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(54) **CONGESTIVE HEART FAILURE MONITOR**

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(57) **ABSTRACT**

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A device-implemented method is disclosed for early detection and monitoring of congestive heart failure in a patient. Ongoing measurements of impedance of a portion of the patient's body generally occupied by the lungs are performed by an implanted device, and, when the impedance measurements are determined by internal circuit components of the device to exceed a predetermined threshold value indicative of a need for immediate attention to a condition of congestive heart failure, a patient and/or physician alert is emitted by the device. An implant site at the left lower anterior lateral hemithorax is preferred.

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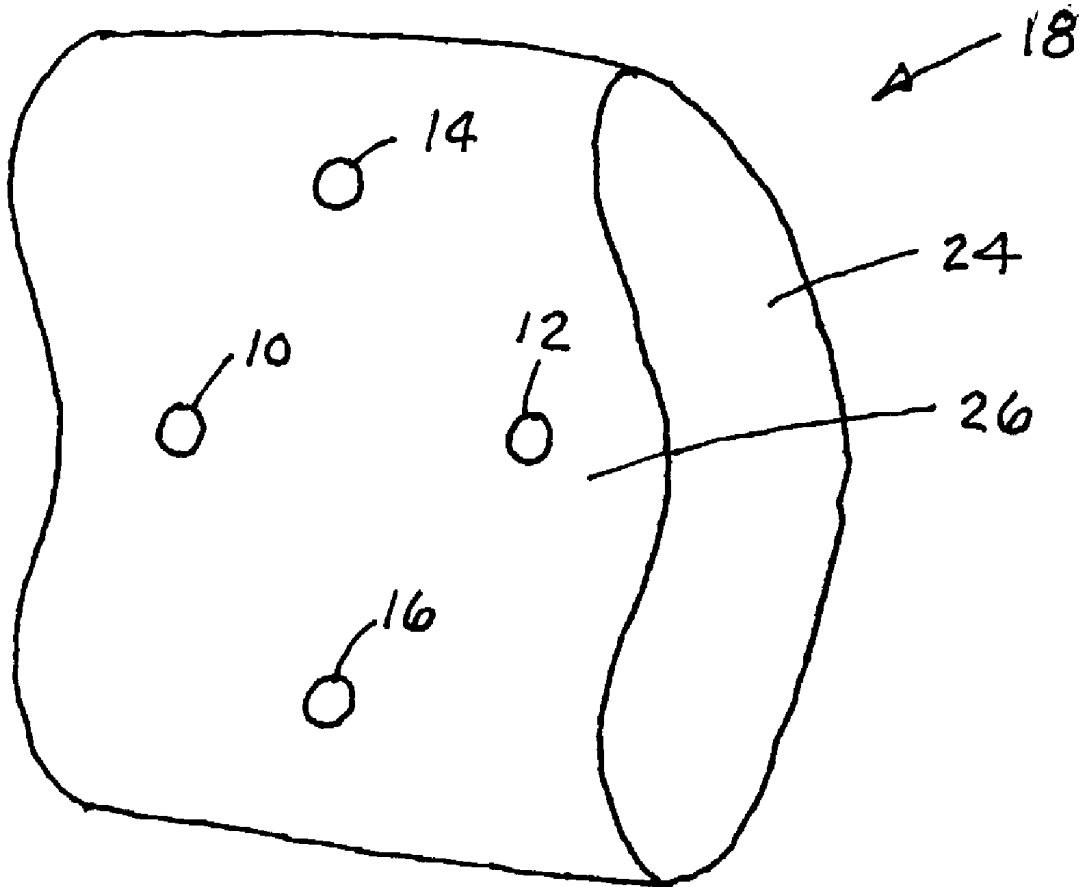


