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- (54) **BLOOD PRESSURE MEASUREMENT METHOD**
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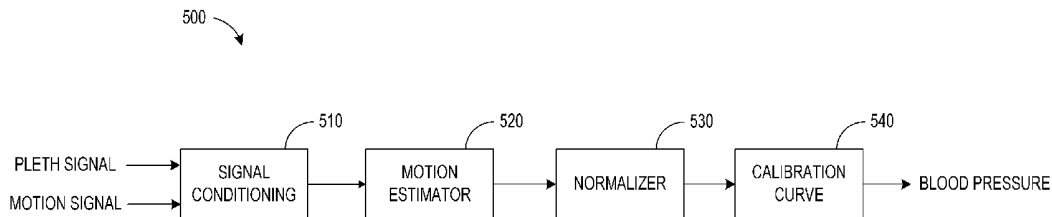
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(57) **ABSTRACT**

A blood pressure measurement system that non-invasively determines an individual's blood pressure can include a noninvasive blood pressure sensor having an optical sensor and a motion sensor. The optical sensor can provide a photoplethysmograph signal obtained from a patient to a processor. The motion sensor can provide a motion signal to the processor responsive to motion of the patient. In one embodiment, the processor calculates or estimates the blood pressure of the patient based on the photoplethysmograph signal and the motion signal. Advantageously, the system can obtain this blood pressure measurement without an occlusive cuff, thereby reducing patient discomfort. In other implementations, the processor calculates a blood pressure-related parameter from the photoplethysmograph and motion signal. The processor can occasionally trigger an occlusive cuff measurement as this parameter changes, thereby reducing the frequency of occlusive cuff measurements.

7 Claims, 27 Drawing Sheets



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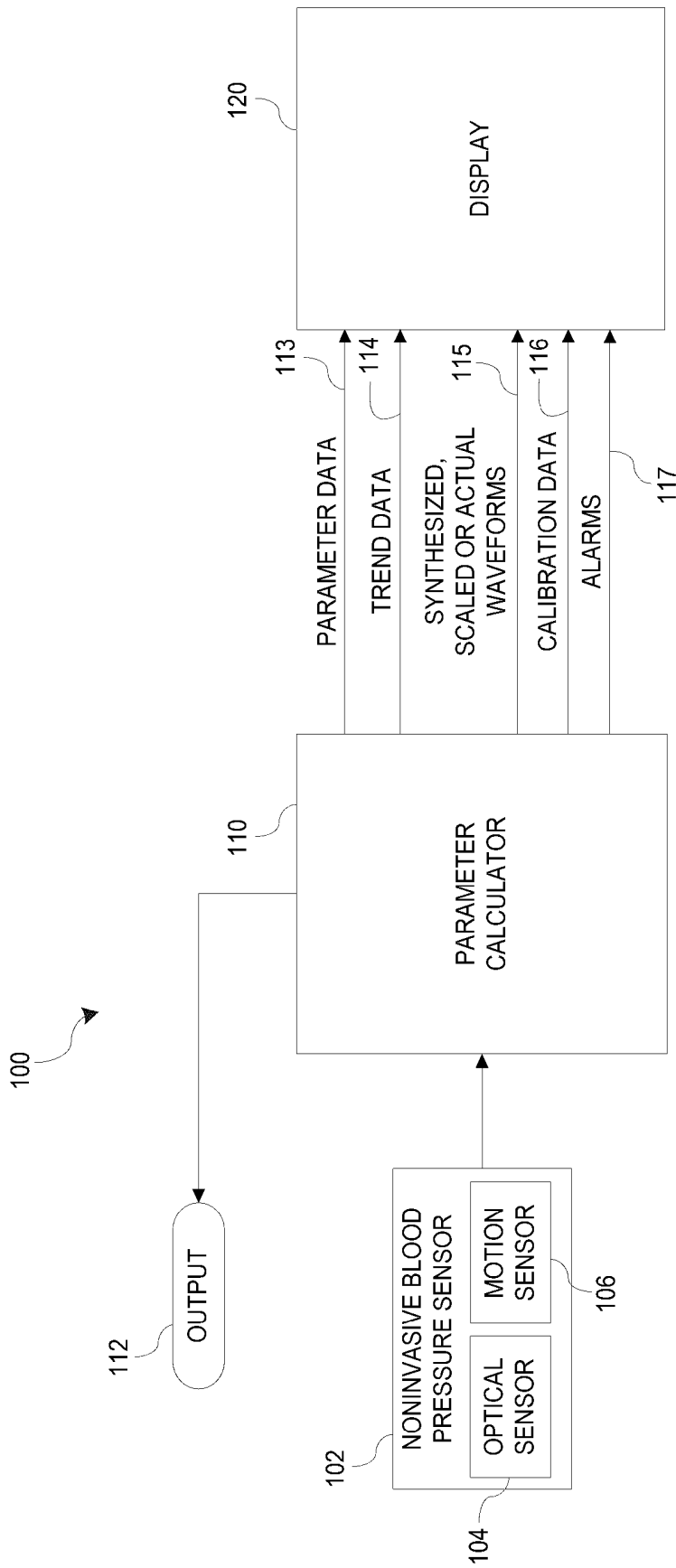


