

US007686012B2

(12) **United States Patent**  
**Orr et al.**

(10) **Patent No.:** **US 7,686,012 B2**  
(45) **Date of Patent:** **\*Mar. 30, 2010**

(54) **APPARATUS FOR NON-INVASIVELY MEASURING CARDIAC OUTPUT**  
  
(75) Inventors: **Joseph A. Orr**, Salt Lake City, UT (US); **Scott A. Kofoed**, Salt Lake City, UT (US); **Dwayne Westenskow**, Salt Lake City, UT (US); **Michael B. Jaffe**, Cheshire, CT (US)

(73) Assignee: **RIC Investments, LLC**, Wilmington, DE (US)

(\* ) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 97 days.

This patent is subject to a terminal disclaimer.

(21) Appl. No.: **11/120,103**

(22) Filed: **May 2, 2005**

(65) **Prior Publication Data**  
US 2005/0203432 A1 Sep. 15, 2005

**Related U.S. Application Data**

(60) Continuation of application No. 10/657,909, filed on Sep. 8, 2003, now Pat. No. 6,908,438, which is a division of application No. 09/767,363, filed on Jan. 23, 2001, now Pat. No. 6,648,831, which is a continuation of application No. 08/770,138, filed on Dec. 19, 1996, now Pat. No. 6,306,098.

(51) **Int. Cl.**  
*A61M 15/00* (2006.01)  
*A61M 16/00* (2006.01)  
*A61B 5/00* (2006.01)

(52) **U.S. Cl.** ..... **128/200.24**

(58) **Field of Classification Search** ..... None  
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

3,910,261 A 10/1975 Ragsdale et al.  
4,192,301 A 3/1980 Hardwick  
4,239,038 A 12/1980 Holmes  
4,265,235 A 5/1981 Fukunaga  
4,941,476 A 7/1990 Fisher

(Continued)

FOREIGN PATENT DOCUMENTS

WO WO 98/12963 4/1998

OTHER PUBLICATIONS

Gama de Abreu, Marcelo, et al., Is the Partial CO<sub>2</sub> Rebreathing Technique a Useful Tool for Trending Pulmonary Capillary Blood Flow During Adjustments of Peep?, Crit. Care Med. (1998), vol. 26, No. 1 (Suppl.), A106, Abstract #237, (1 page).\*

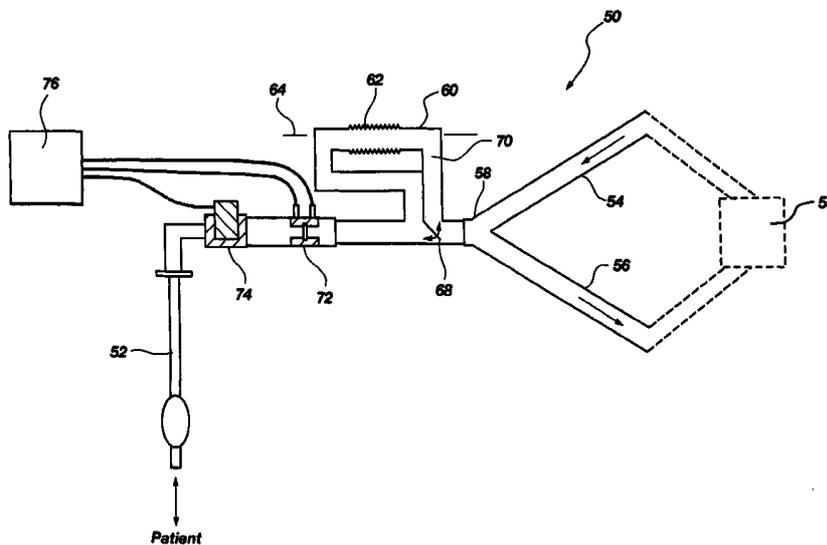
(Continued)

*Primary Examiner*—Robert L Nasser

(57) **ABSTRACT**

Apparatus and methods for non-invasively determining cardiac output using partial re-breathing techniques are disclosed in which the apparatus is constructed with an instantaneously adjustable deadspace for accommodating differences in breathing capacities of various patients. The apparatus is constructed of inexpensive elements, including a single two-way valve which renders the apparatus very simple to use and inexpensive so that the unit may be readily disposable. The method of the invention provides a novel means of estimating cardiac output based on alveolar CO<sub>2</sub> values rather than end-tidal CO<sub>2</sub> values as previously practiced. A program for calculating cardiac output is also disclosed.

**13 Claims, 12 Drawing Sheets**



## U.S. PATENT DOCUMENTS

4,947,860	A	8/1990	Fisher		
4,949,724	A	8/1990	Mahutte et al.		
5,299,579	A	4/1994	Gedeon et al.		
5,402,796	A	4/1995	Packer et al.		
5,642,726	A	7/1997	Owens et al.		
5,752,509	A *	5/1998	Lachmann et al.	.....	128/204.23
5,778,872	A *	7/1998	Fukunaga et al.	.....	128/202.27
5,782,774	A	7/1998	Shmulewitz		
5,836,300	A	11/1998	Mault		
5,971,934	A	10/1999	Scherer et al.		
5,983,891	A	11/1999	Fukunaga		
6,003,511	A	12/1999	Fukunaga et al.		
6,227,196	B1	5/2001	Jaffe et al.		
6,251,082	B1	6/2001	Rayburn		
6,564,799	B2	5/2003	Fukunaga et al.		
6,648,832	B2	11/2003	Orr et al.		
7,018,340	B2	3/2006	Jaffe et al.		

## OTHER PUBLICATIONS

Gama de Abreu, Marcelo, et al., Measurement of Pulmonary Capillary Blood Flow for Trending Mixed Venous Blood Oxygen Saturation and Oxygen Delivery, Crit. Care Med. (1998), vol. 26, No. 1 (Suppl.), A106, Abstract #238, (1 page).\*

Winkler, Tilo, et al., Pulmonary Capillary Blood Flow by Partial CO<sub>2</sub> Rebreathing: A Simulation Study Using a Bicompartmental Model of Gas Exchange, Crit. Care Med. (1998), vol. 26, No. 1 (Suppl.), A105, Abstract #234, (1 page).\*

Article entitled "Noninvasive Measurement of Cardiac Output Using Partial CO<sub>2</sub> Rebreathing" by John M. Capek and Rob J. Roy (pp. 653-661)- Printed in IEEE Transactions On Biomedical Engineering, vol. 35, No. 9—Sep. 1988.

Article entitled "Noninvasive Measurement of Cardiac Output Using Partial Carbon-Dioxide Rebreathing" by John Michael Capek (title, introductory pages and pp. 127-132)—Printed by UMI Dissertation Services—Dec. 1988.

Article entitled "Noninvasive Pulmonary Blood Flow for Optimal Peep" by A. Gedeon, ICOR AB, Ulvsundavägen 178 B, S-161 30 Bromma, Sweden (pp. 49-58).

Article entitled "Non-invasive pulmonary blood flow measurement by means of CO<sub>2</sub> analysis of expiratory gases" by Bosman, R.J., et al., Intensive Care Med (1991) 17:98-102.

Abstract FC 11 of article entitled "a Non-Invasive Technique for Measurement of Lung Perfusion" by H. Blomquist et al., published in "Monitoring, Computer, Instrumentation", Intensive Care Medicine (1986) 12:172.

Sackner, Marvin A., *Measurement of cardiac output by alveolar gas exchange*, Handbook of Physiology—The Respiratory System IV, Chapter 13: Pulmonary Capillary Blood Flow, pp. 233-255.

Jeretin, S., et al., "A Variable-deadspace Device for Use with the Engström Respirator," Anesthesiology, vol. 34, No. 6, pp. 576-577, Jun. 1971.

Keenan, R.L., et al., "How rebreathing anaesthetic systems control PaCO<sub>2</sub>: studies with a mechanical and a mathematical model," Can. Anaesth. Soc. J., vol. 25, No. 2, pp. 117-121, Mar. 1978 (Abstract).

Article entitled "Noninvasive Pulmonary Blood Flow for Optimal Peep" by A. Gedeon, ICOR AB Ulvsundavägen 178 B, S-161 30 Bromma, Sweden (pp. 49-58), 1985.

Sackner, Marvin A., *Measurement of cardiac output by alveolar gas exchange*, Handbook of Physiology—The Respiratory System IV, Chapter 13: Pulmonary Capillary Blood Flow, pp. 233-255, 1986.

de Abreu, M. Game, et al., *Reliability of the Partial CO<sub>2</sub> Rebreathing Technique for Measurement of Cardiac Output*, Proceedings RC IEEE-EMBS & 14th BMESI—1995 (3 pages).

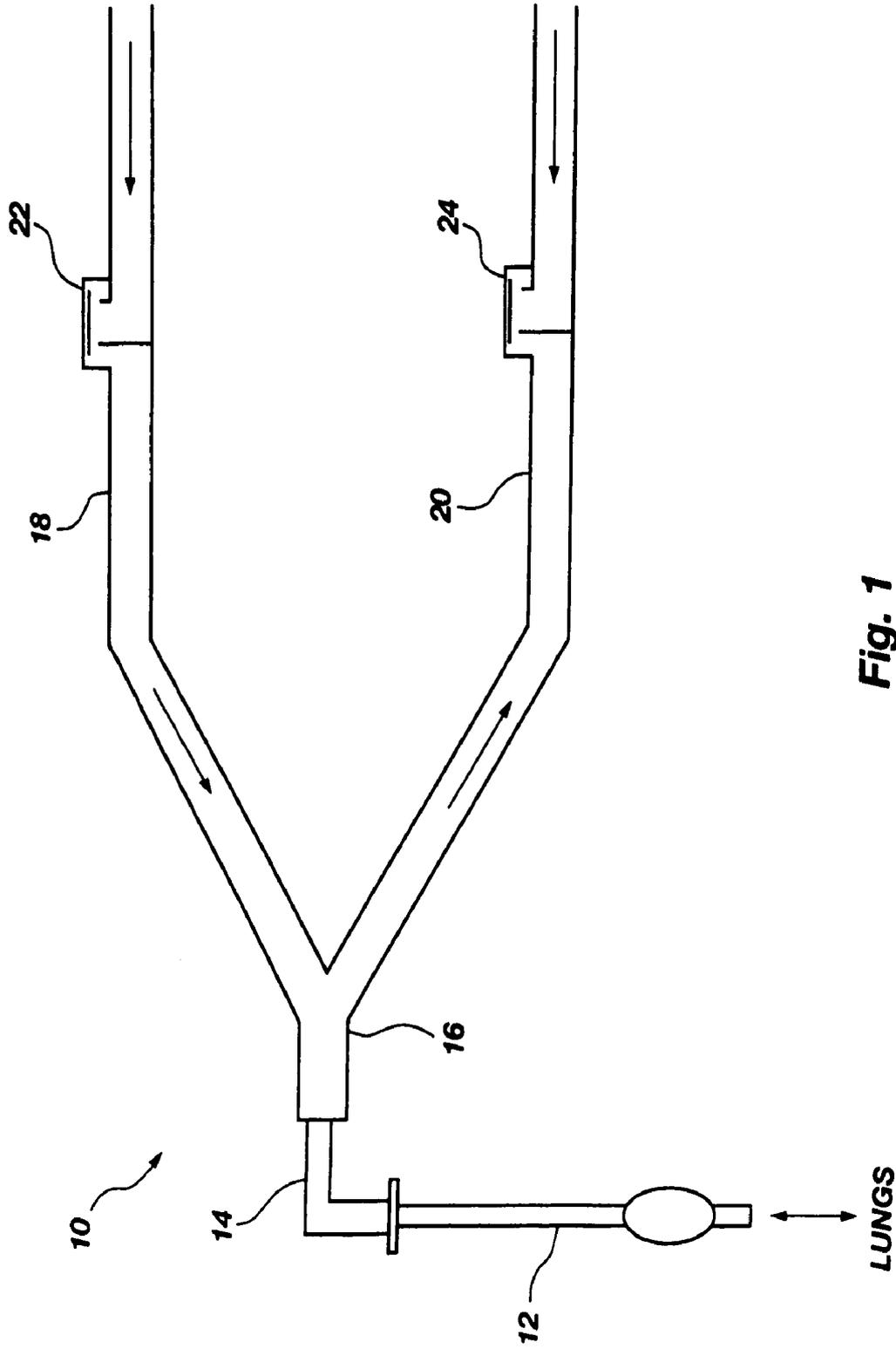
de Abreu, Marcel Gama, et al., *Partial carbon dioxide breathing: A reliable technique for noninvasive measurement of nonshunted pulmonary capillary blood flow*, Crit Care Med 1997, vol. 25, No. 4, pp. 675-683.