FIG. 1

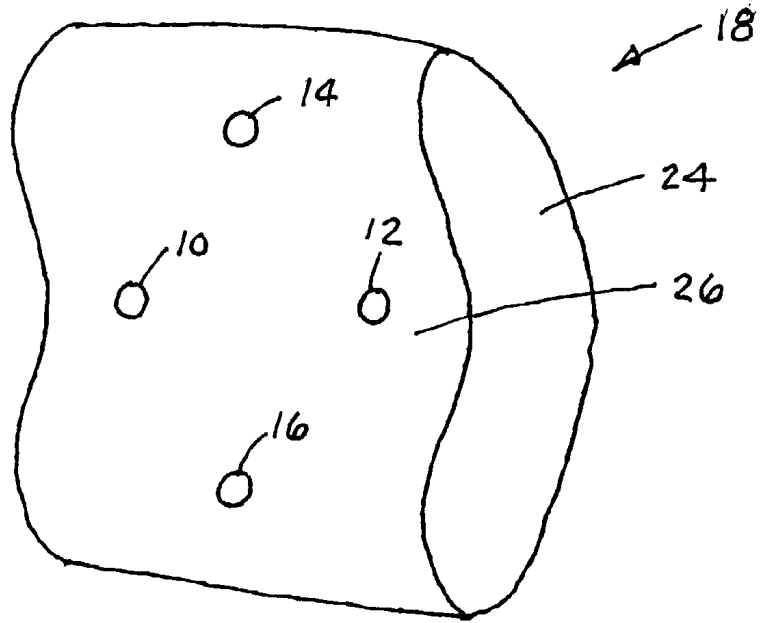
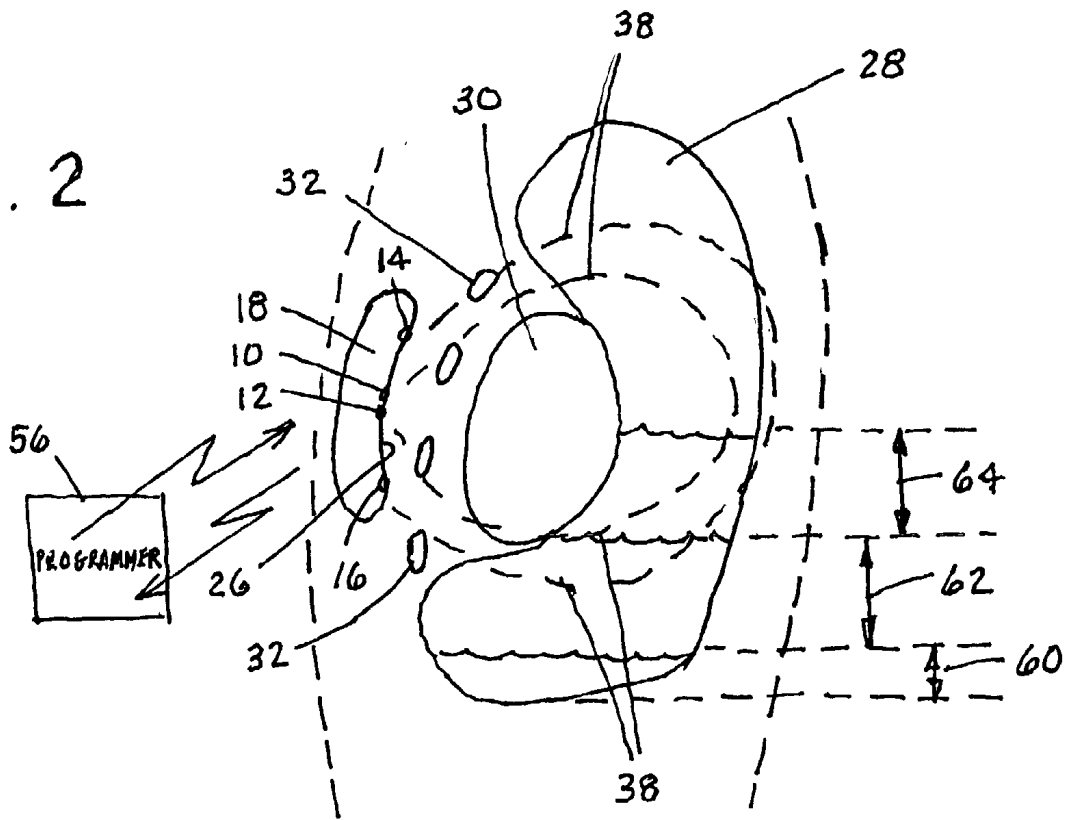