FIG. 1

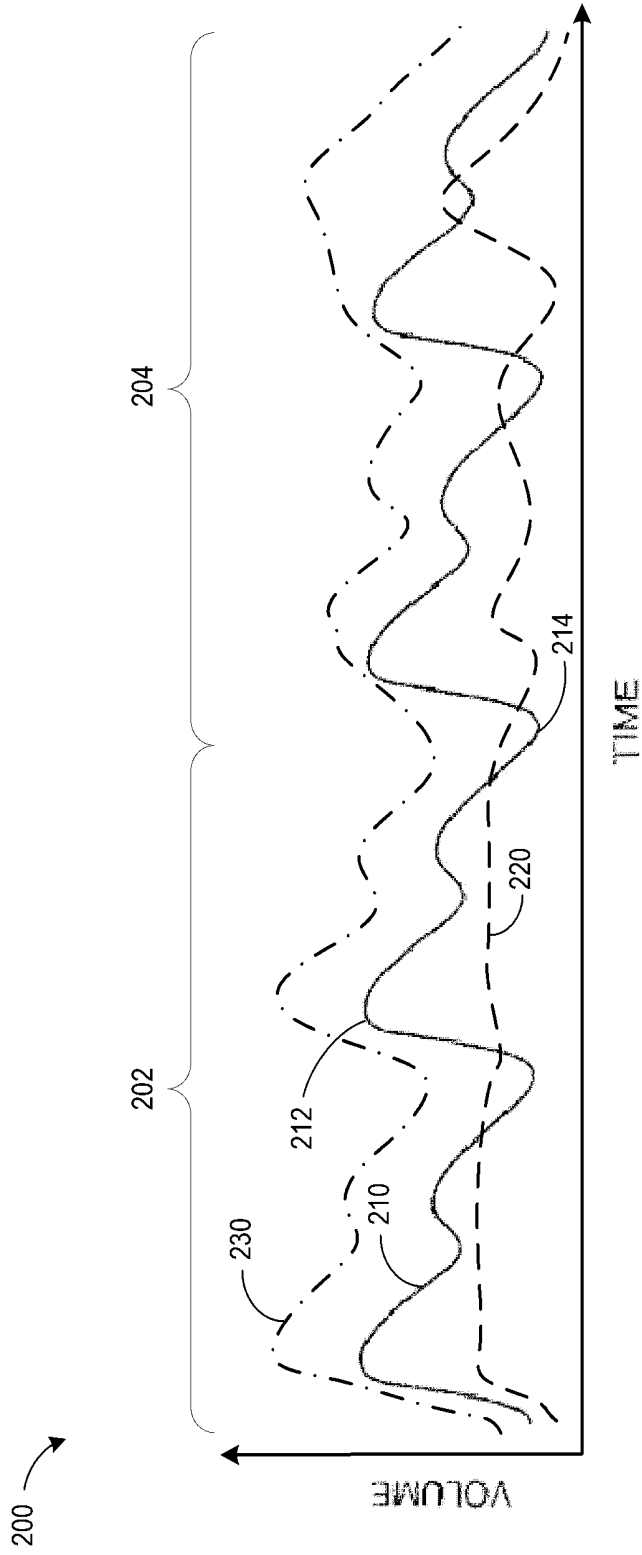


FIG. 2

SPOT-CHECK BLOOD PRESSURE MEASUREMENT
PROCESS

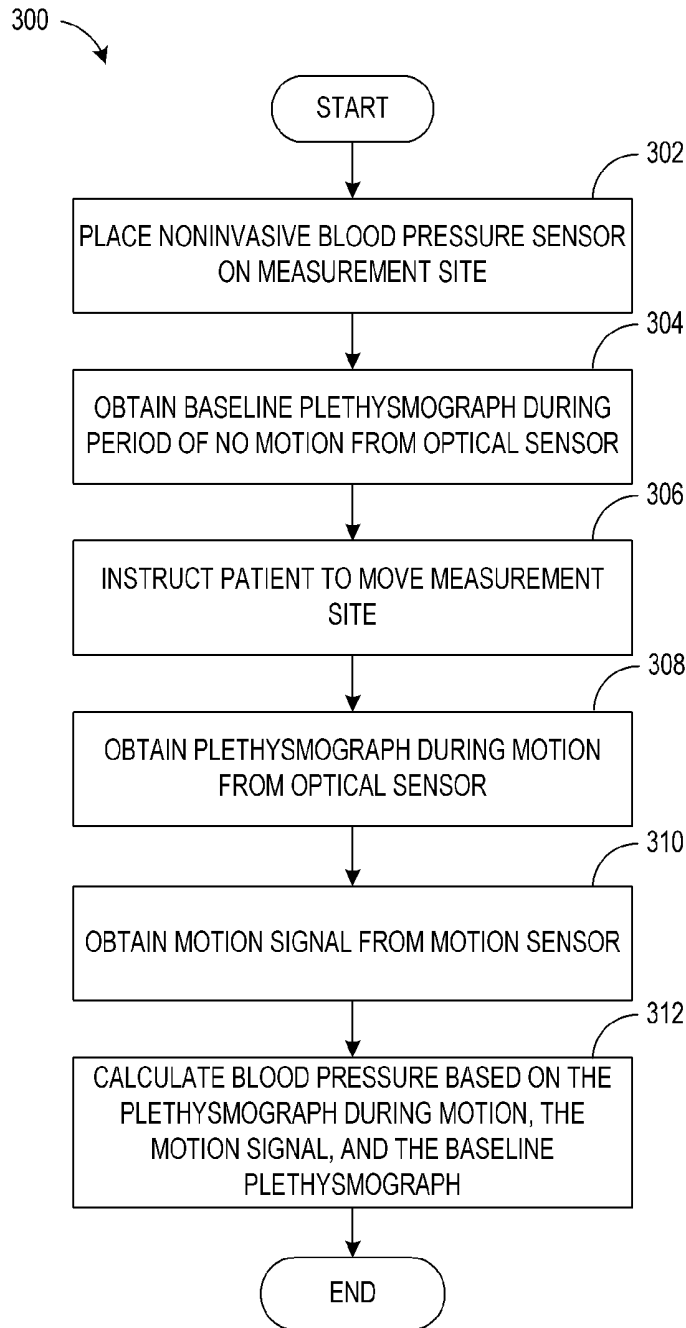


FIG. 3

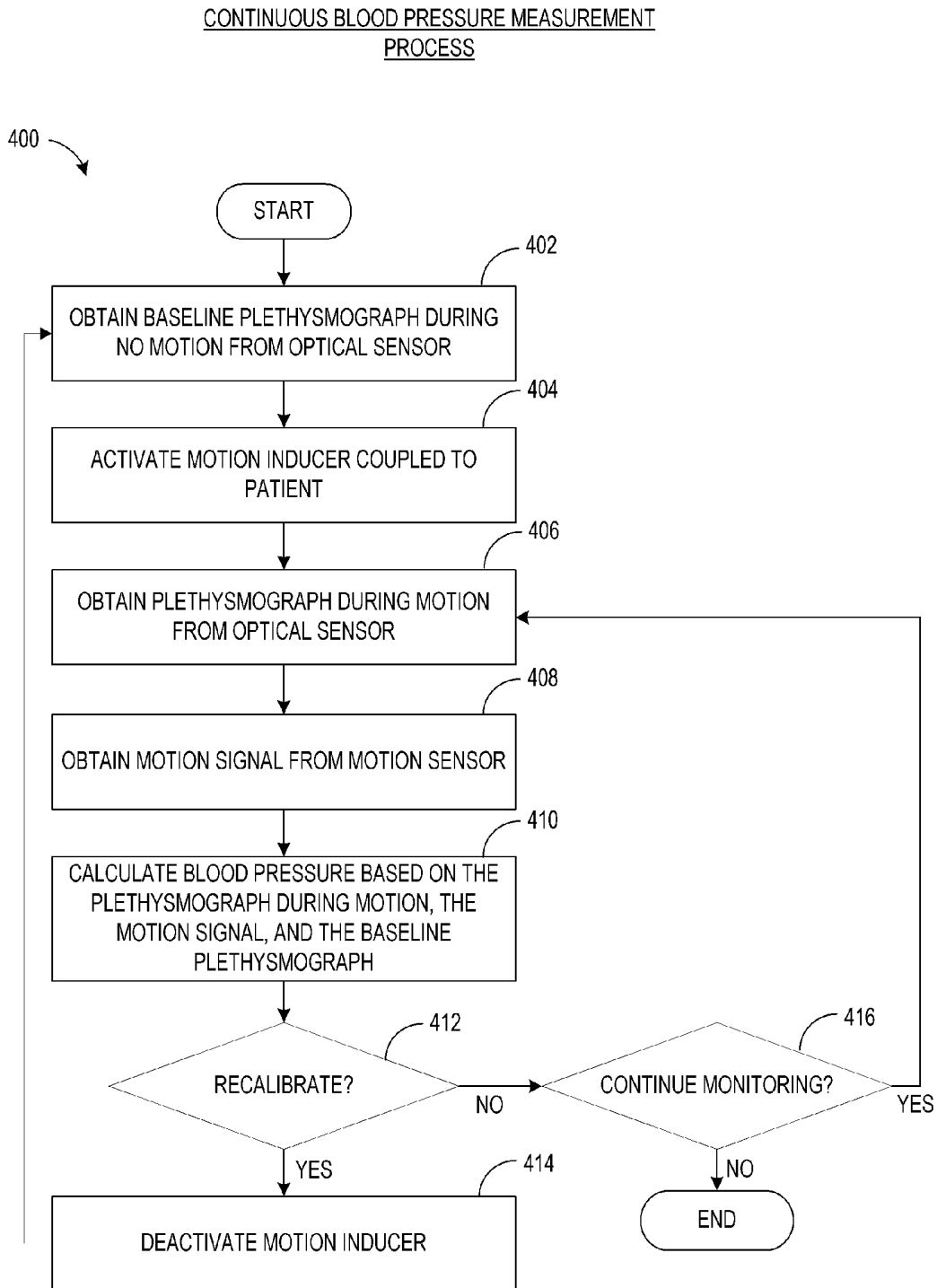


FIG. 4

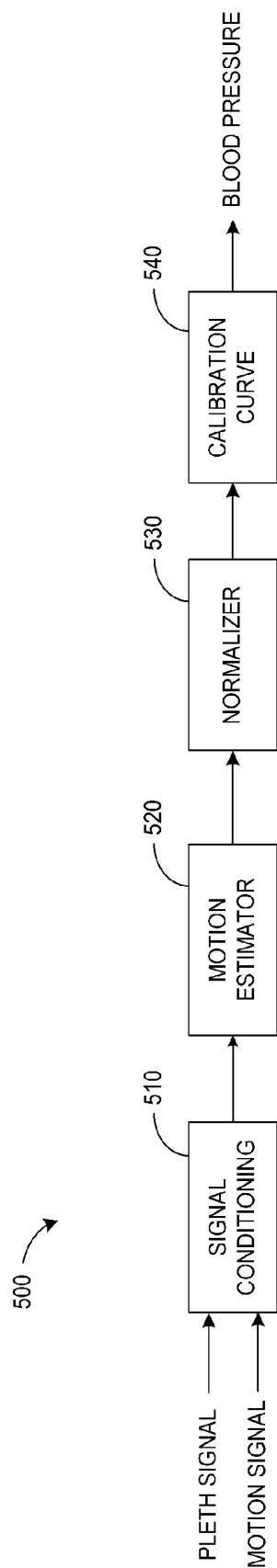


