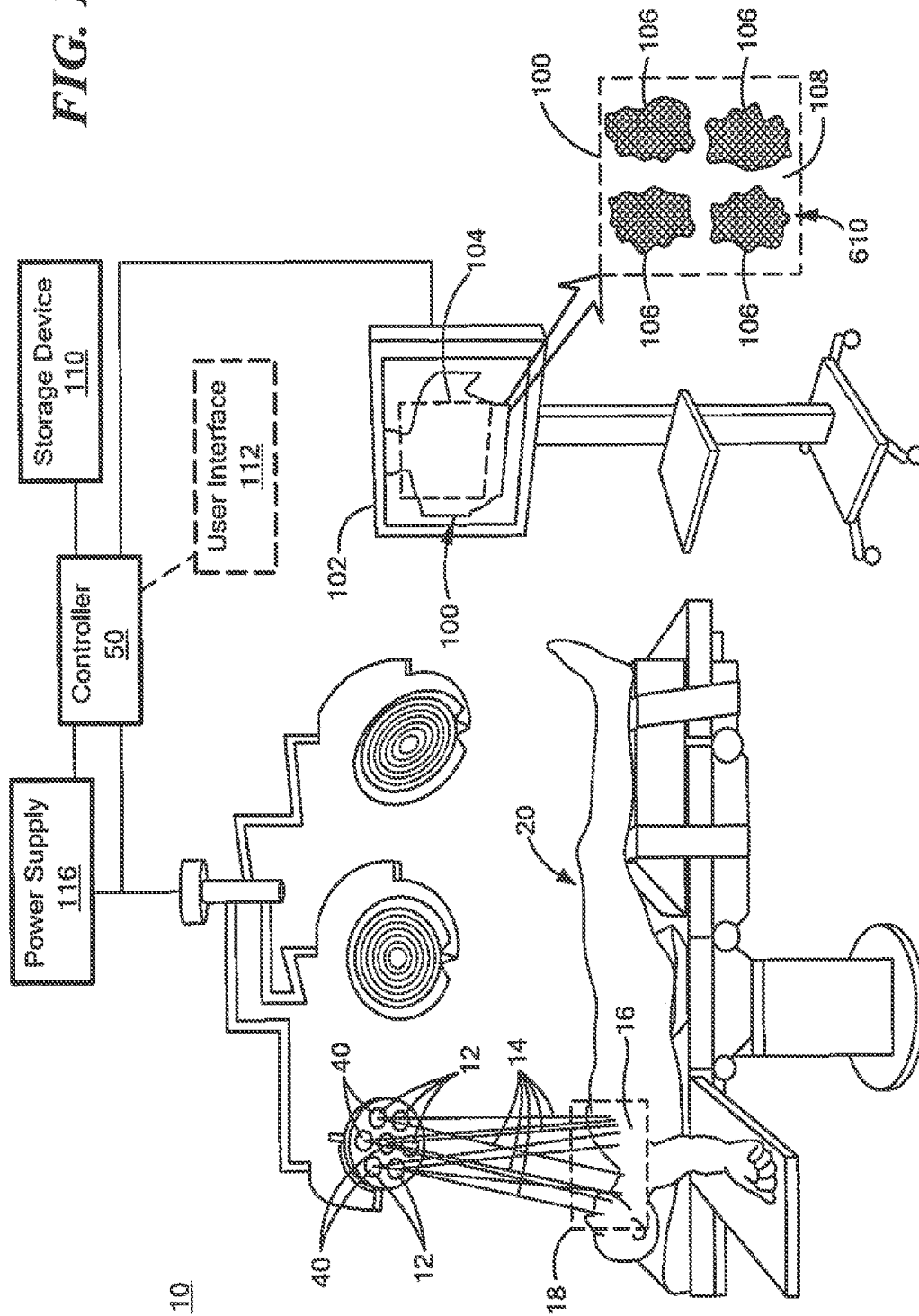
Benya R. et al., "Adverse Reactions of Indocyanine Green: A Case Report and a Review of the Literature; Catheterization and Cardiovascular Diagnosis", 1989 17(4):231-233.

Pierro ML et al., "Validation of a Novel Hemodynamic Model for Coherent Hemodynamics Spectroscopy (CHS) and Functional Brain Studies With fNIRS and fMRI", *NeuroImage*, vol. 85, Part 1, Jan. 15, 2014, (twenty-nine (29) pages).

Nitzan M. et al., "Spontaneous Low-Frequency Fluctuations in Finger Blood Volume, Measured by Photoplethysmography", *Proceedings of SPIE, Event: BIOS Europe '95*, 1995, Barcelona, Spain, vol. 2631, pp. 84-91.

Nitzan M. et al., "Measurement of the Variability of the Skin Blood Volume Using Dynamic Spectroscopy", *Applied Surface Science* 106 (1996):478-482.

