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(54) **HEALTH MONITORING SYSTEMS AND METHODS**

(71) Applicant: **RHYTHM DIAGNOSTIC SYSTEMS, INC.**, San Francisco, CA (US)

(72) Inventors: **George Stefan Golda**, El Granada, CA (US); **Daniel Van Zandt Moyer**, Menlo Park, CA (US); **Mark P. Marriott**, Palo Alto, CA (US); **Sam Eletr**, Paris (FR); **Bruce O'Neil**, San Francisco, CA (US)

(73) Assignee: **RHYTHM DIAGNOSTIC SYSTEMS, INC.**, San Francisco, CA (US)

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*Primary Examiner* — William Thomson

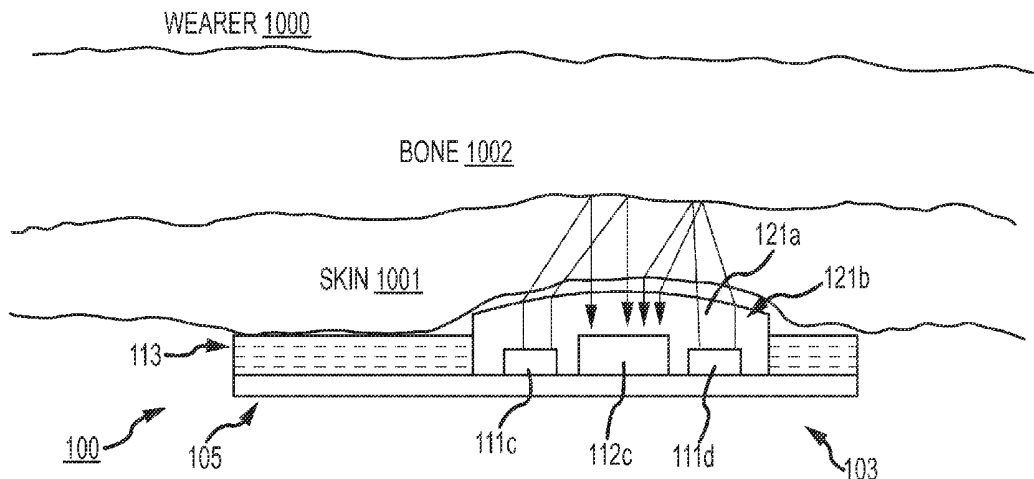
*Assistant Examiner* — Shirley Jian

(74) *Attorney, Agent, or Firm* — Peter B. Scull; Hamilton, DeSanctis & Cha LLP

(57) **ABSTRACT**

Systems, methods and devices for reducing noise in health monitoring including monitoring systems, methods and/or devices receiving a health signal and/or having at least one electrode or sensor for health monitoring.

**15 Claims, 22 Drawing Sheets**



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(56)

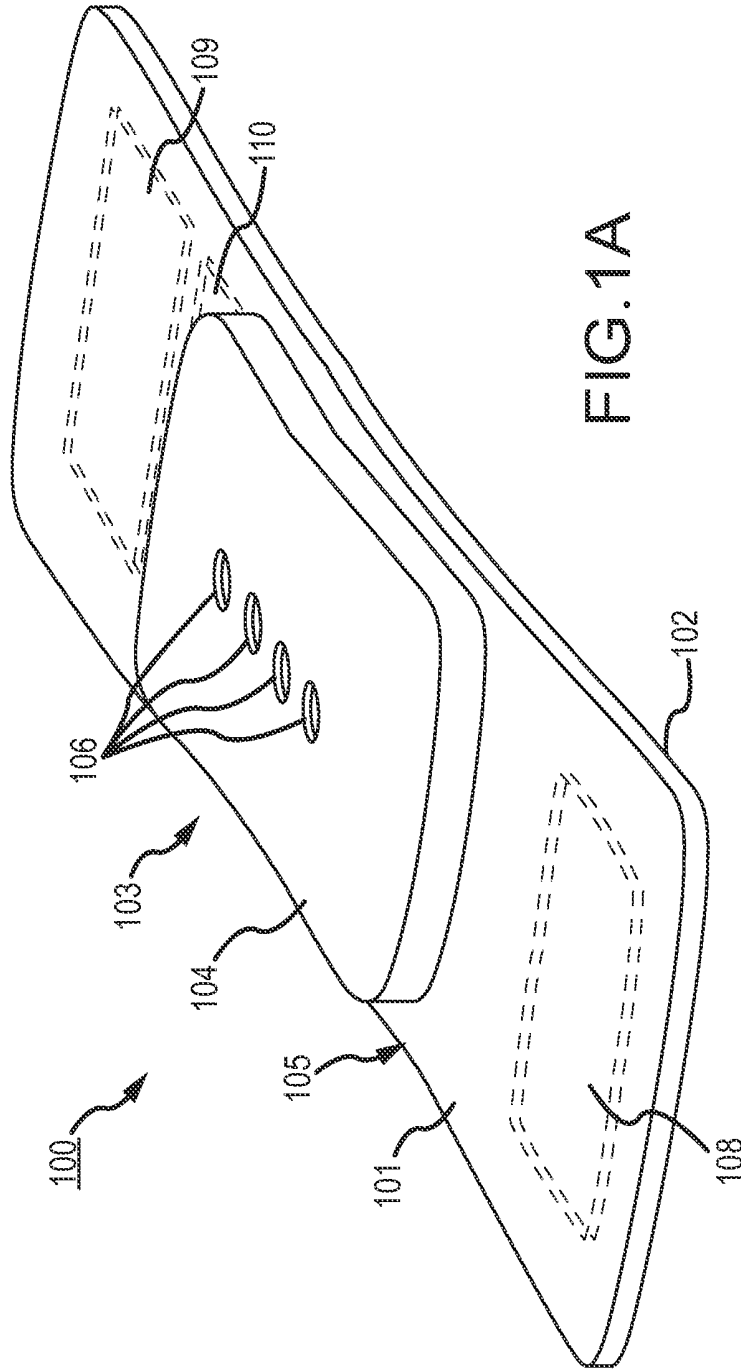
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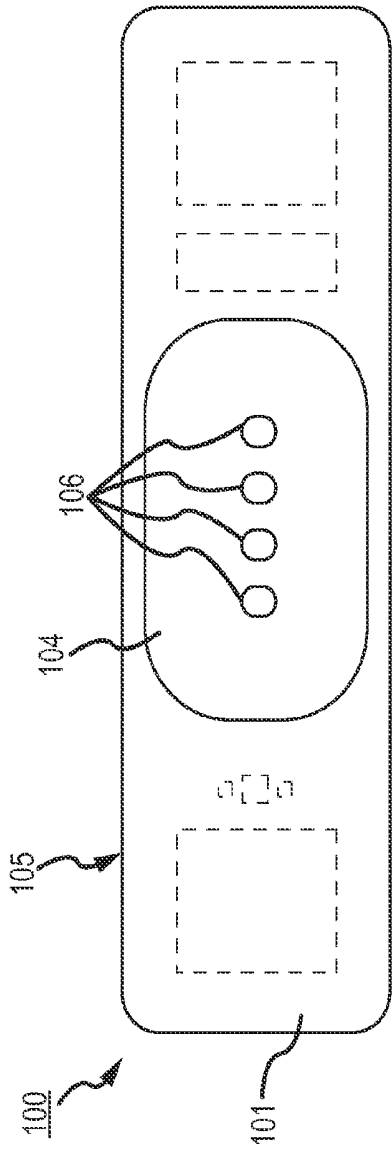