FIG. 5

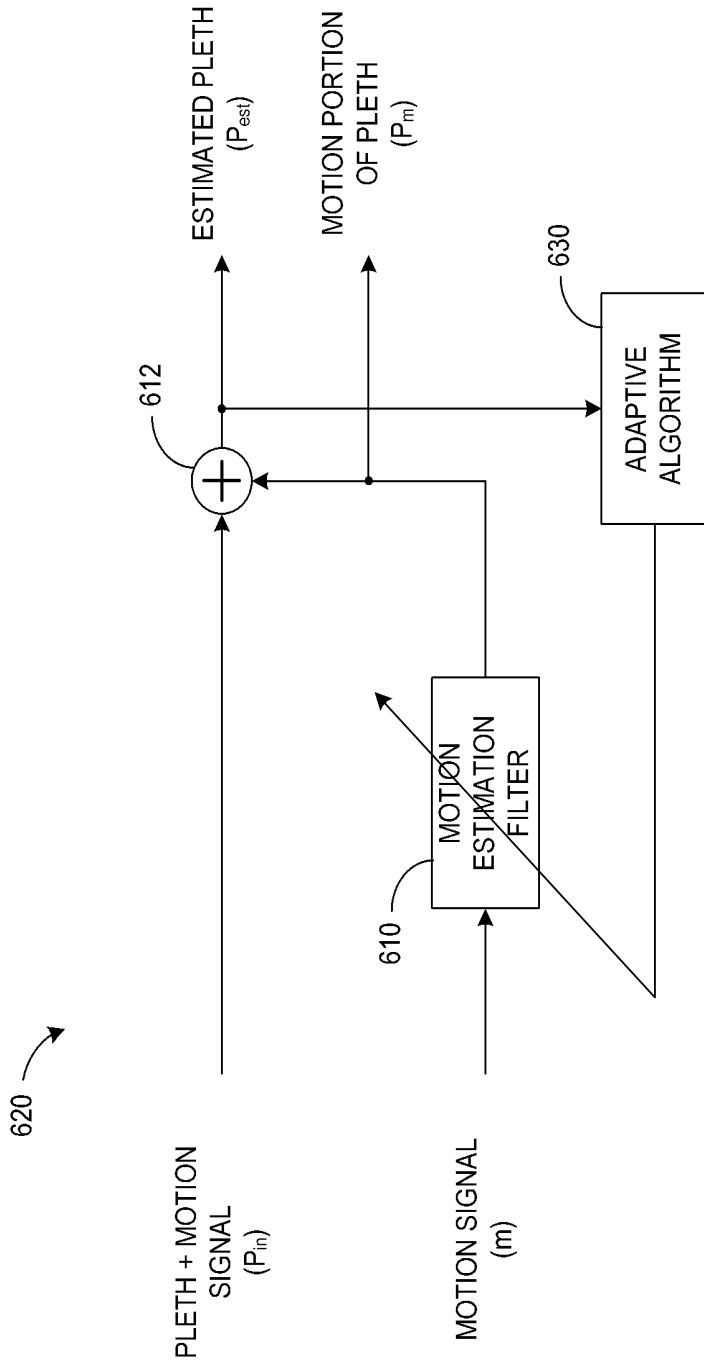


FIG. 6

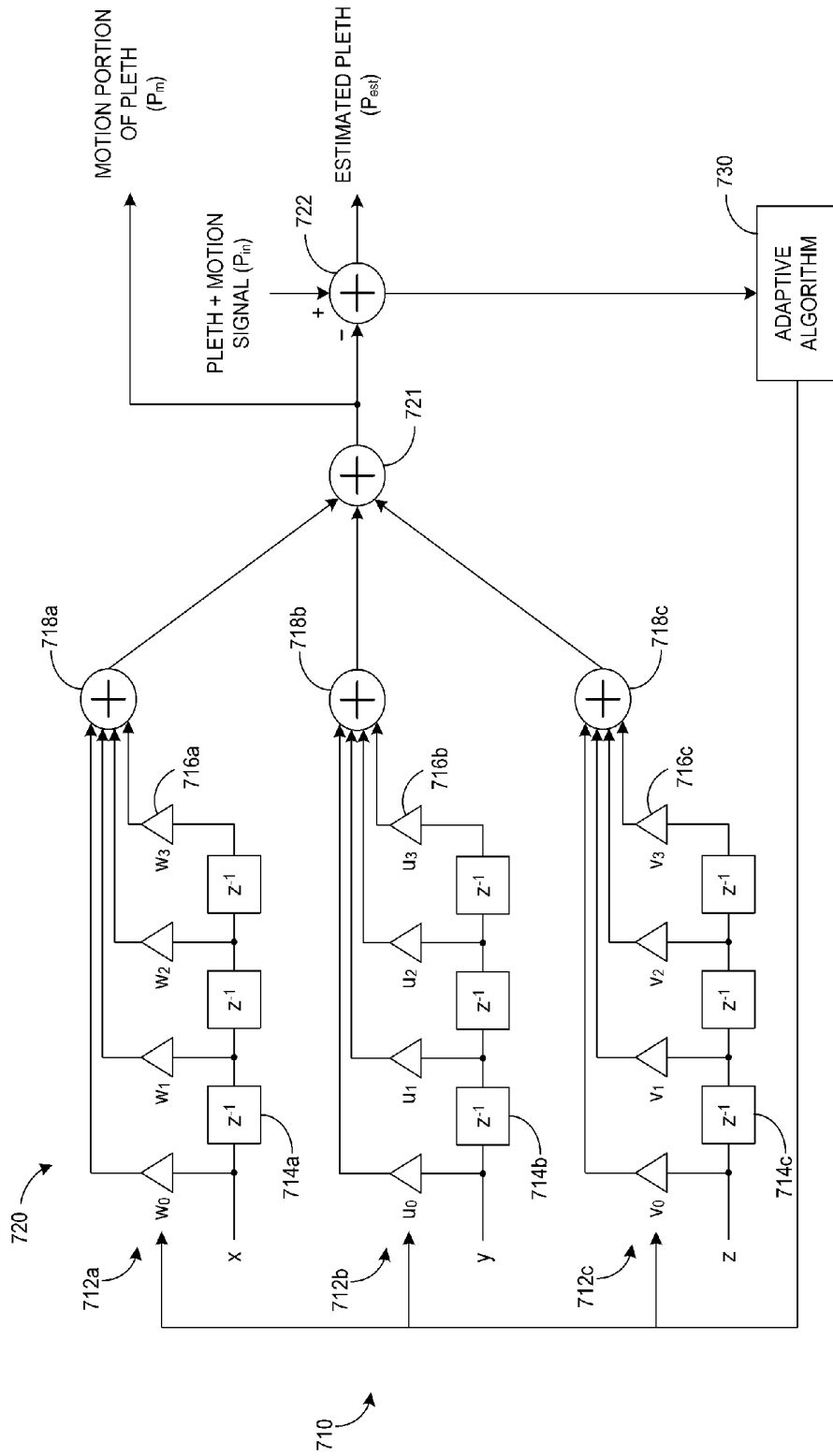


FIG. 7

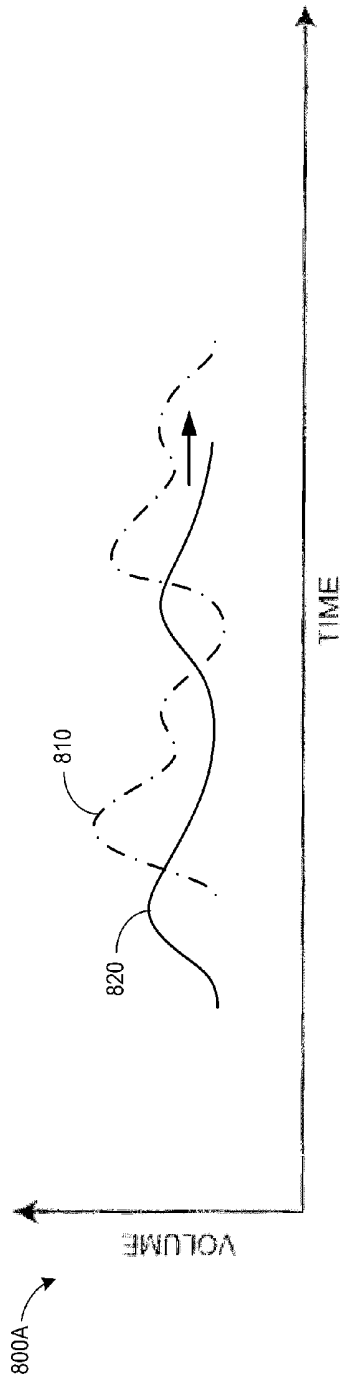


FIG. 8A

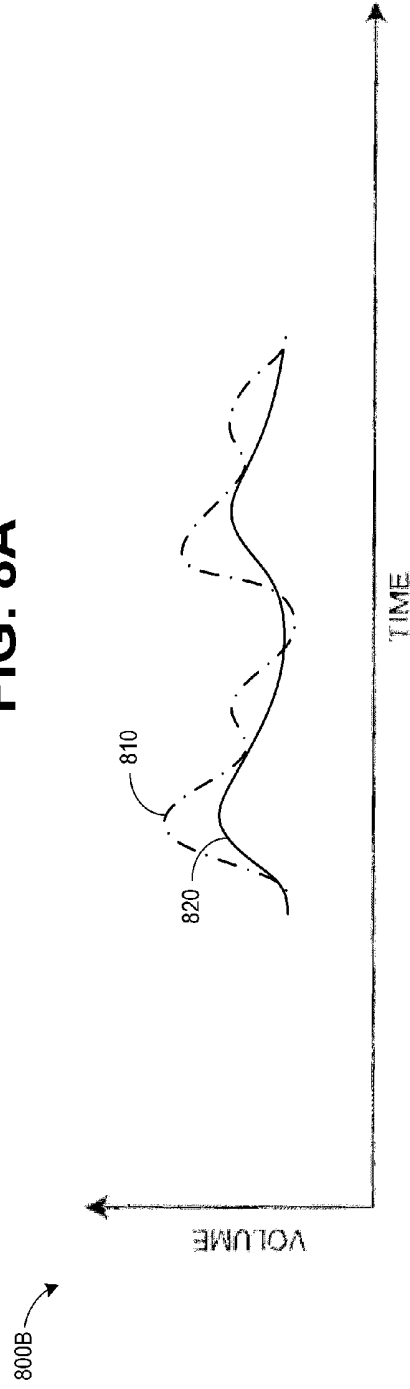


FIG. 8B

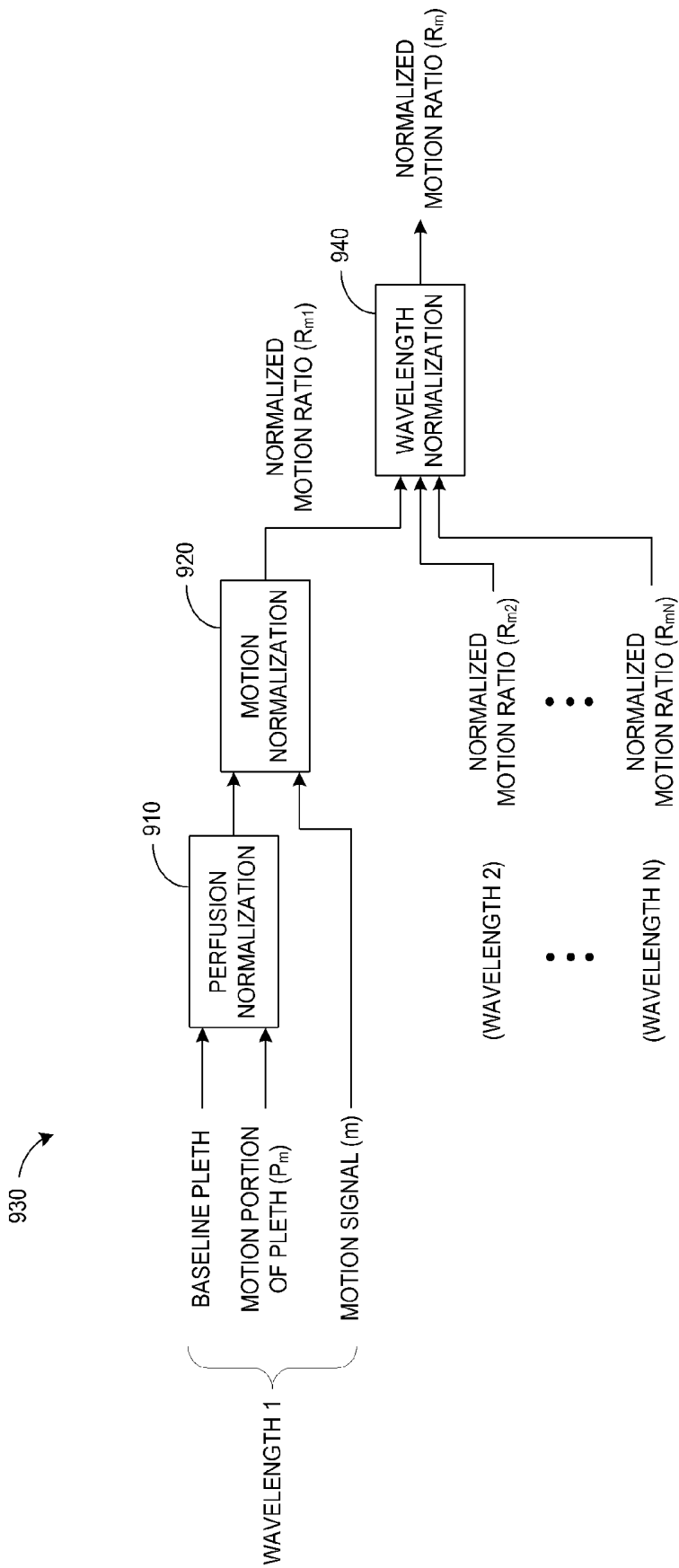