FIG. 1



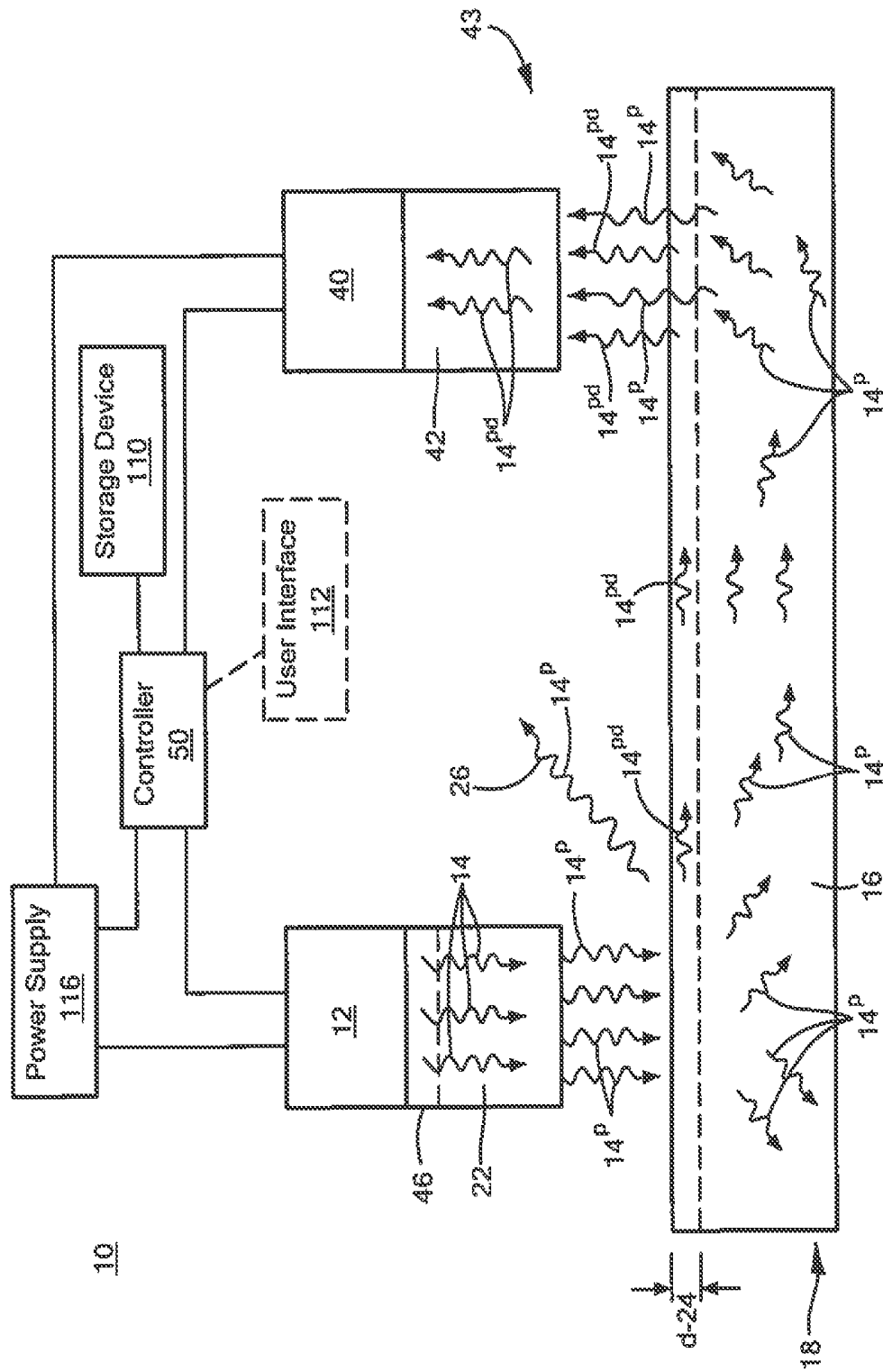


FIG. 2

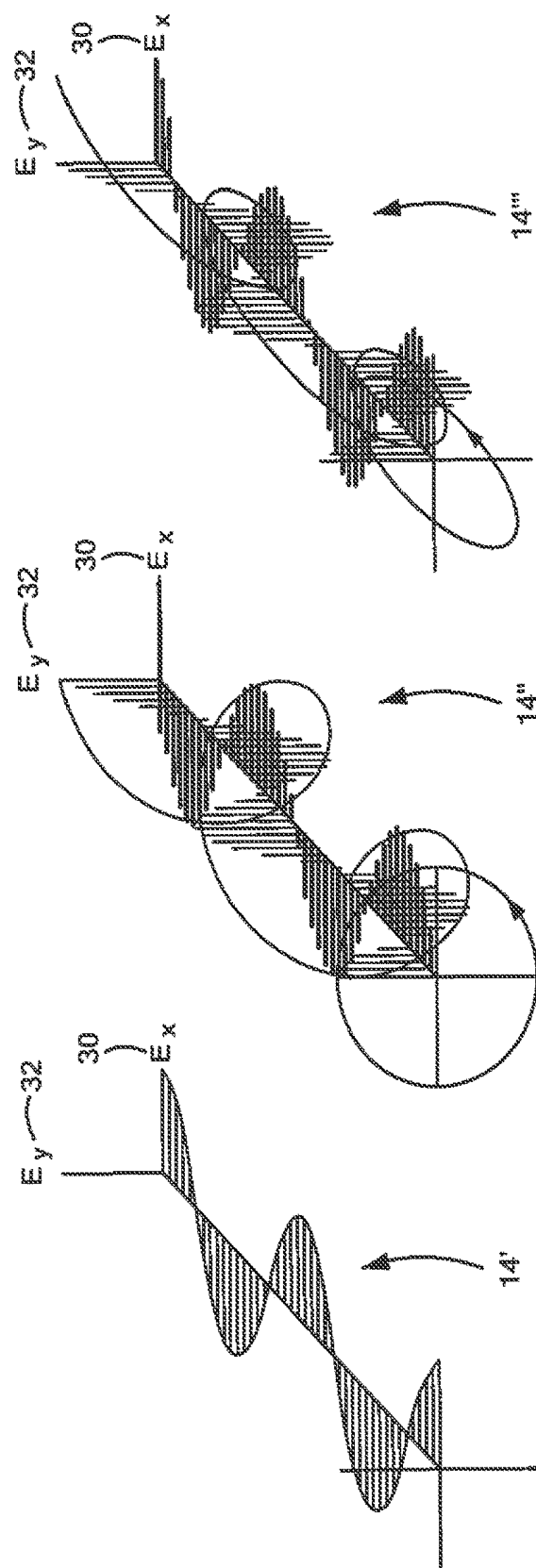


FIG. 3

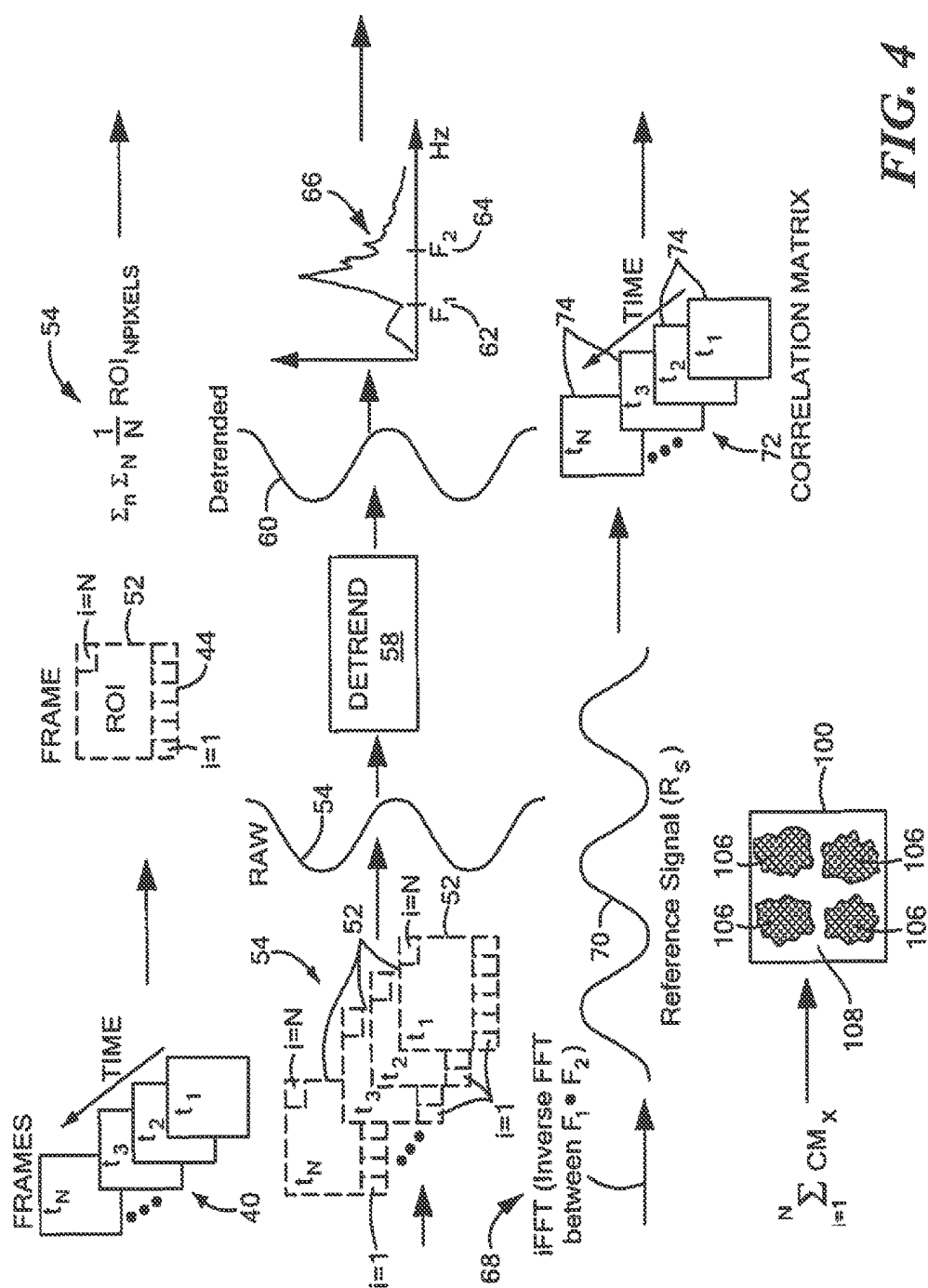