FIG. 1B

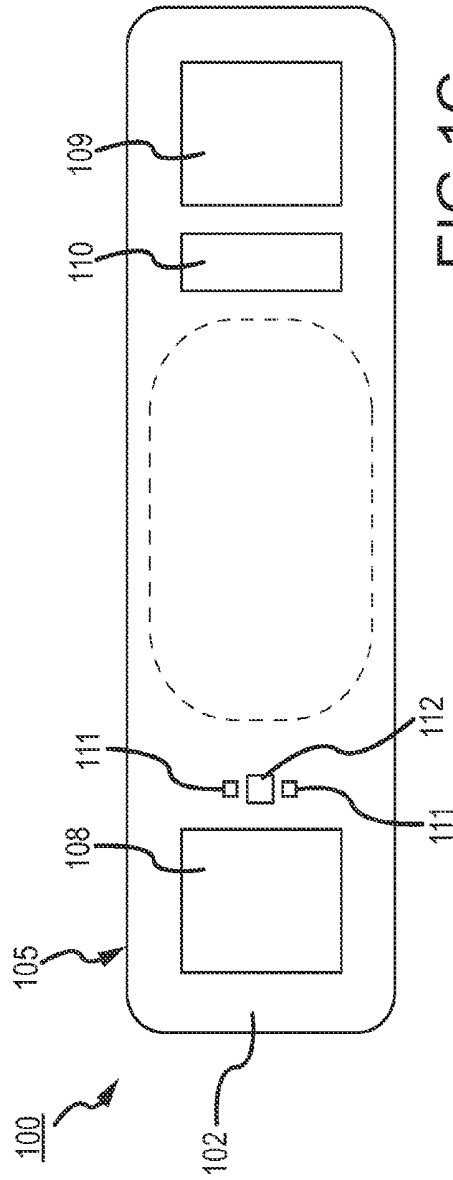


FIG. 1C

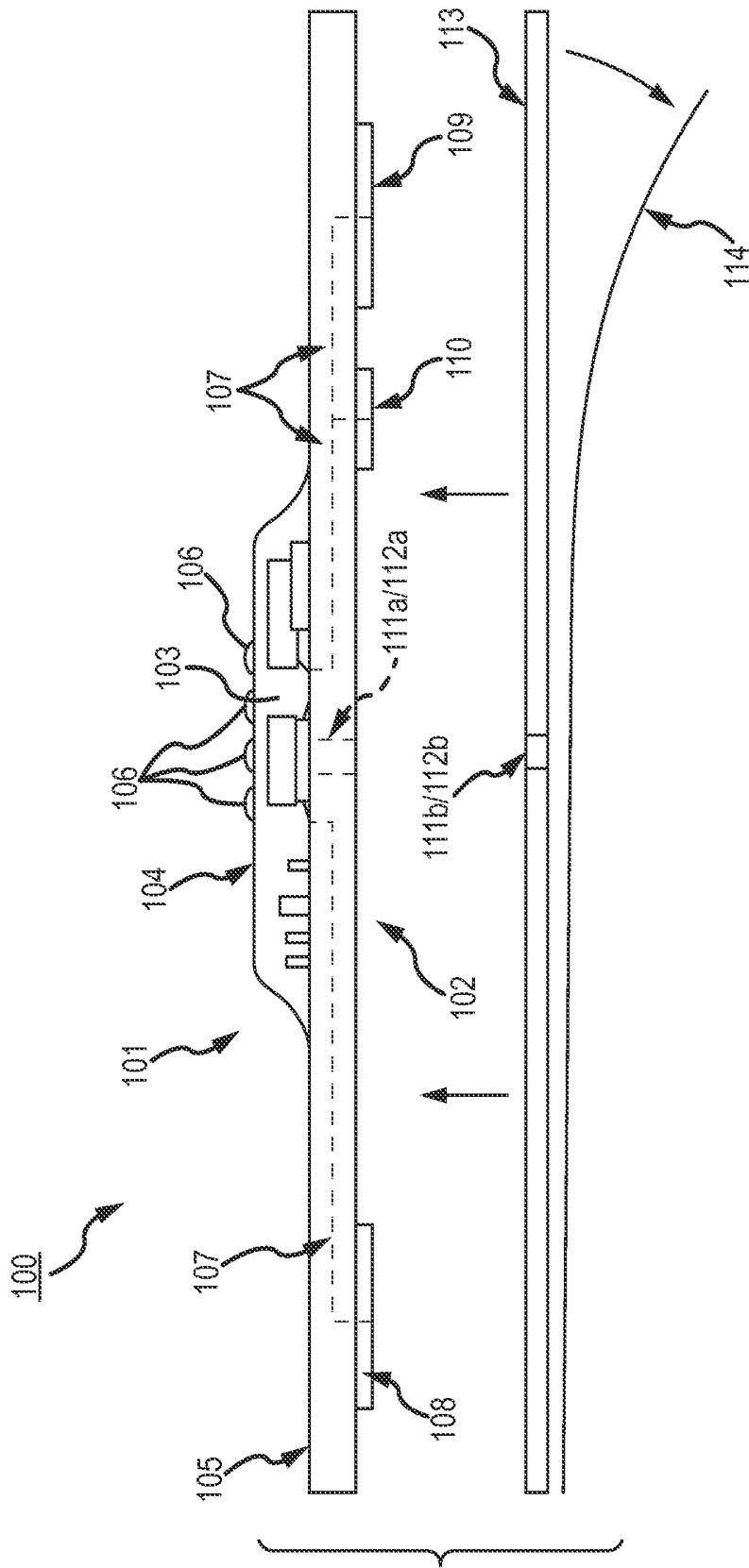


FIG. 1D

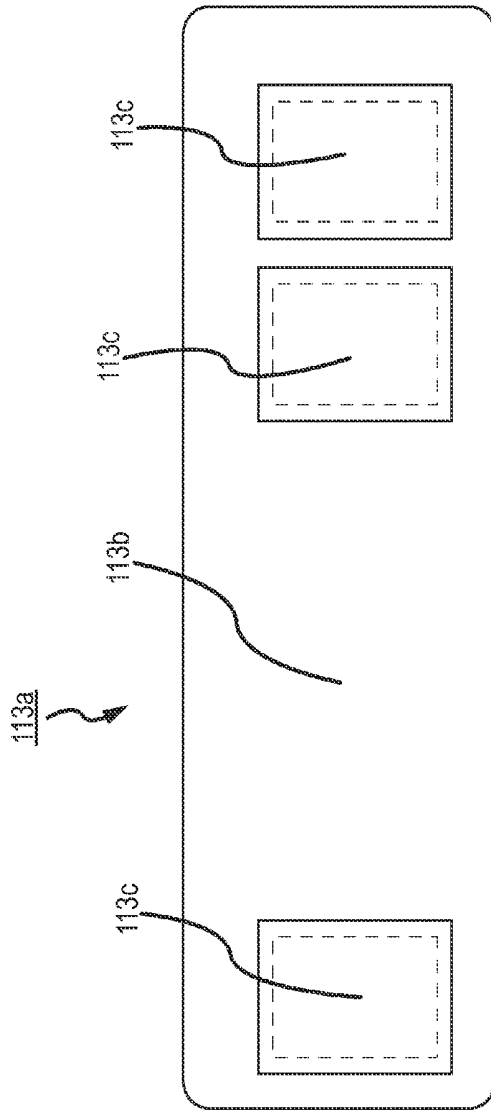


FIG. 1E

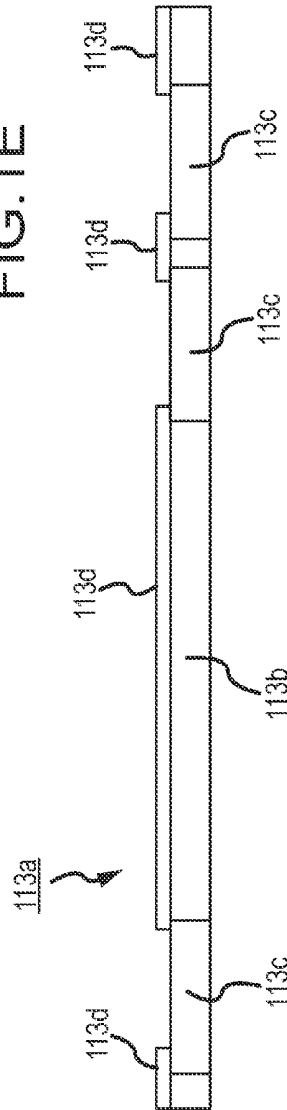


FIG. 1F

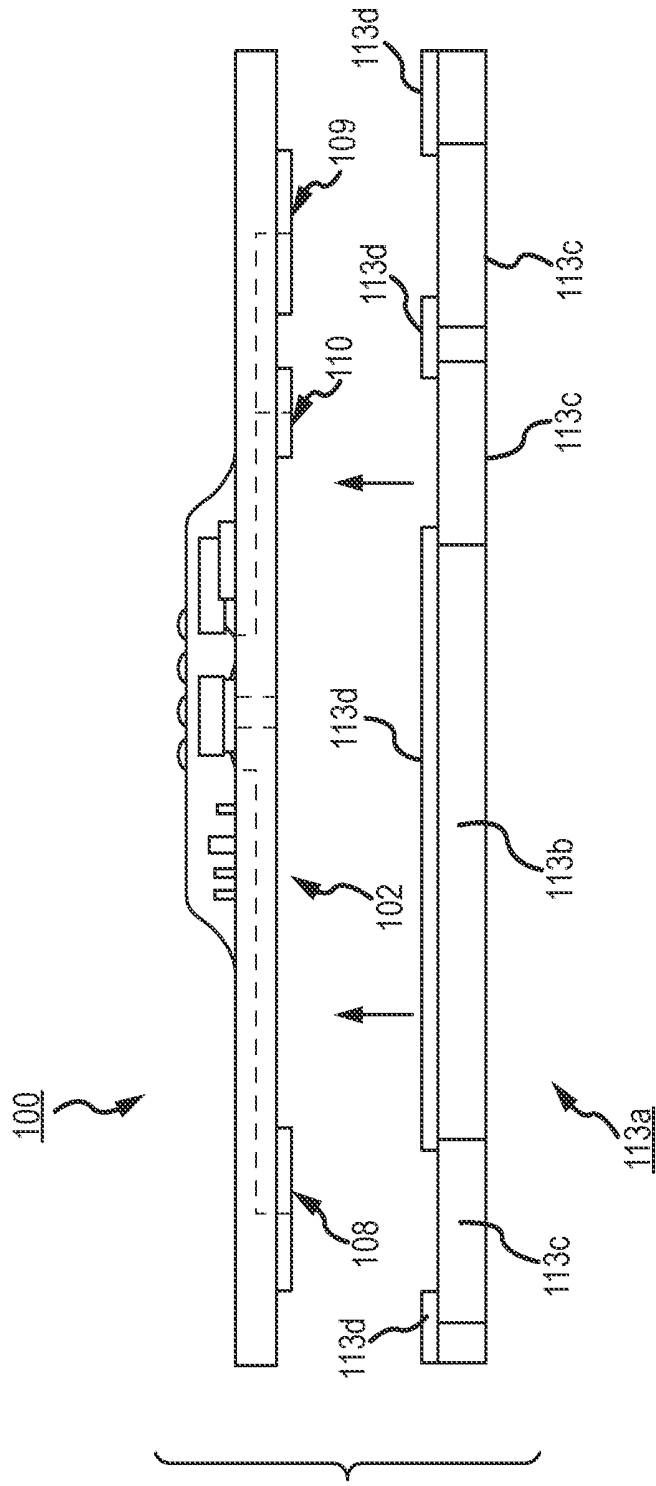
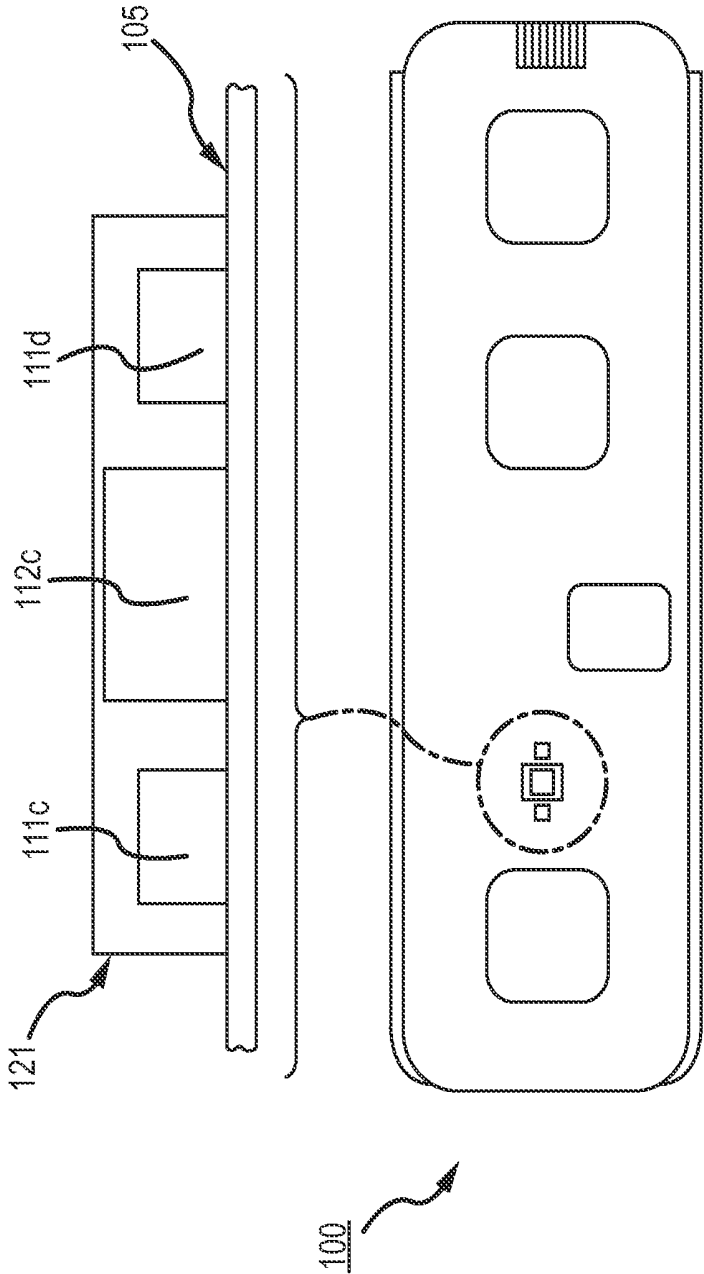