FIG. 9

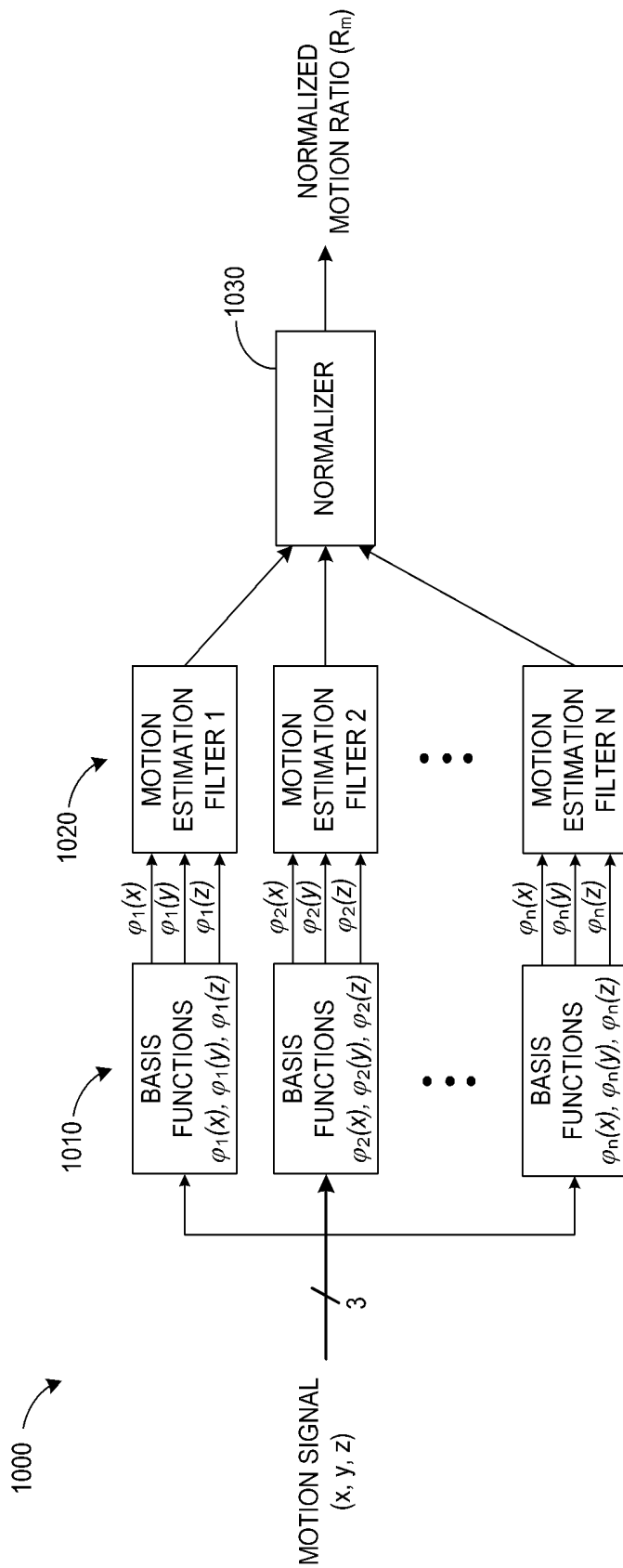


FIG. 10

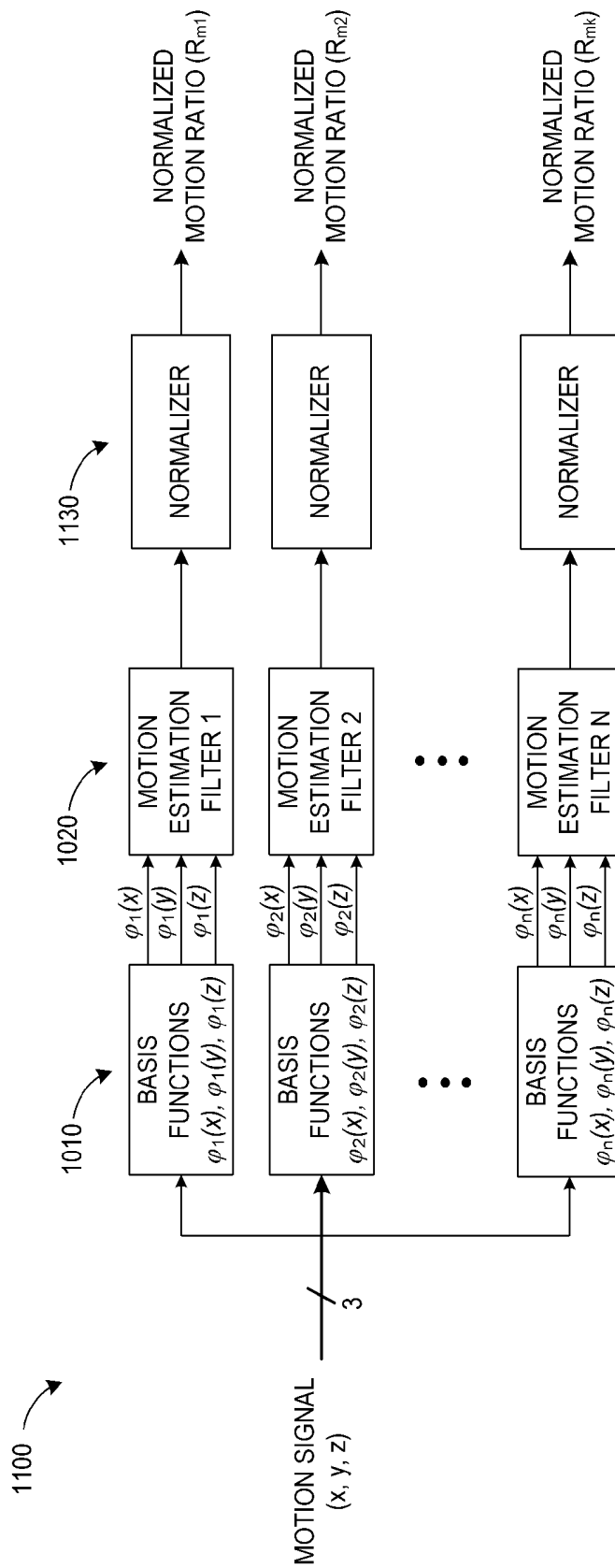


FIG. 11

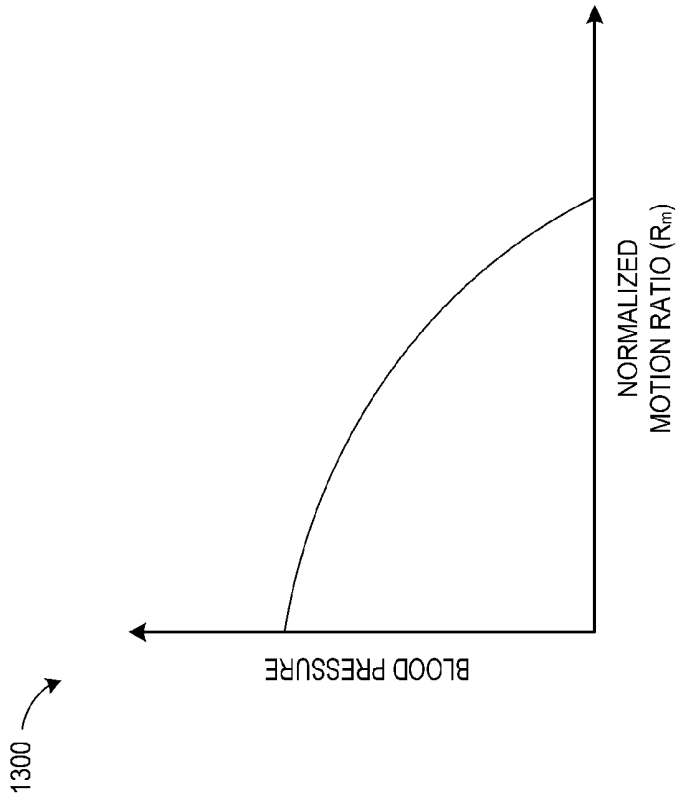


FIG. 13

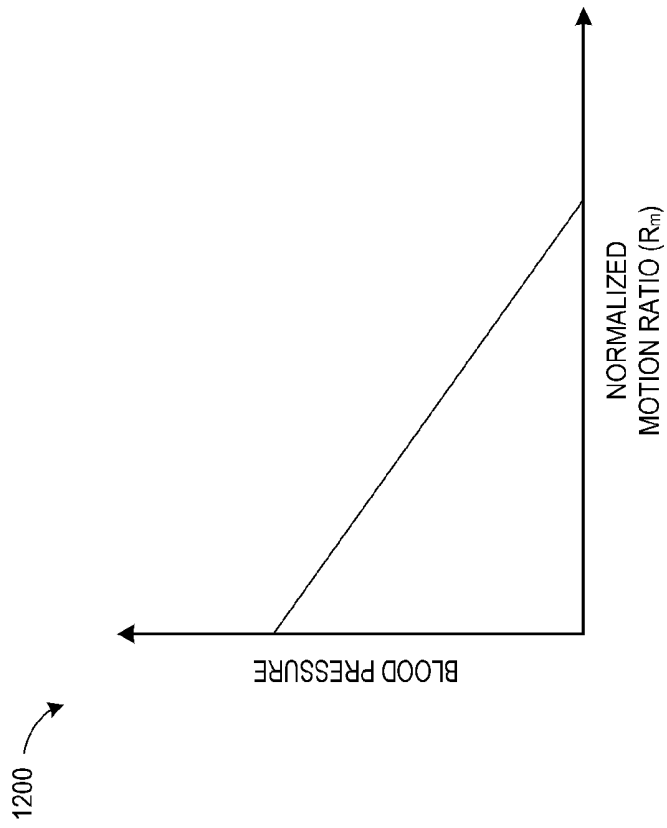


FIG. 12