Osterlund, B., et al., *A new method of using gas exchange measurements for the noninvasive determination of cardiac output: clinical experiences in adults following cardiac surgery*, Acta Anaesthesiologica Scandinavica 39 (1995), pp. 727-732.

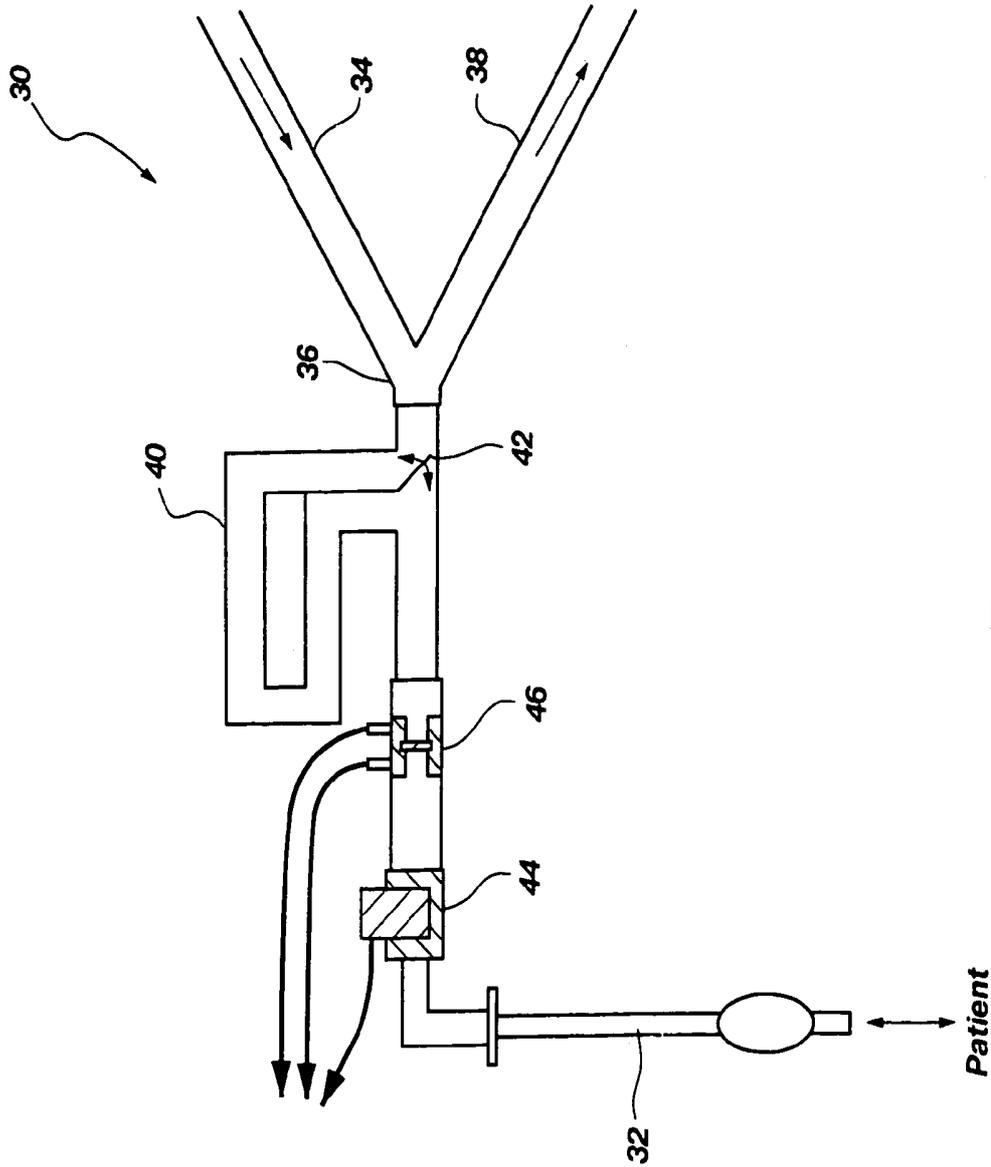
Gedeon, A., et al., *Noninvasive Cardiac Output Determined with a New Method Based on Gas Exchange Measurements and Carbon Dioxide Rebreathing: A Study in Animals/Pigs*, Journal of Clinical Monitoring, vol. 8, No. 4, Oct. 1992, pp. 267-278.

Gedeon, A., et al., *A new method for noninvasive bedside determination of pulmonary blood flow*, Medical & Biological Engineering & Computing, Jul. 1980, pp. 411-418.