FIG. 1G



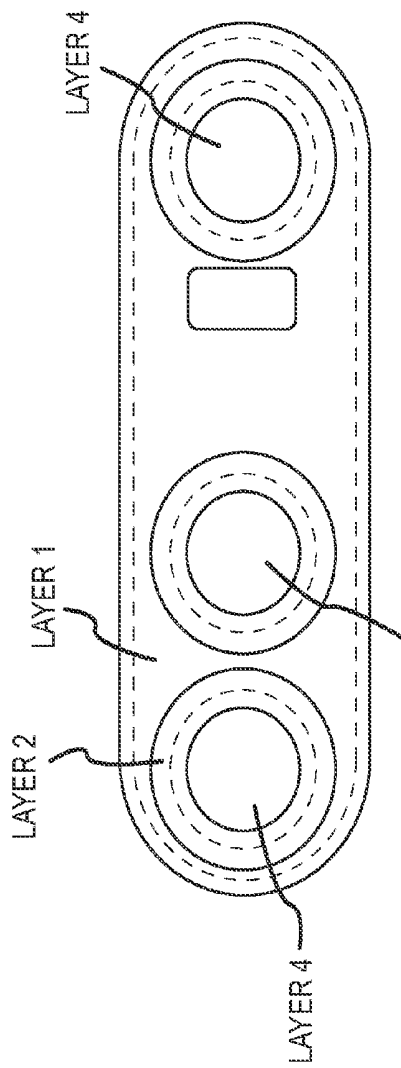


FIG. 11

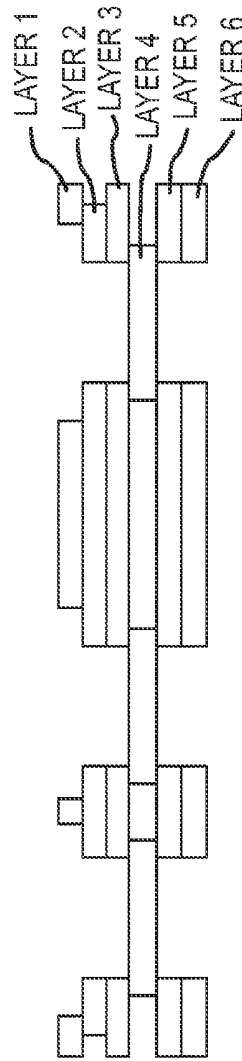


FIG. 1J

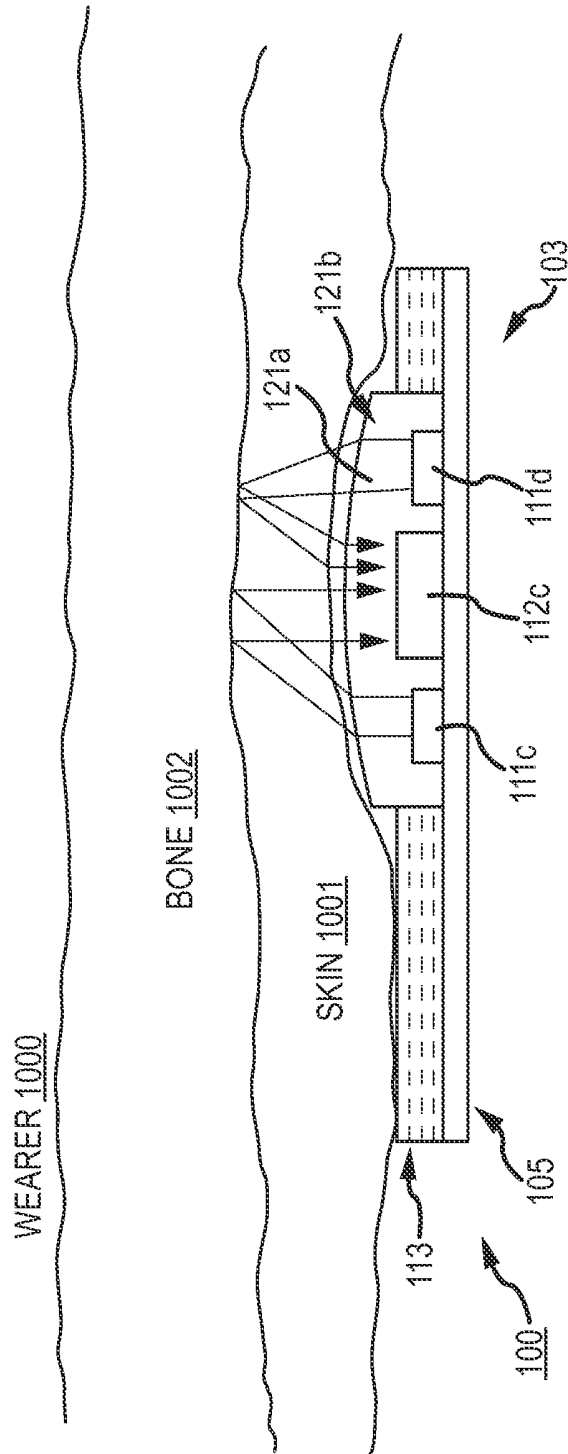


FIG.1K

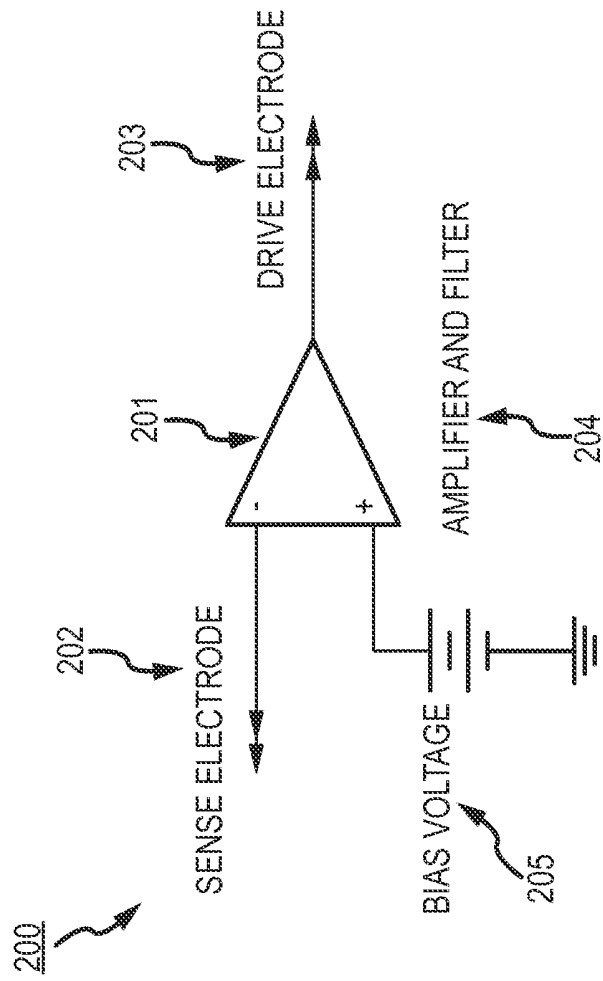


FIG.2A

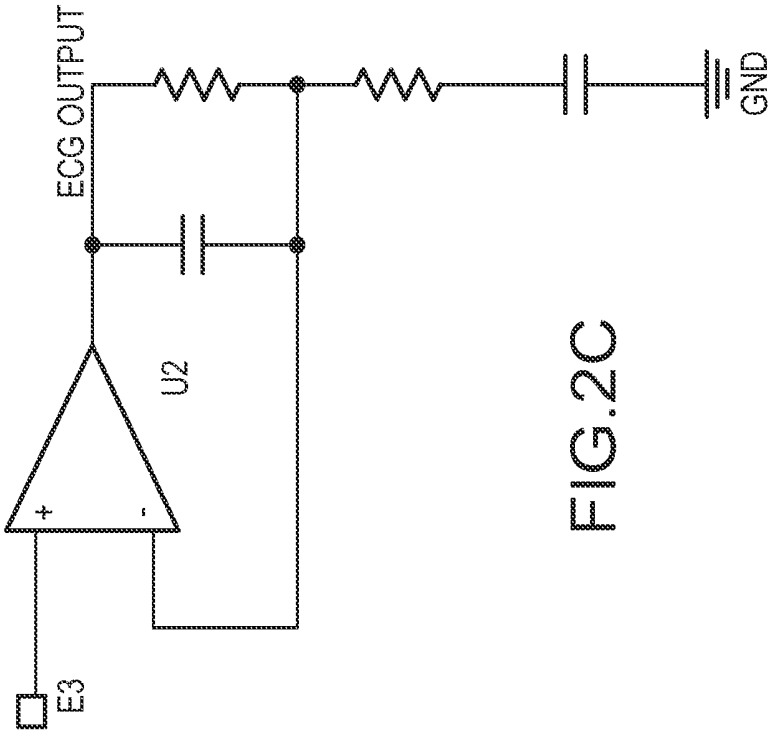


FIG.2C

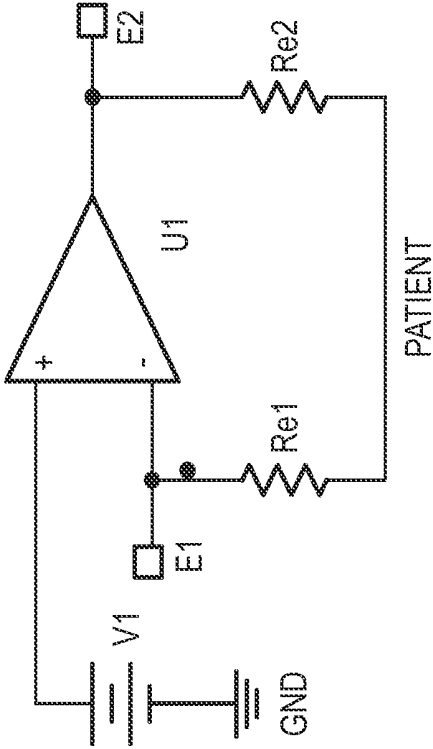


FIG.2B

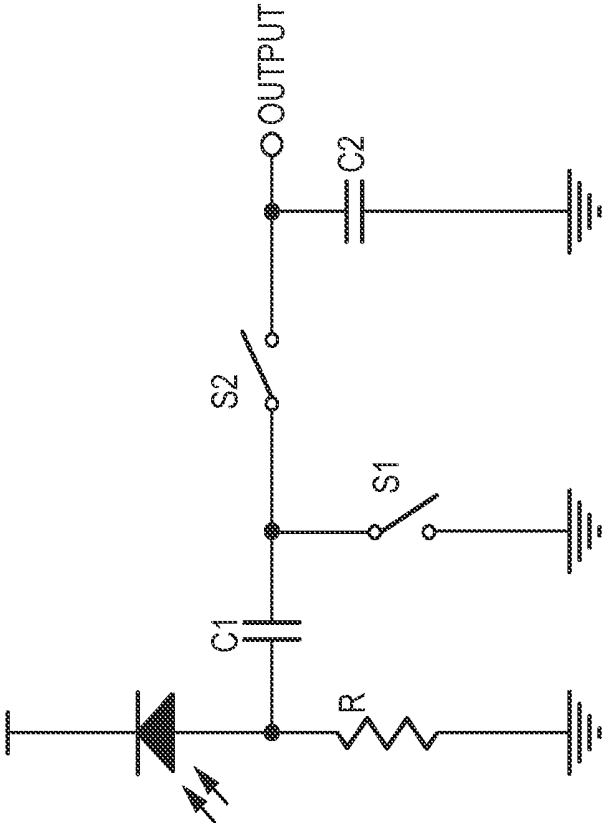


FIG.2D

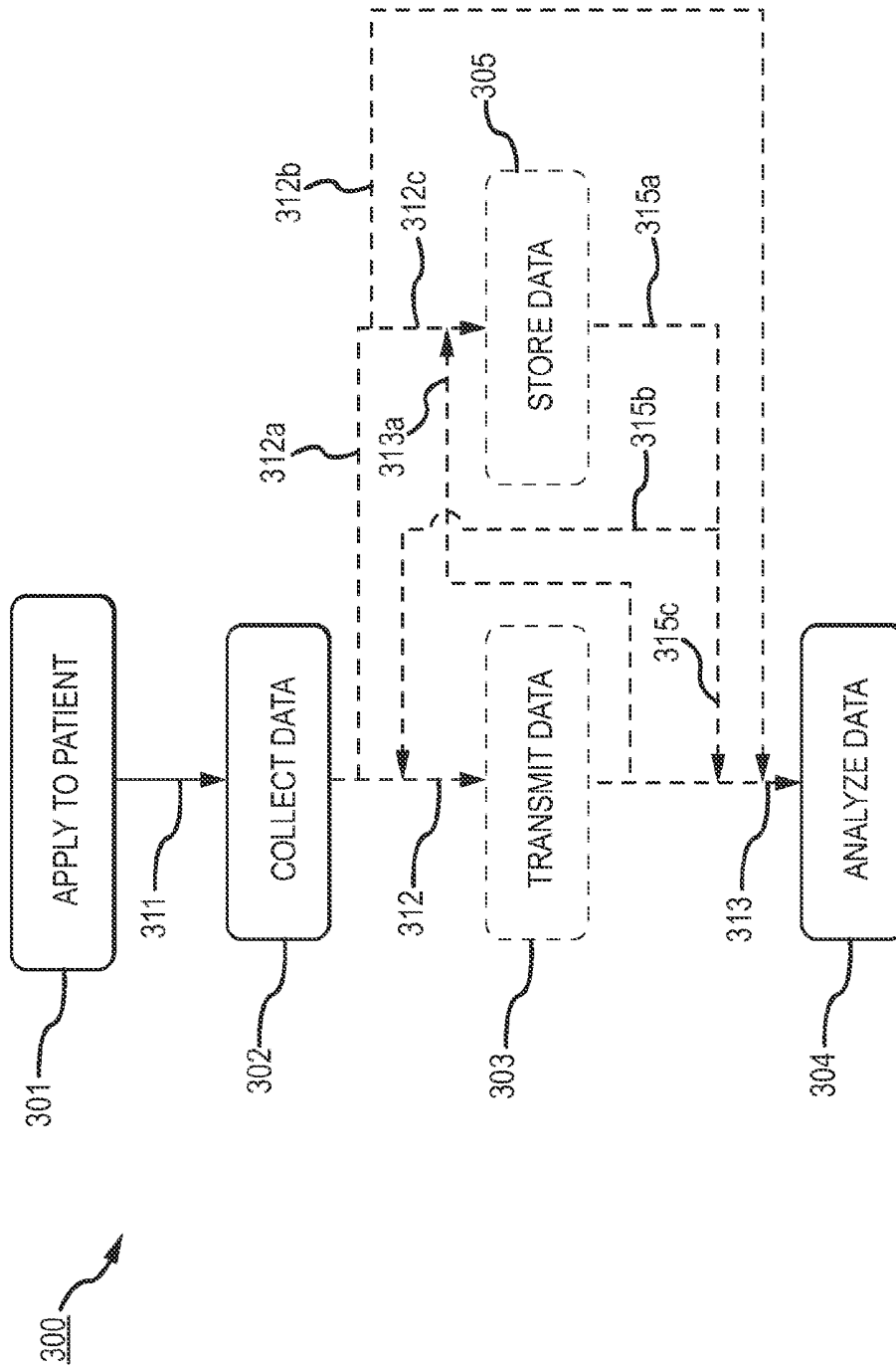


FIG.3

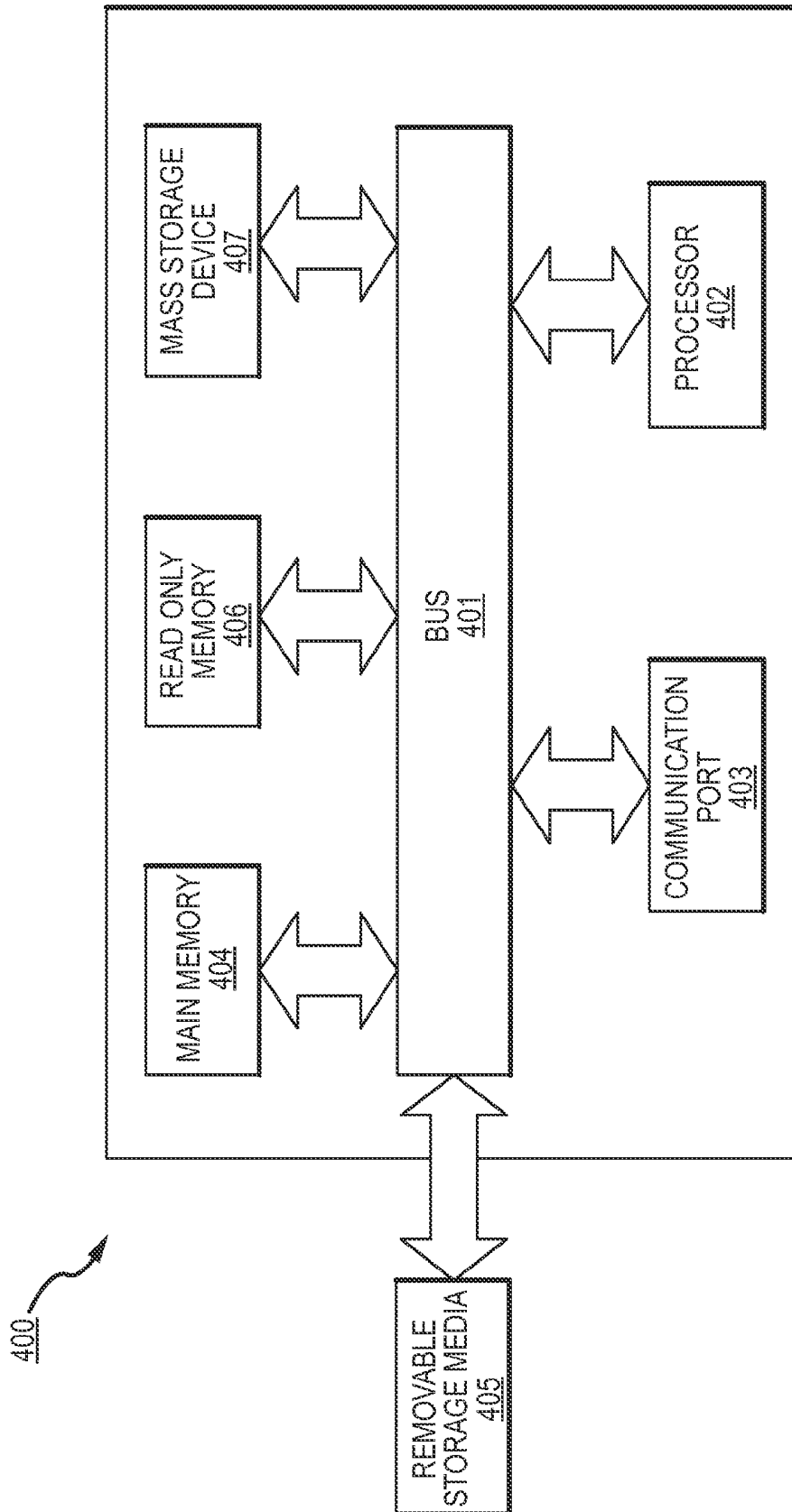


FIG. 4

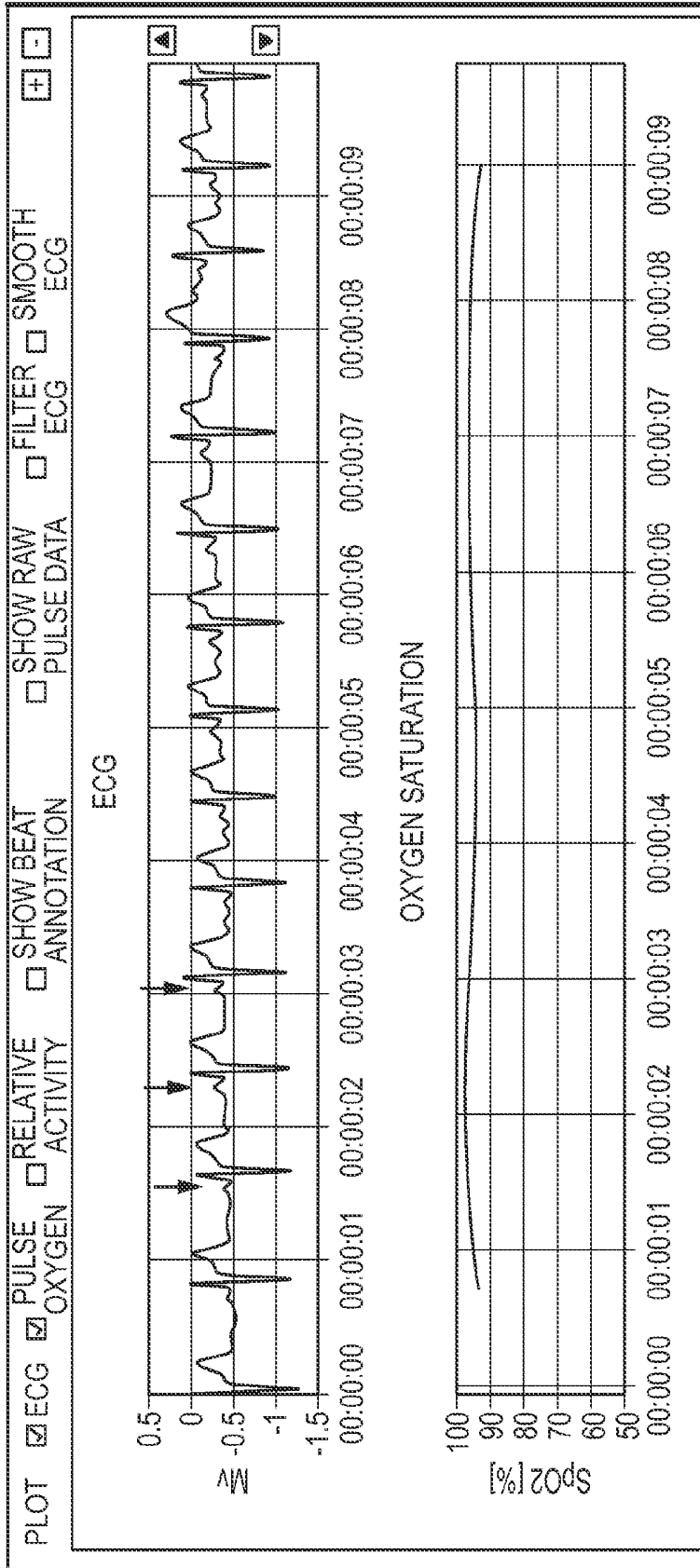


FIG.5A

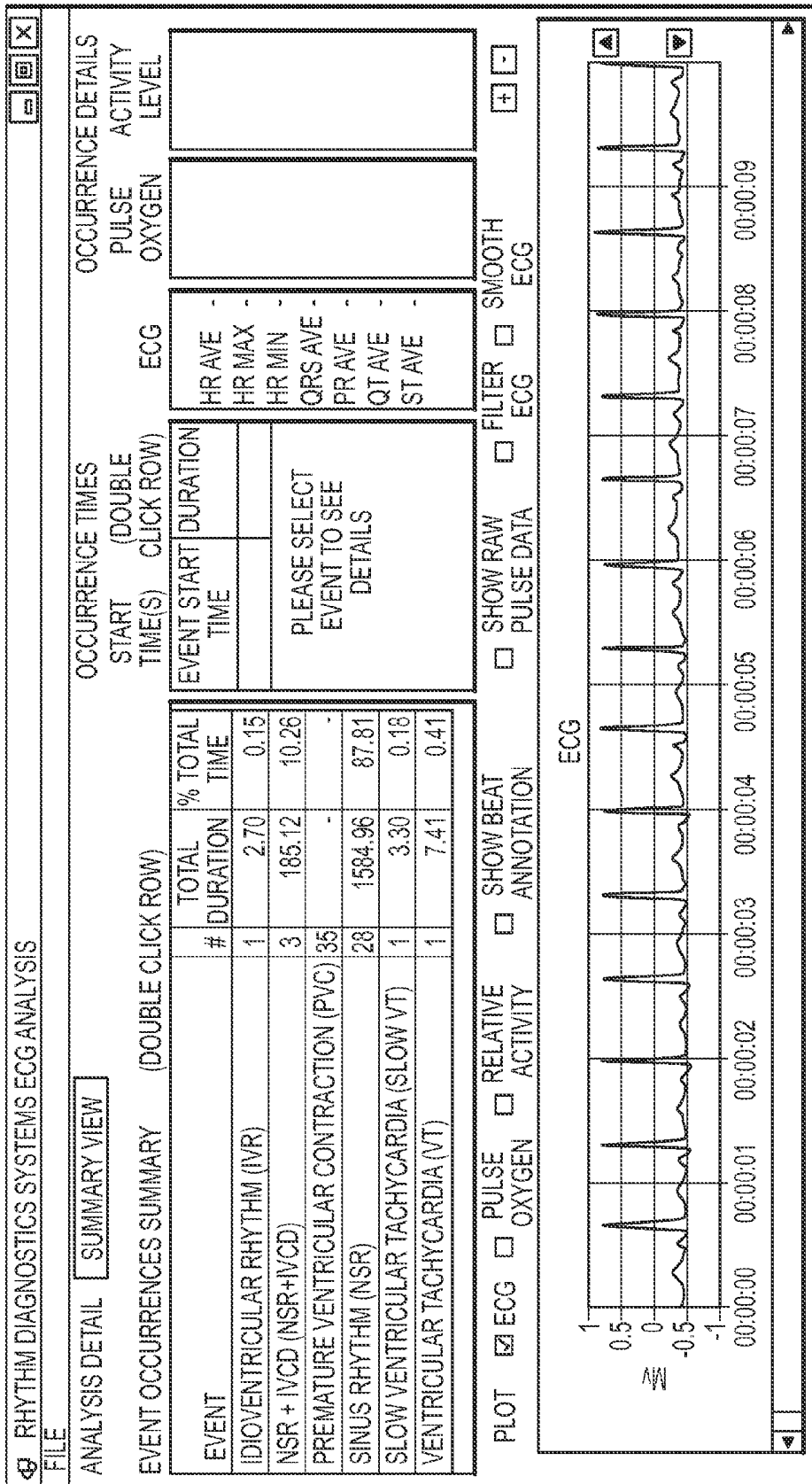


FIG.5B





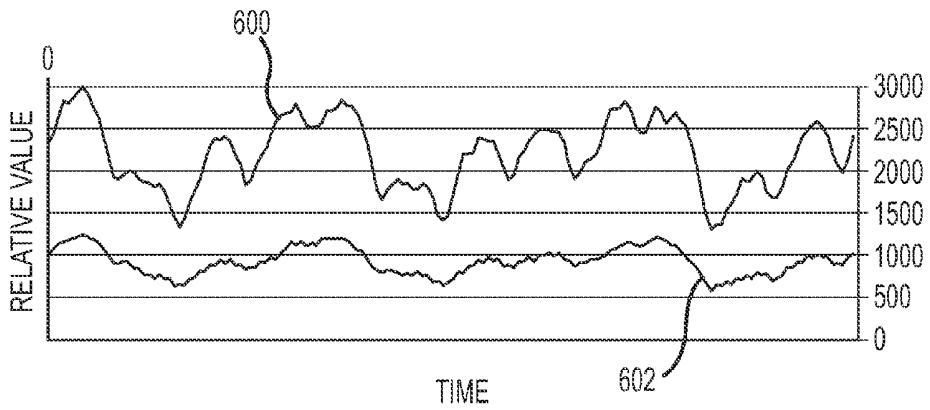


FIG.6A

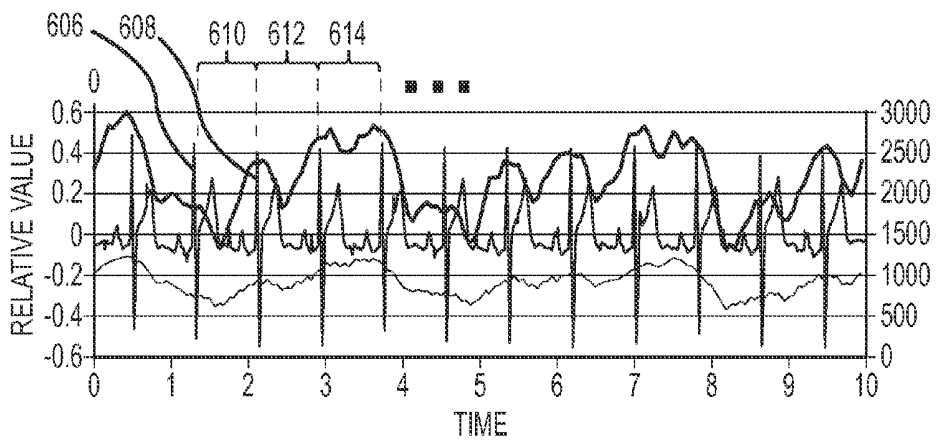


FIG.6B

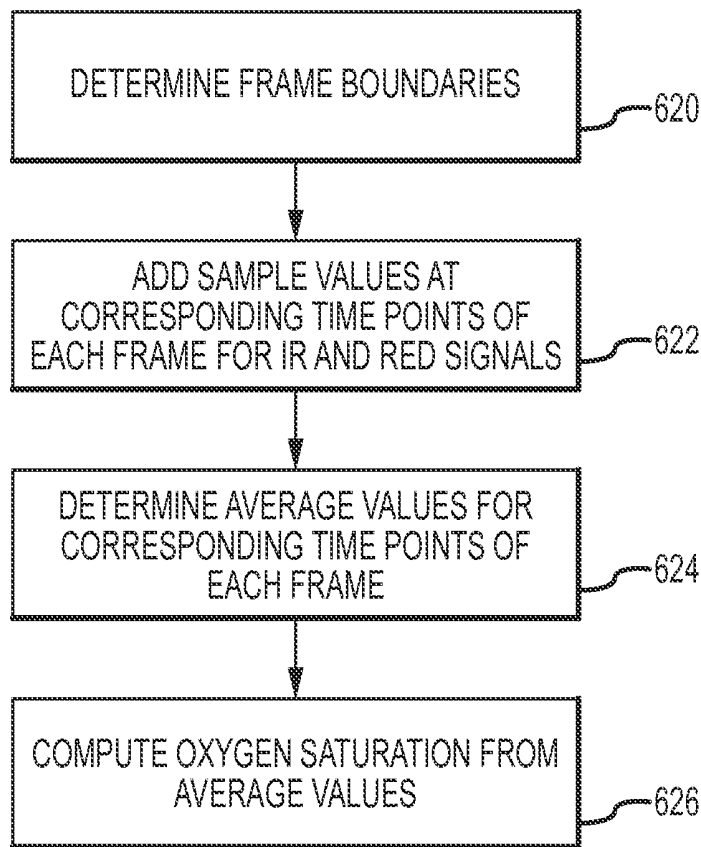


FIG.6C

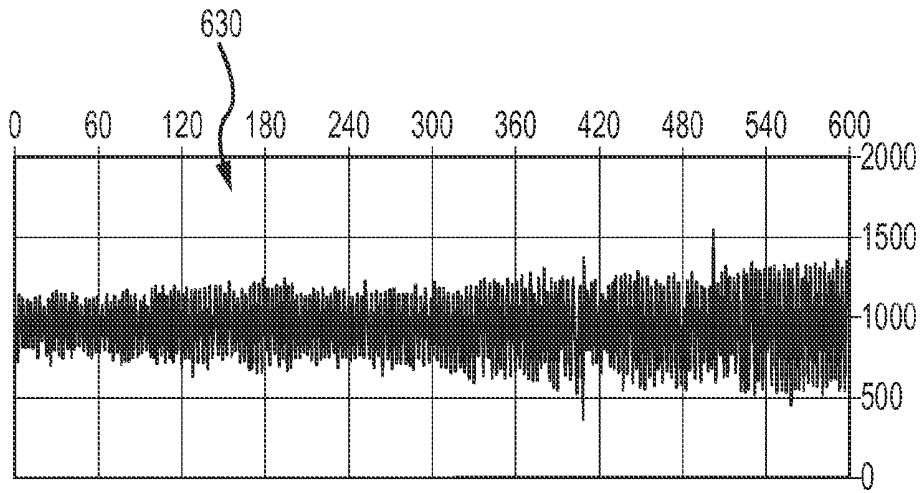


FIG.6D

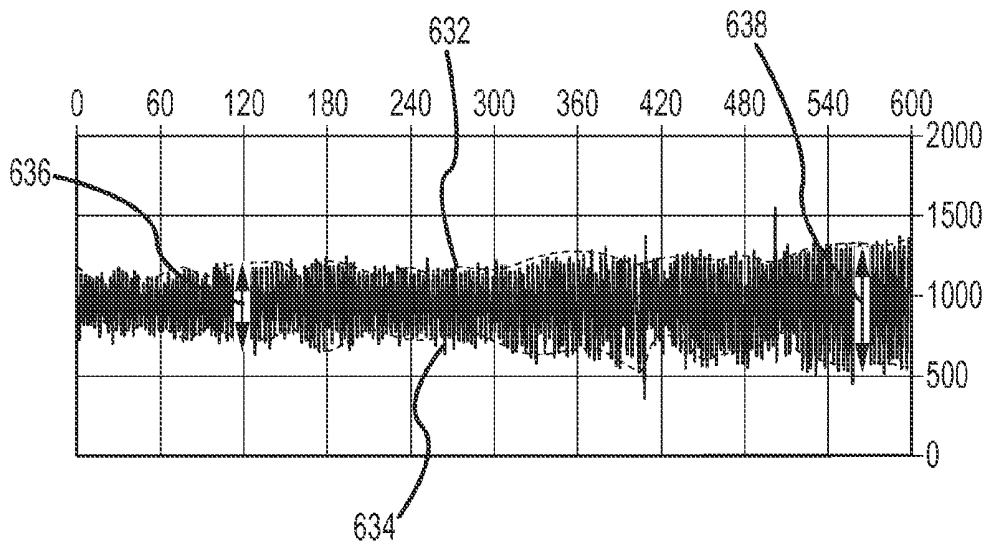
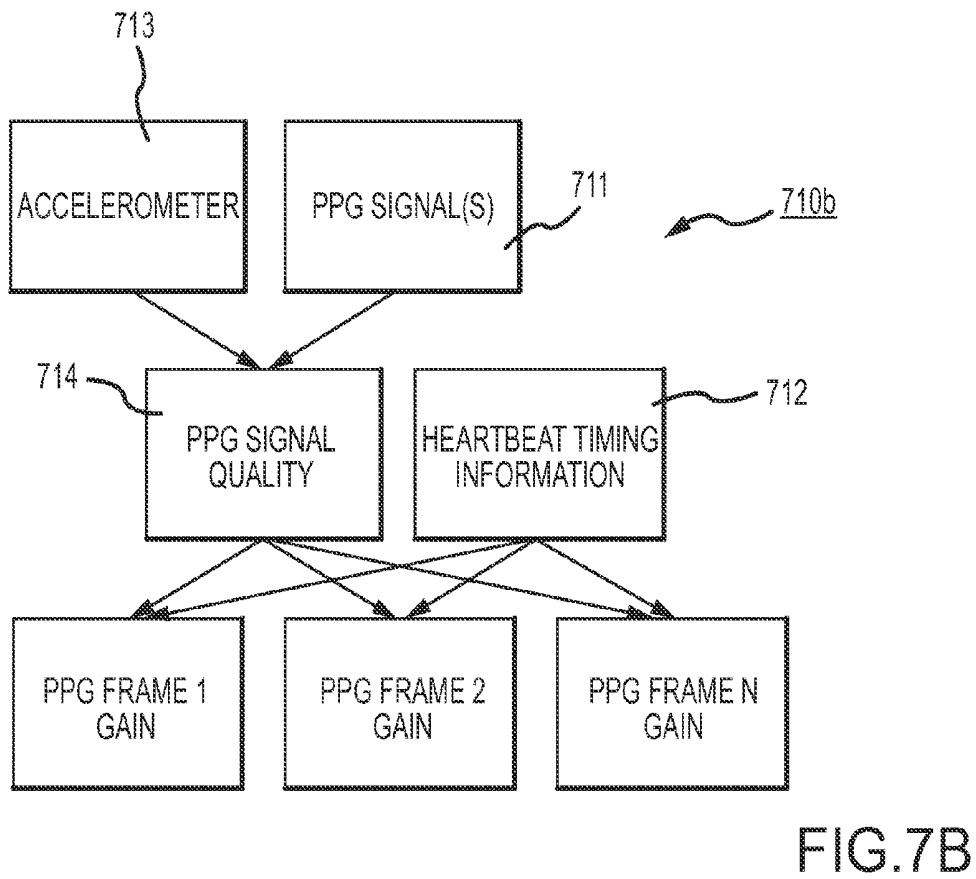
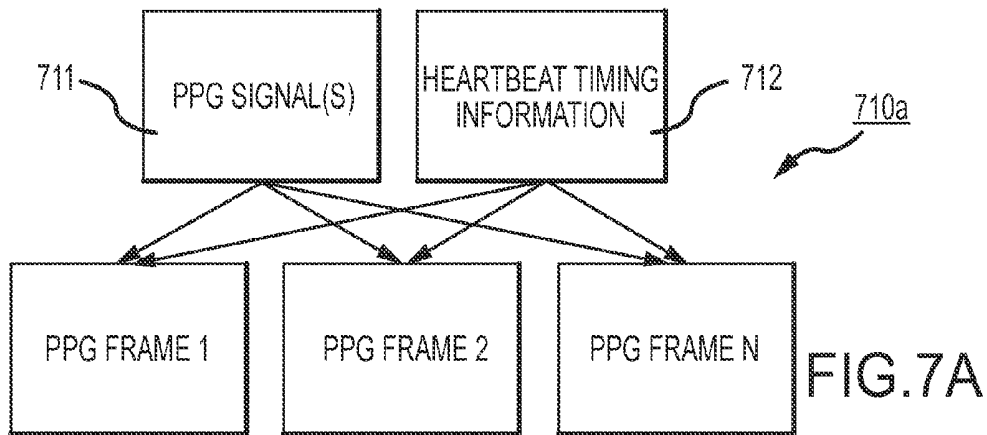


FIG.6E



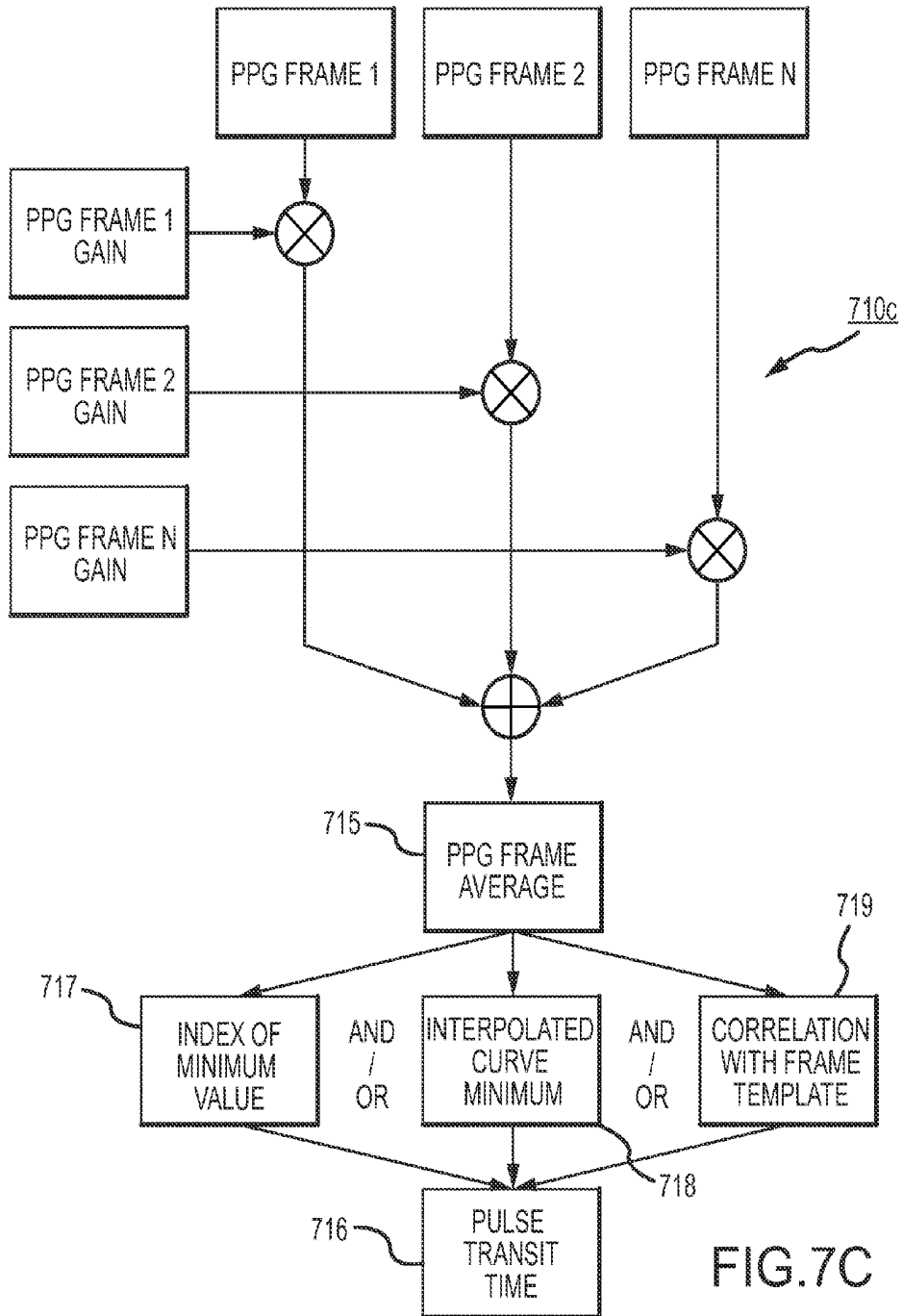


FIG.7C

## HEALTH MONITORING SYSTEMS AND METHODS

### BACKGROUND

Advances in software, electronics, sensor technology and materials science have revolutionized patient monitoring technologies. In particular, many devices and systems are becoming available for a variety of health monitoring applications. However, improvements may yet be desired for health monitoring devices and systems that provide one or more of effective data collection and/or manipulation for parameter determination.

Further alternatives for patients and their physicians may then be developed to include robust and convenient monitors that in some instances may collect and transfer long-term data as well as monitor events in real-time, including multi-variable parameter determination.

### SUMMARY

Described herein are several alternative medical monitoring devices, systems and/or methods for parameter determination, in some instances for long-term sensing and/or recording of cardiac and/or respiratory data of an individual, such as a neonate, athlete, or cardiac patient. A number of alternative implementations and applications are summarized and/or exemplified herein below and throughout this specification.

In one alternative aspect, the developments hereof may include an implementation wherein a health device is configured for monitoring a plurality of physiological parameters of an individual from time-concordant measurements collected by one or a plurality of sensors, including a variety of one or more of, but not limited to, electrodes for measuring ionic potential changes for electrocardiograms (ECGs), a light source and one or more photodetectors, such as LED-photodiode pairs, for optically based oxygen saturation measurements, a temperature sensor, an xyz accelerometer for movement and exertion measurements, and the like. In some implementations, methods and devices of the developments hereof may be used to generate a respiration waveform. Other implementations may include a circuit that mimics a driven right-leg circuit (sometimes referred to herein as “a proxy driven right-leg circuit”) that may permit reduction in common mode noise in a small-footprint device conveniently adhered or having the capacity to be adhered to an individual.

In another alternative aspect hereof, a blood pressure determination may be made from a determination of pulse transit time. The pulse transit time is the time for the cardiac pressure wave to travel from the heart to other locations in the body. Measurements of pulse transit time may then be used to estimate blood pressure. Heart beat timing from ECG or otherwise and photoplethysmogram (aka PPG) signals can be used to generate pulse transit time. Note, such signals may be generated from conventional or other to-be-developed processes and/or devices or systems; or, such signals may be taken from one or more wearable health monitoring devices such as those also described hereinbelow.

In another alternative aspect, the developments hereof may include one or more methods and/or devices for measuring and/or determining oxygen saturation parameters from time concordant pulse oximetry signals and ECG signals. In one implementation, ECG signals may be used to define intervals, or “frames” of pulse oximetry data that are

collected and averaged for determining the constant and main periodic components (e.g., DC and AC components) of the pulse oximetry signals from which, in turn, values for oxygen saturation may be determined. Patient-wearable devices of such implementations with pulse oximetry and ECG sensors may be particularly useful when placed on a patient’s chest for such signal acquisition.