FIG. 2



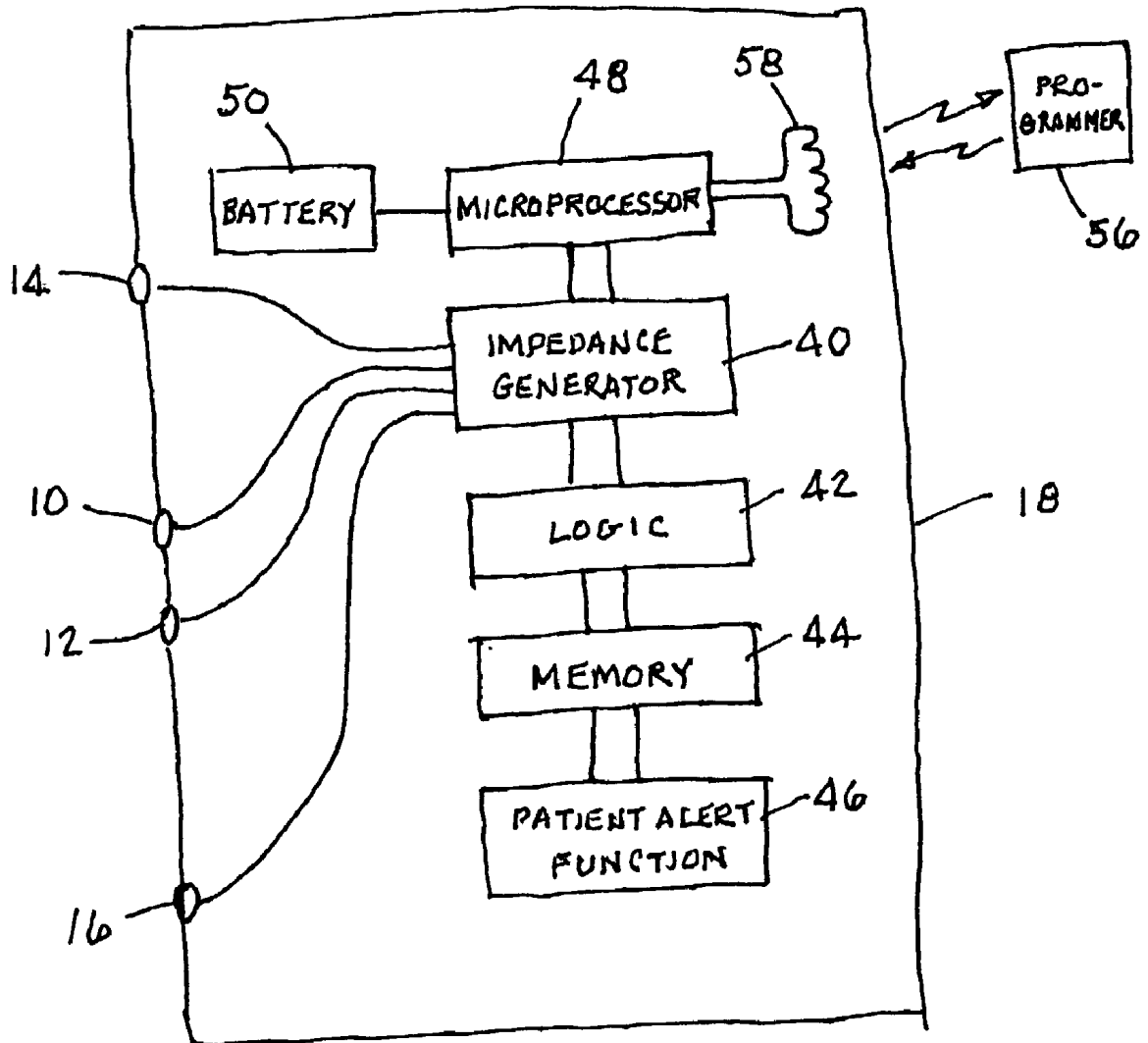


FIG. 3

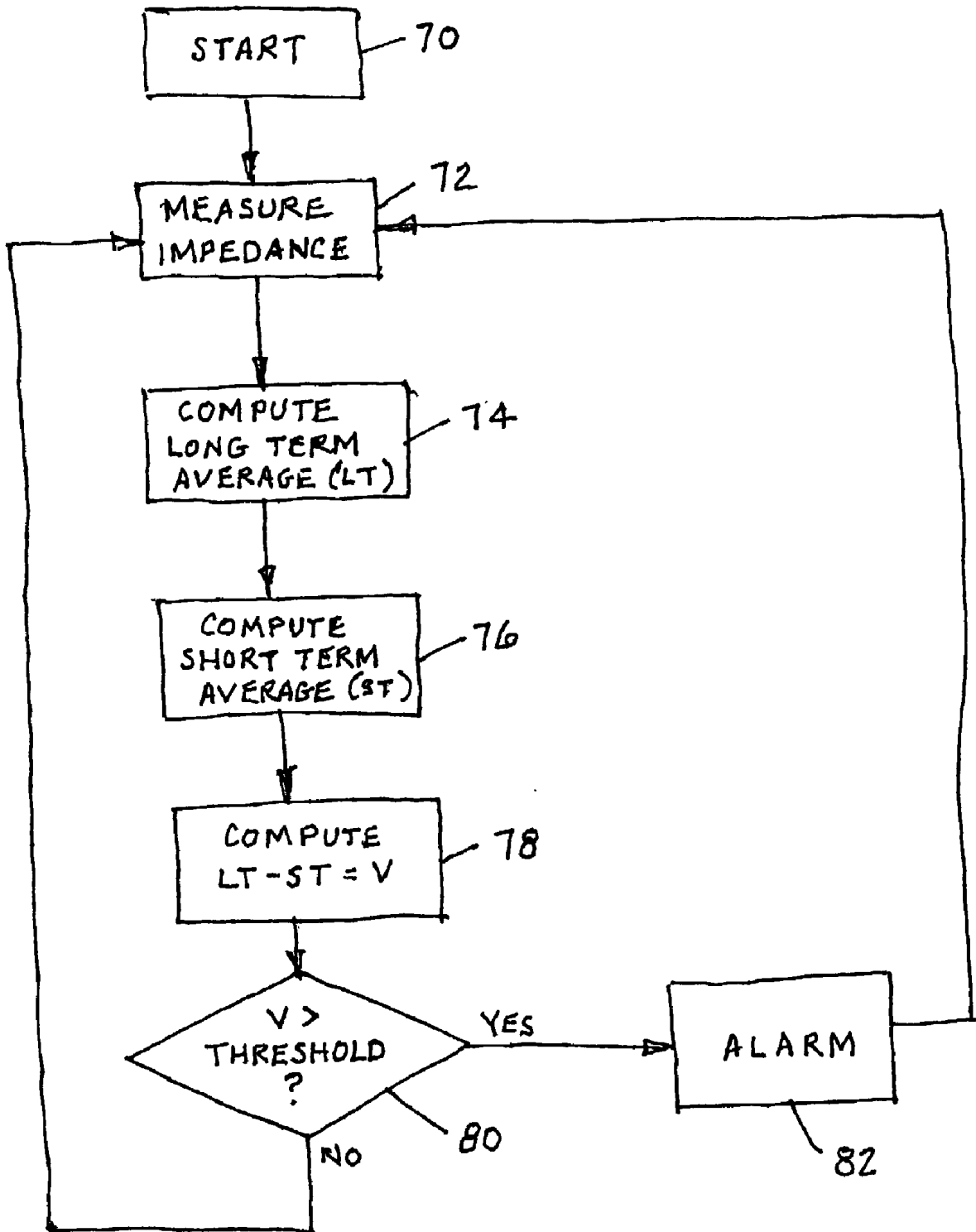


FIG. 4

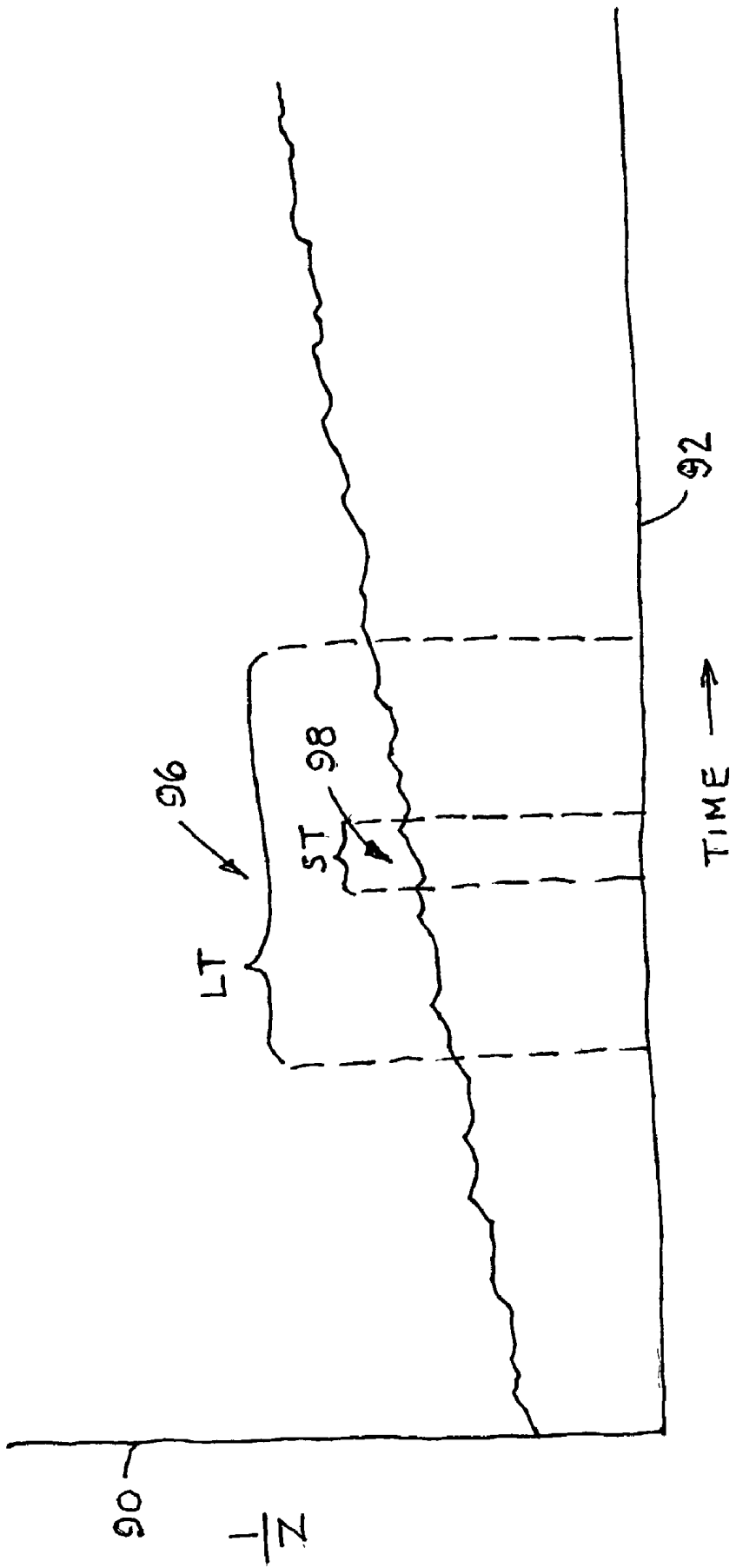


FIG. 5

CONGESTIVE HEART FAILURE MONITOR

BACKGROUND OF THE INVENTION

[0001] The present invention relates generally to implantable medical devices, and more particularly to an implantable device for detecting and monitoring the progression of congestive heart failure.

[0002] Many patients who have suffered one or more myocardial infarctions subsequently require treatment for congestive heart failure (CHF). The left heart fails while the pumping function of the right heart remains adequate, because the latter has only about 20% of the workload of the former. This leads to an increase in blood volume congested to the lungs, resulting in pulmonary congestion, build up of edema, and congestion of internal organs including the stomach and intestines. Increased fluid in the stomach and intestines reduce their ability to absorb drugs prescribed for treatment of CHF, particularly diuretics. The congestion is often accompanied by a worsening of myocardial function, with consequent drop in blood pressure and reduced renal perfusion, which only further aggravates the congestive situation. Thus, late recognition of congestion leads to increased dosages of oral diuretics that are unsuccessful to treat the condition, ultimately requiring that the patient be hospitalized.

[0003] Avoidance of hospitalization and the pitfalls of late treatment require detection of CHF at an early stage, so that the prescribed drugs can be fully absorbed and effective. If detected early, a combination of diuretics and other drugs can slow the progress of the disease and allow the patient to enjoy an improved lifestyle.