FIG. 4

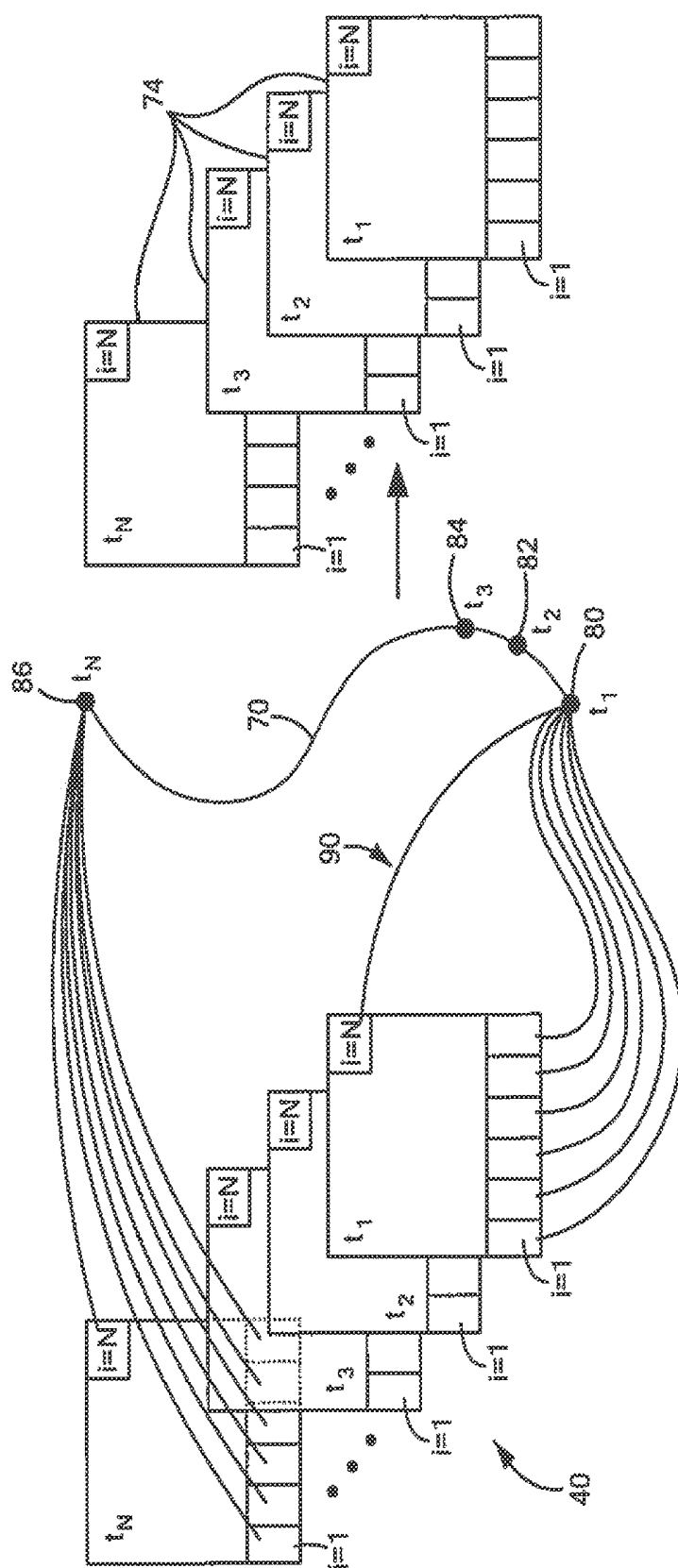
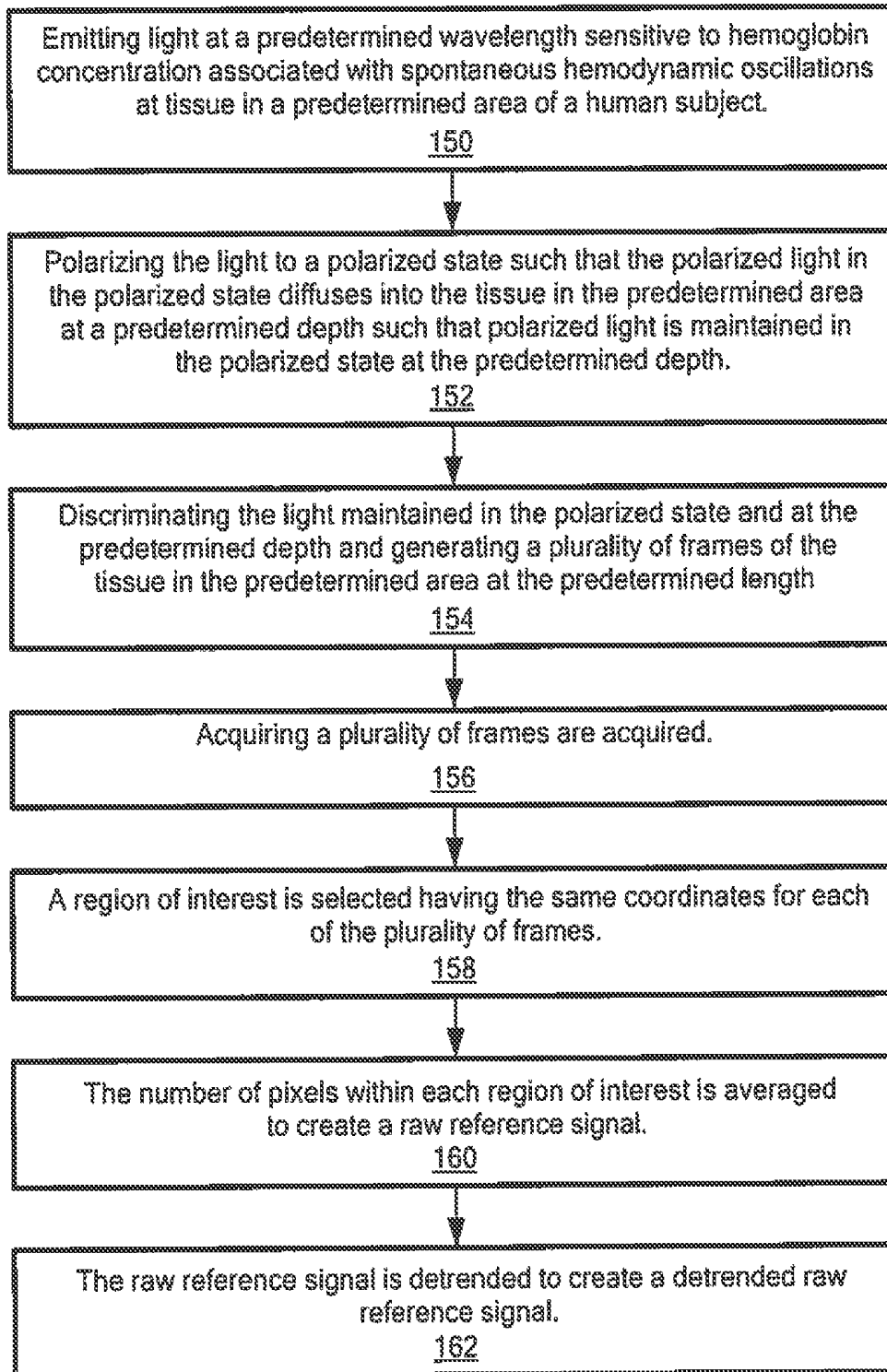
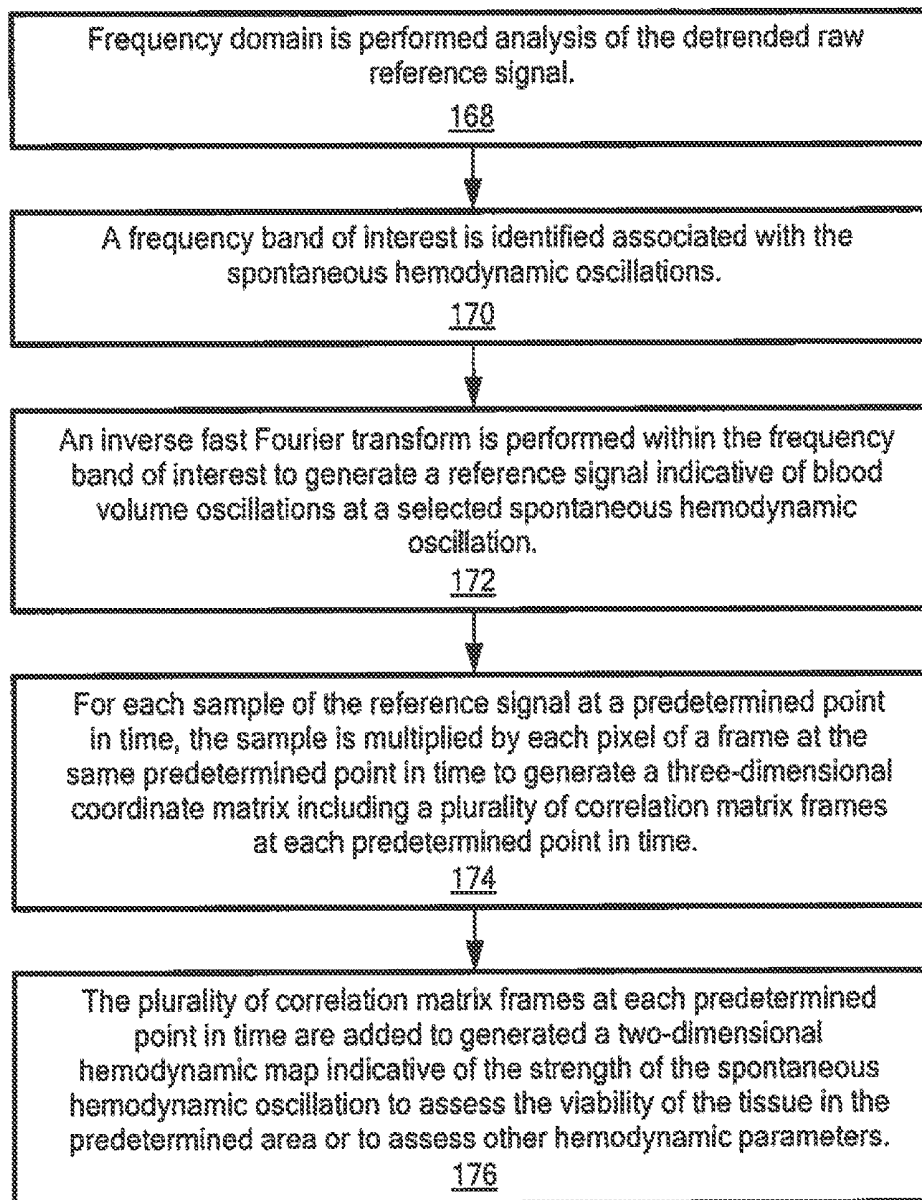