These as well as other alternative and/or additional aspects are exemplified in a number of illustrated alternative and/or additional implementations and applications, some of which are shown in the figures and characterized in the claims section that follows. However, as will be understood by the ordinarily skilled artisan, the above summary and the detailed description below do not describe the entire scope of the inventions hereof and are indeed not intended to describe each illustrated embodiment or every implementation of the present inventions nor provide any limitation on the claims or scope of protection herein set forth below.

### BRIEF DESCRIPTION OF THE DRAWINGS

The drawings include:

FIG. 1, which includes and is defined by sub-part FIGS. 1A-1K, illustrates several alternatives of the present developments, including a variety of isometric, top and bottom plan and elevational views of devices and alternative conductive adhesive structures.

FIG. 2, which includes and is defined by sub-part FIGS. 2A-2D, provides circuit diagrams of alternatives to, in FIGS. 2A-2C, a driven right leg circuit, and in FIG. 2D, pulse oximetry.

FIG. 3 is a flow chart including alternative methods of use.

FIG. 4 illustrates an exemplary computer system or computing resources with which implementations hereof may be utilized.

FIG. 5, which includes and is defined by sub-part FIGS. 5A-5D, provides alternative screenshots of alternative software implementations according hereto.

FIGS. 6A and 6B illustrate features of one embodiment for measuring oxygen saturation using pulse oximetry signals and electrocardiogram signals.

FIG. 6C is a flow chart showing steps of one embodiment for determining oxygen saturation values.

FIGS. 6D and 6E illustrate an embodiment for determining depth of respiration values.

FIGS. 7A, 7B and 7C set forth flow diagrams for alternative methodologies hereof.

### DETAILED DESCRIPTION

While the inventions hereof are amenable to various modifications and alternative forms, specifics thereof have been shown herein by way of example in the drawings and the following description. It should be understood, however, that the intention is not to limit the inventions to the particular embodiments described. The intention is to cover all modifications, equivalents, and alternatives falling within the spirit and scope of the inventions whether described here or otherwise being sufficiently appreciable as included herewithin even if beyond the literal words hereof.

In one aspect, a system hereof may include a device for monitoring physiological parameters such as one or more or all of electrocardiogram (aka ECG or EKG), photoplethysmogram (aka PPG), pulse oximetry, temperature and/or patient acceleration or movement signals.

Moreover, systems hereof may be established to measure and/or process such signals of a patient using or including one or more of the following elements: (a) a circuit, sometimes flexible as in or on or forming a flexible or flex circuit board, embedded in or on a flat elastic substrate or board having a top surface and a bottom surface, the circuit having one or more of (i) at least one sensor mounted in or on or adjacent the bottom surface of the flat elastic substrate, the at least one sensor being capable of electrical or optical communication with the patient, (ii) at least one signal processing module for receiving and/or accepting signals from the at least one sensor in some implementations also providing for transforming such signals for storage as patient data; (iii) at least one memory module for receiving and/or accepting and storing patient data, (iv) at least one data communication module for transferring patient data, stored or otherwise to an external device, and (v) a control module for controlling the timing and operation of the at least one sensor, one or more of the at least one signal processing module, the at least one memory module, the at least one data communication module, and/or the control module capable of receiving commands to implement transfer of patient data by the at least one data communication module and to erase and/or wipe patient data from the at least one memory module; and (b) a conductive adhesive removably attached to the bottom surface of the flat elastic substrate, the conductive adhesive capable of adhering to skin of the patient and of conducting an electrical signal substantially only in a direction perpendicular to the bottom surface of the flat elastic substrate, and/or in some implementations including a conductive portion adjacent the sensor or sensors and a non-conductive portion. In some implementations, the conductive adhesive is an anisotropically conductive adhesive in that it comprises regions of material that conducts current substantially only in a direction perpendicular to the skin (i.e. "z-axis" conduction).