[0004] It is a principal aim of the present invention to provide an implantable heart failure monitor which is capable of achieving very early detection of CHF.

SUMMARY OF THE INVENTION

[0005] The implantable medical device of the present invention is of size smaller than a typical pacemaker device—about the size of a thumb. It is implanted in a subcutaneous pocket formed by the surgeon in the patient's chest, under local anesthesia and minimally invasive requirements. The device includes a hermetically sealed can with appropriate electronic circuitry inside. A set of can-mounted electrodes is used to measure the impedance of the adjacent tissue and most especially the lung tissue. The progressive retention of fluid in the lungs and congestion of the ventricle together result in a reduced impedance measurement that is monitored either continuously or periodically by the device.

[0006] In a preferred mode of operation, the device alerts the patient and the attending physician when a diagnostic threshold is reached which is indicative of the progression of CHF. The overall architecture of the device follows implantable practice, and is a stand-alone monitoring device. However, it should be appreciated that the partitioning of the device is flexible and the division of sensing and analysis structures can be shared between implanted and external (remote, i.e., non-implanted) devices. Conventional programming and telemetry links can be used to connect the implanted device to the remote device.

[0007] For example, the signal processing may be performed entirely internally within the device, or the device

may operate as a data logger and communicate with an external programmer device which participates in data reduction and analysis.