\* cited by examiner



**Fig. 1**  
**(PRIOR ART)**



**Fig. 2**  
**(PRIOR ART)**

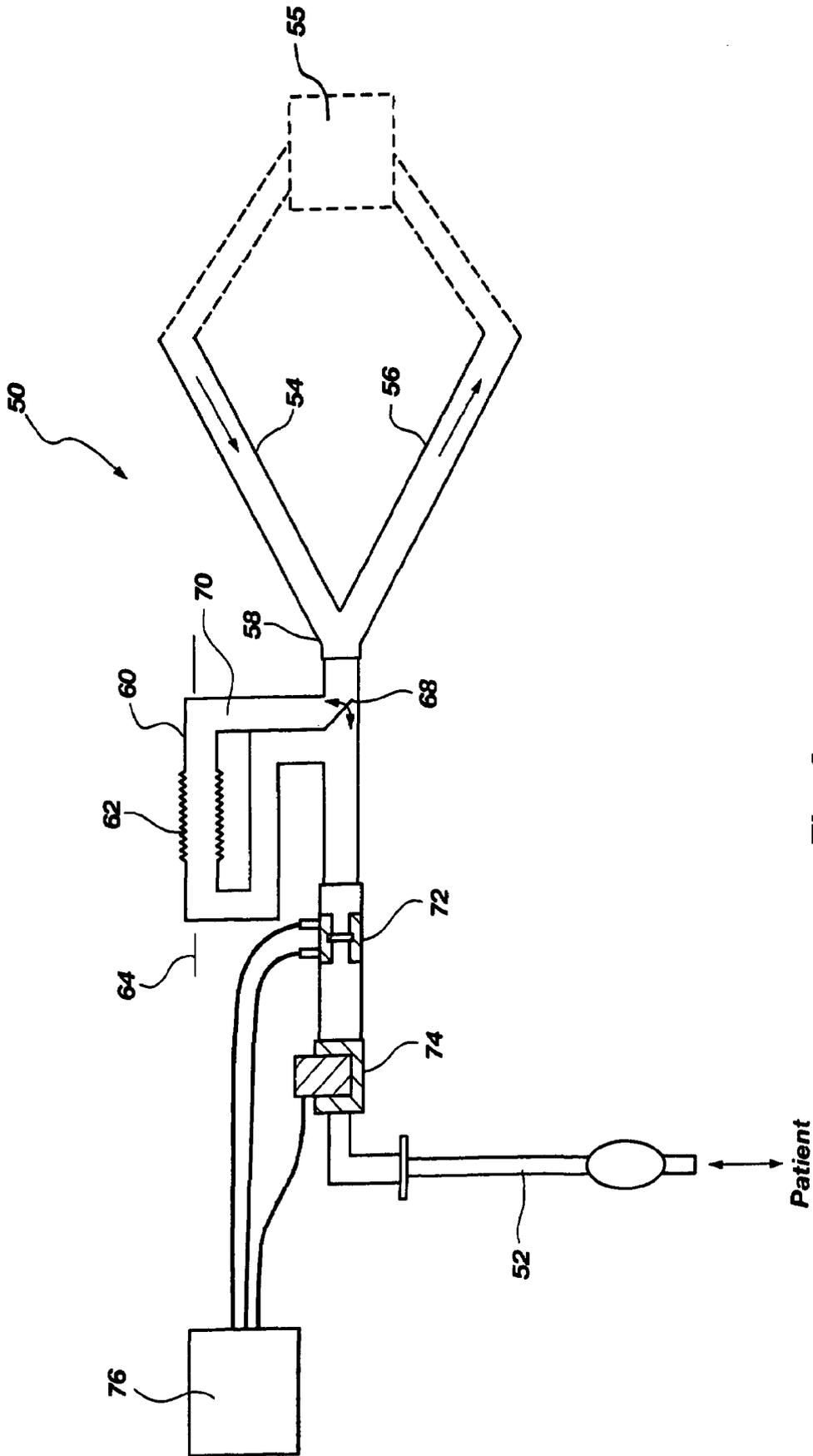


Fig. 3

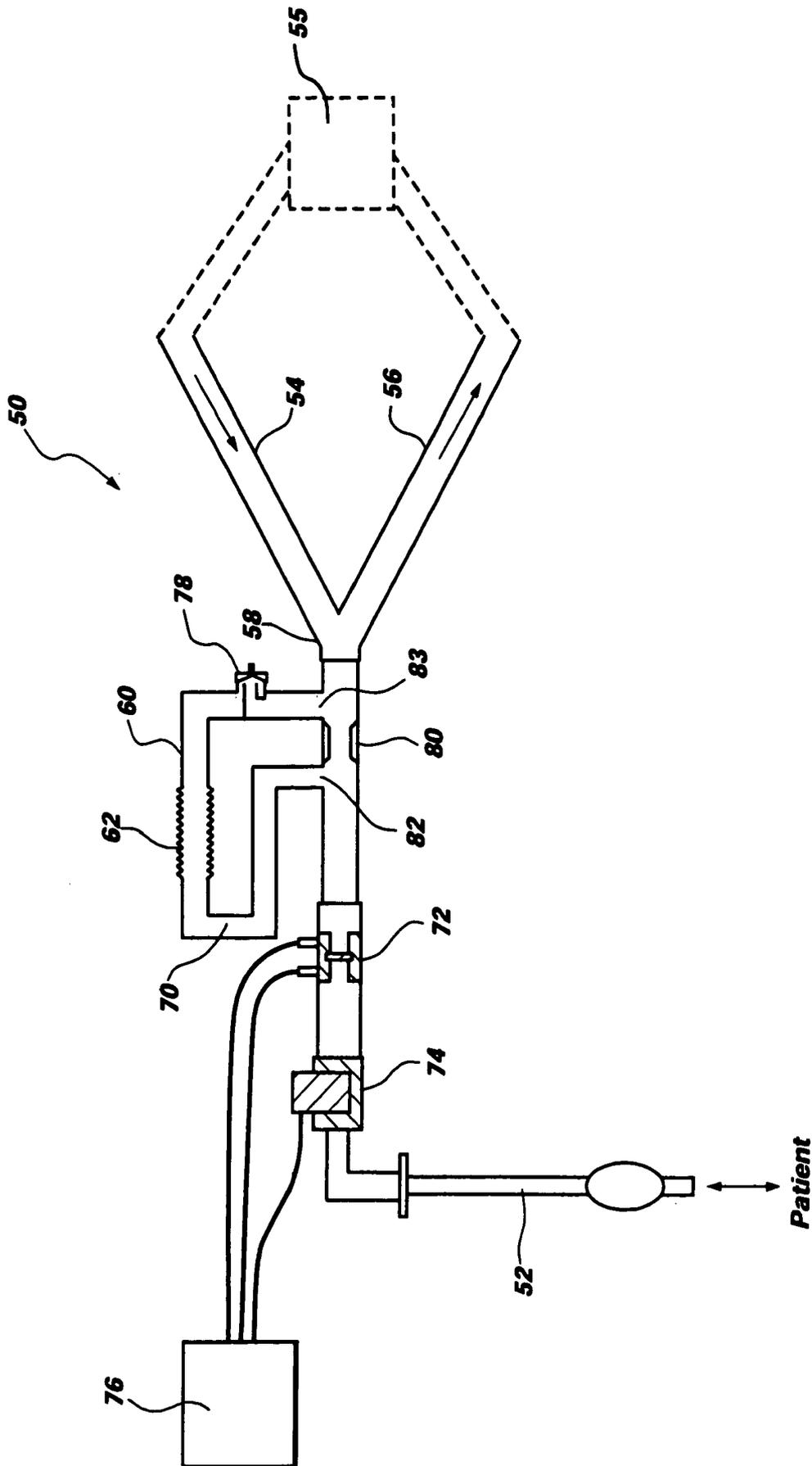


Fig. 4

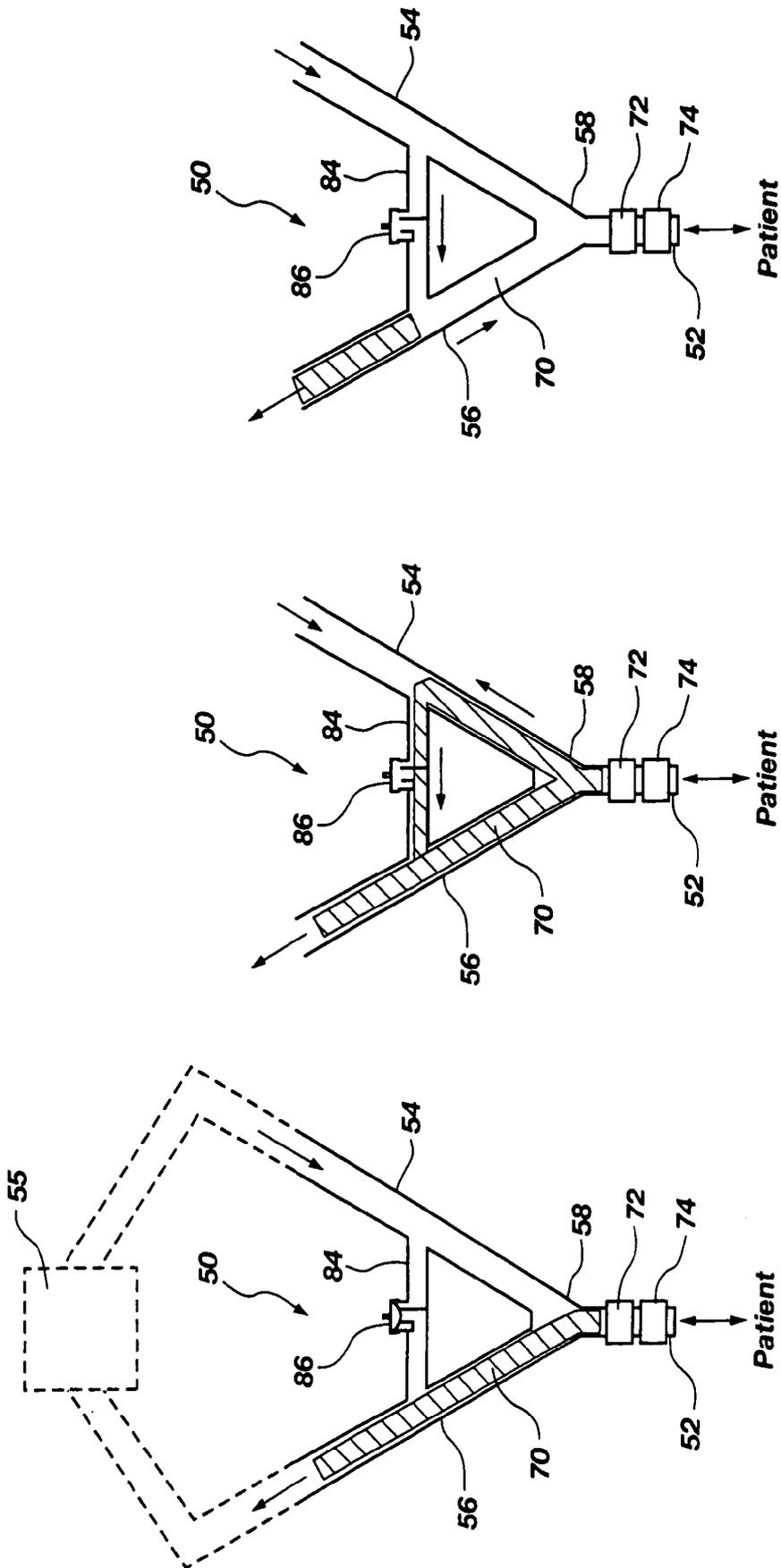


Fig. 5C

Fig. 5B

Fig. 5A

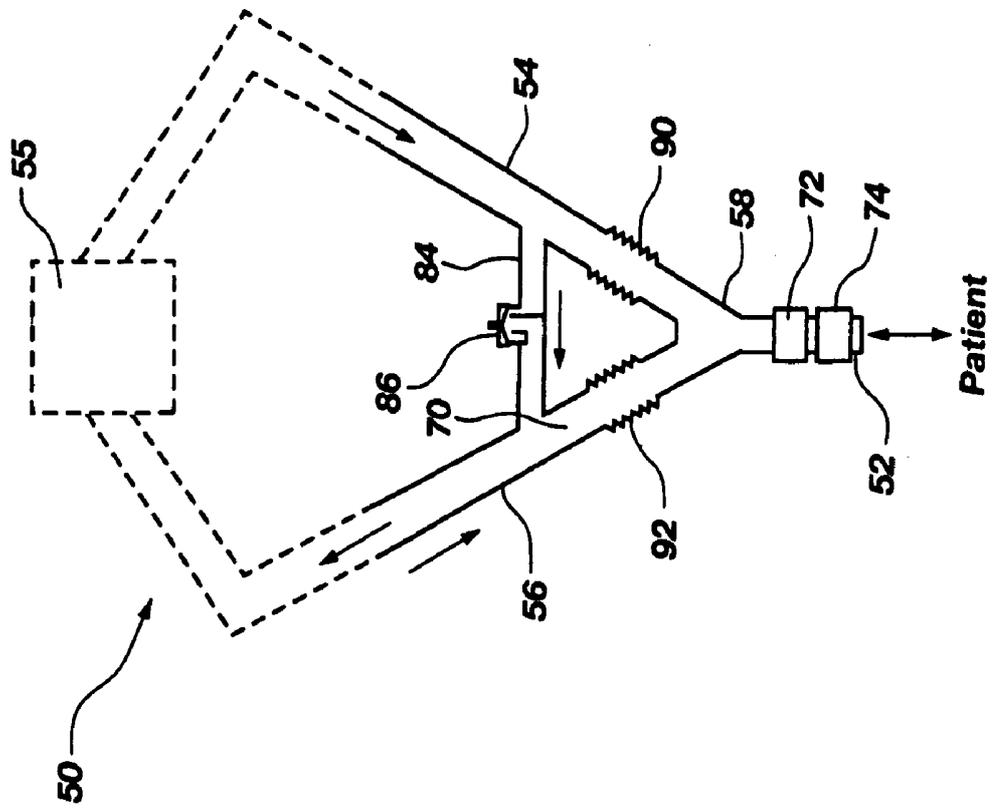


Fig. 6

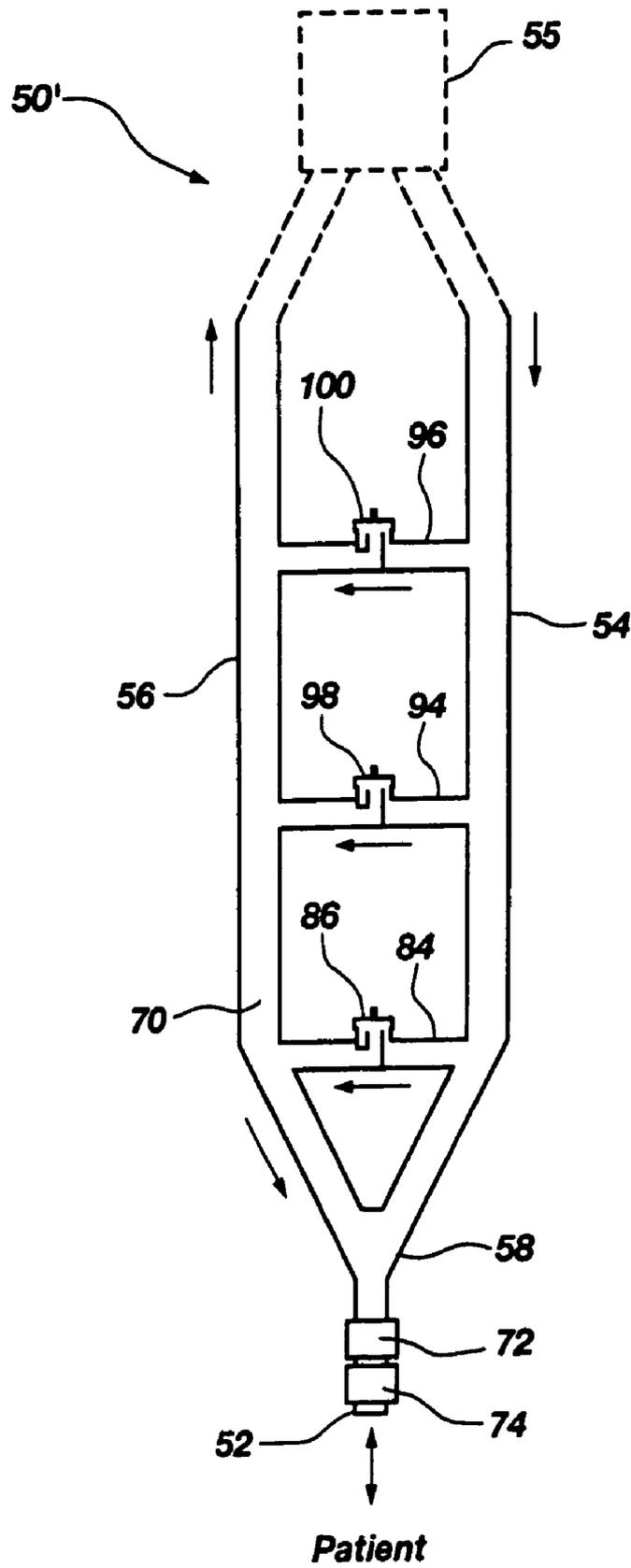


Fig. 7

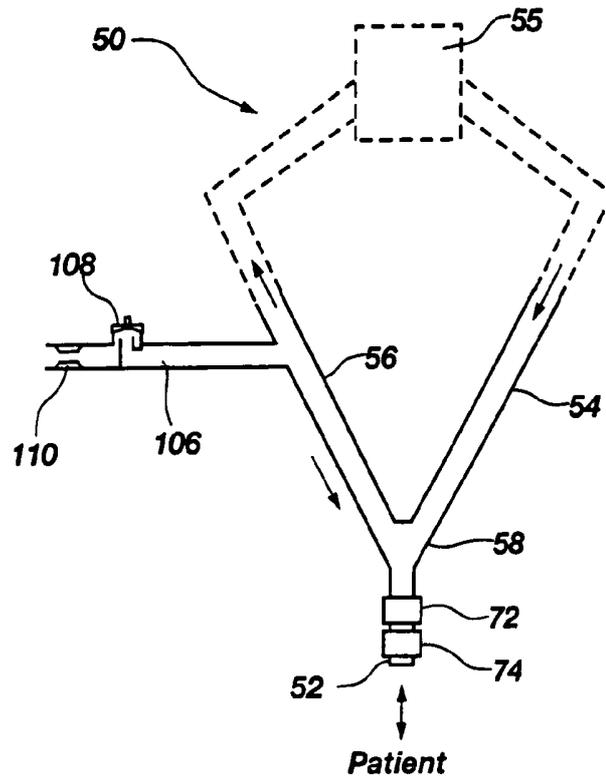


Fig. 8A

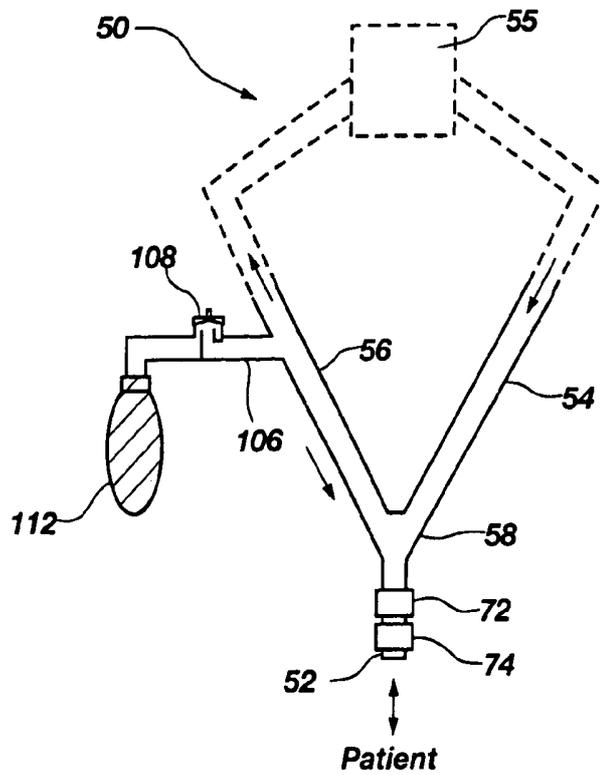


Fig. 8B



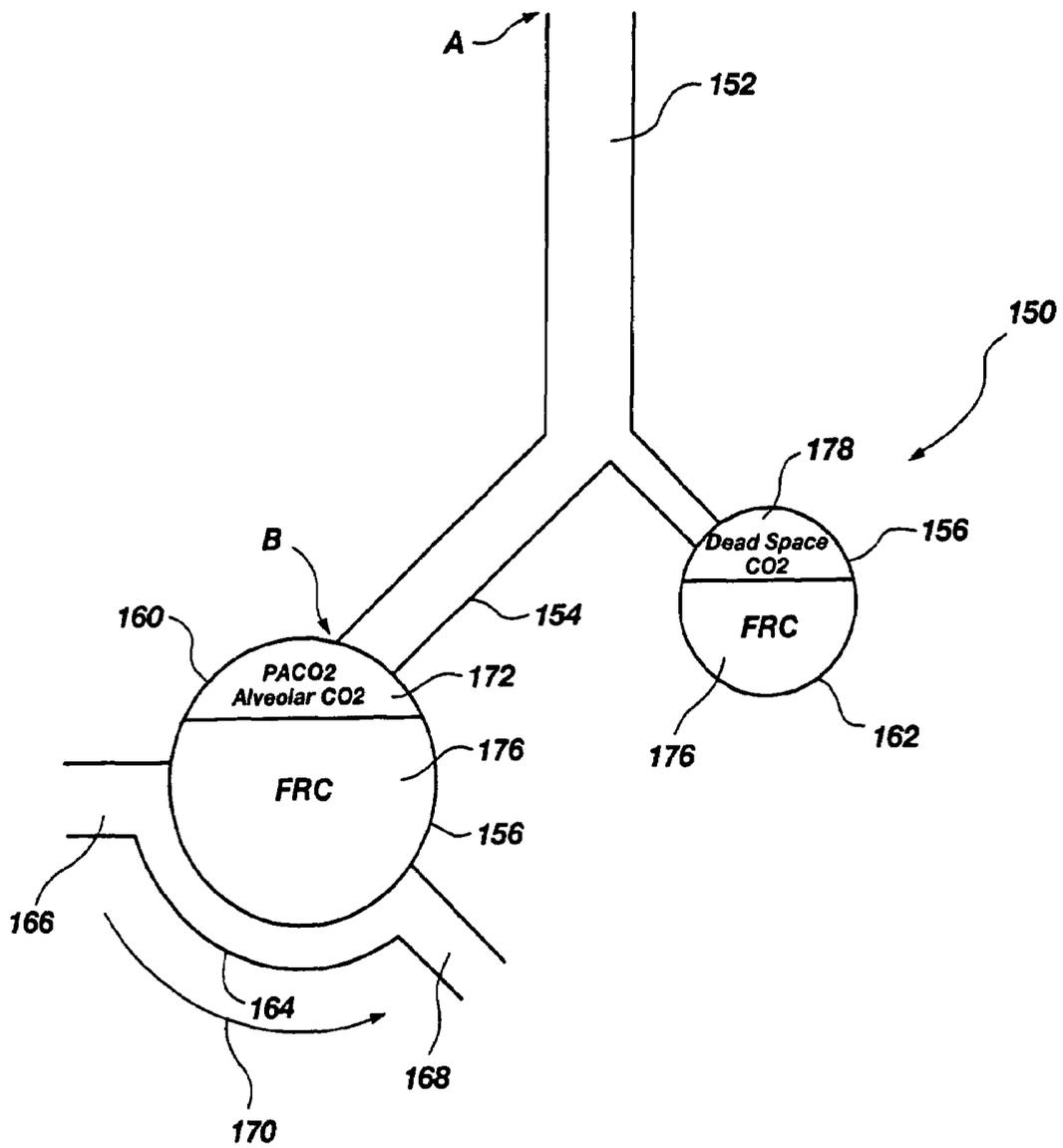


Fig. 10

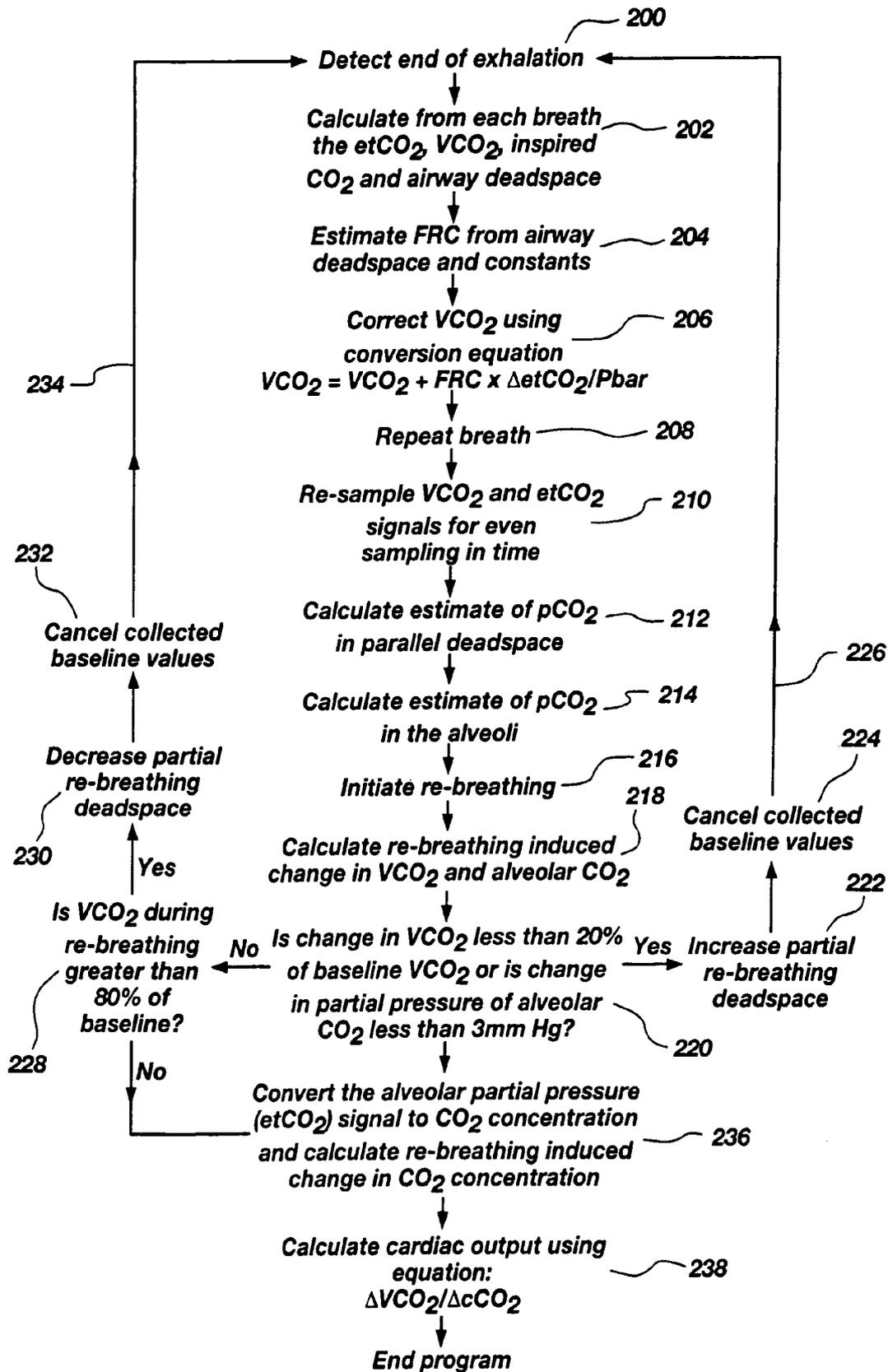