FIG. 5

**FIG. 6**

*FIG. 6 (con't.)*

CONTACTLESS SYSTEM AND METHOD FOR ASSESSING TISSUE VIABILITY AND OTHER HEMODYNAMIC PARAMETERS

RELATED APPLICATIONS

This application claims benefit of and priority to U.S. Provisional Application Ser. No. 62/621,873 filed Jan. 25, 2018, under 35 U.S.C. §§ 119, 120, 363, 365, and 37 C.F.R. § 1.55 and § 1.78, which is incorporated herein by this reference.

GOVERNMENT RIGHTS

This invention was made with government support under contract number W81XWH-17-C-0169, awarded by the Department of Defense. The government has certain rights in the invention.

FIELD OF THE INVENTION

This invention relates to a contactless system and method for assessing tissue viability and other hemodynamic parameters.

BACKGROUND OF THE INVENTION

Burn wounds may be classified into four categories of increasing depth: superficial, intermediate partial thickness, deep partial thickness, and full thickness. The latter two classifications typically require aggressive interventions that involve the debridement of necrotic tissue and the application of split thickness skin grafts. These are more morbid wounds typically wrought with the potential for hypertrophic scarring and contractures and may necessitate early surgical excision and grafting to optimize the outcome. See e.g., Ryan et al., *Objective Estimates of the Probability of Death From Burn Injuries*, N. Engl. J. Med., 1998, 338: 362-6, incorporated by reference herein. Selecting the level of debridement sufficient to minimize inflammation and determining the optimal treatment in a timely fashion is critical given the risks of infection and sepsis. The success of grafting depends on the removal of virtually all necrotic tissue and any biofilm and requires the presence of highly-vascularized granulation tissue. The goal of early debridement for grafting is to remove all the devitalized tissue for skin grafting until only granulation tissue remains. Using a conventional tissue excision procedure, several layers of burned tissue are excised until the viable wound bed is reached, as evidenced by capillary bleeding. See e.g., Orgill et al., *Excision and Skin Grafting Of Thermal Burns*, New England Journal of Medicine, 2009, Feb. 26; 360(9): 893-901, incorporated by reference herein. Although bleeding is typically assumed to mean the tissue is viable, this conventional tissue excision procedure is subjective and imprecise because it relies on visual inspection that does not preclude the possibility that some necrotic tissue or biofilm will be inadvertently left in the wound site.

Given the challenges in objectively determining tissue viability, a number of conventional technologies have been repurposed with the intent of providing metrics of tissue viability, such as Laser Doppler Imaging (LDI) and Indocyanine green angiography (ICG).

Conventional LDI is a highly recognized noninvasive technique for clinical evaluation of burn wound and tissue viability assessment. Several conventional LDI devices are available which estimate the blood flow in the area of

interest. See e.g., Jaskille et al., *Critical Review of Burn Depth Assessment Techniques: Part II, Review of Laser Doppler Technology*, Journal of Burn Care & Research, 2010, Jan. 1; 31(1):151-7, incorporated by reference herein.

However, LDI has several drawbacks. Because flowmetry requires the probe to directly contact with the burn wound, it may increase the risk of wound infection and may inflict trauma to already vulnerable tissue. See e.g., O'Reilly et al., *Laser Doppler Flowmetry Evaluation of Burn Wound Depth*, Journal of Burn Care & Research, 1989, Jan. 1; 10(1):1, incorporated by reference herein. Additionally, because LDI measures perfusion in one spot at the time, assessing a large burn wound may be a time-consuming process. Additionally, there is some risk that LDI may not detect necrotic tissue in the wound bed. See e.g., Atilas et al., *Laser Doppler Flowmetry In Burn Wounds*, Journal of Burn Care & Research, 1995, Jul. 1; 16(4): 388-93, incorporated by reference herein.

Conventional Indocyanine green (ICG) video-angiography provides greater skin imaging penetration compared to LDI. ICG enables visualization of the deep dermal vasculature using a dye. See e.g., Jerath et al., *Burn Wound Assessment in Porcine Skin Using Indocyanine Green Fluorescence*, Journal of Trauma and Acute Care Surgery, 1999, Jun. 1; 46(6): 1085-8, incorporated by reference herein. ICG is based on the fluorescent properties of the dye being used and quantifying the intensity of the dye. ICG provides color-coded maps relative to the perfusion of the investigated area. The major drawback associated with conventional ICG video-angiography is that intravascular dye injection is required. Previous studies have shown a high degree of association between headache, pruritus, urticarial and anaphylactic reaction following the dye injection. See e.g., Benya et al., *Adverse Reactions to Indocyanine Green: A Case Report and a Review of the Literature*. Catheterization and Cardiovascular Diagnosis, 1989, Aug. 1; 17(4):231-3, incorporated by reference herein.

While conventional LDI and ICG each offer a unique approach to detecting tissue viability, both techniques are cumbersome to manipulate in a surgical setting, have a large size, and do not provide for real-time diagnosis, critical for tissue viability assessment during an excision procedure.

SUMMARY OF THE INVENTION

In one aspect, a contactless system for assessing tissue viability and other hemodynamic parameters is featured. The system includes one or more light sources configured to emit lights at a predetermined wavelength sensitive to hemoglobin concentration associated with spontaneous hemodynamic oscillations at tissue in a predetermined area of a human subject. One or more polarizers each coupled to one or more of the one or more light sources are configured to polarize the light to a polarized state such that the polarized light in the polarized state diffuses into the tissue in the predetermined area at a predetermined depth and the polarized light is maintained in the polarized state at the predetermined depth. One or more detectors each including a detector polarizer coupled thereto are configured to discriminate the light maintained in the polarized state and at the predetermined depth and configured to generate a plurality of frames of the tissue in the predetermined area at the predetermined depth. A controller is coupled to the one or more light sources and the one or more detectors and is configured to: acquire the plurality of frames, select a region of interest having the same coordinates for each of the plurality of frames, average the number of pixels within each

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region of interest to create a raw reference signal, detrend the raw reference signal to create a detrended raw reference signal, perform frequency domain analysis of the detrended raw reference signal, identify a frequency band of interest associated with the spontaneous hemodynamic oscillations, perform an inverse fast Fourier transform within the frequency band of interest to generate a reference signal indicative of blood volume oscillations at a selected spontaneous hemodynamic oscillation, for each sample of the reference signal at a predetermined point in time, multiply the sample by each pixel of a frame at the same predetermined point in time to generate a three-dimensional coordinate matrix including a plurality of correlation matrix frames at each predetermined point in time, and add the plurality of correlation matrix frames at each predetermined point in time to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation to assess the viability of the tissue in the predetermined area.