[0008] Although specific structures are shown as being dedicated to specific tasks, it should be apparent that certain functions may be shared if the device is integrated with other diagnostic or therapeutic devices. For example, the electrode set used to determine the impedance of the lungs could be used for additional purposes.

BRIEF DESCRIPTION OF THE DRAWINGS

[0009] The above and other aims, objectives, aspects, features and attendant advantages of the invention will be further understood from a reading of the following detailed description of the best mode presently contemplated for practicing the invention, taken with reference to certain presently preferred implementations and methods, and in conjunction with the accompanying drawings, in which:

[0010] **FIG. 1** is an exterior view of an embodiment of the device;

[0011] **FIG. 2** is a schematic representation of an implantation of the device in the body of a patient;

[0012] **FIG. 3** is a block diagram of the internal circuitry of the device;

[0013] **FIG. 4** is a flow chart illustrating the operation of the device; and

[0014] **FIG. 5** is a graph of the device operation in terms of the reciprocal of impedance over time.

DETAILED DESCRIPTION OF THE PRESENTLY CONTEMPLATED BEST MODE OF PRACTICING THE INVENTION

[0015] The device of the invention is disclosed in the preferred implementation as being a stand-alone diagnostic device to simplify the description of its operation. Throughout the several views of the drawings identical reference numerals indicate identical structure. Views of the device either alone or as implanted are not intended to represent actual or relative sizes.