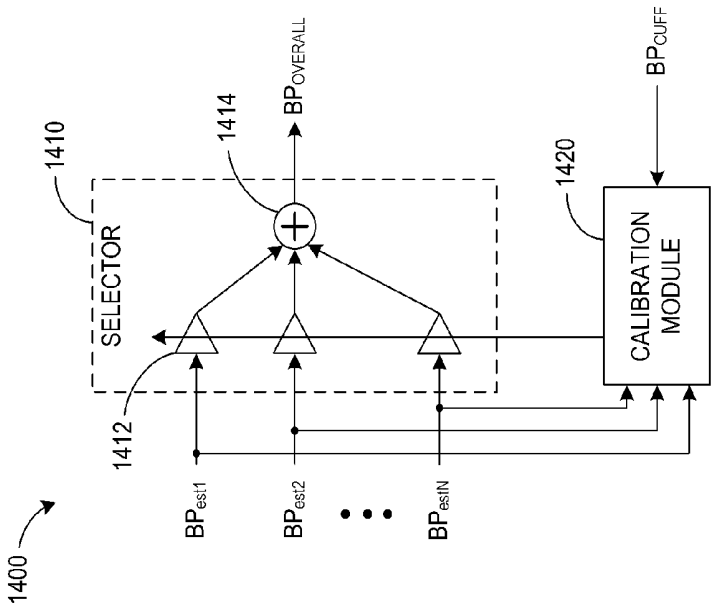


FIG. 14

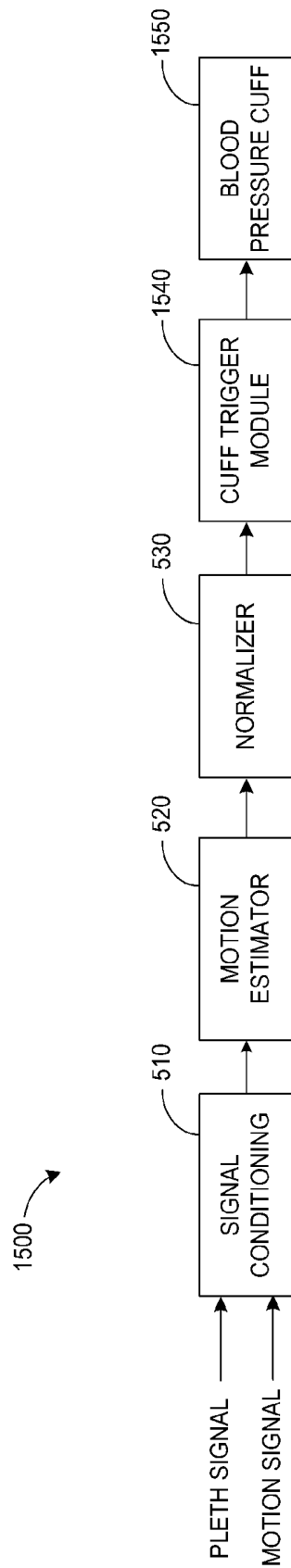


FIG. 15

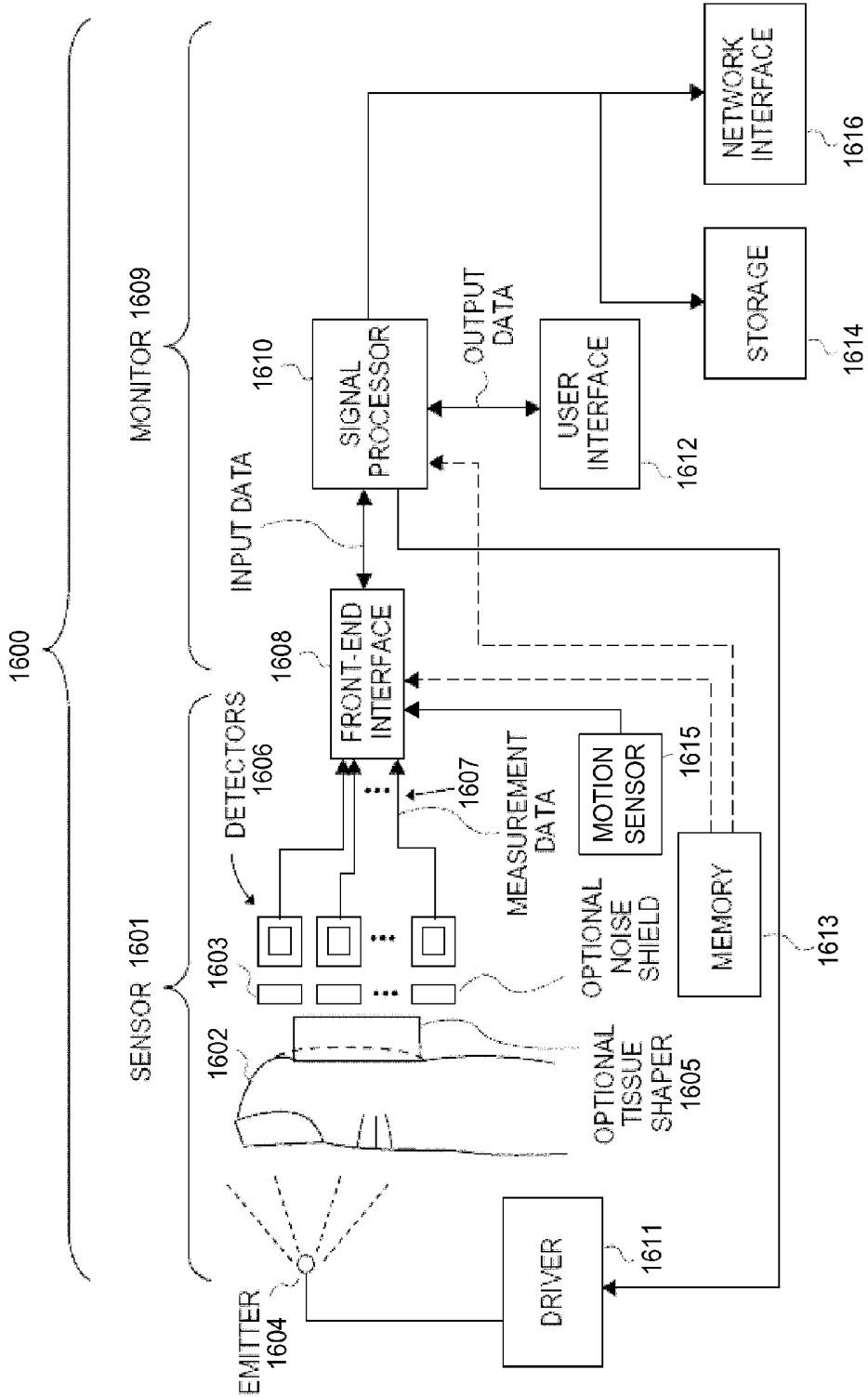


FIG. 16

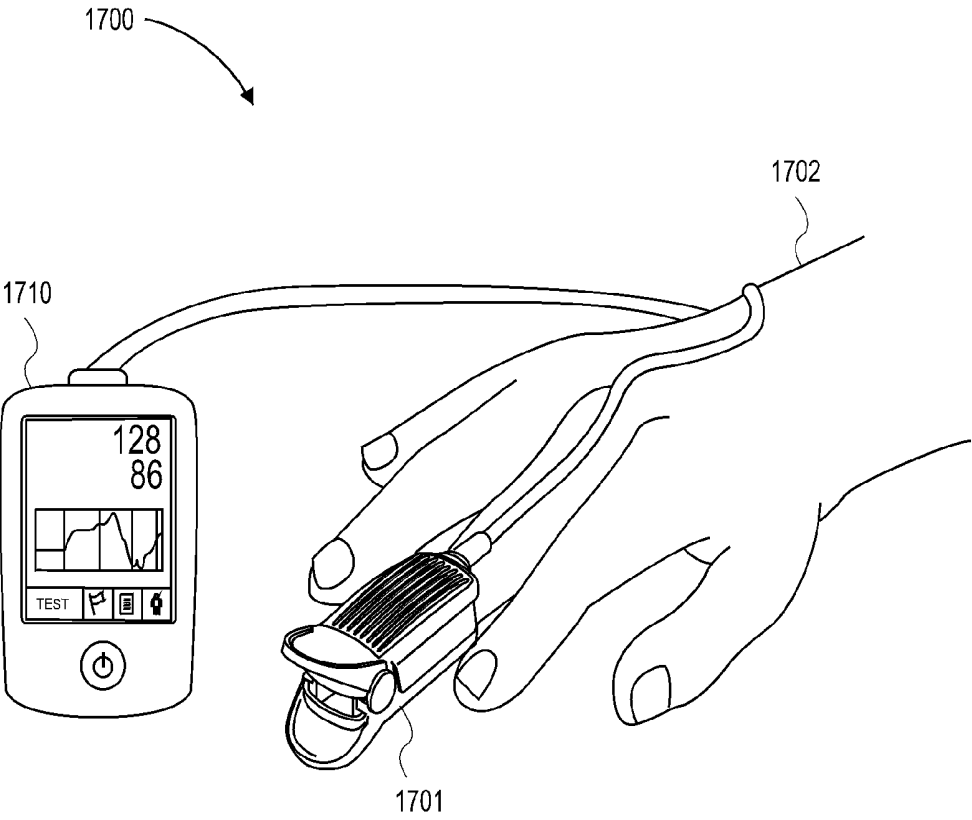


FIG. 17

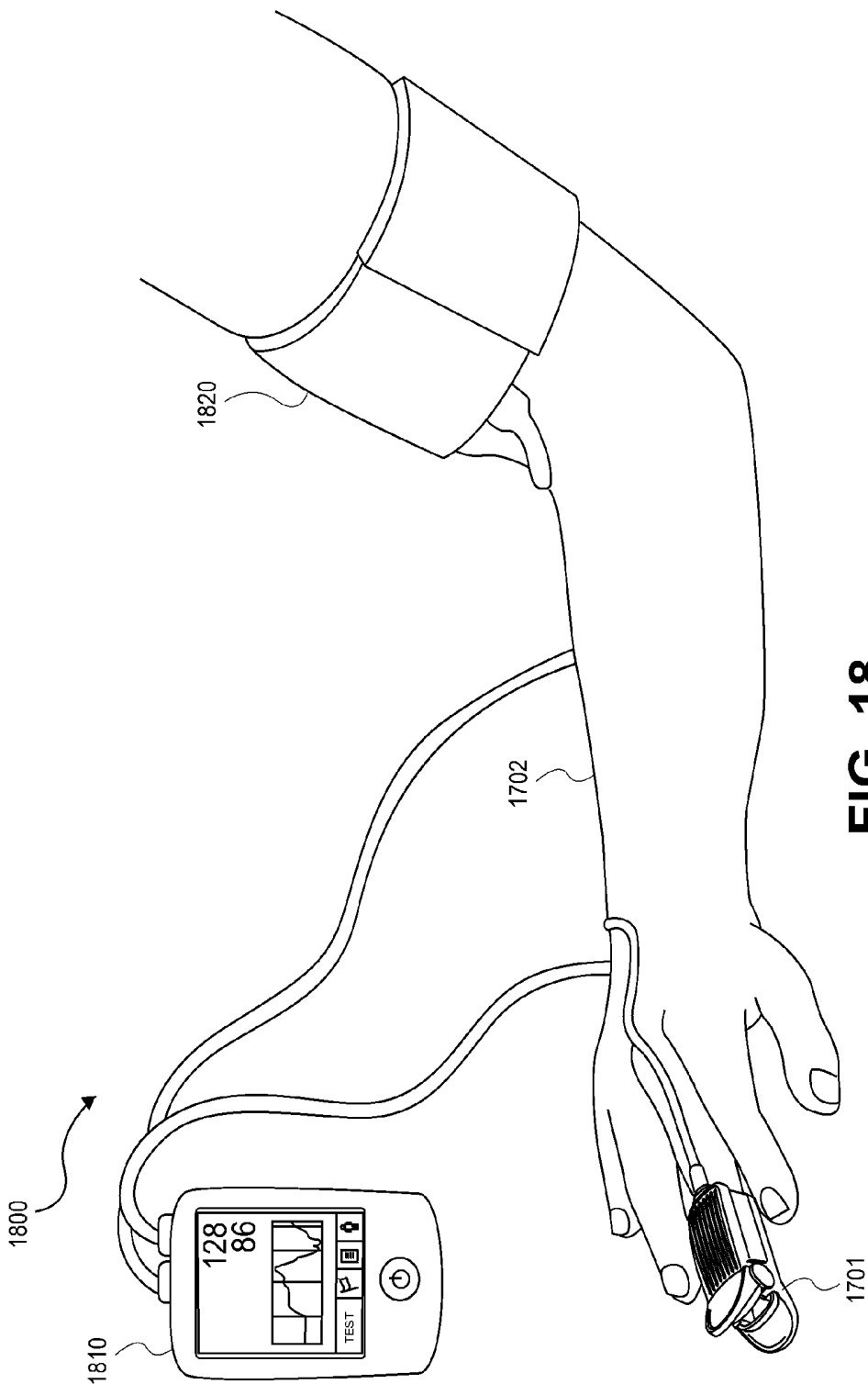