In one embodiment, the spontaneous hemodynamic oscillations may have a frequency in the range of 0.05 Hz to about 1.5 Hz. The predetermined wavelength may be in the range of about 500 nm to about 1,000 nm. The predetermined depth may be in the range of about 0.1 mm to about 0.5 mm. The other hemodynamic parameters may include one or more of: heart rate, resting heart rate, heart rate variability, and tissue saturation for patients suffering from diminished blood circulation, and other similar type hemodynamic parameters. The one or more detectors may include a CCD camera. The one or more detectors may include a CMOS camera. The predetermined area may include a burn area of the human subject. The predetermined area may include a wound area of a human subject. The system may include a light filtering lens coupled to one or more light sources.

In another aspect, a contactless method for assessing tissue viability and other hemodynamic parameters is featured. The method includes emitting light at a predetermined wavelength sensitive to hemoglobin concentration associated with spontaneous hemodynamic oscillations at tissue in a predetermined area of a human subject. The light is polarized to a polarized state such that the polarized light in the polarized state diffuses into the tissue in the predetermined area at a predetermined depth and the polarized light is maintained in the polarized state at the polarized depth. The light maintained in the polarized state and at the predetermined depth is discriminated. A plurality of frames of the tissue in the predetermined area at the predetermined depth are generated and acquired. A region of interest is selected having the same coordinates for each of the plurality of frames. The number of pixels within each region of interest is averaged to create a raw reference signal. The raw reference signal is detrended to create a detrended raw reference signal. A frequency domain analysis of the detrended raw reference signal is performed. A frequency band of interest associated with the spontaneous hemodynamic oscillations is identified. An inverse fast Fourier transform within the frequency band of interest is performed to generate a reference signal indicative of blood volume oscillations at a selected spontaneous hemodynamic oscillation. For each sample of the reference signal at a predetermined point in time, the sample is multiplied by each pixel of a frame at the same predetermined point in time to generate a three-dimensional coordinate matrix including a plurality of correlation matrix frames at each predetermined point in time. The plurality of correlation matrix frames at each predetermined point in time are added to generate a

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two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation to assess the viability of the tissue in the predetermined area.

In one embodiment, the plurality of correlation matrix frames at each predetermined point in time are added to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation to assess the viability of other hemodynamic parameters including one or more of: heart rate, resting heart rate, heart rate variability, and tissue saturation for patients suffering from diminished blood circulation and similar type hemodynamic parameters. The spontaneous hemodynamic oscillations may have a frequency in the range of 0.05 Hz to about 1.5 Hz. The predetermined wavelength may be in the range of about 500 nm to about 1,000 nm. The predetermined depth may be in the range of about 0.1 mm to about 0.5 mm. The predetermined area may include a burn area of the human subject. The predetermined area may include a wound area of a human subject.

The subject invention, however, in other embodiments, need not achieve all these objectives and the claims hereof should not be limited to structures or methods capable of achieving these objectives.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

Other objects, features and advantages will occur to those skilled in the art from the following description of a preferred embodiment and the accompanying drawings, in which:

FIG. 1 is a schematic diagram showing the primary components of one embodiment of the contactless system and method for assessing tissue viability and other hemodynamic parameters;

FIG. 2 is a schematic diagram showing in further detail the interaction of polarized light in a polarized state with tissue in the predetermined area shown in FIG. 1;

FIG. 3 depicts graphs of various types of polarized light which may be provided by the polarizer coupled to the one or more light sources shown in FIG. 1;

FIG. 4 is a block diagram showing one example of the primary steps performed by the controller shown in FIG. 1 to create a hemodynamic map to assess tissue viability and other hemodynamic parameters;

FIG. 5 is a schematic block diagram showing in further detail one example of the step of creating the hemodynamic map shown in FIG. 4; and

FIG. 6 is a schematic block diagram showing one example of the primary steps of one embodiment of the contactless method for assessing tissue viability and other hemodynamic parameters.

DETAILED DESCRIPTION OF THE INVENTION

Aside from the preferred embodiment or embodiments disclosed below, this invention is capable of other embodiments and of being practiced or being carried out in various ways. Thus, it is to be understood that the invention is not limited in its application to the details of construction and the arrangements of components set forth in the following description or illustrated in the drawings. If only one embodiment is described herein, the claims hereof are not to be limited to that embodiment. Moreover, the claims hereof

are not to be read restrictively unless there is clear and convincing evidence manifesting a certain exclusion, restriction, or disclaimer.

FIG. 1 shows one embodiment of contactless system 10 for assessing of tissue viability and other hemodynamic parameters. System 10 preferably includes one or more light sources 12 configured to emit light 14 at a predetermined wavelength sensitive to hemoglobin concentration associated with spontaneous hemodynamic oscillations at tissue 16 in predetermined area 18 of a human subject 20 having a burn wound or similar type wound where the tissue viability of human subject 20 needs to be determined, as discussed in the Background section above. Tissue 16 in predetermined area 18 may be any tissue in any area on human subject 20 having a burn wound or similar type wound, e.g., such as diabetic ulcers or similar type wounds. In the example shown in FIG. 1, predetermined area 18 is located on the face, neck, and upper chest of human subject 20. In other examples, predetermined area 18 may be any area of the human subject 20 having a burn wound or similar type wound where tissue viability needs to be determined. One or more light sources 12 are preferably placed above and proximate tissue 16 in predetermined area 18 and emit or illuminate light 14 having one or more wavelengths sensitive to hemoglobin concentration spontaneous oscillations and capable of probing the human tissue without being completely absorbed, as discussed in further detail below. In one example, one or more light sources 12 preferably emit or illuminate light 14 having wavelengths in an electromagnetic (EM) spectrum, e.g., in the range of about 500 nm to about 1000 nm. In one example, the spontaneous hemodynamic oscillations, e.g., cardiac and respiratory induced oscillations, have a frequency in the range of about 0.05 Hz to about 1.5 Hz associated with blood volume changes. In one design, one or more light sources 12 may include near infrared (NIR) sensors and/or one or more near infrared spectroscopy (NIRS) sensors.

System 10 also includes one or more polarizers each coupled to one or more light sources. FIG. 2 shows an example of polarizer 22 coupled to light source 12. Each of the one or more light sources 12 shown in FIG. 1 similarly has polarizer 22 coupled thereto. Each polarizer 22, FIG. 2, coupled to light source 12 is configured to polarize light 14 to polarized light 14^p in a polarized state such that polarized light 14^p in the polarized state diffuses into tissue 16 in predetermined area 18 and polarized light 14^p is maintained in the polarized state at predetermined depth d-24. In one example, depth d-24 is in the range of about 0.1 mm to about 0.5 mm. For example, when polarized light 14^p is incident on tissue 16 in predetermined area 18, some of the photons polarized light 14^p will reflect off the surface of tissue 16 and some photons will penetrate into tissue 16 where the photons will either be scattered or absorbed as shown. If light polarized 14^p incident light is reflected off the surface of the tissue 16, e.g., indicated at 26, the polarization state is perfectly maintained. However, the polarization state of the penetrating photons of polarized light 14^p may be affected by scattering events in tissue 16 which may be divided into two categories: polarization maintaining or depolarized. If the photons do not travel deep into the tissue of tissue 16 only a limited number of scattering events will occur and the polarization is maintained, but some alterations have likely occurred. However, if photons travel deeper into tissue 16 and more scattering events occur, the polarization of polarized light 14^p becomes increasingly depolarized. Therefore, by utilizing one or more polarizer 22 each coupled to one or more light sources 12, the degree of polarization can be

maintained to discriminate the depth of penetration of light into the tissue of tissue 16, e.g., polarized light 14^p at depth d-24, e.g., is about 0.1 mm to about 0.5 mm. Such a depth is typically needed for real-time assessment of tissue viability of tissue 16 in predetermined area 18 by clinicians in an objective manner, as discussed below.