[0016] **FIG. 1** illustrates the exterior of the device **18** in its presently preferred embodiment. Device **18** includes a circuit module (to be discussed below in conjunction with the description of **FIG. 3**) within a hermetically sealed "can" or case **24** composed, for example, of titanium. The size of the case **24** is clearly dictated by the size of the internal circuit components and wiring included printed circuit board(s) and other forms, but preferably is very small, currently about 5.0 cm long by 2.0 cm wide by less than 1.0 cm thick.

[0017] Case **24** has a curvilinear shape which presents a concave shape or surface **26** on one side (in contrast to an edge of the case) and a convex shape on the opposite side of the case. Four surface mounted electrodes **10**, **12**, **14** and **16** are positioned in spaced-apart relationship on the slightly concave surface **26**, with each electrode being electrically insulated from the case **24** itself. The electrodes should be of low polarization, preferably composed of or coated with iridium oxide. By way of example, "inner" electrodes **10** and **12** are spaced apart on the concave side inward of opposite edges and centrally along the length of the case, while

“outer” electrodes **14** and **16** are spaced further apart—preferably, by at least about 4 cm—on that same side inward of opposite edges and centrally along the width of the case. The shape of the case is designed (and preferred) to conform to the shape of the anatomy of the human chest. With the concave side of the case placed toward the interior of the body within the implant site of device **18**, the device is prevented from turning within its subcutaneous pocket which would otherwise position the surface electrodes at the wrong side—namely, toward the exterior of the patient’s body. The reason for this positioning will become apparent as the description proceeds.

[0018] The most preferred implant site of the device is the left lower anterior lateral hemithorax of the patient’s body as shown in **FIG. 2**. In part, this is because optimal sensing occurs with the device placed slightly to the left of the patient’s midline. **FIG. 2** illustrates in schematic form a side view of a patient (in phantom) with the device **18** implanted in a pectoral of the chest over the basal region of lungs **28** and heart **30**, outside the rib cage **32**. An implantation at the preferred site places the device on the left anterior thorax side between the 5th and 6th intercostals space. In this position of the device, an impedance signal is developed which represents the impedance of the lungs and heart tissue by virtue of current injected into the circuit path that establishes a field through that portion of the body from device **18**.

[0019] **FIG. 3** illustrates the exemplary circuit module within device **18**. An impedance signal generator **40** injects signal current into the body, preferably through “inner” electrodes **10** and **12**. The current traverses the circuit path through the body portion of interest and has a return path through “outer” electrodes **14** and **16**. Field lines **38** (**FIG. 2**) attributable to current flowing from the electrodes emanate from the concave side **26** of device **18**, and, together with the electrode spacing, define the “viewing volume” of the device for the impedance sensing circuitry. Electrode spacing of at least four cm between the outer electrodes **14**, **16** will allow a measurement to a depth of up to 10 cm of lung tissue in the anterior lateral lower left thorax. The field lines produced by current through the circuit path intersect the lung tissue **28** and are somewhat less influenced by the volume of the heart **30**.

[0020] The circuit module within device **18** is powered by a preferably lithium-ion battery **50**. Impedance generator **40** is controlled by microprocessor **48**, as is logic **42** for analysis and memory **44** for data. Measured values of impedance are stored in memory **44**, and used by microprocessor **48** to calculate long-term and short-term averages of the measured impedance values. A threshold detector **46** may be incorporated in device **18** as a patient alert function or alarm (e.g., by emitting an acoustic signal, vibrations, or low level pulses for local muscle contractions, recognizable by the patient) indicative of a need for immediate intervention when impedance associated with fluid level **64**, for example, is detected. Such an alarm condition may also be signaled by telemetry from an antenna or coil **58** within the circuit module at the microprocessor, normally used to transmit the other impedance data, to a remote programmer **56** to monitor and log the progress of the disease and the therapeutic effect of treatment for review by the patient’s physician.

[0021] The device is adapted to monitor impedance at a digital rate of 128 Hz, for partitioned analysis of contractile cardiac function, pulmonary ventilation function and long term pulmonary impedance, over an average of 72 hours or more. Signal processing allows deviation from basic impedance of the body region of interest, especially the lungs, to be detected as an early monitoring of a decrease in lung impedance, indicative of increasing congestion by fluid content in the lungs. The decrease in lung impedance associated with CHF occurs as the lungs fill with fluid, which is a considerably better electrical conductor than the normal lung tissue. Exemplary values of impedance for lung tissue are 400-1,000 ohms per centimeter (Ω/cm), compared with 50 Ω/cm for fluid.

[0022] Representative fluid levels accumulated in the lungs are illustrated in **FIG. 2** at **60**, **62** and **64**. Level **60** represents the relative additional amount of fluid associated with normal lung function. Level **62** represents the relative amount of fluid present for a compromised lung function associated with CHF. And level **64** is the relative still additional amount of fluid associated with severely reduced lung function requiring immediate attention, indicative of advanced CHF.