Fig. 11

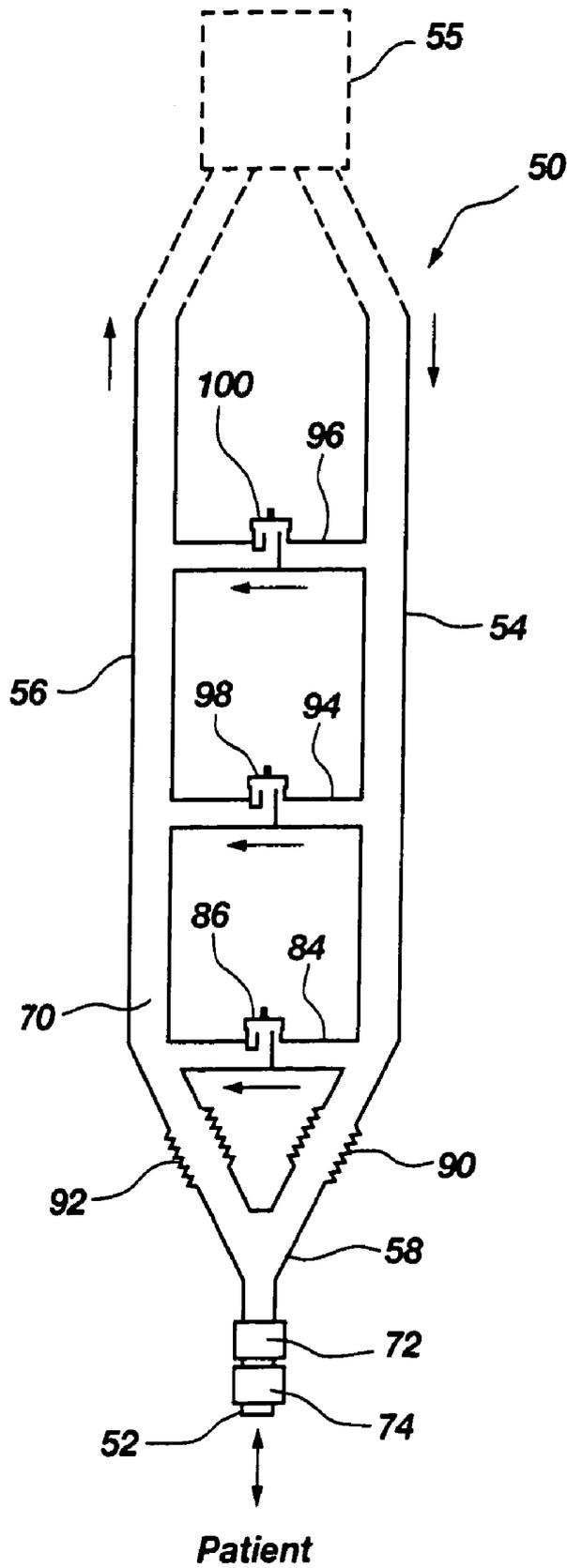


Fig. 12

## APPARATUS FOR NON-INVASIVELY MEASURING CARDIAC OUTPUT

### CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation of application Ser. No. 10/657,909, filed Sep. 8, 2003, now U.S. Pat. No. 6,908,438, issued Jun. 21, 2005, which is a divisional of application Ser. No. 09/767,363, filed Jan. 23, 2001, now U.S. Pat. No. 6,648,831, issued Nov. 18, 2003, which is a continuation of application Ser. No. 08/770,138, filed Dec. 19, 1996, now U.S. Pat. No. 6,306,098, issued Dec. 23, 2001.

### BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

This invention relates to non-invasive means of determining cardiac output in patients, and specifically relates to partial re-breathing systems and methods for determining cardiac output in patients.

#### 2. Background of Related Art

It is important in many medical procedures to determine or monitor the cardiac output of a patient. Techniques are known and used in the art which employ the use of catheters inserted at certain arterial points (e.g., femoral artery, jugular vein, etc.) to monitor blood temperature and pressure in order to determine cardiac output of the patient. Although such techniques can produce a reasonably accurate result, the invasive nature of the procedure has high potential for morbidity and mortality consequences.

Adolph Fick's measurement of cardiac output, first proposed in 1870, has served as the standard by which all other means of determining cardiac output have been evaluated since that date. Fick's well-known equation, written for CO<sub>2</sub>, is:

$$Q = \frac{V_{CO_2}}{(C_{vCO_2} - C_{aCO_2})}$$

where Q is cardiac output, V<sub>CO<sub>2</sub></sub> is the amount of CO<sub>2</sub> excreted by the lungs and C<sub>vCO<sub>2</sub></sub> and C<sub>aCO<sub>2</sub></sub> are the arterial and venous CO<sub>2</sub> concentrations, respectively. Notably, the Fick Equation presumes an invasive method (i.e., catheterization) of calculating cardiac output because the arterial and mixed venous blood must be sampled in order to determine arterial and venous CO<sub>2</sub> concentrations.

It has previously been shown, however, that non-invasive means may be used for determining cardiac output while still using principles embodied in the Fick Equation. That is, expired CO<sub>2</sub> ("pCO<sub>2</sub>") levels can be monitored to estimate arterial CO<sub>2</sub> concentrations and a varied form of the Fick Equation can be applied to evaluate observed changes in pCO<sub>2</sub> to estimate cardiac output. One use of the Fick Equation to determine cardiac output in non-invasive procedures requires the comparison of a "standard" ventilation event to a sudden change in ventilation which causes a change in expired CO<sub>2</sub> values and a change in excreted volume of CO<sub>2</sub>. The commonly practiced means of providing a sudden change in effective ventilation is to cause the ventilated patient to re-breathe a specified amount of previously exhaled air. This technique has commonly been called "re-breathing."

Prior methods of re-breathing have used the partial pressure of end-tidal CO<sub>2</sub> to approximate arterial CO<sub>2</sub> while the

lungs act as a tonometer to measure venous CO<sub>2</sub>. That method of re-breathing has not proven to be a satisfactory means of measuring cardiac output because the patient is required to breathe directly into and from a closed volume in order to produce the necessary effect. However, it is usually impossible for sedated or unconscious patients to actively participate in inhaling and exhaling into a bag. The work of some researchers demonstrated that the Fick Equation could be further modified to eliminate the need to directly calculate venous P<sub>CO<sub>2</sub></sub> (P<sub>vCO<sub>2</sub></sub>) by assuming that the P<sub>vCO<sub>2</sub></sub> does not change within the time period of the perturbation, an assumption that could be made by employing the partial re-breathing method. (See, Capek et al., "Noninvasive Measurement of Cardiac Output Using Partial CO<sub>2</sub> Rebreathing," *IEEE Transactions On Biomedical Engineering*, Vol. 35, No. 9, September 1988, pp. 653-661.)

Known partial re-breathing methods are advantageous over invasive measuring techniques because they 1) are non-invasive, 2) use the accepted Fick principle of calculation, 3) are easily automated, 4) require no patient cooperation and 5) allow cardiac output to be calculated from commonly monitored clinical signals. However, known partial re-breathing methods have significant disadvantages as well. Specifically, known methods 1) are less accurate with non-intubated or spontaneously breathing patients, 2) only allow intermittent measurements (usually about every four minutes), 3) result in an observed slight, but generally clinically insignificant, increase in arterial CO<sub>2</sub> levels, and 4) do not permit measurement of shunted blood flow (that is, blood which does not participate in gas exchange). Further, known apparatus used for partial re-breathing techniques are of standard construction and do not compensate for differences in patient size or capacities. In addition, many devices employ expensive elements, such as three-way valves, which render the devices too expensive to be used as disposable units.

Thus, it would be advantageous to provide a means of measuring cardiac output using partial re-breathing techniques which 1) overcome the disadvantages of prior systems, 2) provide better and more continuous measurement, and 3) require less expensive equipment, thereby making the device suitable for manufacturing as a single-use, or disposable, product. It would also be advantageous to provide partial re-breathing apparatus which is instantaneously adjustable to compensate for various sizes and capacities of patients. Further, it would be advantageous to provide new methods of estimating cardiac output based on alveolar CO<sub>2</sub> output rather than end-tidal CO<sub>2</sub> as is currently used in the art.

### SUMMARY OF THE INVENTION

In accordance with the present invention, apparatus and methods for measuring cardiac output using a modified Fick Equation are provided where the amount of deadspace which is provided in the apparatus can be adjusted to increase or decrease the volume of exhalate to be re-breathed by the patient, thereby decreasing ventilation without changing airway pressure. The apparatus and methods of the present invention also provide an adjustability factor which enables the apparatus to be adjusted to suit any size or capacity of patient. The apparatus of the present invention also employs significantly less expensive elements of construction, thereby rendering the device disposable.

The apparatus and methods of the present invention apply a modified Fick Equation to calculate changes in pCO<sub>2</sub> flow and concentration to evaluate cardiac output. The traditional Fick Equation, written for CO<sub>2</sub> is:

$$Q = \frac{V_{CO_2}}{(C_{vCO_2} - C_{aCO_2})}$$

where Q is cardiac output (when calculated using re-breathing techniques referred to as pulmonary capillary blood flow or "PCBF"),  $V_{CO_2}$  is the output of  $CO_2$  from the lungs and  $C_{vCO_2}$  and  $C_{aCO_2}$  are the arterial and venous  $CO_2$  concentrations, respectively. It has been shown in prior work of others that cardiac output can be estimated from calculating the change in  $pCO_2$ , as estimated by end-tidal  $CO_2$  ("et $CO_2$ "), as a result of a sudden change in ventilation. That can be done by applying a differential form of the Fick Equation as follows:

$$Q = \frac{V_{CO_2_1}}{(C_{v1} - C_{a1})} = \frac{V_{CO_2_2}}{(C_{v2} - C_{a2})}$$

where  $C_a$  is arterial  $CO_2$  concentration,  $C_v$  is venous  $CO_2$  concentration, and the subscripts 1 and 2 reference measured values before a change in ventilation and measured values during a change in ventilation, respectively. The differential form of the Fick Equation can, therefore, be rewritten as:

$$Q = \frac{V_{CO_2_1} - V_{CO_2_2}}{(C_{v1} - C_{a1}) - (C_{v2} - C_{a2})}$$

or

$$Q = \frac{\Delta V_{CO_2}}{\Delta C_{aCO_2}} = \frac{\Delta V_{CO_2}}{s \Delta etCO_2}$$

where  $\Delta V_{CO_2}$  is the change in  $CO_2$  production in response to the change in ventilation,  $\Delta C_{aCO_2}$  is the change in arterial  $CO_2$  concentration in response to the change in ventilation,  $\Delta etCO_2$  is the change in end-tidal  $CO_2$  concentration and s is the slope of the  $CO_2$  dissociation curve. The foregoing differential equation assumes that there is no appreciable change in venous  $CO_2$  concentration during the re-breathing episode, as demonstrated by Capek, et al., in their previous work. Also, a dissociation curve, well-known in the art, is used for determining  $CO_2$  concentration based on partial pressure measurements.

In previous partial re-breathing methods, a deadspace, usually comprising an additional 50-250 ml capacity of air passage, was provided in the ventilation circuit to decrease the effective alveolar ventilation. In the present invention, a ventilation apparatus is provided with an adjustable deadspace to provide the necessary change in ventilation for determining accurate changes in  $CO_2$  production and end-tidal  $CO_2$  commensurate with the requirements of differently sized patients. In one embodiment of the ventilation apparatus, selectively adjustable deadspace is provided through which the patient exhales and inhales. Thus, the adjustable deadspace of the apparatus permits easy adjustment of the deadspace to accommodate any size or capacity of patient, from a small to a large adult. As a result, the patient is provided with a volume of re-breathable gas commensurate with the patient's size which decreases effective ventilation without changing the airway pressure. Because airway and intra-thoracic pressure are not affected by the re-breathing method of the present invention, cardiac output is not significantly affected by re-

breathing. In an alternative method, the deadspace may be effectively lessened by selectively leaking exhaled gas from the ventilation system to atmosphere or to a closed receptacle means during inspiration.

The ventilation apparatus of the present invention includes a tubular portion, which is placed in contact with the patient, and an inhalation conduit and exhalation conduit. In a common configuration, the inhalation conduit and exhalation conduit may be interconnected between a ventilator unit and the patient. Alternatively, however, a ventilator unit (i.e., a source of deliverable gas mechanically operated to assist the patient in breathing) need not be used with the ventilation apparatus and inhaled and exhaled breath is merely taken from or vented to atmosphere. Other conventional equipment commonly used with ventilator units or used in ventilation of a patient may be used with the inventive ventilation apparatus, such as a breathing mask.

An electrical pneumotachometer for measuring flow of gas and a capnograph for measuring  $CO_2$  concentrations are provided in proximity to the tubular portion between the inhalation and exhalation portions of the ventilation apparatus and the patient's lungs. The pneumotachometer and capnograph serve as detection apparatus for detecting changes in gas concentrations and flow and are in electrical communication with a computer having software designed to store and evaluate the measurements taken by the detection apparatus in real time. Other forms of detection apparatus may be used. Adjustable deadspace means are provided in connection with the exhalation portion of the ventilation apparatus, and may interconnect with the inhalation portion of the ventilation apparatus. In one embodiment, the adjustable deadspace means may be manually adjusted. Alternatively, electromechanical means may be interconnected between the computer and the adjustable deadspace means to provide automatic adjustment of the deadspace volume responsive to the size or capacity of the patient and responsive to changes in ventilation.

In an alternative embodiment, a tracheal gas insufflation apparatus is used to provide the change in ventilation necessary to calculate pulmonary  $CO_2$  changes using the differential Fick Equation. Tracheal gas insufflation ("TGI") apparatus is commonly used to flush the deadspace of the alveolar spaces of the lungs and to replace the deadspace with fresh gas infused through insufflation means. That is, fresh gas is introduced to the central airway to improve alveolar ventilation and/or to minimize ventilatory pressure requirements. TGI apparatus is interconnected to a ventilator system and includes a means of introducing fresh gas into the breathing tube as it enters the patient's lungs. The TGI apparatus may be used in the methods of the present invention to determine baseline measurements of  $V_{CO_2}$  and et $CO_2$  during TGI. When the TGI system is turned off, a deadspace is formed by the patient's trachea and the endotracheal tube of the TGI apparatus which allows measurement of a change in  $CO_2$  to be evaluated in accordance with the invention. Further, the catheter of the TGI apparatus may be variably positioned within the trachea of the patient to further adjust the deadspace volume.