Polarized light 14^p emitted from each polarizer 22 provides a relatively low-cost solution to enable real-time assessment of the tissue viability and other hemodynamic parameters of tissue 16 in predetermined area 18. As polarized light 14^p transversely propagates through time and space, it contains both oscillating orthogonal electric and magnetic field vectors. The polarization of polarized light 14^p as disclosed herein refers to the direction and manipulation of the oscillating electric field vector. Polarization may be produced and manipulated by polarizer 22 coupled to one or more light sources 12. Polarizer 22 may be placed in any desired position along path of light 14 from detectors 12, FIGS. 1 and 2, to tissue 16 in predetermined area 18. Polarized light 14 provided by one or more light sources 12 and polarizer 22 coupled thereto may include linearly polarized light 14', FIG. 3, circular polarized 14" or elliptical polarized light 14"', depending on the arrangement of the optical components used. Linearly polarized light 14' may be produced when a single electric field oscillation plane is isolated using polarizer 22 configured as linear polarizer, where one oscillation plane is dictated by the polarizing axis. The resulting electric field vector is considered to oscillate in one plane in which the orthogonal Ex-30 and Ey-32 components are maintained the same phase and amplitude as shown. Circularly polarized light 14" may be provided by polarizer 22 coupled to one or more light sources 12 when one of the two Ex-30 and Ey-32 components of the linearly polarized electric field vector becoming out of phase by exactly ± 90 from the other as shown. Circularly polarized light 14" may be provided by polarizer 22 coupled to one or more light sources 12 when polarizer 22 is configured as a quarter-wave plate rotated 45 degrees relative to the polarizing axis of the linear polarizer. As circularly polarized light propagates through time, the shape of the propagation may be considered as a helix rotating either clockwise or counter-clockwise, which is denoted as right-handed or left-handed respectively. Elliptically polarized light 14"' is provided by polarizer 22 coupled to one or more light sources 12 when linearly polarized light passing through polarizer 22 is configured as a wave plate or birefringent material where the electric field vector components become out of phase by any amount other than ± 90 degrees. Polarized light 14', polarized light 14" or polarized light 14"' provided by polarizer 36 coupled to one or more light sources 12 under these different polarization states will respond differently when focused on a turbid media, such as tissue 16, FIG. 1, of human subject 20 in predetermined area 18.

In the example discussed above with reference to FIG. 2, polarized light 14^p and polarized light 14^p may be one or more of polarized light 14', 14", and/or 14"', FIG. 3.

System 10 may also include one or more light filtering lenses coupled to one or more light sources 12, e.g., light filtering lens 46 shown coupled to polarizer 22. Light filtering lens 46 is preferably configured to be transmissive within the desired operating spectrum discussed above and configured to block EM waves outside of the desired spectrum.

System 10 also includes one or more detectors 40, FIGS. 1 and 2, which each include detector polarizer 42, FIG. 2, coupled thereto. In one example, one or more detectors 40 preferably include one or more high-quality CCD cameras,

one or more CMOS cameras, or similar type detectors. One or more detectors **40** may each include sensors having an analog amplifier and filter configured to increase the gain on the signal and reduces background noise to create clean images.

Each of detector polarizer **42** are configured to discriminate between polarized light 14^{pd} maintained in the polarized state and at the predetermined depth, d-**24**, in from tissue **16** and polarized light 14^p reflected from tissue **16** which has not been maintained in the polarized state and at the predetermined depth. For example, as shown generally by arrow **43**, each detector polarizer **42** coupled to detector **40** discriminates between polarized light 14^{pd} that has been maintained in the polarized state at predetermined depth, d-**24**, in tissue **16** and polarized light 14^p which has not been maintained in the polarized state at predetermined depth, d-**24**.

One or more detectors **40**, FIGS. **1** and **2**, e.g., one or more CCD cameras or CMOS cameras, or similar type devices, are configured to generate a plurality of frames of tissue **16**, FIGS. **1** and **2**, in predetermined area **18** from discriminated polarized light 14^{pd} reflected from tissue **16** in predetermined area **18** at predetermined depth, d-**24**, FIG. **2**, e.g., plurality of frames **40**, FIG. **4**, at different points in time ranging from, $t_1, t_2, t_3 \dots t_N$.

System **10** also includes controller **50**, FIGS. **1** and **2**, coupled to one or more light sources **12** and one or more detectors **40**. Controller **50** may be a processor, one or more processors, an application-specific integrated circuit (ASIC), firmware, hardware, and/or software (including firmware, resident software, micro-code, and the like) or a combination of both hardware and software that may all generally be referred to herein as a "controller", which may be part of contactless system **10** and method thereof for assessing tissue viability and other hemodynamic parameters. Computer program code for the programs for carrying out the instructions or operation of controller **50** may be written in any combination of one or more programming languages, including an object oriented programming language, e.g., C++, Smalltalk, Java, and the like, or conventional procedural programming languages, such as the "C" programming language or similar programming languages.

Controller **50** acquires the plurality of frames **40**, FIG. **4**, to provide image acquisition, preferably at a high rate, e.g., greater than about 5 frames per second (fps). Controller **50** then selects a region of interest (ROI) having the same coordinate for each of the plurality of frames. For example, ROI-**52**, which includes pixels from $i=1$ to $i=N$ as shown, is selected by controller **50** from frame **44** at point t_1 . Similarly, controller **50** selects a ROI-**52** having the same pixel coordinates for each of the plurality of frame **44** at points of time, $t_1, t_2, t_3 \dots t_N$.

Controller **50** then averages the number of pixels from $i=1$ to $i=n$ within each ROI-**52** of each of the plurality of frames **40**, at times $t_1, t_2, t_3 \dots t_N$, indicated at **54**, to create raw reference signal **56**. In one example, controller **50** uses equation (1) below to averages the number of pixels within each ROI-**52**:

$$\sum_N \sum_n \frac{1}{n} ROI_{NPIXELS} \quad (1)$$

where n is the number of pixels in the selected ROI and N is the number of acquired frames.

Controller **50** then detrends raw reference signal **56**, indicated at **58**, to create detrended raw reference signal **60**.

Controller **50** then performs frequency domain analysis of detrended raw reference signal **60** and identifies a frequency band of interest associated with the spontaneous hemodynamic oscillations. In this example, controller **50** has identified the frequency band of interest between F_1 -**62** and F_2 -**64** associated with spontaneous hemodynamic oscillations **66**. The frequency band of interest associated with the spontaneous hemodynamic oscillations is typically in the range of 0.05 Hz to about 1.0 Hz, as discussed above.

Controller **50** then performs inverse fast Fourier transform (iFFT), indicated at **68**, within the frequency band of interest, F_1 -**62** to F_2 -**64**, to generate reference signal (R_s) **70** indicative of blood volume oscillations at selected hemodynamic oscillations.

For each sample of reference signal **70** at a predetermined point in time, controller **50** multiplies the sample by each pixel of a frame at the same predetermined point in time to generate three-dimensional correlation matrix **72** which includes a plurality of correlation matrix frames **74** at each predetermined point in time. As discussed above, each of the plurality of frames **40** is acquired at a various point of time, e.g., time ranging from $t_1, t_2, t_3, \dots t_N$. Reference signal **70**, shown in greater detail in FIG. **5**, includes the same number of samples as the number of plurality of frames **40**, FIG. **4**, e.g., sample-**80**, FIG. **5**, at time t_1 , sample **82** at time t_2 , sample **84** at time t_3 and sample **86** at time t_N . Controller **50** multiplies each sample by each pixel of each of the plurality of frames **40** to generate correlation matrix **72** with a plurality of correlation matrix frames **74**. In this example, sample **80** at time t_1 is shown being multiplied each of the pixels ranging from $i=1$ to $i=n$ of frame **44** at the same time t_1 , as indicated by lines **90**. Similarly, sample **88** at time t_N is shown being multiplied each of the pixels ranging from $i=1$ to $i=n$ of frame **44** at the same time t_N . The same is done for all of the samples at each point in time.

In one example, correlation matrix **72** is generated using equation (2):

$$FRAME_i * R_{Si} \quad (2)$$

where $FRAME_i$ is each individual pixels in specific frame at time i, e.g., $t_1, t_2, t_3, \dots t_N$, and R_{Si} is a sample at time i of the Reference Signal, e.g., $t_1, t_2, t_3, \dots t_N$.