FIG. 18

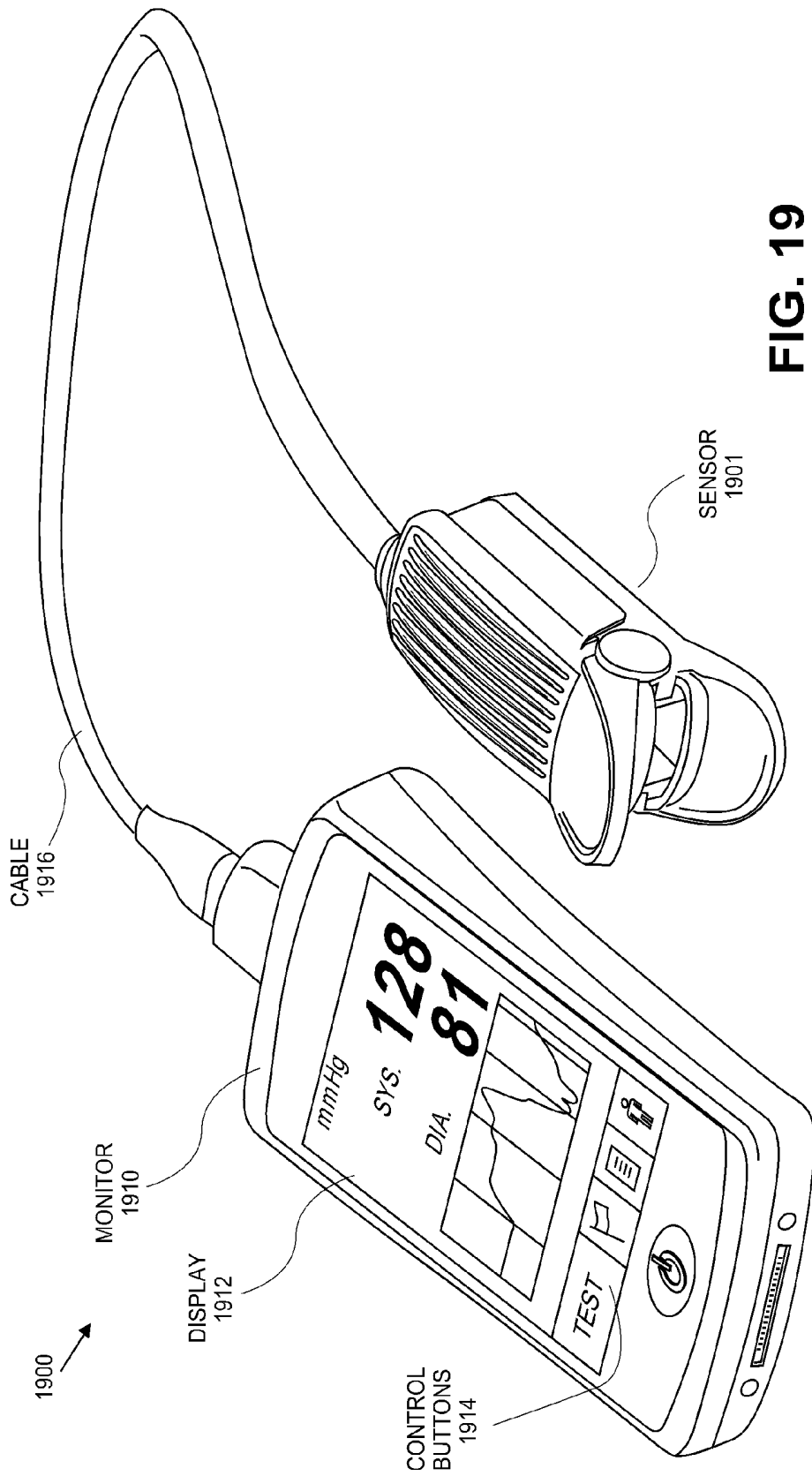


FIG. 19

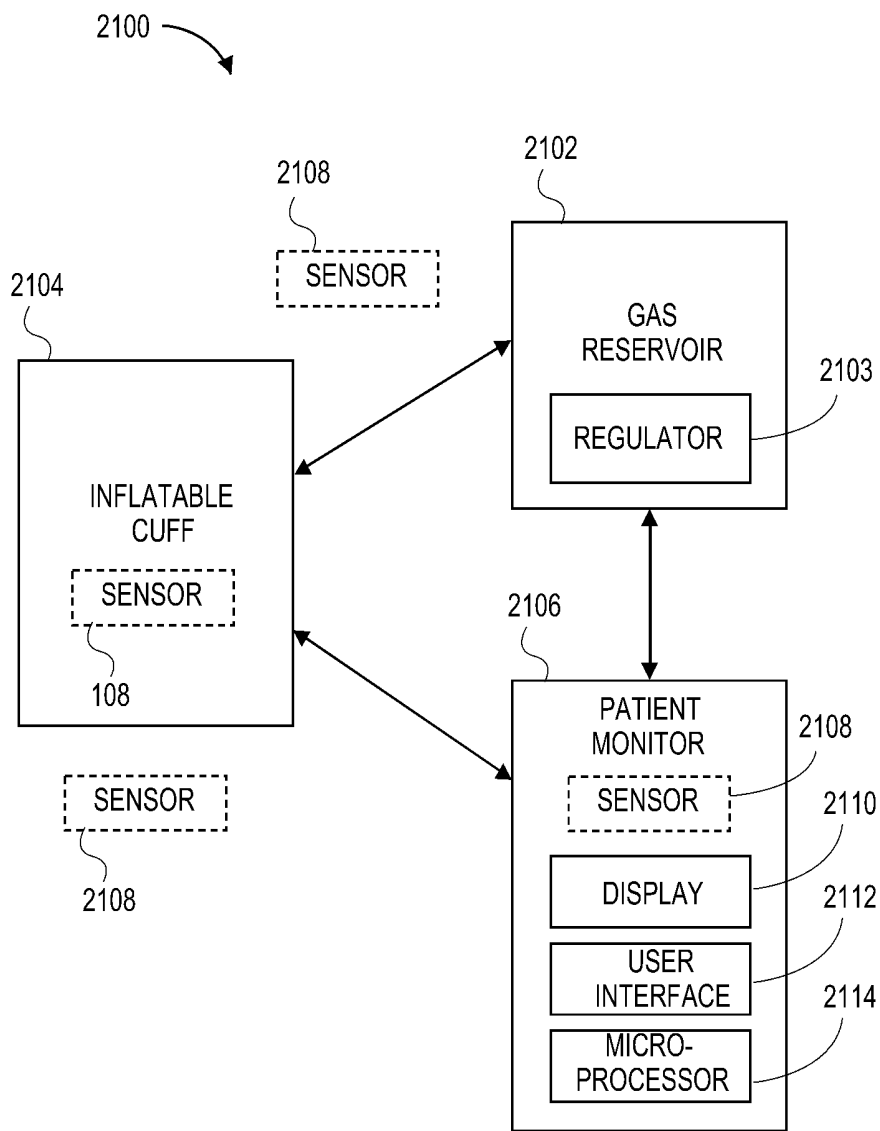
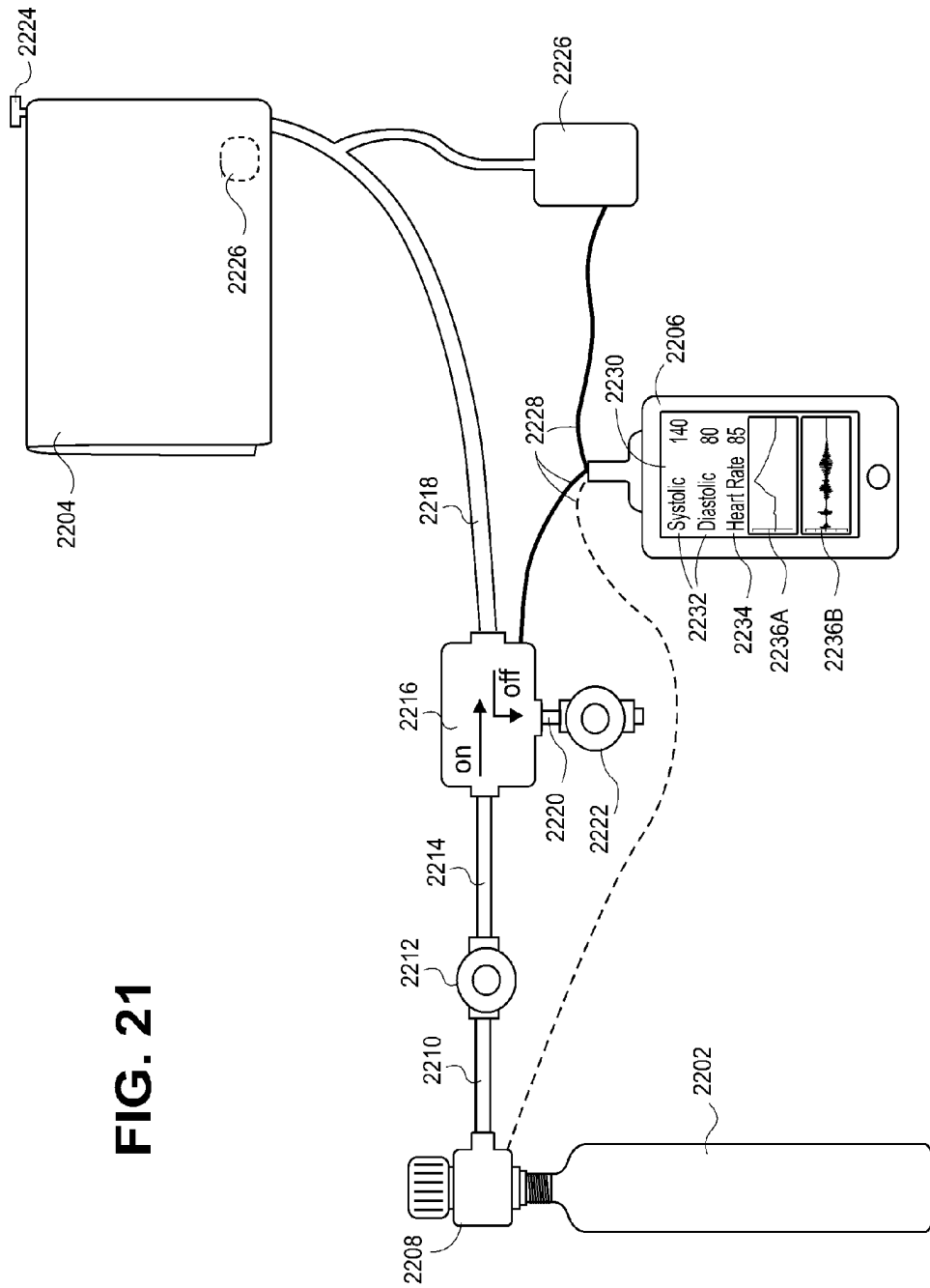


FIG. 20

FIG. 21



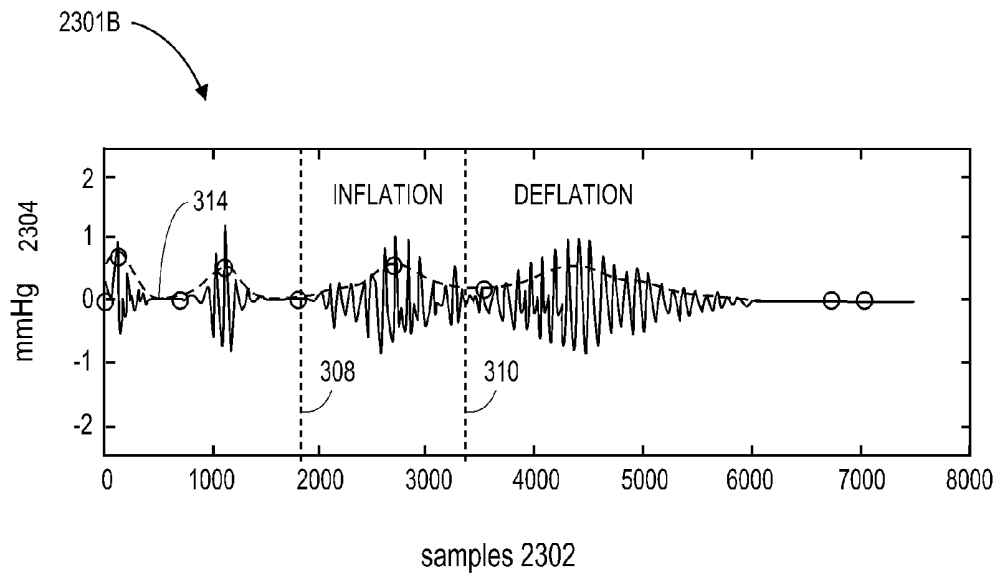
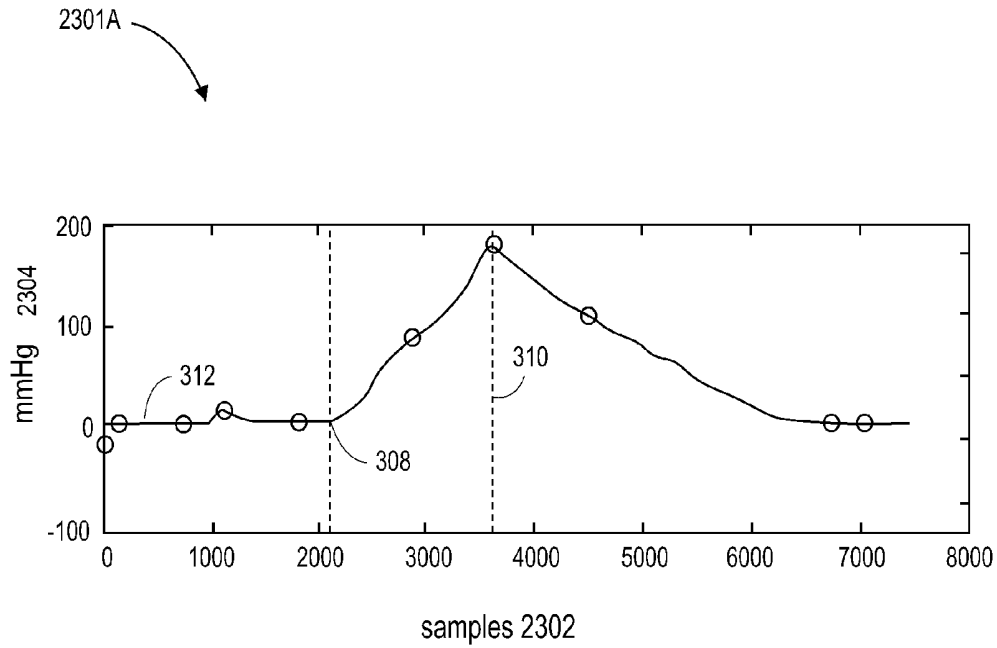