In some implementations, devices hereof will be for comprehensive long-term cardiac monitoring, inter alia. Features of such may include one or more of a Lead I ECG, PPG, pulse oximeter, accelerometer, temperature sensor and/or a button or other indicator for manual patient event marking. Such a device may be adapted to store up to, for example, about two weeks of continuous data (though more or less will also be feasible in alternative implementations), which may in some implementations be downloaded to a clinic or other computer in a short time period, as for one example, in only about 90 seconds (though more or less time will be viable in alternative implementations) via computer connection, whether wireless or wired as in one example by USB or other acceptable data connection. A companion software data analysis package may be adapted to provide automated event capture and/or allow immediate or delayed, local data interpretation.

Intermittent cardiac anomalies are often difficult for physicians to detect and/or diagnose, as they would typically have to occur during a physical examination of the patient. A device hereof may address this problem with what in some implementations may be a continuous or substantially continuous monitoring of one or a number of vital signs.

Some alternative features may include one or more of (i) a driven "Right Leg" circuit with electrodes located only on the chest, (ii) a "z-Axis" or anisotropic conductive adhesive electrode interface that may permit electrical communication only between an electrode and a patient's skin immediately beneath the electrode, (iii) data transmission to and interpretation by a local computer accessible to CCU/ICU

personnel, (iv) a unique combination of hardware that may allow correlation of multiple data sources in time concordance to aid in diagnosis.

In some alternative implementations, devices and systems hereof may provide 1) reusability (in some cases near or greater than about 1000 patients) that may allow recouping cost of the device in just about 10-15 patient tests; 2) one or more of ECG waveform data, inertial exertion sensing, manual event marking, temperature sensing and/or pulse oximetry, any or all of which in time concordance to better detect and analyze arrhythmic events; 3) efficient watertightness or waterproofing (for the patient/wearer to be able to swim while wearing the device); and 4) a comprehensive analysis package for typically immediate, local data interpretation. An alternative device may be adapted to take advantage of flex-circuit technology, to provide a device that is light-weight, thin, durable, and flexible to conform to and move with the patient's skin during patient/wearer movement.

FIGS. 1 and 2 illustrate examples of alternative implementations of devices that may be so adapted.

FIG. 1 shows a device 100 that has a component side or top side 101, patient side or circuit side 102, and one or more inner electrical layer(s), generally identified by the reference 103 and an elongated strip layer 105. The strip layer 105 may have electronics thereon and/or therewithin. FIG. 1A shows isometrically these in what may here be considered a substantially transparent device together with some other elements that may be used herewith. FIG. 1B is more specifically directed to a top side 101 plan view and FIG. 1C to an underside, patient side 102 plan view and FIG. 1D a first elevational, side view.

Many of the electronics hereof may be disposed in the electronics layer or layers 103, and as generally indicated here, the electronics may be encapsulated in a material 104 (see FIGS. 1A, 1B, 1D and 1K for some examples), medical grade silicone, plastic or the like, or potting material, to fix them in operative position on or in or otherwise functionally disposed relative to the elongated strip layer 105. The potting or other material may in many implementations also or alternatively provide a waterproof or watertight or water resistant coverage of the electronics to keep them operative even in water or sweat usage environments. One or more access points, junctions or other functional units 106 may be provided on and/or through any side of the encapsulation material 104 for exterior access and/or communication with the electronics disposed therewithin, or thereunder. FIGS. 1A, 1B and 1D show four such accesses 106 on the top side. These may include high Z data communication ports and/or charging contacts, inter alia. This upper or component side 101 of device 100 may be coated in a silicone compound for protection and/or waterproofing, with only, in some examples, a HS USB connector exposed via one or more ports 106, e.g., for data communication or transfer and/or for charging.

The elongated strip layer 105 may be or may include a circuit or circuit portions such as electrical leads or other inner layer conductors, e.g., leads 107 shown in FIG. 1D, for communication between the electronics 103 and the electrically conductive pads or contacts 108, 109 and 110 described further below (108 and 109 being in some examples, high impedance/high Z silver or copper/silver electrodes for electrocardiograph, ECG, and 110 at times being a reference electrode). In many implementations, the strip layer 105 may be or may include flex circuitry understood to provide acceptable deformation, twisting, bending and the like, and yet retain robust electrical circuitry con-

nections therewithin. Note, though the electronics **103** and electrodes **108**, **109**, **110** are shown attached to layer **105**; on top for electronics **103**, and to the bottom or patient side for electrodes **108**, **109**, **110**; it may be that such elements may be formed in or otherwise disposed within the layer **105**, or at least be relatively indistinguishably disposed in relative operational positions in one or more layers with or on or adjacent layer **105** in practice. Similarly, the leads or traces **107** are shown embedded (by dashed line representation in FIG. 1D); however, these may be on the top or bottom side, though more likely top side to insulate from other skin side electrical communications. If initially top side (or bottom), the traces may be subsequently covered with an insulative encapsulant or like protective cover (not separately shown), in many implementations, a flexible material to maintain a flexible alternative for the entire, or majority of layer **105**.

On the patient side **102**, the ECG electrodes **108**, **109** and **110** may be left exposed for substantially direct patient skin contact (though likely with at least a conductive gel applied therebetween); and/or, in many implementations, the patient side electrodes **108**, **109** and/or **110** may be covered by a conductive adhesive material as will be described below. The electrodes may be plated with or may be a robust high conductive material, as for example, silver/silver chloride for biocompatibility and high signal quality, and in some implementations may be highly robust and, for one non-limiting example, be adapted to withstand over about 1000 alcohol cleaning cycles between patients. Windows or other communication channels or openings **111**, **112** (FIG. 1C) may be provided for a pulse oximeter, for example, for LEDs and a sensor. Such openings **111**, **112** would typically be disposed for optimum light communication to and from the patient skin. An alternative disposition of one or more light conduits **111a/112a** (and **111b/112b**) is shown in a non-limiting example in FIG. 1D more nearly disposed and/or connected to the electronics **103**. A variety of alternative placements may be usable herein/herewith.

In some implementations, sampling of the ambient light (with the LEDs off) may be provided, and then subtracting this from each of the pulse-ox signals in order to cancel out the noise caused by sunlight or other ambient light sources.

The LEDs and photodiode sensor may also and/or alternatively be covered with a layer of silicone to remove any air gap between the sensor/LEDs and the patient skin. Two examples of such are set forth in respective FIGS. 1H and 1K; where a silicone layer or covering **121** is shown covering/surrounding the light conduits and/or sensors/LEDs **111c/111d/112c**. LED **111c** (FIGS. 1H and 1K) might be a Red LED, LED **111d** (FIGS. 1H and 1K) might be an IR (infrared) LED and the device **112c** (FIGS. 1H and 1K) might be a sensor. This may reduce the light lost to reflection off the skin, and thereby greatly increase the signal and reduce the noise caused by motion of the skin relative to the sensor. In some implementations this silicone might be referred to as a light pipe and in some situations may be clear, colorless, and/or medical grade silicone. As described further below, the silicone layer or covering **121** may also/alternatively be referred to as a light pipe or lens **121/121a/121b** herein inasmuch as how it may be involved in light transmitting or to be transmitted therethrough, whether upon emission or received upon reflection or both.

In one or more implementations, a lens **121/121a/121b** hereof may be made from a medical grade silicone that is one or more of clear, colorless, soft, low durometer. Exemplars of such specialized silicones that may be used herewith are known as "tacky gels" (several suppliers), and typically have very high-tack adhesives, preferably embedded on both

sides. A low durometer silicone combined with double-sided adhesive on the tacky gel allows the construction of a lens **121/121a/121b** that may be both conforming to the electronic sensors and skin, as well as, in some implementations, exhibiting properties of motion artifact reduction by limiting movement between the skin-lens-sensor interface. A lens according hereto may also/alternatively be specially shaped such that it can be trapped between layers of the composite adhesive strip (see e.g., alternatives of FIGS. 1D, 1G and 1I and 1J), and in some implementations, with a raised portion the size of the opening, often a rectangular opening, in the adhesive strip that allows the lens to protrude slightly on the patient side of the adhesive strip (see further detail relative to FIG. 1K, described below).

In FIG. 1K an implementation of a further alternative silicone covering or encapsulant **121a** for the LEDs and sensor **111c/111d/112c**, may include a convex lens at or adjacent the covering external surface **121b**. In many implementations, the external surface and lens are one and the same and/or the lens may be defined by the surface **121b** of the encapsulant material **121a**. What this provides is a structure and method for interfacing pulse oximetry LED emitters **111c/111d** and one or more photodiode sensors **112c** with the skin surface, whether chest or forehead (e.g., infant or neonate) or otherwise mounted on the patient or user body.

More particularly, as otherwise described herein, a system and/or device **100** hereof may utilize one or multiple LED emitters **111c/111d** of selected wavelengths and one or multiple photodiode sensors. However, in order to maximize coupling of the LED/sensor combination to the skin **1001** of a wearer **1000**, a lens **121b** comprised of optically clear, medical grade silicone may be molded onto or molded such that it may be later attached in covering relationship on the LED/sensor combination **111c/111d/112c**. In many implementations, the lens **121b** may be partially spherical or perhaps hemispherical in nature, though it need not be. Curvature of other shapes may be useful as well. Curvature reduces loss of skin contact when the device **100** may be moved, whether by wearer motion or otherwise. I.e., motion of the wearer **1000** or the device **100** relative to the wearer **1000** can result in a quasi-rolling contact of the lens on and in relation to the skin **1001**. Better maintained skin contact means better data acquisition without interruption and/or with reduced noise.

Moreover, related to the function of maintaining contact is the light piping effect that may be achieved when LEDs and sensors, even of different heights are communicating without air gap interruption through the light pipe of the encapsulant material **121a**. With no air gap from emitter to and through the light pipe **121a** and with curved surface substantially constant contact with the skin, there is thus no air gap interruption in transmission into and through and reflected back on return from within the skin and back to the sensor via the same light pipe material **121a** (transmission and reflection both referring to light travel). This reduces inefficiencies caused by light wave scattering at air gap interfaces (air gaps allow for light to bounce off the skin or other surface). I.e., encapsulation of the LEDs and the sensor; provides no air-gap and a light pipe effect to and the curved surface provides high quality low scattering transmission into the skin and reception of reflection from the skin and bone. The light pipe and curved lens surface maintain uninterrupted contact skin and lens reduces lost signals due skin reflection. The signal to noise ratio goes down and data acquisition goes up in quality.

Such a lens **121b** may thus serve one or multiple purposes, including in some instances, inter alia: 1) providing a “light-pipe” effect to assure equal or otherwise high quality coupling of the different height LEDs and sensors, as well as substantially constant coupling to the skin to reduce motion artifact; 2) focusing of emitted light through the skin to the bone; and, 3) focusing of reflected light through the skin to the photodiode sensors.

As a further note, the radius of the lens may be designed to maximize 1) through 3). The height of the lens is designed to allow it to protrude above composite adhesive **113** of the device **100** and into the skin, but not deep enough to disturb the capillary bed which would also result in bad data. Moreover, the radius of curvature and the angles of LED lightwave emission are not necessarily highly controlled and need not be because the LEDs used to penetrate the skin, e.g., the red and infra-red LEDs; provide a very wide array of angles of emission, and thus a large number of reflected array of lightwaves will be focused back to the sensor by a large variety of curved surfaces. I.e., the curved surface is helpful for maintaining contact through movement (accidental or on purpose), and is less important to the angles of transmission through the skin and reflection back to the sensor. In other words, many different radii of curvature will be effective with very little difference in data/wave transmission and reflection; the wide angle emission of LED takes care of what might be a variety of radii. Rather, the curvature may have more limitation in the maintenance of contact due to movement of the device **100**—e.g., flatter curvatures won't roll readily, and very small radii of curvature will not transmit or receive as much data.

In some implementations, a radii of curvature found useful have been between about 20 and 40 (both 20.34 mm and 39.94 mm radii of curvature have been found useful) for a device having LEDs and sensors in a compartment of about 12.6 mm by 6.6 mm. It may be noted further that LEDs may be on one side or another or on two opposing sides or perhaps at four or more substantially equi-distant points around a sensor and may provide desirable results.

Note further, pulse oximetry hereof may be with multiple light sources and/or sensors as may be one interpretation of the dispositions of FIGS. **1H** and **1K**. Typical pulse oximetry circuitry uses one light source (LED) per wavelength (typically red, infrared, and others). However, devices and/or methods hereof may make use of multiple light sources for each wavelength. This allows interrogation of a wider area of capillary bed in/on the patient/wearer in order to reduce the effects of a local motion artifact. Similarly, multiple sensors may be used for the same purpose or advantage.

Furthermore, a combination of driven right leg and/or proxy driven right leg together with pulse oximetry can provide additional benefits. The right leg circuit, proxy right leg and/or driven right leg, whether for chest or forehead or other electrode placement, can remove common mode and power line noise that would/might otherwise be capacitively-coupled into the pulse oximetry sensor and reduce effectiveness thereof. A combination of driven right leg and/or proxy driven right leg and improved pulse oximetry with a lens as described in and for FIG. **1K** can significantly reduce such noise, and thereby enhance data acquisition. For driven electrodes see further detail below.

FIG. **1D** provides a first example of an adhesive **113** that may be used herewith. The adhesive layer **113** is here a double-sided adhesive for application to the bottom side **102** of the device **100**, and a second side, perhaps with a different type of adhesive for adhering to the skin of the human patient (not shown). Different types of materials for adhe-

sion might be used in that the material of choice to which the adhesive layer is to be attached are different; typically, circuit or circuit board material for connection to the device **100**, and patient skin (not separately shown) on the patient side. A protective backing **114** may be employed on the patient side until application to the patient is desired. Note, in many applications, the adhesive **113** is anisotropic in that it may preferably be only conductive in a single or substantially a single direction, e.g., the axis perpendicular to the surface of adhesive contact. Thus, good electrically conductive contact for signal communication can be had through such adhesive to/through the adhesive to the electrical contacts or electrodes, **108**, **109** and **110**. Note, a corresponding one or more light apertures **111b/112b** are shown in the adhesive of **113** of the example of FIG. **1D** to communicate light therethrough in cooperation with the light conduit(s) **111a/112a** in/through layer **105** for communication of light data typically involved in pulse oximetry.

The adhesive may thus be placed or disposed on the device **100**, in some implementations substantially permanently, or with some replaceability. In some implementations, the device as shown in FIGS. **1A-1D** and/or **1G** without (or with in some implementations) the adhesive may be reusable. In many such cases, the adhesive layer **113** may be removed and replaced before each subsequent use, though subsequent re-use of and with a layer **113** is not foreclosed. In a first or subsequent use with a replaceable adhesive layer **113**, it may be that the user applying the device to the patient, e.g., the physician or technician or even the patient, him/herself, applies the conductive transfer adhesive **113** to the patient side **102** of the device **100**. The protective backing **114** may then be removed, and the device adhered to the patient and activated.

Activation of the device after application to a patient/wearer may occur in a number of ways; in some, it may be pre-set that an affirmative activation interaction may not be necessary from the doctor or patient or like due to either an inertial and/or a pulse oximeter activation which may be substantially automatically activating, e.g., upon receiving sufficient minimum input (movement in case of inertial system or light reflection of blood flow for pulse oximetry); however, a button may be provided at an access **106** or in some other location adjacent the electronics to allow the patient to start or stop the device or otherwise mark an event if desired. In one exemplar implementation the device may be worn for a period such as two weeks for collection of data substantially continuously, or at intervals as may be preferred and established in or by the systems hereof.

After a monitoring period is over, a physician, technician, patient or other person may then remove the device from the patient body, in some instances remove the adhesive, in some instances with alcohol, and may establish a data communication connection for data transfer, e.g., by wireless communication or by insertion/connection of a USB or like data connector to download the data. The data may then be processed and/or interpreted and in many instances, interpreted immediately if desired. A power source on board may include a battery and this can then also be re-charged between uses, in some implementations, fully recharged quickly as within about 24 hours, after which the device could then be considered ready for the next patient or next use.

Some alternative conductive adhesives may be used herewith. FIGS. **1E**, **1F** and **1G** show one such alternative conductive adhesive **113a**; a bottom plan view in FIG. **1E** and elevational side views thereof in FIGS. **1F** and **1G** (as being connected to a device **100** in FIG. **1G**). In some

implementations, the conductivity may be anisotropic as introduced above; in some conductive primarily if not entirely in the direction of the Z-Axis; perpendicular to the page (into and/or out of the page) in FIG. 1E, and/or vertically or transversally relative to the long horizontal shown axis of device **100** in the implementation view of FIG. 1F.

The implementation of this particular example includes a composite adhesive **113a** which itself may include some non-conductive portion(s) **113b** and some one or more conductive portions **113c**. The adhesive composite **113a** may, as described for adhesive **113** above be double sided such that one side adheres to the patient while the other side would adhere to the underside **102** of the device **100** (see FIG. 1G) so that one or more conductive portions **113c** may be disposed or placed in electrically communicative and/or conductive contact with the integrated electrodes on the electronic monitoring device **100**. Since the electrodes would operate better where they may be electrically isolated or insulated from each other, yet each making electrical contact or communication with the patient's skin, the adhesive may further be more specifically disposed in some implementations as follows.