Controller **50** then adds the plurality of correlation matrix frames **74** at each predetermined point in time to generate two-dimensional hemodynamic map **100**, FIG. **4**, indicative of the strength of spontaneous hemodynamic oscillations to assess the viability of tissue **16** in predetermined area **18**. In one example, equation (3) below is used to generate two-dimensional hemodynamic map **100**:

$$\sum_{i=1}^N CMx \quad (3)$$

where i is correlation matrix at time, i, e.g., $t_1, t_2, t_3, \dots t_N$. N is the total amount of is acquired frames, and CMx is the hemodynamic map showing areas of viable tissue.

In one design, system **10**, FIG. **1**, preferably includes display device **102** coupled electronically or wirelessly to controller **50**, e.g., a computer monitor, a smart phone, a tablet, or similarly type device, which displays two-dimensional hemodynamic map **100**.

The result is system **10** provides hemodynamic map **100**, FIGS. **1** and **2**, of tissue **16** in predetermined area **18** and at a depth of about 0.1 mm to about 0.5 mm needed for real-time assessment of the viability of tissue **16** in predetermined area **18** or other hemodynamic parameters, e.g., heart rate, resting heart rate, heart rate variability, tissue

saturation for patients suffering from diminished blood circulation, and the like. In one design, system **10** provides hemodynamic map **100** which shows viable and necrotic tissue areas. If hemodynamic oscillations are detected and shown on hemodynamic map **100**, e.g. indicated at **106** in caption **108**, or shown in FIG. **4**, the tissue is viable. If hemodynamic oscillations are not shown, and therefore not detected by the procedure described above, on hemodynamic map **100**, the tissue is necrotic, e.g., indicated at **108**, FIGS. **1** and **4**.

Hemodynamic map **100**, FIGS. **2** and **4**, preferably has a maximum field of view (FOV) of tissue **16** in predetermined area **18** where tissue viability needs to be determined. In one design, the FOV, e.g., FOV-**104**, FIG. **1**, displayed on display device **102** provides a real-time view of tissue **16** in predetermined area **18** needed for real-time assessment of tissue viability in an objective manner. In one example, FOV-**104** of tissue **16** in predetermined area **18** may be about 10 inches by 10 inches. In other examples, FOV-**104** of tissue **16** in predetermined area **18** may be larger or smaller than 10 inches by 10 inches as needed.

Controller **50**, FIGS. **1** and **2**, is also preferably configured to store data associated with one or more hemodynamic maps **100** created by controller **100** in storage device **110**. Storage device **110** may include any combination of computer-readable media or memory. The computer-readable media or memory may be a computer-readable signal medium or a computer-readable storage medium. A computer-readable storage medium or memory may be, an electronic, magnetic, optical, electromagnetic, infrared, or semiconductor system, apparatus, or device, or any suitable combination of the foregoing. Other examples may include an electrical connection having one or more wires, a portable computer diskette, a hard disk, a random access memory (RAM), a read-only memory (ROM), an erasable programmable read-only memory (EPROM or Flash memory), an optical fiber, a portable compact disc read-only memory (CD-ROM), an optical storage device, a magnetic storage device, or any suitable combination of the foregoing. As disclosed herein, the computer-readable storage medium or memory may be any tangible medium that can contain, or store one or more programs for use by or in connection with one or more processors on a computing device such as a computer, a tablet, a cell phone, a smart device, or similar type device. Controller **50** may also be configured to compress the data associated with the hemodynamic maps.

To reduce and minimize the impact of uncontrolled ambient light changes, system **10** and the method thereof may implement spectral estimation techniques of the ambient illumination to remove uncontrolled ambient light changes. In other designs, system **10** and the method thereof may remove ambient lighting artifacts at the acquisition level by removing temporal changes in ambient illumination measured during programmed periods of non-active tissue illumination.

System **10** also preferably includes user interface **112** coupled to controller **50** electronically or wirelessly which may allow a user of system **10** to visualize and interact with the stored or real-time data. Data may be retrieved from controller **50** and storage device **110** via a data jack or by wireless communication, as known by those skilled in the art. System **10** also includes power supply **116** configured to provide power to one or more light sources **12**, one or more detectors **20**, controller **50**, and/or display device **102**. In one design, power supply **116** may include batteries for portable applications.

In other designs, contactless system **10** and method for assessing tissue viability and other hemodynamic parameters may be a standalone device for operation room, a portable device, or integrated into wearable tools wore by medical personnel.

One example of the method for assessing tissue viability and other hemodynamic parameters includes emitting light at a predetermined wavelength sensitive to hemoglobin concentration associated with spontaneous hemodynamic oscillations at tissue in a predetermined area of a human subject, step **150**, FIG. **6**. The method also includes polarizing the light to a polarized state such that the polarized light in the polarized state diffuses into the tissue in the predetermined area at a predetermined depth such that the polarized light is maintained in the polarized state at the polarized depth, step **152**. The method also includes discriminating the light maintained in the polarized state and at the predetermined depth and generating a plurality of frames of the tissue in the predetermined area at the predetermined depth, step **154**. A plurality of frames are then acquired, step **156**. A region of interest is then selected having the same coordinates for each of the plurality of frames, step **158**. The number of pixels within each region of interest is averaged to create a raw reference signal, step **160**. The raw reference signal is detrended to create a detrended raw reference signal, step **162**. Frequency domain analysis is performed of the detrended raw reference signal, step **168**. A frequency band of interest is identified associated with the spontaneous hemodynamic oscillations, step **170**. An inverse fast Fourier transform (iFFT) is performed within the frequency band of interest to generate a raw reference signal indicative of blood volume oscillations at a selected spontaneous hemodynamic oscillation, step **172**. For each sample of the raw reference signal at a predetermined point in time, the sample is multiplied by each pixel of a frame at the same predetermined point in time to generate a three-dimensional coordinate matrix including a plurality of correlation matrix frames at each predetermined point in time, step **174**. The plurality of correlation matrix frames at each predetermined point in time are added to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillations to assess the viability of tissue in the predetermined area or assess the viability of other hemodynamic parameters, step **176**.

The result is system **10** and the method thereof provides a contactless real-time assessment of tissue viability and other hemodynamic parameters that allows a user to quantitatively assess the tissue health to provide objective metrics to support and guide accurate tissue excision of a burn wound or similar type wound. System **10** and the method thereof allows clinicians to selecting a level of debridement of a burn wound at a desired depth to minimize inflammation and determine the optimal treatment and remove virtually all the necrotic tissue in the burn wound or similar type wound in a time efficient manner. System **10** and the method thereof eliminates the need for intrusive tissue contact and preferably provides for long distance tissue viability assessment monitoring when compared to more conventional invasive imaging systems and methods discussed in the Background section. System **10** and the method thereof may provide opportunities in settings where multi-individual assessment may be extremely difficult or not feasible, such as intensive care units, emergency rooms, or where the condition of the patient may not allow for contact measurements.

One advantage of system **10** and the method thereof relying on spontaneous hemodynamic oscillation measurements discussed above with reference to one or more of FIG.

1-6, rather than absolute concentration measurements of chromophores present in the cardiovascular system, is an optical path length factor approximation is not required by system 10 and the method thereof. This may eliminate the need to rely on estimation errors. System 10 and method thereof, unlike conventional near infrared spectroscopy (NIRS) techniques, preferably does not require absolute concentration retrieval of the chromophores present in the cardiovascular system of tissue 16 of predetermined area 18 of human subject 16. Instead, system 10 and the method thereof preferably utilizes controller 50, one or more light sources 12, and one or more detectors 20. In one example.