The deadspace provided in the apparatus of the present invention causes a rapid drop in  $V_{CO_2}$  which thereafter increases slightly and slowly as the functional residual lung gas capacity equilibrates with the increase in alveolar  $CO_2$  level. The change in et $CO_2$  rises more slowly after the addition of deadspace, depending on alveolar deadspace and cardiac output, but then stabilizes to a new level. A "standard," or baseline, breathing episode is conducted for a selected period of time immediately preceding the introduction of a dead-

space (i.e., re-breathing) and  $V_{CO_2}$  and  $etCO_2$  values are determined based on measurements made during the "standard" breathing event. Those values are substituted as the values  $V_{CO_2}$  and  $C_{CO_2}$  in the differential Fick Equation.  $V_{CO_2}$  and  $etCO_2$  values are also determined from measurements taken approximately thirty seconds following the introduction of a deadspace during partial re-breathing to provide the second values (subscript 2 values) in the differential Fick Equation. The period of time during which partial re-breathing occurs and during which normal breathing occurs may be determined by the individual size and lung capacity of the patient. Additionally, the period of time between a re-breathing episode and a subsequent normal breathing episode may vary between patients, depending on a particular patient's size and breath capacity. Thus, a thirty second time period for a breathing episode is only an average time and may be greater or lesser.

Cardiac output is determined, in the present invention, by estimating alveolar  $CO_2$  concentration rather than basing output on end-tidal  $CO_2$  concentration, as is practiced in the prior art. Partial pressure values that are obtained from  $CO_2$  measurements are converted to a value for gas content in the blood using the dissociation equation known in the art. Thus, a more accurate cardiac output can be determined. In addition, the accuracy of cardiac output is increased by correcting  $V_{CO_2}$  values to account for flow of  $CO_2$  into the functional residual capacity of the lungs, defined as the volume of gas left in the lungs at the end of an expired breath. The determination of values based on experiential data is processed by the software program to determine cardiac output.

The ventilation apparatus of the present invention employs inexpensive yet accurate monitoring systems as compared to the systems currently used in the art. The methods of the invention allow automatic adjustability of the apparatus for accommodating patients of different sizes and provide consistent monitoring with modest recovery time. Further, the present apparatus and methods can be used equally with non-responsive, intubated patients as well as non-intubated, responsive patients.

#### BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

In the drawings, which illustrate what is currently considered to be the best mode for carrying out the invention:

FIG. 1 is a schematic representation of conventional ventilation systems used for assisting patient breathing;

FIG. 2 is a schematic representation of prior art re-breathing systems;

FIG. 3 is a schematic first embodiment of the ventilation apparatus of the present invention illustrating an adjustably expandable deadspace;

FIG. 4 is a schematic representation of an alternative embodiment of the present invention where the re-breathing circuit is constructed with a leak valve;

FIGS. 5(A)-(C) are schematic representations of another alternative embodiment of the present invention where the inhalation portion and exhalation portion of the ventilation circuit are interconnected and have a two-way closeable valve;

FIG. 6 is a schematic representation of an alternative embodiment similar to the embodiment shown in FIGS. 5(A)-(C), but where the inhalation and exhalation portions are adjustably expandable;

FIG. 7 is a schematic representation of another embodiment of the invention where a series of valves is provided along the length of the inhalation and exhalation portions to

provide a selectable volume of deadspace dependent upon the size and/or capacity of the patient;

FIGS. 8(A) and (B) are schematic representations of another embodiment of the invention where a leak valve is provided, both with a vent to atmosphere and to a parallel compliance chamber;

FIG. 9 is a schematic representation of a tracheal gas insufflation apparatus of the present invention which can be used to provide a necessary change in ventilation with a deadspace;

FIG. 10 is a schematic representation of human lungs illustrating the concepts of parallel deadspace, alveolar deadspace and serial deadspace in the lungs of a patient;

FIG. 11 is a flow diagram briefly describing the calculations made in the software program to calculate cardiac output from the measured values of normal breathing and partial re-breathing; and

FIG. 12 is a schematic representation of an alternative embodiment of the invention shown in FIG. 7 which includes variably expandable inhalation and exhalation portions.

#### DETAILED DESCRIPTION OF THE INVENTION

For comparative purposes, FIG. 1 schematically illustrates a conventional ventilation system which is typically used with patients who require assisted breathing during an illness, a surgical procedure or recovery from a surgical procedure. The conventional ventilator system 10 includes a tubular portion 12 which is inserted into the trachea by intubation procedures. The distal end 14 of the tubular portion 12 is fitted with a Y-piece 16 which interconnects an inspiratory hose 18 and an expiratory hose 20. Both the inspiratory hose 18 and expiratory hose 20 are connected to a ventilator machine (not shown) which delivers air to the inspiratory hose 18. A one-way valve 22 is positioned on the inspiratory hose 18 to prevent exhaled gas from entering the inspiratory hose 18 beyond the valve 22. A similar one-way valve 24 on the expiratory hose 20 limits movement of inspiratory gas into the expiratory hose 20. Exhaled air flows passively into the expiratory hose 20.

In known re-breathing ventilation circuits 30, as shown in FIG. 2, the tubular portion 32 is inserted into the trachea of the patient by intubation procedures, and gas is provided to the patient from a ventilator machine (not shown) via an inspiratory hose 34 which is interconnected by a Y-piece 36 to an expiratory hose 38. An additional length of hose 40 is provided between the tubular portion 32 and the Y-piece 36 which acts as a deadspace for receiving exhaled gas. A three-way valve 42, generally positioned between the Y-piece 36 and the opening to the additional length of hose 40, is constructed for intermittent actuation to selectively direct the flow of gas. That is, at one setting, the valve 42 allows inspiratory gas to enter the tubular portion 32 while preventing movement of the gas into the additional length of hose 40. In a second setting, the valve 42 allows exhaled gas to enter into the expiratory hose 38 while preventing movement of gas into the additional length of hose 40. In a third setting, the three-way valve 42 directs exhaled air to enter into the additional length of hose 40 and causes the patient to re-breathe the exhaled air on the following breath to thereby cause a change in effective ventilation.

The change in  $V_{CO_2}$  and end-tidal  $CO_2$  caused by the change in ventilation in the prior art system of FIG. 2 can then be used to calculate cardiac output. Sensing and/or monitoring devices may be attached to the re-breathing ventilation circuit 30 between the additional length of hose 40 and the tubular portion 32. The sensing and/or monitoring devices may include, for example, means for detecting  $CO_2$  concen-

tration 44 and means for detecting flow parameters 46 during inhalation and exhalation. Those sensing and/or monitoring devices are typically connected to data recording and display equipment (not shown). One problem encountered in use of the prior art system is that the deadspace provided by the additional length of hose 40 is fixed and may not be adjusted. As a result, the amount of deadspace provided in the circuit for a small adult to effect re-breathing is the same amount of deadspace available for a large adult to effect re-breathing, and the resulting changes in CO<sub>2</sub> values for patients of different size, derived from fixed-deadspace systems, can produce inadequate evaluation of cardiac output. Further, the three-way valve 42 of the system is expensive and significantly increases the cost of the ventilation device.

FIG. 3 illustrates the ventilation apparatus of the present invention which provides an improvement over known ventilation devices used to detect or monitor cardiac output. The present ventilation apparatus 50 comprises a tubular airway 52 which is placed in communication with the patient's lungs. Although the present ventilation apparatus 50 may be placed in communication with the trachea by intubation procedures as is done in the prior art, the present ventilation apparatus 50 need not be inserted directly into the trachea of the patient. Alternatively, a breathing mask may be used for positioning over the patient's nose and mouth. Thus, the present invention may be used with unconscious or uncooperative patients needing ventilation assistance and may be used with equal efficacy with patients who are conscious. The ventilation apparatus 50 also includes an inspiratory hose 54 and an expiratory hose 56 which may each be ventilated to atmosphere or connected to a ventilator machine 55 (shown in phantom) which provides gas for delivery to the patient through the inspiratory hose 54. The inspiratory hose 54 and expiratory hose 56 may be joined together by a Y-piece 58.

The Y-piece 58 connects to an additional length of conduit or hose 60 which provides a deadspace for receiving exhaled gas from the patient. However, the additional length of hose 60 is structured to be selectively expandable to readily enable the volume of deadspace to be adjusted commensurate with the size or lung capacity of the patient, or to other ventilation parameters, such as increased or decreased tidal volume or modified respiration rate. As suggested by the schematic drawing of FIG. 3, selective expansion of the deadspace may be accomplished by structuring the additional length of hose 60 with an expandable section 62 made of, for example, a piece of corrugated hose which can be lengthened or shortened by simply pulling or pushing the expandable section 62 along its longitudinal axis 64. The corrugated hose will retain the length at which it is positioned until adjusted again. Other suitable means of providing adjustable expansion of the volume of the deadspace are available, extending the length of the hose 60 being but one approach. A three-way valve 68 may be connected to the additional length of hose 60 to force inspiratory gas to enter the deadspace 70 upon inhalation. The three-way valve 68 is also structured to selectively prevent exhaled gas from entering the deadspace 70 during normal breathing or to direct exhaled gas into deadspace 70 during re-breathing episodes so that the patient is forced to re-breathe exhaled gas from the deadspace 70.

A flow meter 72, or pneumotachometer, is attached to the ventilation apparatus 50 at a point between the tubular airway 52 and the additional length of hose 60. The flow meter 72 detects gas flow through the ventilation apparatus 50. A CO<sub>2</sub> sensor 74, or capnograph, is also connected to the ventilation apparatus 50 between the tubular airway 52 and the additional length of hose 60. The CO<sub>2</sub> sensor 74 detects changes in CO<sub>2</sub> resulting from a change in ventilation, the data from which is

used to calculate cardiac output. The CO<sub>2</sub> sensor 74 may be an "on airway" sensor, a sampling sensor of the type which withdraws a side stream sample of gas for testing, or any other suitable CO<sub>2</sub> sensor. Both the flow meter 72 and CO<sub>2</sub> sensor 74 are connected to a computer 76 which is programmed to store and analyze data from the flow meter 72 and CO<sub>2</sub> sensor 74, and to calculate from the data the estimated cardiac output of the patient.

As previously described herein, the differential Fick Equation requires a change in pulmonary gas concentration and output to be induced in the patient in order to estimate cardiac output. Re-breathing gas previously exhaled by the patient increases the amount of CO<sub>2</sub> breathed in by the patient and enables the evaluation of increased CO<sub>2</sub> levels during a change in effective ventilation as compared to standard CO<sub>2</sub> levels during normal ventilation. The ventilation apparatus of the present invention provides the ability to selectively adjust the deadspace required in re-breathing to increase the amount of gas (CO<sub>2</sub>) re-breathed by the patient from the previous exhalation. The ventilation apparatus of the present invention also allows the ventilation circuit to be adjusted automatically in accordance with the size or capacity of a patient, and in response to ventilation parameters. That is, if the detected change in etCO<sub>2</sub> is less than 3 mm Hg, or the change in V<sub>CO<sub>2</sub></sub> is less than 0.2 times the V<sub>CO<sub>2</sub></sub>, then the deadspace volume should be increased by twenty percent.

In an alternative embodiment of the apparatus 50 of the invention, as shown in FIG. 4, the expense of using a three-way valve may be eliminated by structuring the additional length of hose 60 with an inexpensive two-way valve 78 and by positioning a flow restrictor 80 between the inlet 82 and outlet 83 of the deadspace 70. Thus, when the two-way valve 78 is closed, gas to and from the ventilator machine 55 will be directed through the flow restrictor 80 and to the patient. During a re-breathing episode, the two-way valve 78 is open so that the exhaled air encountering the flow restrictor 80 follows the course of less resistance through the deadspace 70. Thus, the deadspace 70 may be adjusted at the expandable section 62 to provide the necessary deadspace 70 for calculating changes in cardiac output.