FIG. 22A

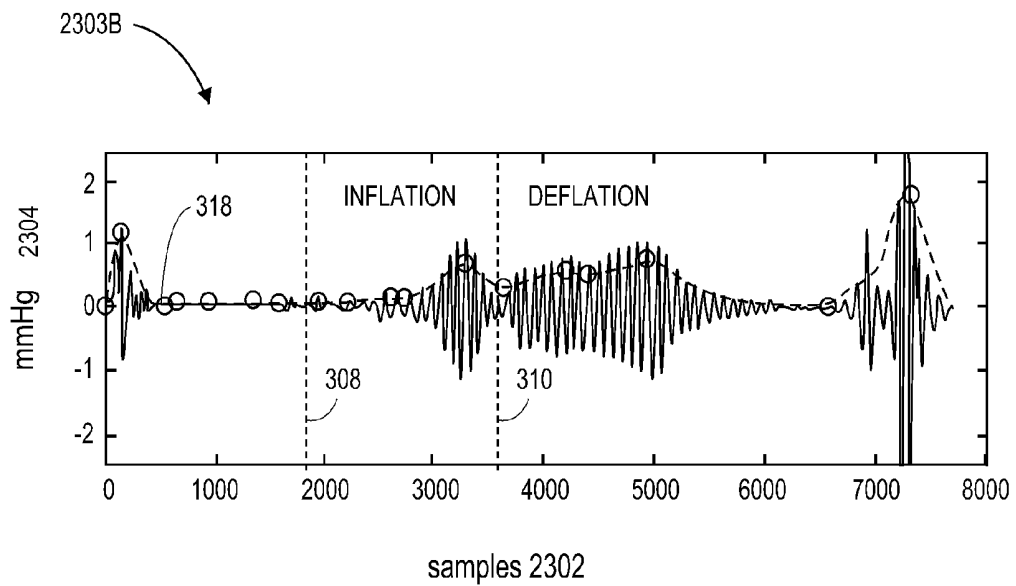
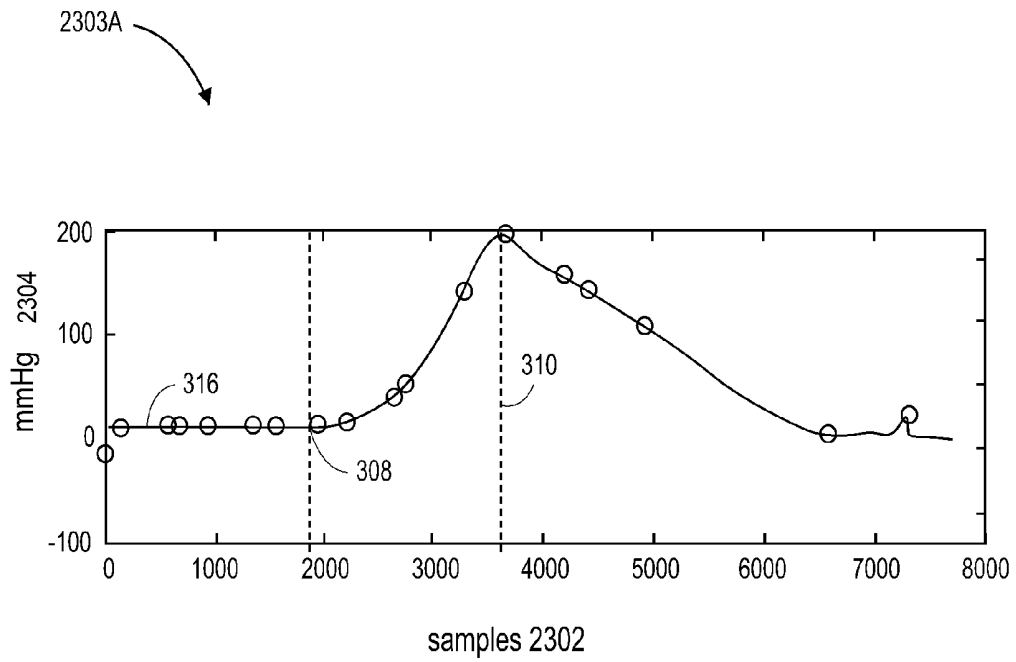


FIG. 22B

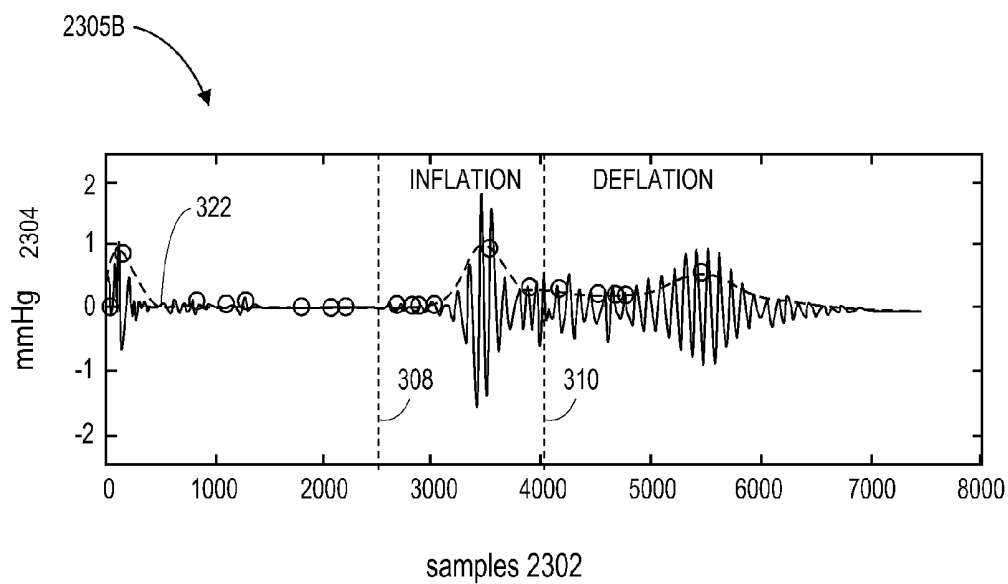
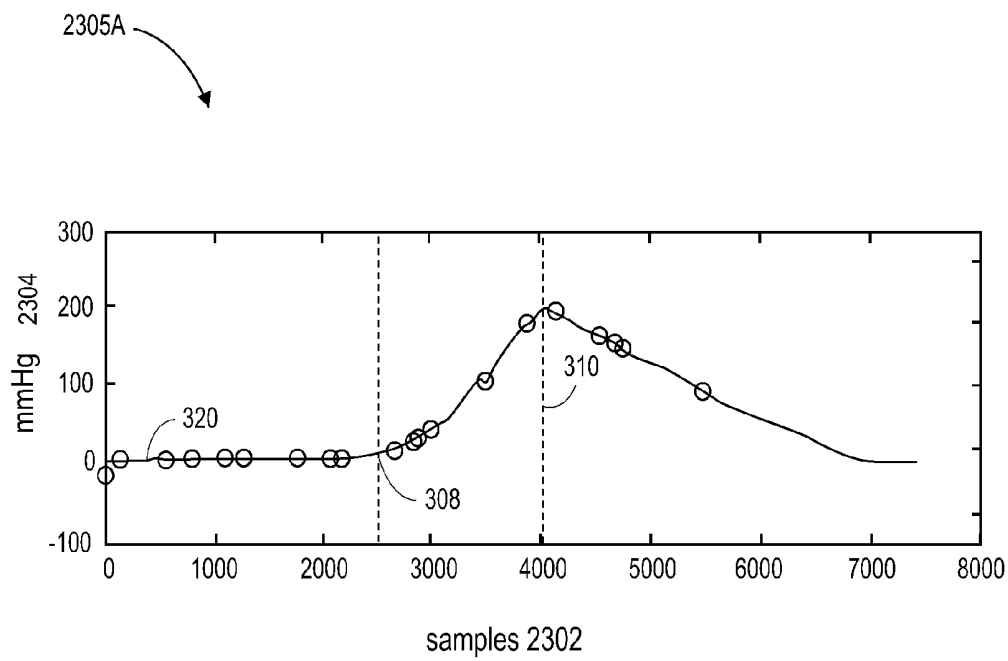