For enablement purposes only, the following code portions are provided which can be executed on one or more processor, a computing device, or computer to carry out the primary steps and/or functions of contactless system 10 and method for assessing tissue viability and other hemodynamic parameters discussed above with reference to one or more of FIGS. 1-6. Other equivalent algorithms and code can be designed by a software engineer and/or programmer skilled in the art using the information provided herein.

```
%Acquire image
Frame = get frame (n,m) from camera/sensors etc.
%Determine ROI (region of interest)
maskmother = zeros(n,m) %set to zero a matrix equal to the size of the acquired image
% Set to 1 an area of interest where reference signal will be calculated from
mask_1 = ones (maskmother (n,m) )
%Average pixels within selected ROI:
im = Frame.* mask_1
%Detrend im signal
im = im - im_Trend
%Identify frequency components in im signal by FFT (Fast Fourier Transform)
PSD = FFT (im)
%Extrapolate Reference Signal by performing Inverse Fourier Transform only between frequency range of interest (for example HR, respiration rate etc.).
Discard imaginary part
Ref = Real [FFT-1( PSD(C1<f<C2) )]
%Integrate reference signal and acquired images product over time to obtain hemodynamic map (S):
S = sumt (Ref.*Frame)
```

Although specific features of the invention are shown in some drawings and not in others, this is for convenience only as each feature may be combined with any or all of the other features in accordance with the invention. The words “including”, “comprising”, “having”, and “with” as used herein are to be interpreted broadly and comprehensively and are not limited to any physical interconnection. Moreover, any embodiments disclosed in the subject application are not to be taken as the only possible embodiments.

In addition, any amendment presented during the prosecution of the patent application for this patent is not a disclaimer of any claim element presented in the application as filed: those skilled in the art cannot reasonably be expected to draft a claim that would literally encompass all possible equivalents, many equivalents will be unforeseeable at the time of the amendment and are beyond a fair interpretation of what is to be surrendered (if anything), the rationale underlying the amendment may bear no more than a tangential relation to many equivalents, and/or there are many other reasons the applicants cannot be expected to describe certain insubstantial substitutes for any claim element amended.

Other embodiments will occur to those skilled in the art and are within the following claims.

What is claimed is:

1. A contactless system for assessing tissue viability and other hemodynamic parameters, the system comprising:
 - one or more light sources configured to emit lights at a predetermined wavelength sensitive to hemoglobin concentration associated with spontaneous hemodynamic oscillations at tissue in a predetermined area of a human subject;
 - one or more polarizers each coupled to one or more of the one or more light sources configured to polarize the light to a polarized state such that the polarized light in the polarized state diffuses into the tissue in the predetermined area at a predetermined depth and the polarized light is maintained in the polarized state at the predetermined depth;
 - one or more detectors each including a detector polarizer coupled thereto configured to discriminate the light maintained in the polarized state and at the predetermined depth and configured to generate a plurality of frames of the tissue in the predetermined area at the predetermined depth; and
 - a controller coupled to the one or more light sources and the one or more detectors, the controller configured to:

acquire the plurality of frames,
 select a region of interest having the same coordinates for each of the plurality of frames,
 average the number of pixels within each region of interest to create a raw reference signal,
 detrend the raw reference signal to create a detrended raw reference signal,
 perform frequency domain analysis of the detrended raw reference signal,
 identify a frequency band of interest associated with the spontaneous hemodynamic oscillations,
 perform an inverse fast Fourier transform within the frequency band of interest to generate a reference signal indicative of blood volume oscillations at a selected spontaneous hemodynamic oscillation,
 for each sample of the reference signal at a predetermined point in time, multiply the sample by each pixel of a frame at the same predetermined point in time to generate a three-dimensional coordinate matrix including a plurality of correlation matrix frames at each predetermined point in time, and
 add the plurality of correlation matrix frames at each predetermined point in time to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation to assess the viability of the tissue in the predetermined area.

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2. The system of claim 1 in which the spontaneous hemodynamic oscillations have a frequency in the range of 0.05 Hz to about 1.5 Hz.

3. The system of claim 1 in which the predetermined wavelength is in the range of about 500 nm to about 1,000 nm.

4. The system of claim 1 in which the predetermined depth is in the range of about 0.1 mm to about 0.5 mm.

5. The system of claim 1 in which the other hemodynamic parameters include one or more of: heart rate, resting heart rate, heart rate variability, and tissue saturation for patients suffering from diminished blood circulation.

6. The system of claim 1 in which the one or more detectors include a CCD camera.

7. The system of claim 1 in which the one or more detectors include a CMOS camera.

8. The system of claim 1 in which the predetermined area includes a burn area of the human subject.

9. The system of claim 1 in which the predetermined area includes a wound area of a human subject.

10. The system of claim 1 further including a light filtering lens coupled to one or more light sources.

11. A contactless method for assessing tissue viability and other hemodynamic parameters, the method comprising:

emitting light at a predetermined wavelength sensitive to hemoglobin concentration associated with spontaneous hemodynamic oscillations at tissue in a predetermined area of a human subject;

polarizing the light to a polarized state such that the polarized light in the polarized state diffuses into the tissue in the predetermined area at a predetermined depth and the polarized light is maintained in the polarized state at the polarized depth;

discriminating the light maintained in the polarized state and at the predetermined depth and generating a plurality of frames of the tissue in the predetermined area at the predetermined depth;

acquiring the plurality of frames;

selecting a region of interest having the same coordinates for each of the plurality of frames;

averaging the number of pixels within each region of interest to create a raw reference signal;

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detrending the raw reference signal to create a detrended raw reference signal;

performing frequency domain analysis of the detrended raw reference signal;

identifying a frequency band of interest associated with the spontaneous hemodynamic oscillations;

performing an inverse fast Fourier transform within the frequency band of interest to generate a reference signal indicative of blood volume oscillations at a selected spontaneous hemodynamic oscillation;

for each sample of the reference signal at a predetermined point in time, multiplying the sample by each pixel of a frame at the same predetermined point in time to generate a three-dimensional coordinate matrix including a plurality of correlation matrix frames at each predetermined point in time; and

adding the plurality of correlation matrix frames at each predetermined point in time to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation to assess the viability of the tissue in the predetermined area.

12. The method of claim 11 in which adding the plurality of correlation matrix frames at each predetermined point in time to generate a two-dimensional hemodynamic map indicative of the strength of the spontaneous hemodynamic oscillation assess the viability of other hemodynamic parameters including one or more of: heart rate, resting heart rate, heart rate variability, and tissue saturation for patients suffering from diminished blood circulation.

13. The method of claim 11 in which the spontaneous hemodynamic oscillations have a frequency in the range of 0.05 Hz to about 1.5 Hz.

14. The method of claim 11 in which the predetermined wavelength is in the range of about 500 nm to about 1,000 nm.

15. The method of claim 11 in which the predetermined depth is in the range of about 0.1 mm to about 0.5 mm.

16. The method of claim 11 in which the predetermined area includes a burn area of the human subject.

17. The method of claim 11 in which the predetermined area includes a wound area of a human subject.

* * * * *

专利名称(译)	用于评估组织活力和其他血液动力学参数的非接触式系统和方法		
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[标]发明人	PIERRO MICHELE		
发明人	PIERRO, MICHELE QUINN, KYLE WOESSNER, ALAN		
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摘要(译)

用于评估组织生存力和其他血液动力学参数的非接触式系统包括一个或多个光源，该光源被配置为以预定波长发射光，该波长对与人类受试者预定区域中的组织的自发性血液动力学振荡相关的血红蛋白浓度敏感。一个或多个偏振器各自耦合至一个或多个光源中的一个或多个，并且被配置为将光偏振至偏振状态，使得处于偏振状态的偏振光以预定深度扩散到预定区域中的组织中。偏振光在预定深度保持偏振状态。一个或多个探测器，每个探测器包括耦合到其上的探测器偏振器，该探测器被配置为区分保持在偏振状态和预定深度的光，并被配置为在预定区域中以预定深度产生组织的多个帧。控制器耦合到一个或多个光源和一个或多个检测器。控制器被配置为：获取多个帧，为多个帧中的每个选择具有相同坐标的关注区域，平均每个关注区域内的像素数以创建原始参考信号，对原始参考进行去趋势化信号以创建去趋势的原始参考信号，对去趋势的原始参考信号进行频域分析，识别与自发性血液动力学振荡相关的目标频带，并在目标频带内执行快速傅里叶逆变换以生成参考表示在选定的自发血液动力学振荡时血容量振荡的信号。对于在预定时间点的参考信号的每个样本，控制器将样本与相同预定时间点的帧的每个像素相乘以生成三维坐标在每个预定时间点包括多个相关矩阵帧的矩阵。控制器在每个预定的时间点添加多个相关矩阵帧，以产生二维血液动力学图，该二维血液动力学图指示自发的血液动力学振荡的强度，以评估在预定区域中组织的生存力。