In another alternative embodiment of the ventilation apparatus 50 of the present invention, as shown in FIGS. 5(A)-(C), a shunt line 84 is positioned between the inspiratory hose 54 and the expiratory hose 56 to provide selectively sized deadspace 70 in the circuit. The structure of the embodiment shown in FIGS. 5(A)-(C) causes the inspiratory hose 54 and expiratory hose 56 to act as part of the deadspace 70, as well. A two-way shunt valve 86 positioned on the shunt line 84 selectively directs the flow of inspired and expired gas dependent upon whether the two-way shunt valve 86 is open or closed. Thus, when the ventilation apparatus 50 is configured for normal or baseline breathing, as depicted in FIG. 5(A), exhaled air (represented by the shaded area) will enter the expiratory hose 56. During normal breathing, the two-way shunt valve 86 is closed. When the ventilation apparatus 50 is configured for a re-breathing episode, as depicted in FIG. 5(B), the two-way shunt valve 86 is opened and exhaled gas may fill a portion of the inspiratory hose 54, all of the expiratory hose 56 and the shunt line 84, all of which serve as the deadspace 70.

The deadspace 70 in the embodiment shown in FIGS. 5(A)-(C) may be rendered adjustably expandable, as shown in FIG. 6, by structuring the inspiratory hose 54 with an expandable section 90 positioned between the shunt line 84 and the Y-piece 58, and by structuring the expiratory hose 56 with an expandable section 92 positioned between the shunt line 84 and the Y-piece 58. Thus, the deadspace 70 can be

selectively adjusted in accordance with the size or capacity of the patient, or responsive to operating conditions, by increasing that portion of the inspiratory hose **54** and expiratory hose **56** extending from the Y-piece **58**. Any suitable adjustably expandable means may be used. As suggested by FIG. 6, however, the expandable section **90**, **92** may be made from corrugated plastic material, the length of which can be easily expanded or contracted, and the plastic material will maintain its adjusted length until repositioned. The embodiment of FIG. 6 provides a particularly simple and inexpensive construction rendering a particularly preferred embodiment because of its ease of use and disposability.

In yet another embodiment of the ventilation apparatus **50'** of the present invention, as shown in FIG. 7, the amount of available deadspace **70** may be selectively adjusted by providing a plurality of shunt lines **84**, **94**, **96** positioned between the inspiratory hose **54** and the expiratory hose **56**, with each shunt line **84**, **94**, **96** being structured with a two-way shunt valve **86**, **98**, **100**. In operation, the amount of deadspace **70** required, as dictated by the size or capacity of the patient, may be selectively provided by using any suitable number of shunt lines **84**, **94**, **96** to allow exhaled gas to move through the ventilation apparatus **50'**. For example, given a patient of average size or lung capacity, it may be appropriate to use the first shunt line **84** and the second shunt line **94** as potential deadspace **70**. Thus, as the patient exhales in a re-breathing episode, the two-way shunt valves **86**, **98** associated with the first shunt line **84** and second shunt line **94** may be opened, allowing exhaled and re-breathable gas to fill the expiratory hose **56**, the inspiratory hose **54** between the second shunt line **94** and the Y-piece **58**, the first shunt line **84** and the second shunt line **94**. With a patient of larger size or greater lung capacity, it may be necessary to use the third shunt line **96** as well in providing sufficient deadspace **70** for re-breathing. Notably, each two-way shunt valve **86**, **98**, **100** may be in electromechanical communication with the computer **76** (not shown in FIG. 7) so that the computer may determine from the pneumotachometer, for example, that additional deadspace **70** is required and cause the opening of one or more of the two-way shunt valves **86**, **98**, **100** to provide sufficient additional deadspace **70**. In an alternative embodiment, the ventilation apparatus **50'** shown in FIG. 7 may be modified by the addition of selectively expandable sections **90**, **92** as shown in FIG. 12.

In the several alternative embodiments of the invention previously illustrated and described, the amount or volume of the deadspace has been selectively adjustable by providing means for adjusting the volume of the deadspace, such as by providing length-expanding means. It may be equally appropriate, however, to provide a change in ventilation, as required by the differential Fick Equation, by leaking some of the exhaled gas out of the system during the inspiration phase of a breath. Thus, as illustrated by FIG. 8(A), the ventilation apparatus **50** of the present invention may be structured with an evacuation line **106** connected to the expiratory hose **56** of the ventilation apparatus **50**. The evacuation line **106** may be structured with gas releasing structure, such as a simple valve **108** connected thereto which, when opened, allows exhaled gas to move through the evacuation line **106**. An orifice **110** positioned at the end of the evacuation line **106** allows some of the exhaled gas to escape to the atmosphere.

When and how much exhaled gas should be leaked from the ventilation apparatus **50** during a re-breathing event may be determined by the computer (not shown in FIG. 8) in response to flow conditions, CO<sub>2</sub> conditions and/or the size or lung capacity of the patient. The valve **108**, in electromechanical communication with the computer, may be selec-

tively actuated according to ventilation or patient conditions. Where a patient is anesthetized or is otherwise exhaling gas which is undesirable for venting to the atmosphere, a compliant chamber **112**, such as an expandable bag shown in FIG. 8(B), may be attached to the evacuation line **106** to receive the exhaled gas leaked from the ventilation circuit.

FIG. 9 schematically illustrates the use of a tracheal gas insufflation (TGI) apparatus **120** to provide the necessary deadspace in determining cardiac output in patients. TGI apparatus is typically used to ventilate sick patients who require the injection of fresh gas into their central airway for the improvement of alveolar ventilation. TGI apparatus can be configured to provide continuous or phasic (e.g., only during inhalation) injections of gas. The TGI apparatus supplies gas, or an oxygen/gas mixture, to the lungs with every breath. As shown in FIG. 9, the TGI apparatus comprises an endotracheal tube **122** which is inserted into the trachea **124** of the patient by intubation procedures. A catheter **126** extends through the endotracheal tube **122** and into the patient's lungs, typically just above the carina. Gas or an oxygen/gas blend is provided from a gas source **128** and is directed through gas tubing **130** into the catheter **126**. A flow meter **132** may assist in determining the optimum amount of gas to be introduced into the lungs.

An adaptor fitting **134** may be used to connect a ventilation circuit **136** of a type previously described to the TGI apparatus **120**. That is, a ventilation circuit **136** comprising a Y-piece **58** from which extends an inspiratory hose **54** and an expiratory hose **56** is structured with a flow meter line **71** (not shown) attachable to a flow meter **72** and a CO<sub>2</sub> sensor **74** for collecting data derived during a re-breathing event. In the illustrated TGI apparatus **120**, the endotracheal tube **122** provides deadspace required for re-breathing in addition to the ventilation circuit **136** as previously described. To act as a deadspace, however, the TGI apparatus (i.e., the gas source **128** and flow meter **132**) must be turned off, reduced or otherwise disabled. Exhaled air is thereby allowed to fill the endotracheal tube **122** and enter through the Y-piece **58**. The endotracheal tube **122** and ventilation circuit **136** serve as deadspace when the TGI apparatus **120** is turned off. The volume of deadspace provided by the TGI apparatus configuration may be further increased or decreased, as necessary, by varying the depth to which the catheter **126** is positioned in the patient's trachea.

The computer to which the flow meter **72** and CO<sub>2</sub> sensor **74** are connected is programmed to receive data collected by the flow meter **72** and CO<sub>2</sub> sensor **74** and to analyze the data to calculate an estimated cardiac output. The parameters which are required by the software program to analyze the data and to estimate cardiac output are described hereafter.

The calculation of cardiac output for a given patient is based on the collection of data from the CO<sub>2</sub> sensor and flow meter attached to the ventilation apparatus of the present invention. Raw flow and CO<sub>2</sub> signals from the flow meter and CO<sub>2</sub> sensor **74** are filtered to remove artifacts and the flow signals, CO<sub>2</sub> signals and pressure signals are stored in a buffer in the software program. When the flow signal crosses a prescribed threshold (e.g., 15 liters/minute), the buffer is searched to find the most recent zero-crossing. The zero-crossing is identified as the start of a new breath. All data stored in the buffer since the last zero-crossing and the crossing of the prescribed threshold (i.e., the new zero-crossing) is established as one breathing cycle. For each breathing cycle, the parameters of the breathing phase are calculated as follows:

- 1) etCO<sub>2</sub>: The average concentration of CO<sub>2</sub> during the final 5% of expiratory tidal volume is taken as end-tidal CO<sub>2</sub>.
- 2) V<sub>CO<sub>2</sub></sub>: The integral of flow (in milliliters) multiplied by concentration of CO<sub>2</sub> over the entire breath is V<sub>CO<sub>2</sub></sub>.
- 3) Inspired CO<sub>2</sub>: This is the concentration of inspired CO<sub>2</sub>. It is the integral of CO<sub>2</sub> concentration times the volume (in milliliters) of air flow during inspiration (i.e., negative flow).
- 4) Airway deadspace: Determined as the expired volume (in milliliters) at which CO<sub>2</sub> concentration crosses a selected threshold set at, for example, 0.5 times etCO<sub>2</sub>.

The initial values of V<sub>CO<sub>2</sub></sub> and etCO<sub>2</sub> are filtered employing a three-point median filter. The etCO<sub>2</sub> and V<sub>CO<sub>2</sub></sub> signals are straight-line interpolated and re-sampled at 0.5 Hz.

A correction is made in the V<sub>CO<sub>2</sub></sub> value to account for alveolar deadspace. That is, the correction in V<sub>CO<sub>2</sub></sub> corrects for the flow of CO<sub>2</sub> into lung stores such as the functional residual capacity (FRC) in the lungs, or, in other words, the volume of gas left in the lungs at the end of a breath. Alveolar deadspace is demonstrated more clearly in FIG. 10, which schematically illustrates the lungs 150 of a patient. The lungs 150 generally comprise the trachea 152, bronchi 154 and alveoli 156. The trachea 152 and bronchi 154 generally comprise what is known as the anatomic or serial deadspace, which exists in the region indicated between arrows A and B. In the lungs 150, there are alveoli 156 which are perfused with blood (i.e., in contact with blood flow to provide oxygenation to the blood) and alveoli which are not perfused, though both perfused and unperfused alveoli 156 may be ventilated.

Perfused alveoli 160 and unperfused alveoli 162 are illustrated in FIG. 10. The perfused alveoli 160 are contacted with blood flowing through minute capillaries 164 surrounding the alveoli 160, 162 the venous blood 166 flowing toward the alveoli 160 and the arterial blood 168 flowing away from the alveoli 160 in the direction of arrow 170. In the alveoli 160, 162 a volume of gas known as the functional residual capacity (FRC) 176 remains following exhalation. A portion 172 of the alveoli 160, 162 which is evacuated upon exhalation (i.e., is ventilated) is representational of alveolar CO<sub>2</sub> (PACO<sub>2</sub>). In unperfused alveoli 162, the FRC 176 contains gas which is not evacuated during a breath, and the ventilated portion 178 of the alveoli 162 forms a space containing gas or CO<sub>2</sub> which is ventilated but not perfused. It is the ventilated portion 178 existing in the unperfused alveoli 162 which comprises parallel deadspace (PDS), so called because it is ventilated in parallel with the perfused alveoli.

In the present invention, the software program compensates, or accounts, for the functional residual capacity of the patient's lungs and the alveolar deadspace which exists. The correction is equal to the FRC times the change in end-tidal concentration or

$$V_{CO_2} = V_{CO_2} + FRC \times \Delta etCO_2 / P_{bar},$$

where "Pbar" is barometric pressure. FRC is estimated as a function of body weight as estimated by the deadspace volume using the equation

$$FRC = FRC - factor \times airway\ deadspace + an\ offset\ value,$$

where the FRC-factor is a value experimentally determined or is based on published data known in the art and the offset value is a fixed constant which is added to compensate for breathing masks or other equipment components which may add deadspace to the circuit and thereby unacceptably skew the relationship between FRC and deadspace. The airway

deadspace is the volume at which CO<sub>2</sub> crosses a selected threshold e.g., (0.5 etCO<sub>2</sub>). Dry gas is assumed in all equations.