As shown in FIGS. 1E and 1F, three isolated conductive portions **113c** may be disposed separated from each other by a body portion **113b** which may be non-conductive. These could then correspond to the electrodes **108**, **109**, **110** from the above-described examples, and as more particularly shown schematically in FIG. 1G (note the scale is exaggerated for the adhesive **113a** and thus, exact matching to the electrodes of device **100** is not necessarily shown). In some examples, the electrode areas **113c** may be a conductive hydrogel that may or may not be adhesive, and in some examples, may be made of a conductive an adhesive conductive material such as 3M Corporation 9880 Hydrogel adhesive (3M Company, St. Paul, Minn.). These areas **113c** may then be isolated from each other by a non-conductive material **113b** such as 3M Corporation 9836 tape or 3M double-sided Transfer Adhesive 9917 (3M, St. Paul, Minn.) or equivalent. The additional layer **113d**, if used, might be a 3M 9917 adhesive together with the **113b** of a 9836 material. These constructs may provide the effect of creating a low electrical impedance path in the Z-axis direction (perpendicular to page for FIG. 1E and vertically/transversally for FIGS. 1F and 1G) for the electrode areas **113c**, and high electrical impedance path between the electrodes in the X/Y directions. (See FIGS. 1E, 1F and 1G; coplanar with the page in FIG. 1E and horizontal and perpendicular to the page in FIGS. 1F and 1G). Thus, a composite adhesive strip can ensure not only device adhering to the patient, but also that the electrodes whether two or as shown three electrodes are conductively connected by conductive portions of the adhesive strip, where the combination of conductive and non-conductive portions can then reduce signal noise and/or enhance noise free characteristics. Electrodes that move relative to skin can introduce noise; that is, electrodes electrically communicative/connected to the skin via a gel may move relative to the skin and thus introduce noise. However, with one or more conductive adhesive portions in a composite adhesive connected to respective electrodes and then substantially securely connected to the skin will keep the respective electrodes substantially fixed relative to the skin and thereby reduce or even eliminate electrode movement relative to the skin. Removal of such movement would then remove noise which would thereby provide a clean signal that can allow for monitoring cardiac P waves which

enhances the possibility to detect arrhythmias that couldn't otherwise be detected. Further description is set forth below.

In some implementations, a further optional connective and/or insulative structure **113d** may be implemented as shown in FIG. **113d** to provide further structural and insulative separation between electrodes with connected to a device **100** on the underside **102** thereof (see FIG. 1G). Though shown separate in FIGS. 1F and 1G, it may be contiguous with the insulative adhesive **113b** of these views.

Further alternatives related to the adhesive may be used. In some implementations, a composite adhesive strip may be used having properties to reduce one or more motion artifacts. Typical ECG attachment systems use a conductive gel located over the electrode. Here, however, a hydrogel adhesive may be used which is embedded in a continuous sheet of laminated adhesives that cover the selected regions or the entire footprint of the device. The fact that the hydrogel itself has strong adhesive properties coupled with the complete coverage of the device with adhesives may assure a strong bond between the device and the patient's skin. Contributing to motion artifact reduction may be an alternative vertical placement of the device on the sternum which results in reduced motion artifacts for one or more of ECG signals, photoplethysmography waveforms, and oxygen saturation signals.

In some implementations, composite adhesive improvements may include water-proof encapsulation of the hydrogel adhesive to prevent ohmic impedance reduction resulting in reduction of signal amplitude. This may also help prevent hydrocolloid adhesive degradation. In particular, as shown the non-limitative alternative exemplar in FIGS. 1I and 1J; several layers may be used. Herein, Layer 1 may be a hydrocolloid that is an adhesive designed for long term skin contact by absorbing sweat and cells. Layer 2 may then also be a layer designed for long-term skin contact, however, this layer 2 isolates Layer 3 from contacting the skin. The smaller dimensions of Layer 2 create a gap between Layers 1 and 3. When Layer 1 and 3 bond together, it forms a water-tight seal around Layer 2. This layer, Layer 2, also isolates the Hydrocolloid from the Hydrogel Adhesive, protecting the adhesive properties of the Hydrocolloid. Layers 3 and 5 would then generally be waterproof layers that are electrically isolating, double-sided adhesives. These two layers encapsulate the hydrogel adhesive, preventing a "short circuit" described relative to layer 4 below. Layer 4 is the hydrogel adhesive that is the conductive element hereof. The three islands of hydrogel adhesive of Layer 4 must be kept electrically isolated from each other. However as the hydrocolloid in layer 1 absorbs sweat, it too becomes conductive and creates a potential "short circuit" between the three islands of hydrogel adhesive in Layer 4, reducing signal amplitude. Nevertheless, this "short circuit" may be prevented by layers 3 and 5, described above.

Some alternative implementations hereof may include a driven right leg ECG circuit with one or more chest only electrodes ("Driven Chest Electrode"). In addition to the electrodes used to measure a single or multiple lead electrocardiogram signal, a device **100** may use an additional electrode, as for example the reference electrode **110** (see FIGS. 1A, 1C, 1D and 1G, e.g.) to reduce common mode noise. Such an electrode may function in a manner similar to the commonly-used driven right leg electrode, but may here be located on the patient's chest rather than on the patient's right leg but nevertheless this third/reference electrode may play the role of the leg electrode. This chest electrode may thus mimic a right leg electrode and/or be considered a proxy driven right leg electrode. A circuit, or

portion of an overall circuit, adapted to operate in this fashion may include a number of amplifier stages to provide gain, as well as filtering to ensure circuit stability and to shape the overall frequency response. Such a circuit may be biased to control the common mode bias of the electrocardiogram signal. This driven chest electrode implementation may be used in conjunction with a differential or instrumentation amplifier to reduce common mode noise. In this case, the sense electrode may be used as one of the electrocardiogram electrodes. Alternatively, a single-ended electrocardiogram amplifier may be used where the differential electrocardiogram signal is referenced to ground or to some other known voltage.

A circuit or sub-circuit **200** using a transistor **201** as shown in FIG. 2 may be such a circuit (aka module) and may thus include as further shown in FIG. 2A, a sense electrode **202**, a drive electrode **203**, and an amplifier **204**. Both the sense and drive electrodes **202**, **203** are placed on the patient's chest such that they provide an electrical connection to the patient. The amplifier **204** may include gain and filtering. The amplifier output is connected to the drive electrode, the inverting input to the sense electrode, and the non-inverting input to a bias voltage **205**. The amplifier maintains the voltage of the sense electrode at a level close to the bias voltage. An electrocardiogram signal may then be measured using additional electrodes. Indeed, as was the case for the improved conductivity through use of anisotropic adhesive portions above, here also or alternatively, the use of this third electrode as a proxy for a right leg electrode (i.e., proxy driven right leg electrode) can provide signal reception otherwise unavailable. Clean signals may thus allow for receiving cardiac P waves which enhances the possibility to detect arrhythmias that couldn't otherwise be detected.

Further alternative descriptions of circuitry include that which is shown in FIGS. 2B and 2C; in which are shown non-limiting alternatives in which three adjacent electrodes E1, E2, and E3 may be used to pick up the ECG signal, one of which electrodes playing the role of the distant limb electrode of traditional ECG monitors. Because the electrode-patient interface has an associated impedance (Re1 and Re2), current flowing through this interface will cause a difference in voltage between the patient and the electrode. The circuit may use a sense electrode (E1) to detect the patient voltage. Because this exemplar circuit node has a high impedance to circuit ground (GND), very little current flows through the electrode interface, so that the voltage drop between the patient and this node is minimized. The first of these alternative, non-limiting circuits (FIG. 2B) also contains an amplifier (U1) whose low-impedance output is connected to a separate drive electrode (E2). The amplifier uses negative feedback to control the drive electrode such that the patient voltage (as measured by the sense electrode E1) is equal to the bias voltage (V1). This may effectively maintain the patient voltage equal to the bias voltage despite any voltage difference between the driven electrode (E2) and the patient. This can include voltage differences caused by power line-induced current flowing between the drive electrode and the patient (through Re2). This arrangement differs from a traditional 'driven-right-leg' circuit in at least two ways: the driven electrode is placed on the patient's chest (rather than the right leg), and the ECG signal is a single-ended (not differential) measurement taken from a third electrode (E3). Because all electrodes are located on the patient's chest in a chest-mounted example, a small device placed there may contain all the necessary electrodes for ECG measurement. One possible benefit of the single-ended

measurement is that gain and filtering circuitry (U2 and associated components (FIG. 2C)) necessary to condition the ECG signal prior to recording (ECG Output) requires fewer components and may be less sensitive to component tolerance matching. The examples of FIGS. 2A, 2B and 2C are non-limiting examples and not intended to limit the scope of the claims hereto as other circuits with other circuit elements can be formed by skilled artisans in view hereof and yet remain within the spirit and scope of claims hereof.

In many implementations, a system hereof may include other circuitry operative together with the ECG electrodes, which may thus be accompanied by other sensors to provide time concordant traces of: i) ECG p-, qrs-, and t-waves; ii) O2 Saturation, as measured by Pulse Oxymetry; and/or iii) xyz acceleration, to provide an index of physical activity. Such circuitry may be implemented to one or more of the following electrical specifications. The overall system might in some implementations include as much as two weeks (or more) of continuous run time; gathering data during such time. Some implementations may be adapted to provide as many or even greater than 1000 uses. Alternatives may include operability even after or during exposure to fluids or wetness; in some such examples being water resistant, or waterproof, or watertight, in some cases continuing to be fully operable when fully submerged (in low saline water). Other implementations may include fast data transfer, as for an example where using an HS USB for full data transfer in less than about 90 seconds. A rechargeable battery may typically be used.

A further alternative implementation may include an electronic "ground": In a device hereof, mounted entirely on a flexible circuit board, the ground plane function may be provided by coaxial ground leads adjacent to the signal leads. The main contribution of this type of grounding system may be that it may allow the device the flexibility required to conform and adhere to the skin.

For electrocardiograph; EKG or ECG, some implementations may include greater than about 10 Meg Ohms input impedance; some implementations may operate with a 0.1-48 Hz bandwidth; and some with an approximate 256 Hz Sampling Rate; and may be implementing 12 Bit Resolution. For PPG and Pulse Oximeter, operation may be with 660 and 940 nm Wavelength; about 80-100 SpO2 Range; a 0.05-4.8 Hz Bandwidth; a 16 Hz Sampling Rate; and 12 bit resolution. For an accelerometer: a 3-Axis Measurement may be employed, and in some implementations using a  $\pm 2$  G Range; with a 16 Hz Sampling Rate; and a 12 Bit Resolution.

For pulse oximetry, an option for PPG ambient light subtraction may be included. A method and circuitry for reducing errors in pulse oximetry caused by ambient light is described and a circuitry option shown in FIG. 2D. Here a correlated double sampling technique is shown for use to remove the effect of ambient light, photo-detector dark current, and flicker noise.

The schematic shown in FIG. 2D may be used where, first, the noise signal may be measured. The light sources are turned off, switch S1 is closed, and switch S2 is open. This allows charge proportional to the noise signal to accumulate on C1. Then switch S1 is opened. At this point the voltage on C1 is equal to the noise signal voltage. Next, the light signal may be measured. The light source is turned on, switch S2 is closed, and charge is allowed to flow through C1 and C2 in series. Then, S2 is opened, and the voltage is held on C2 until the next measurement cycle when the whole process is repeated.

If  $C1$  is much larger than  $C2$ , nearly all the voltage will appear on  $C2$ , and the voltage on  $C2$  will be equal to the noise-free signal ( $s$ ). Otherwise, the voltage on  $C2$  will be a linear combination of the previous  $C2$  voltage ( $p$ ) and the noise-free signal:  $(C2*s+C1*p)/(C1+C2)$ . This has the effect of applying a first-order, low-pass, IIR discrete-time filter to the signal. If this filtering effect is not desired, the voltage on  $C2$  may be discharged to zero before the signal is measured each cycle, so that the signal held on  $C2$  is simply:  $(C2*s)/(C1+C2)$ .

This circuit may be used with a trans-impedance amplifier in place of resistor  $R$ , a phototransistor in place of the photodiode, and FETs in place of the switches. The output may be followed by additional buffering, amplification, filtering and processing stages.

Some summary methodologies may now be understood with relation to FIG. 3, though others may be understood through and as parts of the remainder of the disclosure hereof. A flow chart 300 as in FIG. 3 may demonstrate some of the alternatives; where an initial maneuver 301 might be the application of the device 100 to the patient. Indeed, this might include some one or more of the alternatives for adhesive application as described here above, whether by/through use of an adhesive such as that 113 of FIG. 1D, or that of FIGS. 1E, 1F and/or 1G. Then, as shown, in moving by flow line 311, a data collection operation 302 may be implemented. Note, this might include a continuous or substantially continuous collection or an interval or periodic collection or perhaps even a one-time event collection. This may depend upon the type of data to be collected and/or be dependent upon other features or alternatives, as for example whether a long term quantity of data is desired, for ECG for example, or whether for example a relative single data point might be useful, as in some cases of pulse oximetry (sometimes a single saturation point might be of interest, as for example, if clearly too low, though comparison data showing trending over time, may indeed be more typical).

Several alternatives then present in FIG. 3, flow chart 300; a first such might be the following of flowline 312 to the transmission of data operation 303, which could then involve either wireless or wired (e.g., USB or other) data communication from the device 100 to data analysis and/or storage devices and/or systems (not separately shown in FIG. 3; could include computing devices, see e.g., FIG. 4 described below, or the like). Options from this point also appear; however, a first such might include following flow line 313 to the data analysis operation 304 for analyzing the data for determination of the relative health and/or for condition diagnosis of a patient. Computing systems, e.g., a computer (could be of many types, whether hand-held, personal or mainframe or other; see FIG. 4 and description below) could be used for this analysis; however, it could be that sufficient intelligence might be incorporated within the electronics 103 of device 100 such that some analysis might be operable on or within device 100 itself. A non-limiting example, might be a threshold comparison, as for example relative to pulse oximetry where when a low (or in some examples, perhaps a high) threshold level is reached an indicator or alarm might be activated all on/by the electronics 103 of the device 100.

A similar such example, might be considered by the optional alternative flow path 312a which itself branches into parts 312b and 312c. Following flow path 312 a, and then, in a first example path 312b, a skip of the transmit data operation 303 can be understood whereby analysis 304 might be achieved without substantial data transfer. This

could explain on board analysis, whether as for example according to the threshold example above, or might in some instances include more detailed analysis depending upon how much intelligence is incorporated on/in the electronics 103. Another view is relative to how much transmission may be involved even if the transmission operation 303 is used; inasmuch as this could include at one level the transmission of data from the patient skin through the conductors 108, 109 and/or 110 through the traces 107 to the electronics 103 for analysis there. In other examples, of course, the transmission may include off-board downloading to other computing resources (e.g., FIG. 4). In some cases, such off-loading of the data may allow or provide for more sophisticated analysis using higher computing power resources.

Further alternatives primarily may involve data storage, both when and where, if used. As with intelligence, it may be that either some or no storage or memory may be made available in/by the electronics 103 on-board device 100. If some storage, whether a little or a lot, is made available on device 100, then, flow path 312a to and through path 312c may be used to achieve some storing of data 305. This may in many cases then, though not necessarily be before transmission or analysis (note, for some types of data multiple paths may be taken simultaneously, in parallel though perhaps not at the same time or serially (e.g., paths 312b and 312c need not be taken totally to the exclusion of the other), so that storage and transmission or storage and analysis may occur without necessarily requiring a completion of any particular operation before beginning or otherwise implementing another). Thus, after (or during) storage 305, flow path 315a may be followed for stored data which may then be transmitted, by path 315b to operation 303, and/or analyzed, by path 315c to operation 304. In such a storage example, which in many cases may also be an on-board storage example, data can be collected then stored in local memory and later off-loaded/transmitted to one or more robust computing resources (e.g., FIG. 4) for analysis. Frequently, this can include long term data collection, e.g., in the manner of days or weeks or even longer, and may thus include remote collection when a patient is away from a doctor's office or other medical facilities. Thus, data can be collected from the patient in the patient's real world circumstances. Then, after collection, the data can be transmitted from its storage on device 100 back to the desired computing resource (FIG. 4, e.g.), and such transmission might be wireless or wired or come combination of both, as for example a blue tooth or Wi-Fi connection to a personal computer (FIG. 4 for one example) which might then communicate the data over the internet to the designated computer for final analysis. Another example might include a USB connection to a computer, either to a PC or a mainframe (FIG. 4), and may be to the patient computer or to the doctor computer for analysis.

If little or no storage or memory is resident on device 100 (or in some examples even where there may be a large amount of resident memory available), then, relatively soon after collection, the data would need to or otherwise might desirably either or both be transmitted and then stored, see path 313a after operation 303, and/or transmitted and analyzed, paths 312 and 313. If path 313a is used, then, more typically, the data storage may be in/on computing resources (not shown in FIG. 3, but see FIG. 4 described below) off-board (though on-board memory could be used as well), and then, any of paths 315a, 315b and 315c may be used.

A feature hereof may include an overall system including one or more devices 100 and computing resources (see FIG.

4, for example) whether on-board device(s) 100, or separate, as for example in personal or mobile or hand-held computing devices (generally by FIG. 4), the overall system then providing the ability for the physician or doctor to have immediate, in-office analysis and presentation of collected test data. This would in some implementations allow for on-site data analysis from the device without utilization of a third party for data extraction and analysis.

Alternative implementations hereof may thus include one or more hardware and software combinations for multiple alternative data source interpretations. As noted above, a device 100 hereof includes hardware that monitors one or more of various physiologic parameters, then generates and stores the associated data representative of the monitored parameters. Then, a system which includes hardware such as device 100 and/or the parts thereof, and software and computing resources (FIG. 4, generally) for the processing thereof. The system then includes not only the collection of data but also interpretation and correlation of the data.