[0023] The device **18** may be designed to provide a threshold or trigger level at an accumulation of fluid corresponding approximately to level **64**. Algorithms are used to convert real time measurements into a diagnostic indication of congestion. The device may be operated continuously and the impedance data are then analyzed in kind. ECG data may be used additionally, detected at the outer electrodes **14** and **16** to improve the capability of the device to discern impedance changes in the heart.

[0024] **FIG. 4** is a flow chart of an exemplary detection algorithm used by the device **18**. On commencement counters are initialized and impedance generator **40** is turned on to inject signal current into the body via the inner pair of electrodes **10**, **12** (start, **70**). The impedance signal current is preferably a rectangular biphasic pulse wave at a rate of 128 Hz and a peak-to-peak amplitude of 1 milliampere (ma), or, alternatively, an alternating current in a range from 5 microamperes (μa) to 10 μa . The pulses may be injected with considerably higher energy content than the AC wave because of their very short duration (e.g., 15 μsec or less), with no risk of myocardial depolarization, and are capable of detecting cardiac changes as well as pulmonary changes.

[0025] Impedance is then calculated (**72**) from a measurement of the resulting voltage at the outer pair of electrodes **14**, **16**. Alternatively, a fixed voltage may be applied across the excitation (inner) electrodes and the resulting current measured at the measurement (outer) electrodes reflects the impedance. A long-term average of the impedance value is computed (**74**), covering a period ranging from days to weeks as a running average. A short-term average of the impedance value is also computed (**76**), covering a period from hours to days. The difference between the long-term (LT) and short-term (ST) averages is calculated (**78**) as a slope measurement (V) indicative of deterioration of the lung condition, to detect accelerating lung congestion. If the value V exceeds a predetermined threshold (slope) value (**80**), an alarm condition is indicated and the patient alert function (**46**, **FIG. 3**) is initiated. In either case (an alarm condition or not), another impedance measurement is performed (**72**) and the processing cycle is repeated.

[0026] In the description of FIG. 2, the detection of lung congestion requiring immediate attention was the result of a simple volume measurement. In practice, however, a slope measurement is preferred to determine when an alarm condition is occurring or has occurred, because the variability of impedance signals makes it more difficult to achieve accurate threshold detection by volume measurement.

[0027] FIG. 5 is a graph of the device operation using the exemplary detection algorithm represented by the flow chart of FIG. 4. The vertical axis 90 is conductance, the reciprocal of impedance ($1/Z$). Therefore, the greater the lung congestion (i.e., the larger the fluid volume in the patient's lungs), the higher the value of the term $1/Z$. The horizontal axis 92 represents time. The long-term average of the impedance measurement has a characteristic value that filters out the short-term variations of the measurement. In the Figure, the LT value 96 of curve or slope 94 exhibits a more gradual slope than the ST value 98. The difference between the two is used to determine whether an alarm condition is occurring ($LT-ST=V \geq \text{threshold}$).

[0028] In addition to the baseline impedance, impedance measurements at the frequency of 128 Hz can detect impedance changes with every pumping cycle, to provide indirect information on stroke volume, heart rate, and cardiac output calculated therefrom. Additionally, by adequate low pass filtering, the indirect tidal volume of ventilation can be separated out, as well as respiratory rate. Typically, ventilation is in a range from 0.2 Hz to 0.8 Hz, while cardiac events are in a range from 1 Hz to 3 Hz. Both subsignals, cardiac and ventilation, are used in addition to determine congestive heart failure indicated by increase in stroke volume, decrease in tidal volume, increase in heart rate, and increase in ventilation rate.

[0029] A power saving can be achieved in the device by limiting the impedance measurement to fixed periods separated by intervals of no measurement, or even sporadic measurements, rather than performing continuous impedance measurements.

[0030] The impedance measurement electrodes may be used to monitor the patient's ECG, as well as to obtain the raw data necessary for calculating absolute impedance and long- and short-term averages of impedance. Also, the cardiac- and ventilation-derived impedance phenomena may be correlated to the ECG for better evaluation.

[0031] It is important to consider the factor of where the measurements are taken as well as the manner of obtaining the measurements. For example, the spacing between the measurement electrodes 14, 16 determines the volume and area of measurement. By spacing these electrodes at least 4 cm apart, the depth of measurement is increased beyond only the tissue in the immediate vicinity of the electrode, to the tissue for which specific impedance and impedance changes are sought to be measured, typically to a depth of up to 10 cm of lung tissue. Also, performing the measurements on the patient's left side rather than the right side, and particularly on the anterior lateral lower left thorax, enables early detection of changes in left ventricular parameters and congestion in the lung circulatory system, rather than limiting the measurement to tissue and liver impedance which is primarily a function of congestion of the right heart. Additionally, at this preferred location for conducting the measurements, the cardiac phenomena and stroke volume

dependent impedance changes are more easily detected than on the right side or the upper left thorax where impedance changes primarily follow blood circulation.