Compensation is also made for parallel deadspace (See FIG. 10). Parallel deadspace CO<sub>2</sub> concentration is calculated as a low-pass filtered version of the mixed inspired CO<sub>2</sub> plus the airway deadspace times the previous end-tidal CO<sub>2</sub> concentration. The average CO<sub>2PDS</sub> is etCO<sub>2</sub> times airway deadspace plus inspired CO<sub>2</sub> volume divided by the tidal volume. Breath-by-breath calculation of parallel deadspace, or unperfused space, concentration is therefore:

$$PDS_{CO_2}(n) = \{ [FRC / (FRC + V_t)] \times PDS_{CO_2}(n-1) + \{ [V_i CO_2 + (deadspace \times etCO_2(n-1))] / V_t \} \times V_t / (V_t + FRC) \},$$

where V<sub>t</sub> is the tidal volume (the volume of the breath), PDS is parallel deadspace (i.e., space in the lung that is ventilated but not perfused by blood flow), etCO<sub>2</sub> is the concentration of CO<sub>2</sub> at the end of the exhaled breath, or "end-tidal," "deadspace" is the volume in the trachea and bronchi through which air must pass to get to the alveoli but in which no gas exchange occurs (also defined as "serial deadspace," See FIG. 10) and (n-1) indicates the previous breath.

Alveolar CO<sub>2</sub> partial pressure ("P<sub>A</sub>CO<sub>2</sub>") is calculated from the end-tidal CO<sub>2</sub> and the CO<sub>2</sub> in the parallel deadspace. Thus, if

$$etCO_2 = r \times (P_A CO_2) + (1-r) PDS_{CO_2},$$

then

$$(P_A CO_2) = [etCO_2 - (1-r) \times PDS_{CO_2}] / r,$$

where r is the perfusion ratio calculated as the ratio of perfused alveolar ventilation divided by total alveolar ventilation, or (V<sub>A</sub> - V<sub>PDS</sub>) / V<sub>A</sub>. The perfusion ratio r is estimated to be about 0.92. Perfusion ratio can also be estimated by direct analysis of arterial blood.

The (P<sub>A</sub>CO<sub>2</sub>) signal is then converted to CO<sub>2</sub> content using the following equation:

$$C_{CO_2} = (6.957 \times Hb + 94.864) \times \ln(1 + 0.1933(P_{CO_2})),$$

where C<sub>CO<sub>2</sub></sub> is the concentration of CO<sub>2</sub> and Hb is hemoglobin concentration. In some instances, a hemoglobin count may be readily available and is used in the equation. If hemoglobin (Hb) concentration is not available, the value of 11.0 is used in the software program.

Baseline values of etCO<sub>2</sub> and V<sub>CO<sub>2</sub></sub>, also referred to herein as "before CO<sub>2</sub> and before V<sub>CO<sub>2</sub></sub>," are those values which exist during normal breathing and are calculated as the average of all samples between 27 and 0 seconds before the start of re-breathing. Once a re-breathing episode begins, the V<sub>CO<sub>2</sub></sub> value during re-breathing, also referred to herein as "during V<sub>CO<sub>2</sub></sub>," is calculated as the average V<sub>CO<sub>2</sub></sub> between 25 and 30 seconds of re-breathing. The calculation of C<sub>CO<sub>2</sub></sub> during a re-breathing episode is determined using a regression line to predict the stable concentration of alveolar CO<sub>2</sub> (C<sub>CO<sub>2</sub></sub>). To predict the C<sub>CO<sub>2</sub></sub> at which the signal will be stable (i.e., unchanging), the C<sub>CO<sub>2</sub></sub> is plotted versus the breath-to-breath change in concentration. The line is regressed and the intersection between the C<sub>CO<sub>2</sub></sub> and zero ΔC<sub>CO<sub>2</sub></sub> is the predicted stable point.

Cardiac output is then calculated as follows:

$$CO_2 = [before\ V_{CO_2} - during\ V_{CO_2}] / [during\ C_{CO_2} - before\ C_{CO_2}].$$

The operation logic of the software program is briefly illustrated in the flow chart of FIG. 11. The computer is

programmed to detect the end of an exhalation **200**, at which point the computer collects data from the CO<sub>2</sub> sensor and the flow meter and calculates CO<sub>2</sub>, V<sub>CO<sub>2</sub></sub>, inspired CO<sub>2</sub> and airway deadspace values **202**. The program then calculates FRC, at **204**, according to the equation previously noted. The program also corrects the V<sub>CO<sub>2</sub></sub> value, at **206**, in accordance with the equation previously described. At thirty second intervals (thirty seconds only being an average time, which may be adjusted higher or lower commensurate with the size of the patient), at **208**, the CO<sub>2</sub> and V<sub>CO<sub>2</sub></sub> values are recalculated, at **210**, to provide an average of those values based on time, not on the variable time at which exhalation may end.

The program then calculates the estimated pCO<sub>2</sub> in the parallel deadspace **212** and calculates the estimated pCO<sub>2</sub> in the alveoli **214** using the equations previously described. At that point, a re-breathing episode is initiated **216** and a deadspace is introduced. Again, the computer collects data from the CO<sub>2</sub> sensor and the flow monitor of the apparatus and from that data, the change in V<sub>CO<sub>2</sub></sub> and alveolar CO<sub>2</sub> induced by the introduction of the deadspace is calculated **218**. If the calculated change in V<sub>CO<sub>2</sub></sub> is less than twenty percent (20%) of the baseline V<sub>CO<sub>2</sub></sub>, or if the change in partial pressure of alveolar CO<sub>2</sub> is less than 3 mm Hg **220**, then the operator is notified to increase the partial re-breathing deadspace **222** by increasing the expandable volumetric dimension of the adjustable deadspace of the apparatus. Baseline values are cancelled **224**, then recalculated, as suggested by arrow **226**. If, however, the change in V<sub>CO<sub>2</sub></sub> during re-breathing is greater than 80% of baseline values **228**, then the operator is notified to decrease the adjustable deadspace of the apparatus by decreasing the volumetric dimension of the adjustable deadspace **230**. The baseline values are cancelled **232** and recalculated, as suggested by arrow **234**. Notably, the computer may notify the operator to make the necessary changes in the adjustable deadspace or, in an alternative embodiment, the computer may signal mechanical means connected to the adjustable deadspace to increase or decrease the volumetric dimension of the deadspace automatically.

Upon proper adjustment of the adjustable deadspace and the recalculation of baseline CO<sub>2</sub>, V<sub>CO<sub>2</sub></sub>, inspired CO<sub>2</sub> and airway deadspace values, the alveolar partial pressure (etCO<sub>2</sub>) is converted by the software program to CO<sub>2</sub> content and the change in CO<sub>2</sub> content induced by the introduction of deadspace in the re-breathing episode is calculated **236**. From those values, cardiac output is calculated **238** in accordance with the equation previously described.

All references to times of data collection assume a thirty (30) second re-breathing period. However, the actual length of time for periods of re-breathing is dependent upon the patient's size, lung capacity and cardiac output determined from previous breathing cycles. The program also controls the operation of the shunt valve or valves in the re-breathing apparatus. The valve or valves are opened based on a timer value determined by patient size, capacity and/or cardiac output.

The ventilation apparatus of the present invention provides a new and more accurate means of determining cardiac output in patients. The structure and electronic capabilities of the present invention may be modified, however, to meet the demands of the particular application. Hence, reference herein to specific details of the illustrated embodiments is by way of example and not by way of limitation. It will be apparent to those skilled in the art that many additions, deletions and modifications to the illustrated embodiments of the

invention may be made without departing from the spirit and scope of the invention as defined by the following claims.

What is claimed is:

1. Apparatus configured to facilitate rebreathing by a subject, comprising:
  - an airway conduit configured to communicate with a respiratory system of a patient;
  - a volume-adjustable deadspace conduit comprising an alternate pathway to at least a portion of the airway conduit and including ends secured to and in at least selective communication with the airway conduit, the volume-adjustable deadspace conduit configured to be adjusted to one of more than two fixed volumes to provide a volume-adjustable deadspace from which the subject may rebreathe; and
  - a flow control element comprising a single one two-way valve for selectively controlling flow into and out of the volume-adjustable deadspace conduit.
2. The apparatus of claim 1, wherein the airway conduit comprises at least a portion of the volume-adjustable deadspace.
3. The apparatus of claim 1, wherein the airway conduit includes a breathing tube including a first end for interfacing with a subject and an opposite second end, a Y-piece at the second end of the breathing tube, an inspiratory conduit connected to a first branch of the Y-piece, and an expiratory conduit connected to a second branch of the Y-piece.
4. The apparatus of claim 3, wherein the inspiratory conduit comprises at least a portion of the volume-adjustable deadspace.
5. The apparatus of claim 3, wherein the expiratory conduit comprises at least a portion of the volume-adjustable deadspace.
6. The apparatus of claim 1, wherein the volume-adjustable deadspace conduit comprises at least one volume-expandable and volume-contractible element.
7. The apparatus of claim 1, wherein the single one two-way valve is located adjacent to a junction between the airway conduit and the volume-adjustable deadspace conduit.
8. The apparatus of claim 7, further comprising:
  - a flow restrictor located along a length of the airway conduit to, in conjunction with the single one two-way valve, facilitate selective direction of gas into the volume-adjustable deadspace conduit.
9. The apparatus of claim 1, further comprising:
  - a volume-adjustable element positionable between the airway conduit and a source of ventilation gas.
10. The apparatus of claim 1, wherein the volume-adjustable deadspace comprises an evacuation line for collecting exhaled gas and a gas-release element associated with the evacuation line for tailoring an amount or carbon dioxide concentration of the exhaled gas within the evacuation line.
11. The apparatus of claim 6, wherein the at least one volume-expandable and volume-contractible element comprises a section of corrugated tubing.
12. The apparatus of claim 11, wherein the single two-way valve is located to facilitate selective direction of gas into the at least one volume-expandable and volume-contractible element.
13. The apparatus of claim 12, further comprising:
  - a flow restrictor located along a length of the airway conduit to, in conjunction with the single two-way valve, facilitate selective direction of gas into the at least one volume-expandable and volume-contractible element.

专利名称(译)	用于非侵入性地测量心输出量的装置		
公开(公告)号	<a href="#">US7686012</a>	公开(公告)日	2010-03-30
申请号	US11/120103	申请日	2005-05-02
[标]申请(专利权)人(译)	ORR约瑟夫 KOFOED斯科特 WESTENSKOW DWAYNE JAFJE MICHAEL 乙		
申请(专利权)人(译)	ORR JOSEPH A. KOFOED SCOTT A. WESTENSKOW DWAYNE JAFJE MICHAEL B.		
当前申请(专利权)人(译)	RIC投资有限责任公司		
[标]发明人	ORR JOSEPH A KOFOED SCOTT A WESTENSKOW DWAYNE JAFJE MICHAEL B		
发明人	ORR, JOSEPH A. KOFOED, SCOTT A. WESTENSKOW, DWAYNE JAFJE, MICHAEL B.		
IPC分类号	A61M15/00 A61M16/00 A61B5/00 A61B5/026 A61B5/029 A61B5/08 A61B5/083 A61B5/087 A61B5/097 A61B10/00 G01N33/00		
CPC分类号	A61B5/029 A61B5/0836 A61M16/0045 A61M2016/0036 A61M2230/432 G01N33/004 A61M16/0833 Y02A50/243		
其他公开文献	US20050203432A1		
外部链接	<a href="#">Espacenet</a> <a href="#">USPTO</a>		

摘要(译)

公开了使用部分再呼吸技术非侵入性地确定心输出量的装置和方法，其中该装置构造有可瞬时调节的死腔，用于适应各种患者的呼吸能力差异。该装置由廉价的元件构成，包括单个双向阀，这使得该装置使用起来非常简单并且便宜，因此该装置可以容易地丢弃。本发明的方法提供了一种基于肺泡CO<sub>2</sub>值而不是如先前实践的呼气末CO<sub>2</sub>值估计心输出量的新方法。还公开了一种用于计算心输出量的程序。