For example, an electrocardiogram trace that reveals a ventricular arrhythmia during intense exercise may be interpreted differently than the same arrhythmia during a period of rest. Blood oxygen saturation levels that vary greatly with movement can indicate conditions that may be more serious than when at rest, inter alia. Many more combinations of the four physiologic parameters are possible, and the ability of software hereof to display and highlight possible problems will greatly aid the physician in diagnosis. Thus, a system as described hereof can provide beneficial data interpretation.

Some of the features which can assist toward this end may be subsumed within one or more of operations 303 and 304 of FIG. 3, wherein data collected on a device 100 can rather simply be communicated/transmitted to computing resources (again, whether on-board device 100 or discrete therefrom as e.g., FIG. 4). For an example, when a patient having had a device applied (operation 301) may return to a physician's office after a test period wherein data was collected (operation 302) the device is connected via one or more data transmission alternatives, as for example, USB to a computer (Windows or Mac) (generally with reference to FIG. 4 and description thereof) in the office, allowing immediate analysis by the physician while the patient waits (note, the device 100 may first have been removed from the patient or might remain thereon pending transmission and analysis for determination of whether more data may be desired). In some implementations, data analysis time may be relatively quick, at approximately 15 minutes in some implementations, and might be achieved with a user-friendly GUI (Graphic User Interface) to guide the physician through the analysis software.

The analysis/software package may be disposed to present the physician with results in a variety of formats. In some implementations, an overview of the test results may be presented, either together with or in lieu of more detailed results. In either case, a summary of detected anomalies and/or patient-triggered events may be provided, either as part of an overview and/or as part of the more detailed presentation. Selecting individual anomalies or patient-triggered events may provide desirable flexibility to allow a physician to view additional detail, including raw data from the ECG and/or from other sensors. The package may also allow data to be printed and saved with annotations in industry-standard EHR formats.

In one implementation, patient data may be analyzed with software having the one or more of the following specifications. Some alternative capabilities may include: 1. Data Acquisition; i.e., loading of data files from device; 2. Data

Formatting; i.e., formatting raw data to industry standard file formats (whether, e.g., aECG (xml); DICOM; or SCP-ECG) (note, such data formatting may be a part of Acquisition, Storage or Analysis, or may have translation from one to another (e.g., data might be better stored in a compact format that may need translation or other un-packing to analyze)); 3. Data Storage (whether local, at a clinic/medical facility level or e.g., in the Cloud (optional and allows offline portable browser based presentation/analysis)); 4. Analysis which inter alia, may include, e.g., noise filtering (High pass/Low pass digital filtering); and/or QRS (Beat) detection (in some cases, may include Continuous Wave Transform (CWT) for speed and accuracy); and/or 5. Data/Results Presentation, whether including one or more graphical user interface(s) (GUIs) perhaps more particularly with an overall Summary and/or General Statistics and/or Anomaly Summary of Patient triggered event(s); presentation of additional levels of detail whether of Strip view(s) of anomaly data by incident (previous, next) Blood Oxygen saturation, stress correlation or the like; and/or allowing care provider bookmarking/annotations/notes by incident and/or Print capability.

Further, on alternative combinations of hardware with proprietary software packages: I) One on-device software package may be adapted to store the measurements from the data signals acquired from one or more of EKG/ECG (whether right leg and/or p-, qrs- and/or t-waves), or O2 saturation, or xyz acceleration, in a time concordant manner, so that a physician may access a temporal history of the measurements (say, in some examples, over a 1-2 week interval), which would provide useful information on what the patient's activity level was prior to, during, and after the occurrence of a cardiac event. ii) an alternative to alternately manage the real-time transmission of the real-time measured parameters to a nearby station or relay. And/or; iii) an off-device ECG analysis software aimed at recognizing arrhythmias.

The software mentioned above may be industry understood software provided by a 3rd party, or specially adapted for the data developed and transmitted by and/or received from a wearable device 100 hereof. Thorough testing using standard (MIT-BIH/AHA/NST) arrhythmia databases, FDA 510(k) approvals preferred. Such software may be adapted to allow one or more of automated ECG analysis and interpretation by providing callable functions for ECG signal processing, QRS detection and measurement, QRS feature extraction, classification of normal and ventricular ectopic beats, heart rate measurement, measurement of PR and QT intervals, and rhythm interpretation.

In many implementations, the software may be adapted to provide and/or may be made capable of supplying one or more of the following measurements:

TABLE 1

- 
1. Heart Rate Min, Max and Average
  2. QRS duration average
  3. PR interval average
  4. QT interval average
  5. ST deviation average
- 

and, may be adapted to recognize a broad range of arrhythmias such as those set forth here:

TABLE 2A

1. SINUS RHYTHM
2. SINUS RHYTHM + IVCD
3. SINUS BRADYCARDIA
4. SINUS BRADYCARDIA + IVCD
5. SINUS TACHYCARDIA
6. PAUSE
7. UNCLASSIFIED RHYTHM
8. ARTIFACT

This first group of 8 given above are arrhythmia types that may be recognizable even if there is no discernible P wave. They are the ones typically recognized by existing products in the outpatient monitoring market that we propose to address.

A second set or group of arrhythmias; below, may require a discernible and measurable P wave. Some implementations hereof may be adapted to be able to detect and recognize them, as device 100 may be able as described above to detect P waves, depending of course, and for example, on whether the strength of the P wave which may be affected by device 100 placement or patient physiology.

TABLE 2B

9. ATRIAL FIBRILLATION/FLUTTER SVR (slow)
10. ATRIAL FIBRILLATION/FLUTTER CVR (normal rate)
11. ATRIAL FIBRILLATION/FLUTTER RVR (rapid)
12. FIRST DEGREE AV BLOCK + SINUS RHYTHM
13. FIRST DEGREE AV BLOCK + SINUS TACHYCARDIA
14. FIRST DEGREE AV BLOCK + SINUS BRADYCARDIA
15. SECOND DEGREE AV BLOCK
16. THIRD DEGREE AV BLOCK
17. PREMATURE ATRIAL CONTRACTION
18. SUPRA VENTRICULAR TACHYCARDIA
19. PREMATURE VENTRICULAR CONTRACTION
20. VENTRICULAR COUPLETT
21. VENTRICULAR BIGEMINY
22. VENTRICULAR TRIGEMINY
23. IDIOVENTRICULAR RHYTHM
24. VENTRICULAR TACHYCARDIA
25. SLOW VENTRICULAR TACHYCARDIA

Further in alternative software implementations; some sample screenshots are shown in FIG. 5. A first such alternative is shown in FIG. 5A, which is an example screenshot showing ECG and Oxygen Saturation data taken by using a patch device such as a device 100 hereof. An extremely clean signal is shown (no filtering or smoothing has been done on this data). Distinct p-waves are also shown (3 of which are shown as an example with arrows). P wave detection can be extremely important for ECG anomaly detection. Oxygen Saturation, as measured by Pulse Oximetry, is shown on the bottom plot. This is data taken by a device on the chest, and is taken in time concordance with the ECG data.

Another alternative is shown in FIG. 5B, which is an example screenshot of Analysis Software. This is a sample of ECG data taken from the MIT-BIH Arrhythmia Database, Record 205. As analyzed by the Analysis system hereof, we see in the Event Occurrences Summary list (top, left) five (5) anomaly types (plus normal sinus rhythm). This list also shows the number of occurrences of each anomaly, total duration of the anomaly in the complete ECG, and the percent time this anomaly occurs in the complete ECG. To view specific instances of each anomaly, the user double clicks the specific row in the Event Occurrences Summary list, as shown in FIG. 5C.

As introduced, FIG. 5C is an example screenshot showing specific instance of Ventricular Tachycardia. The ECG plot

automatically navigates to the specific time in the ECG waveform, and marks the beginning and end of the event. More detailed data about this specific event is now shown in the Occurrence Details: HR Average, HR Max, etc. for the duration of this event. To show the instances of another anomaly in this ECT, the user can click on the Premature Ventricular Contraction (PVC) row of the Event Occurrences Summary, as shown FIG. 5D.

As introduced, FIG. 5D is an example screenshot showing specific instance of Premature Ventricular Contraction. This shows occurrences of the PVC. The Start Times list (middle top) shows all instances of PVC occurrences in this ECG, and lists the start time for each occurrence. In this case, the user can click on the PVC that starts at 00:15:27 (the 11<sup>th</sup> occurrence). The ECG plot is automatically taken to this point in time to show and indicate the PVC instances in the waveform. Since there are 3 instances of a PVC in this timeslot, all 3 occurrences are marked.

As mentioned above, in one aspect of the developments hereof, ECG signals collected in time concordance with pulse oximetry signals may be used to reduce the noise in the pulse oximetry signals and to permit the calculation of values for oxygen saturation, particularly in circumstances where sensors pulse oximetry data are placed on noise-prone locations of a patient, such as the chest. In some embodiments, this aspect may be implemented by the following steps: (a) measuring an electrocardiogram signal over multiple heart beats; (b) measuring one or more pulse oximetry signals over multiple heart beats such that the electrocardiogram signal and the one or more pulse oximetry signals are in time concordance over one or more heart beats; (c) comparing a portion of the electrocardiogram signal and the one or more pulse oximetry signals in time concordance over one or more heart beats to determine a constant component and a primary periodic component of each of the one or more pulse oximetry signals; and (d) determining oxygen saturation from the constant components and primary periodic components of the one or more pulse oximetry signals. Measurement of the ECG signals and pulse oximetry signals may be implemented by embodiments of devices hereof. In particular, pulse oximetry signals may be a reflective infrared signal and a reflective red light signal collected by a photodetector in a device hereof. Intervals of pulse oximetry signals corresponding to heart beats may be determined by comparing such signals to the time concordant ECG signals. For example (not intended to be limiting), successive R-wave peaks of a time concordant ECG signal may be used to identify such intervals, although other features of the ECG signal may be used as well. Once such intervals are identified, values at corresponding times within the intervals may be averaged to reduce signal noise and to obtain more reliable values for the constant components (sometimes referred to as the "DC components") and the main periodic components (sometimes referred to as the "AC components") of the pulse oximetry signals, e.g. Warner et al, Anesthesiology, 108: 950-958 (2008). The number of signal values recorded in an interval depends on the signal sampling rate of the detectors and processing electronics employed. Also, as the intervals may vary in duration, the averaging may be applied to a subset of values in the intervals. As described below, oxygen saturation values may be computed from such DC and AC components using conventional algorithms. The number of heart beats or intervals over which such averages may be computed may vary widely, as noted below. In some embodiments, signals from one or more heart beats or intervals may be analyzed; in other embodiments, signals from a plurality of heart beats

or intervals may be analyzed; and in some embodiments, such plurality may be in the range of from 2 to 25, or in the range of from 5 to 20, or in the range of from 10 to 20.

In further alternative implementations, a linear regression algorithm for Oxygen Saturation may be used. As such, the patient's ECG signal may be used to determine when heart beats occur. The beat locations allow correlated time averaging of each of the two photoplethysmogram signals. A linear regression of the ensemble averages may then be used to determine the linear gain factor between the two signals. This gain factor can be used to determine the patient oxygen saturation.

ECG data may be recorded in time-concordance with two or more photoplethysmographs of different light wavelengths. The heart beats are detected in the ECG signal. These heart beats allow for definition of a 'frame' of photoplethysmogram data for the time between two adjacent heart beats. Two or more of these frames can then be averaged together at each point in time to create an average frame for the time interval. Because the photoplethysmogram is correlated with the heartbeat, the photoplethysmogram signal is reinforced by this averaging. However, any motion artifact or other noise source that is uncorrelated in time with the heartbeat is diminished. Thus, the signal-to-noise ratio of the average frame is typically higher than that of the individual frames.

Having constructed an average frame for at least two photoplethysmographs of different light wavelengths, linear regression can then be used to estimate the gain between the two average frame signals. This gain value may be used to estimate blood oxygen saturation information or other components present in the blood such as hemoglobin, carbon dioxide or others. The process may be repeated for additional light wavelengths in order to do so.

An exemplar/alternative method hereof may include determining the gain between particular signals, as between the red and IR frame signals, if/when such may be used. These may be found by averaging the two frames together first. This may result in a signal with reduced noise. The gain is found by performing linear regression of the red versus combined and IR versus combined and then finding the ratio of these two results.

Another method involves selecting a possible gain value, multiplying the average frame signal by it, and determining the residual error with respect to an average frame of a different wavelength. This process may be repeated for a number of potential gain values. While simple linear regression finds the global minimum gain value, this method allows for finding local minima. Thus, if it is likely that the global minimum represents correlation caused by motion artifact, venous blood movement or another noise source, it may be ignored, and a local minimum may be selected instead.

As mentioned above, patient wearable devices hereof for implementing the above aspects may be particularly useful for monitoring oxygen saturation in noisy regions for such measurements, for example, where there is significant local skin movement, such as the chest location.

One embodiment of the above aspect hereof is illustrated in FIGS. 6A-6C. In FIG. 6A, curve A (600) illustrates time varying output of the photodiode of a device hereof for infrared (IR) reflection and curve B (602) illustrates time varying output of the photodiode of the device for red light reflection. In some embodiments, the skin is alternatively illuminated by the red and IR LEDs to generate the signals collected by the same photodiode. In FIG. 6B, time synchronized (i.e. time concordant) ECG data, illustrated by

curve C (604), is added to the plot of FIG. 6A. Peak values in the ECG data (e.g. peaks 606 and 608) may be used to define frames or intervals of pulse oximetry data. Additional consecutive frames or intervals are indicated by 612 and 614, and further frames may be similarly determined. In accordance with this aspect, pulse oximetry data from a plurality of frames is collected. The magnitude of the plurality may vary widely depending on particular applications. In some embodiments, the plurality of frames collected is from 5 to 25; in one embodiment, a plurality is between 8 and 10 frames. Typically, frames or intervals of pulse oximetry data contain different numbers of signal samples. That is, output from the sensors may be sampled at a predetermined rate, such a 32 samples per second. If the time between ECG peaks varies, then the number of samples per frame will vary. In one embodiment, features in the ECG data serving as the starting points of a frame are selected so that an associated peak in the pulse oximetry data is approximately in the mid-point, or center, of the frame, after which a predetermined number of signal samples are recorded for each frame. Preferably in this embodiment, the predetermined number is selected to be large enough to ensure that the pulse oximetry signal peak is roughly mid-frame. Sample values corresponding to time points above the predetermined value are not used. After a plurality of frames of data is collected, averages of the values at corresponding time points of the frames are computed. The values from such averages AC and DC components of the pulse oximetry data are determined and are then used to compute relative oxygen saturation by conventional methods, such as the ratio-of-ratios algorithm, e.g. Cypress Semiconductor document No. 001-26779 Rev A (Jan. 18, 2010). This basic procedure is summarized in the flow chart of FIG. 6C. Frame size (in terms of number of samples) is determined (620). Values of samples at corresponding time points within each frame are summed (622), after which average values for each time point are computed which, in turn, give the AC and DC components of IR and red light reflection with reduced noise. In some embodiments, values for these components can be used to compute oxygen saturation using conventional algorithms (626). Relative values for oxygen saturation may be converted into absolute values by calibrating the measurements for particular embodiments. Calibration may be carried out in controlled environments where individuals are exposed to varying atmospheric concentrations of oxygen and measured oxygen saturation values are related to corresponding oxygen levels.

In addition to the above embodiment for comparing ECG signals with pulse oximetry signals, a range of other embodiments for such comparing is within the comprehension of those of ordinary skill in the art. For example, in order to find peaks of the AC component of pulse oximetry signals in the presence of noise, features of the time concordant ECG signal that are located at characteristic times preceding and succeeding the pulse oximetry maximum and/or minimum values may be used to reliably determine the pulse oximetry peak and minimum values when averaged over a plurality of heart beats (without the need to average all values of the pulse oximetry signal over the heart beats). For example, if, within an interval, the R wave peak of an ECG signal characteristically preceded a pulse oximetry signal maximum by x milliseconds and trailed a pulse oximetry signal minimum by y milliseconds, then the essential information about the AC component of the pulse oximetry signal may be obtained by repeated measurements of just two values of pulse oximetry signals.

In some embodiments, values for IR or red reflection measured by the photodiode may be used to estimate depth and/or rate of respiration. In FIG. 6D, a curve (630) of Red or IR values over time is illustrated. In FIG. 6E, maximum values and minimum values of curve (630) are shown by dashed curves (632) and (634), respectively. The difference between the maximum and minimum values at a time point is monotonically related to the depth of breath in an individual being monitored. Thus, as illustrated, breaths at time (636) are shallower than those at time (638). In some embodiments, depth of breath versus time may be computed and monitored in an individual. Over time, the rate of respiration can be evaluated from the curve of maximum and minimum values over time.

Moreover, moving from an appreciation of a derivation of a respiration waveform from ECG R-S amplitude and/or R-R intervals, it has been found that a PPG and/or pulse oximeter as described herein can be used to relatively directly estimate a respiration waveform. As the chest expands and contracts during breathing, the motion hereof shows up as a wandering baseline artifact on the PPG signals. The respiration signal may be isolated by filtering out the PPG data to focus on the breathing/respiration signal. This may be particularly so with a chest-mounted PPG.

In addition, a chest mounted accelerometer may also or alternatively be used to measure the respiration waveform, especially when the user is lying on his/her back. As the chest expands and contracts, the chest accelerates up and down (or transversely, or otherwise depending upon orientation), which can be measured by the accelerometer.

Either of these, PPG and/or accelerometer, devices and/or methods may be used discretely or in combination with each other and/or with the above-described ECG-based respiration estimation technique. Using multiple methods may improve accuracy when compared to estimates based on a single method. Respiration rate and depth may then be estimated from the respiration signal using time-domain and/or frequency domain methods.