[0032] Although a presently contemplated best mode, preferred embodiment and method of practicing the invention have been described in this specification, it will be apparent to those skilled in the art from a consideration of the foregoing description, that variations and modifications of the disclosed embodiments and methods may be made without departing from the spirit and scope of the invention. It is therefore intended that the invention shall be limited only to the extent required by the appended claims and the rules and principles of applicable law.

What is claimed is:

1. A device-implemented method of detecting and monitoring congestive heart failure in a patient, which comprises the steps of:

performing ongoing measurements of impedance of a portion of the patient's body generally occupied by the lungs, and

determining when the impedance measurements exceed a predetermined threshold value indicative of a need for immediate attention to a condition of congestive heart failure.

2. The device-implemented method of claim 1, including performing said ongoing measurements continuously.

3. The device-implemented method of claim 1, including performing said ongoing measurements periodically to reduce power consumption of the device.

4. The device-implemented method of claim 1, including performing said ongoing measurements from time to time to reduce power consumption of the device.

5. The device-implemented method of claim 1, including performing said impedance measurements in part by injecting electrical current into said body portion.

6. The device-implemented method of claim 5, including injecting said electrical current into said body portion through surface electrodes of the device.

7. The device-implemented method of claim 5, including performing said impedance measurements in part by monitoring said injected electrical current returning via surface electrodes of the device positioned in said body portion.

8. The device-implemented method of claim 5, including injecting said electrical current in the form of a biphasic pulse wave.

9. The device-implemented method of claim 1, including performing said impedance measurements outside the patient's thoracic cage.

10. The device-implemented method of claim 9, including performing said impedance measurements using electrodes of the device outside the patient's vascular system.

11. The device-implemented method of claim 1, including averaging said impedance measurements over long term and short term periods, and calculating the difference between the long term and short term averages representative of the slope of the reciprocal of impedance over time.

12. The device-implemented method of claim 11, including comparing said slope of the reciprocal of impedance over time against said predetermined threshold value, and triggering a patient alert signal when said slope exceeds the predetermined threshold value.

13. The device-implemented method of claim 7, including using said surface electrodes of the device additionally to monitor the patient's ECG.

14. The device-implemented method of claim 1, including performing said impedance measurements with the device implanted on the lower left anterior lateral hemithorax.

15. The device-implemented method of claim 1, wherein said body portion further encompasses the patient's heart, including performing said impedance measurements by means of a signal injected into said body portion from the device and retrieved as a signal subdivided into a cardiac portion, a pulmonary portion, and a total impedance portion.

16. A body-implantable device adapted to detect and monitor congestive heart failure in a patient, comprising a circuit module having surface electrodes of the device arranged and adapted, when the device is implanted, for exposure to tissue in a portion of the patient's body generally occupied by the lungs, to perform ongoing measurements of impedance of said body portion and to determine when the impedance measurements exceed a predetermined threshold value indicative of a need for immediate attention to a condition of congestive heart failure.

17. The device of claim 16, wherein said circuit module includes a current generator for injecting current into said body portion through an excitation pair of said surface electrodes.

18. The device of claim 16, wherein said circuit module includes detection apparatus for monitoring at a measurement pair of said surface electrodes an electrical parameter attributable to said injected current, reflecting impedance changes.

19. The device of claim 18, wherein the electrodes of said measurement pair of surface electrodes are spaced apart by at least 4 cm.

20. The device of claim 16, wherein said circuit module performs said impedance measurements according to an algorithm in which the measured impedance is averaged over long term and short term periods, the difference between the long term and short term averages is calculated as representing the slope of the reciprocal of impedance over time for comparison with said predetermined threshold value.

21. The device of claim 16, wherein said circuit module is contained within a case having a curvilinear shape adapted to conform to the shape of a portion of the patient's body at the implant site.

22. The device of claim 21, wherein said curvilinear shape of the case conforms to the curvature of the patient's rib cage in the vicinity of the implant site.

23. A body-implantable medical device for monitoring the condition of a patient suffering from congestive heart failure, comprising circuitry including plural surface electrodes on the device for measuring impedance between a measurement pair of said electrodes from a predetermined electrical parameter injected in a circuit path between an excitation pair of said electrodes, such that when said device is implanted at a site where said circuit path includes the patient's heart and lungs said impedance measurement is indicative of lung congestion.

24. The device of claim 21, wherein said device is shaped to be implanted at a site on the left lower anterior lateral hemithorax of the patient's body.

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摘要(译)

公开了一种设备实现的方法，用于早期检测和监测患者的充血性心力衰竭。通常由肺部占据的患者身体的一部分的阻抗的持续测量由植入装置执行，并且当阻抗测量由装置的内部电路部件确定为超过指示需要立即的预定阈值时注意充血性心力衰竭的情况，设备发出患者和/或医生警报。左下前外侧半胸的植入部位是优选的。