In some implementations, heart beat timing (e.g., from ECG) and PPG signals can be used to determine pulse transit time; i.e., the time for the pressure wave to travel from the heart to other locations in the body. Measurements of pulse transit time may then be used to determine or estimate blood pressure. Note, the heartbeat timing, ECG and/or PPG signals may be generated by conventional or other to-be-developed methods, systems or devices, or may be developed by wearable devices such as those otherwise described herein. I.e., the algorithms hereof may be separately usable, as well as being usable in the wearable cardiac device.

As disclosed herein elsewhere, the PPG signals of several heart beats may be averaged by correlating each with a respective heartbeat. The result is a PPG frame where the heart rate-correlated PPG signal is reinforced while uncorrelated noise is diminished. Moreover, because the PPG frame is already correlated to the timing of the heartbeat, pulse transit time may be estimated by determining the location of either the peak or minimum with respect to either the beginning or end of the frame itself. This may be done either by finding the minimum and/or maximum sample(s), or by interpolating the signal to find points between measured samples. For example, interpolation may be done with a quadratic fit, a cubic spline, digital filtering, or many other methods.

The pulse transit time may also be estimated by correlating the PPG frame with a sample signal. By shifting the two signals with respect to each other, the time shift resulting in the maximum correlation may be determined. If the sample

signal is an approximation of the expected PPG frame, then the time shift with maximum correlation may be used to determine the pulse transit time.

An exemplar methodology or algorithm herefor is described here and shown in the drawing FIGS. 7A, 7B and 7C. Initially, such a method 710 (which includes and/or is defined by parts 710a, 710b and/or 710c) takes at least one heartbeat (typical ECG) signal 712 and at least one PPG signal 711 as input as shown in FIG. 7A, e.g. The heartbeat timing information/signal 712 is used to generate heartbeat timing information by detecting the R-wave or other ECG feature from each beat; multiple ECG signals (i.e. different leads from locations on the body) may be used to obtain a better estimate of the heartbeat timing information. The PPG 711 may use a single light wavelength or signals from multiple light wavelengths. Using the corresponding heartbeat timing information related to each PPG signal 711, each PPG signal 711 is segmented into "frames," see PPG Frame 1, PPG Frame 2 and PPG Frame N in FIG. 7A, where each frame contains the PPG signal of a single wavelength for the duration of one corresponding beat of the heart.

Optionally, but, typically, a PPG signal quality estimate may also be performed. An example of this is shown as method part 710b in FIG. 7B. This estimate may consider the variance of the PPG signal, the estimated signal-to-noise ratio of the PPG signal, PPG signal saturation, patient motion information from an accelerometer or gyroscope, an ECG or impedance measurement noise estimate, or other information about the PPG signal quality. Shown in FIG. 7B is an exemplar using accelerometer signal 713 in conjunction with PPG signal 711 to generate a PPG Signal Quality Value/Estimate 714. This signal quality estimate 714 may then be used in conjunction with the heartbeat timing information 712 to generate the gain for each frame, see PPG Frame 1 Gain, PPG Frame 2 Gain and PPG Frame N Gain in FIG. 7B, where lower signal quality results in a lower gain. To reduce computation time, the signal quality estimate 714 may be omitted and a constant may be used for the gain information.

As shown in FIG. 7C, the gain information (PPG Frame 1 Gain, PPG Frame 2 Gain and PPG Frame N Gain from FIG. 7B) may be used (here shown as combined/manipulated) with the frame information (PPG Frame 1, PPG Frame 2 and PPG Frame N from FIG. 7A) to create a weighted, n-sample moving-average frame 715, where the PPG signal that is correlated with the heartbeat timing is reinforced while the uncorrelated noise is reduced. The number of samples included in the frame (n) 715 may be adapted to reduce noise or decrease response time. The frames may be additionally weighted by time in order to increase the contribution of recent or near-future frames with respect to frames that are further away and potentially less-relevant. This additional weighting by time may be implemented using an IIR or FIR filter.

Once the average frame 715 has been produced for a given instant in time, the pulse transit time 716 may be determined by finding the shift in the frame signal with respect to the heartbeat. This may be done simply by finding the sample index 717 where the signal is at a minimum or maximum and comparing it with the frame boundary (heartbeat timing) to determine the pulse transit time. For a more precise result, the signal may be interpolated 718 using a spline or polynomial fit around the minimum or maximum values, allowing the minimum or maximum to be determined with greater precision than the sample rate. Finally, the frame may be compared 719 to a reference frame template, where the average frame is shifted with respect to

the template. The shift with the highest correlation between the average frame and the template indicates the transit time **716**. This reference template may be a predetermined signal, or it may be allowed to adapt by using a long-term frame average with a known transit time.

Note, such methodologies may be used with PPG and heartbeat timing information obtained from a variety of sources, including but not limited to conventional and/or to-be-developed technologies; or, may be obtained one or the other alone or together and/or together with quality signal (PPG variance, estimated PPG signal-to-noise ratio, PPG signal saturation, patient motion accelerometer or gyroscope data, an ECG or impedance measurement noise estimate, or other information about the PPG signal quality) obtained from a wearable device and/or system as described further hereinbelow.

Some further alternatives may include data transmission and/or interpretation by local medical facilities, whether physician or doctor offices or e.g., ICU/CCU (Intensive Care/Coronary Care Units). Accordingly, a device **100** hereof that will measure one or more of a variety of physiologic signals, possibly including electrocardiogram, photoplethysmogram, pulse oximetry and/or patient acceleration signals will be placed on the patient's chest and held with an adhesive as described herein. The device transmits the physiologic signals wirelessly or by wire (e.g., USB) to a nearby base station for interpretation and further transmission, if desired. The wireless transmission may use Bluetooth, Wi-Fi, Infrared, RFID (Radio Frequency Identification) or another wireless protocol. The device may be powered by wireless induction, battery, or a combination of the two. The device **100** monitors physiological signals and/or collects data representative thereof. The collected data may then be transmitted wirelessly or by wire connection, in real time, to the nearby base station. The device may be wirelessly powered by the base station or by battery, removing the need for wires between the patient and the station.

Relatedly and/or alternatively, patients or wearers may be monitored wirelessly in a hospital, including an ICU (Intensive Care Unit) or other facility. As such, an ECG signal may be measured on a patient using a small, wireless patch device hereof. The signal is then digitized and transmitted wirelessly to a receiver. The receiver converts the signal back to analog, such that it approximates the original ECG signal in amplitude. This output is then presented to an existing hospital ECG monitor through the standard electrode leads. This allows the patient to be monitored using existing hospital infrastructure without any lead wires necessarily connecting the patient to the monitor. Patient chest impedance may be measured as well, allowing the reconstructed signal to approximate the ECG signal not only in amplitude, but in output impedance as well. This can be used to detect a disconnected patch. The output impedance may be continuously variable, or it may have discrete values that may be selected (e.g. one low value for a connected device and one high value to signify the patch has come loose). The impedance may also be used to signify problems with the wireless transmission.

Other alternative implementations may include coupling one or multiple sensors mounted to the forehead of an infant. Initially, a method of obtaining oxygen saturation data by mounting a device in the forehead of an infant might be used as introduced. However, an expansion or alternative may include coupling oxygen saturation sensors with relative position and temperature sensors on the same forehead-

mounted device. The combined data can be utilized to ascertain if an infant is in any danger of suffocation due to a face-down position.

Thus, some of the alternative combinations hereof may include one or more of: 1) medical grade adhesives (from many possible sources) selected for their ability to maintain in intimate contact with the skin without damaging it, for several days (up to, say 10 days or two weeks in some examples), as well as operability with different types of sensors; 2) conductive electrodes or photo-sensitive detectors able to supply electrical signals from the skin or from the photo-response of cutaneous or subcutaneous tissues to photo-excitation; 3) amplifiers, microprocessors and memories, capable of treating these signals and storing them; 4) power supply for the electronics hereof with stored or with wirelessly accessible re-chargeability; 5) flex circuits capable of tying the above elements together within a flexible strip capable of conforming to a cutaneous region of interest.

Examples of physiological parameters that may be subject to monitoring, recordation/collection and/or analyzing may include one or more of: electrocardiograms, photo responses of photo-excited tissues for e.g., oxygen saturation of blood; pulse rates and associated fluctuations; indications of physical activity/acceleration. One or more of these may be used in monitoring ambulatory cardiac outpatients over several days and nights, which could thereby provide for recording, for post-test analysis, several days' worth of continuous ECG signals together with simultaneous recording of O<sub>2</sub> saturation and an index of physical exertion. Similarly, one or more of these may be used in monitoring ambulatory pulmonary outpatients over several days and nights for recording, for post-test analysis, O<sub>2</sub> saturation together with simultaneous recording of an index of physical activity. Alternatively and/or additionally, one or more of these could be used for monitoring in-patients or other patients of interest, as for example neonates, wirelessly (or in some cases wired), whether in clinics, emergency rooms, or ICUs, in some instances detecting the parameters of EKG, O<sub>2</sub> and/or physical exertion, but instead of storing them would transmit them wirelessly to either a bedside monitor or a central station monitor, thus freeing the patient from attachment to physical wires. In particular, devices hereof may be adhered to the forehead of a neonate for monitoring respiration and oxygen saturation. In further alternatives, devices hereof may be used to monitor respiration and ECG of patients suffering from sleep apnea.

An exemplary computer system or computing resources which may be used herewith will now be described, though it should be noted that many alternatives in computing systems and resources may be available and operable within the reasonably foreseeable scope hereof so that the following is intended in no way to be limiting of the myriad possible computational alternatives properly intended within both the spirit and scope hereof.

Some of the implementations of the present developments include various steps. A variety of these steps may be performed by hardware components or may be embodied in machine-executable instructions, which may be used to cause a general-purpose or special-purpose processor programmed with the instructions to perform the steps. Alternatively, the steps may be performed by a combination of hardware, software, and/or firmware. As such, FIG. 4 is an example of computing resources or a computer system **400** with which implementations hereof may be utilized. According to the present example, a sample such computer system **400** may include a bus **401**, at least one processor **402**, at

least one communication port **403**, a main memory **404**, a removable storage media **405**, a read only memory **406**, and a mass storage **407**. More or fewer of these elements may be used in a particular implementation hereof.

Processor(s) **402** can be any known processor, such as, but not limited to, an Intel® Itanium® or Itanium 2® processor(s), or AMD® Opteron® or Athlon MP® processor(s), or Motorola® lines of processors. Communication port(s) **403** can be any of an RS-232 port for use with a modem based dialup connection, a 10/100 Ethernet port, a Universal Serial Bus (USB) port, or a Gigabit port using copper or fiber. Communication port(s) **403** may be chosen depending on a network such a Local Area Network (LAN), Wide Area Network (WAN), or any network to which the computer system **400** connects or may be adapted to connect.

Main memory **404** can be Random Access Memory (RAM), or any other dynamic storage device(s) commonly known in the art. Read only memory **406** can be any static storage device(s) such as Programmable Read Only Memory (PROM) chips for storing static information such as instructions for processor **402**.

Mass storage **407** can be used to store information and instructions. For example, hard disks such as the Adaptec® family of SCSI drives, an optical disc, an array of disks such as RAID, such as the Adaptec family of RAID drives, or any other mass storage devices may be used.

Bus **401** communicatively couples processor(s) **402** with the other memory, storage and communication blocks. Bus **401** can be a PCI/PCI-X or SCSI based system bus depending on the storage devices used.

Removable storage media **405** can be any kind of external hard-drives, floppy drives, IOMEGA® Zip Drives, Compact Disc-Read Only Memory (CD-ROM), Compact Disc-Recordable (CD-RW), Digital Video Dis-Read Only Memory (DVD-ROM).

The components described above are meant to exemplify some types of possibilities. In no way should the aforementioned examples limit the scope of the invention, as they are only exemplary embodiments.

Embodiments of the present invention relate to devices, systems, methods, media, and arrangements for monitoring and processing cardiac parameters and data, inter alia. While detailed descriptions of one or more embodiments of the invention have been given above, various alternatives, modifications, and equivalents will be apparent to those skilled in the art without varying from the spirit of the invention. Therefore, the above description should not be taken as limiting the scope of the invention, which is defined by the appended claims.

What is claimed is:

1. A device for monitoring one or more physiological parameters, the one or more physiological parameters including blood oxygenation, the device being adapted to be adhered to the skin of a subject for the physiological parameter monitoring; the device comprising:

- a substrate;
- a conductive sensor connected to the substrate;
- a plurality of pulse oximetry sensors connected to the substrate, and,
- a plurality of light sources for one or more wavelengths; and,
- an encapsulant that is configured to encapsulate the sensor, the plurality of pulse oximetry sensors and the plurality of light sources and is in operative contact with the sensor, the plurality of pulse oximetry sensors and the plurality of light sources and is configured for

light transmission therethrough and to not allow an interference airgap between the sensor, the plurality of pulse oximetry sensors and the plurality of light sources and the encapsulant, providing no internal reflective surface;

the encapsulant also being configured to be disposed in operative contact with the skin of a subject without any other cover between the skin and the encapsulant; and, the encapsulant also being configured to provide at least one radius of curvature of at or between 20 mm and 40 mm.

2. A device according to claim 1 the plurality of pulse oximetry sensors and light sources being configured to provide for interrogation of a wider area of capillary bed in order to reduce local motion artifact effects; wider area defined by being wider than achievable by a single sensor or a single light source per wavelength.

3. A device for reducing noise in health monitoring including a wearable health monitoring device having at least one sensor for health monitoring;

the wearable health monitoring device having:

a composite adhesive having at least one conductive portion applied adjacent the sensor; and, including one or more structural adaptations for the at least one sensor for receiving signals with reduced noise;

the one or more structural adaptations including a convex lens for light transmission therethrough;

the convex lens being an encapsulant that encapsulates the sensor and is in operative contact with the sensor and is configured for light transmission therethrough and to not allow an interference airgap between the sensor and the encapsulant, providing no internal reflective surface;

the encapsulant also being configured to be disposed in operative contact with the skin of a subject without any other cover to be disposed between the skin and the encapsulant; and,

the encapsulant also being configured to provide at least one radius of curvature of at or between 20 mm and 40 mm.

4. A device according to claim 3 the convex lens being configured to be disposed in operative contact with a wearer's skin.

5. A device according to claim 3 the convex lens being configured to be disposed in operative contact with a wearer's skin at or adjacent the wearer's/user's forehead or chest.

6. A device according to claim 3 further comprising one or more LEDs, the convex lens encapsulant being configured to encapsulate the one or more LEDs.

7. A device according to claim 3 the convex lens encapsulant being configured to encapsulate the one or more LEDs and being in operative contact with at least one of the one or more LEDs not allowing an interference airgap between the at least one of the one or more LEDs and the encapsulant.

8. A device according to claim 3 the convex lens being one or more of clear, colorless, silicone and medical grade silicone.

9. A device according to claim 8 the convex lens being made from medical grade silicone that is one or more of clear, colorless, soft, low durometer, tacky gel, or has high-tack adhesives embedded on both sides.

10. A device according to claim 9 the silicone comprising one or both:

conformance of the lens to one or both the electronic sensors and skin, or

exhibition of motion artifact reduction by limiting movement between the skin-lens-sensor interface.

11. A device according to claim 9 the convex lens being configured to be trapped between layers of the composite adhesive strip of a wearable health monitoring device, with a raised portion the size of a rectangular opening in the adhesive strip that allows the convex lens to protrude slightly on the patient side of the adhesive strip. 5

12. A device according to claim 3 the one or more structural adaptations being used for pulse oximetry. 10

13. A device according to claim 3 the one or more structural adaptations being disposed for and configured for maintained indented operative contact with the wearer's/user's skin.

14. A device according to claim 3 being configured for providing for transmission of LED waves therethrough to the wearer's skin without interfering transmission thereinto. 15

15. A device according to claim 14 being configured for providing for reception of reflected transmissions of LED waves therethrough from the wearer's skin to the sensor without interfering transmission therethrough. 20

\* \* \* \* \*

专利名称(译)	健康监测系统和方法		
公开(公告)号	<a href="#">US10080527</a>	公开(公告)日	2018-09-25
申请号	US14/565414	申请日	2014-12-09
[标]申请(专利权)人(译)	RHYTHM诊断SYST		
申请(专利权)人(译)	RHYTHM诊断系统公司.		
当前申请(专利权)人(译)	RHYTHM诊断系统, INC.		
[标]发明人	GOLDA GEORGE STEFAN MOYER DANIEL VAN ZANDT MARRIOTT MARK P ELETR SAM ONEIL BRUCE		
发明人	GOLDA, GEORGE STEFAN MOYER, DANIEL VAN ZANDT MARRIOTT, MARK P. ELETR, SAM O'NEIL, BRUCE		
IPC分类号	A61B5/00 A61B5/0205 A61B5/026 A61B5/0295 A61B5/0408 A61B5/11 A61B5/0432 A61B5/0402 A61B5/08 A61B5/021 A61B5/024 A61B5/0456 A61B5/1455		
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审查员(译)	THOMSON, WILLIAM		
优先权	61/932094 2014-01-27 US 61/932100 2014-01-27 US 62/000975 2014-05-20 US 62/008959 2014-06-06 US 61/710768 2012-10-07 US 62/038768 2014-08-18 US		
其他公开文献	US20150094552A1		
外部链接	<a href="#">Espacenet</a>		

#### 摘要(译)

用于降低健康监测中的噪声的系统, 方法和设备包括监测系统, 接收健康信号的方法和/或设备和/或具有至少一个用于健康监测的电极或传感器。