FIG. 22C

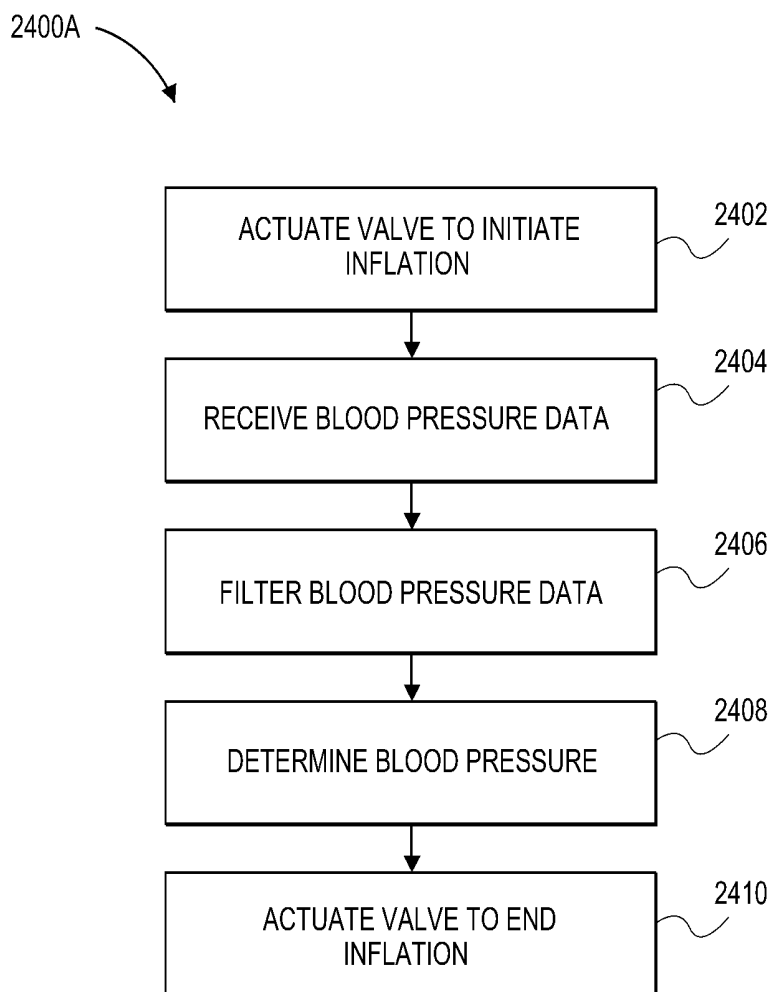


FIG. 23A

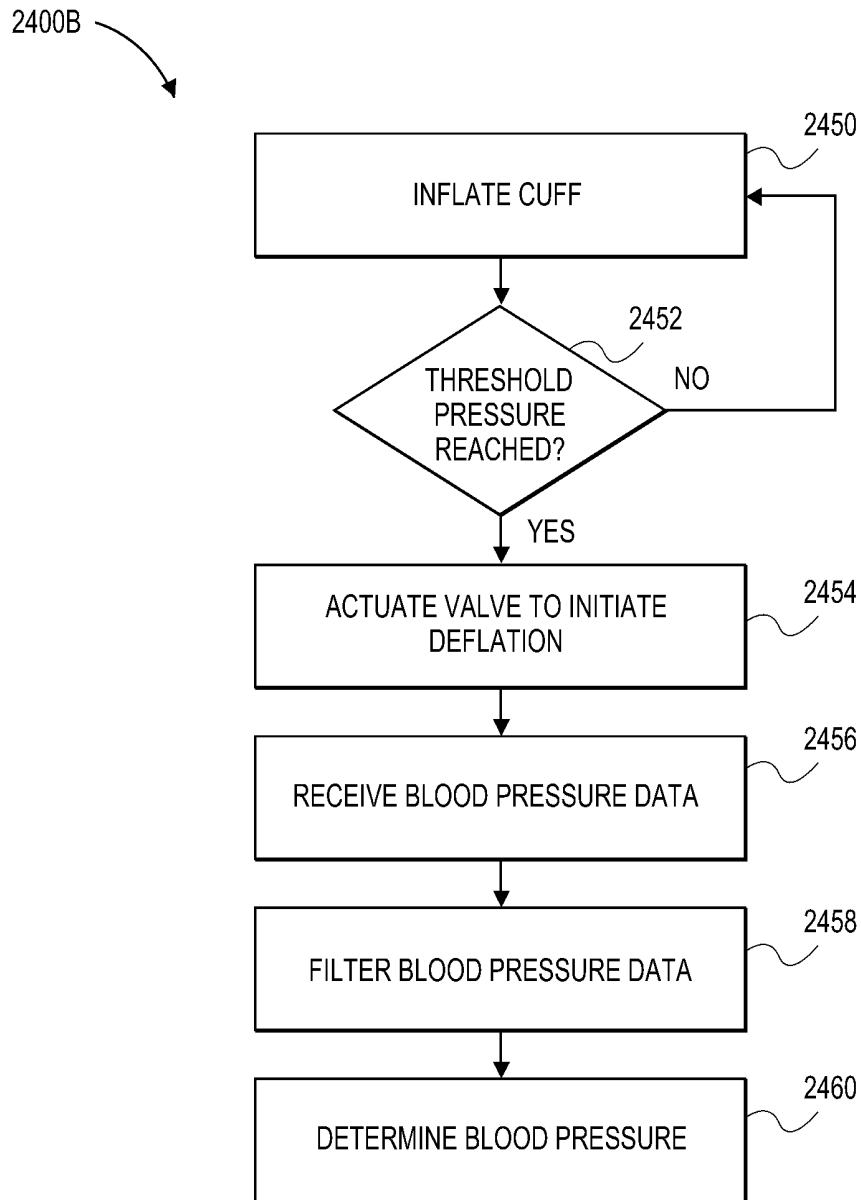


FIG. 23B

2011

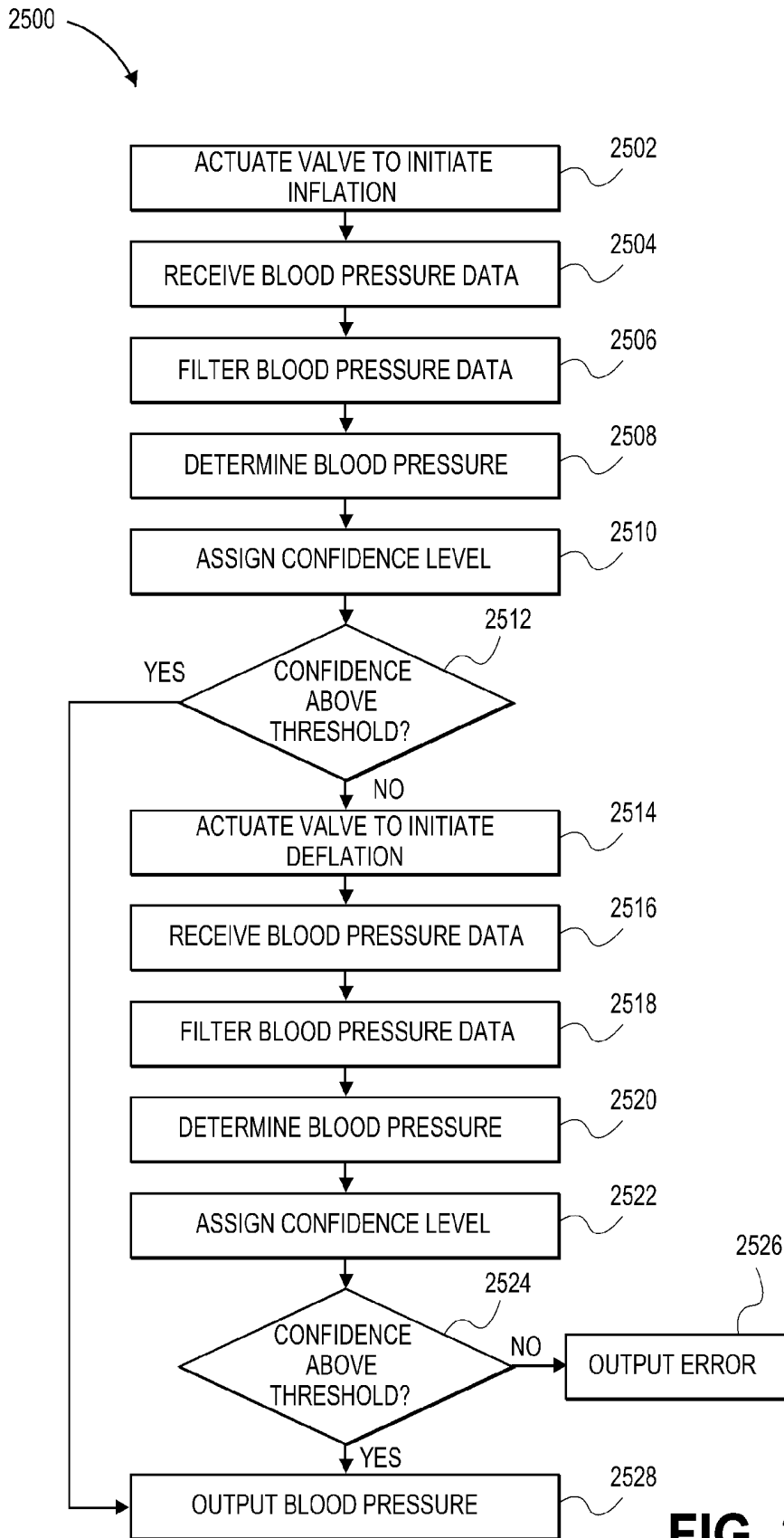


FIG. 24

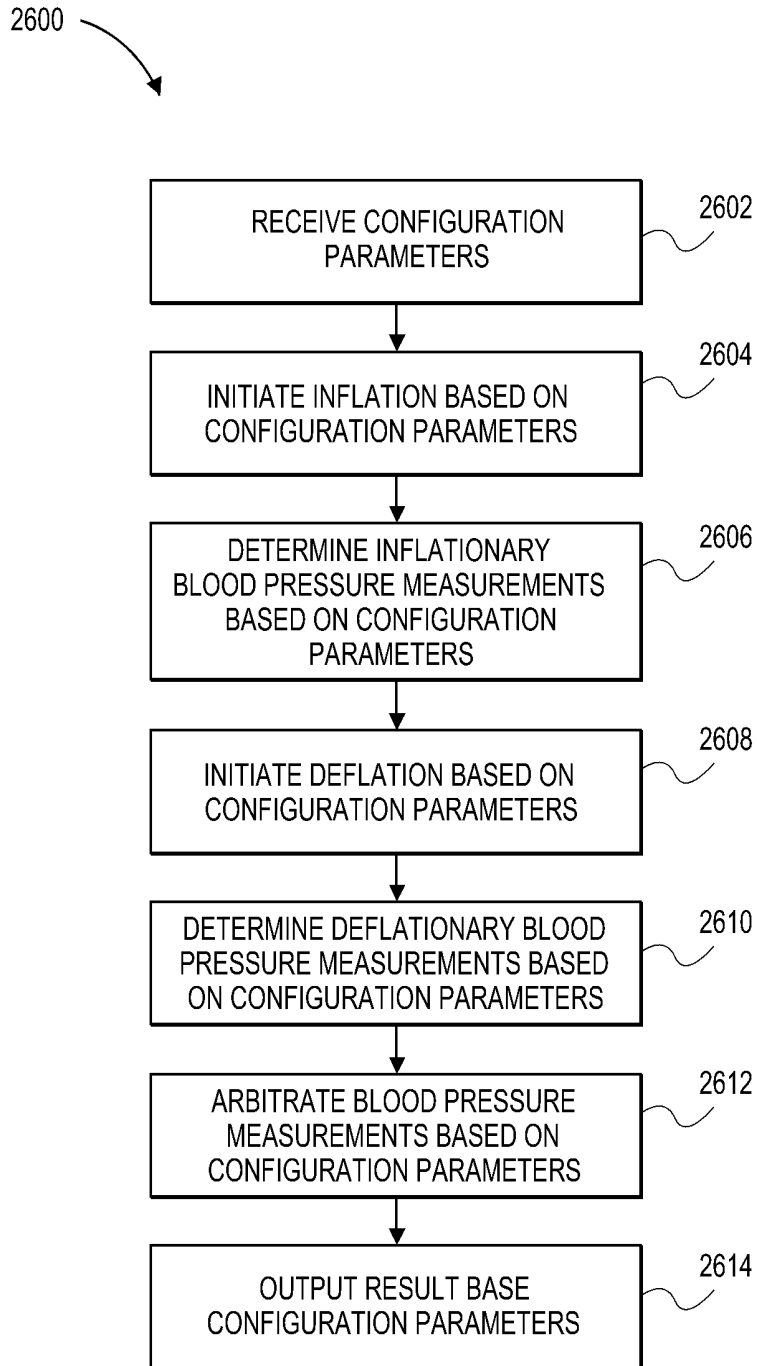


FIG. 25

BLOOD PRESSURE MEASUREMENT METHOD

RELATED APPLICATION

This application claims priority under 35 U.S.C. §119(e) to U.S. Provisional Application No. 61/377,192 filed Aug. 26, 2010, entitled "Pulse Oximetry System for Monitoring Blood Pressure," and 61/499,515, filed Jun. 21, 2011, entitled "Blood Pressure Monitoring System," the disclosures of both of which are hereby incorporated by reference in their entirety.

BACKGROUND

Prolonged reduction or loss of blood pressure in a patient severely limits the amount of tissue perfusion of the patient and therefore causes damage to or death of the tissue. Although some tissues can tolerate hypoperfusion for long periods of time, the brain, heart and kidneys are very sensitive to a reduction in blood flow. Thus, during and after medical procedures and at other times, blood pressure is a frequently monitored vital sign. Blood pressure can be affected by the type of medical procedure performed and by physiological factors such as the body's reaction to the medical procedure. Moreover, blood pressure is often manipulated and controlled using various medications. Medical procedures, physiological factors, and medications can cause the blood pressure of a patient to change rapidly.

The traditional method of measuring blood pressure is with a stethoscope, occlusive cuff, and pressure manometer. However, this technique is slow, subjective in nature, involves the intervention of a skilled clinician, and often does not provide timely measurements. Blood pressure cuff instruments make only spot-check measurements, so repetitive interval measurements are often used to trend patient status. More frequent intervals improve vigilance at the expense of patient discomfort and possible patient injury (e.g., due to occlusion of blood vessels or nerve damage).

SUMMARY

In certain embodiments, a sensor for measuring blood pressure includes an optical sensor having an emitter configured to emit light on a measurement site of a patient and a detector configured to detect the light after attenuation by the measurement site and to output a photoplethysmograph signal responsive to the attenuated light. The sensor may further include a motion sensor configured to sense motion of the patient at the measurement site and to provide a motion signal responsive to the sensed motion, wherein the photoplethysmograph signal and the motion signal are configured to be used to derive a blood pressure of the patient.

Additionally, in some embodiments, a method of measuring blood pressure includes obtaining a photoplethysmograph signal from an optical sensor coupled with a patient at a measurement site that is in motion, obtaining a motion signal from a motion sensor coupled with the measurement site, and calculating a blood pressure measurement based at least in part on the photoplethysmograph signal and the motion signal.

In other embodiments, a method for measuring blood pressure includes attaching an inflatable cuff to a person, inflating the cuff at an approximately constant rate using gas from a gas reservoir, and measuring blood pressure of the person while the cuff is inflating. Further, some embodiments include a method of measuring blood pressure that

includes obtaining a photoplethysmograph signal from an optical sensor coupled with a patient at a measurement site that is in motion, obtaining a motion signal corresponding to a motion portion of the photoplethysmograph signal, where the motion portion is at least partially induced by the motion at the measurement site, and triggering a blood pressure cuff to take a measurement responsive to the photoplethysmograph signal and the motion signal.

Various embodiments of a blood pressure monitoring system include an inflatable cuff attachable to a wearer, a gas reservoir configured to provide gas to the inflatable cuff via a gas pathway, a sensor configured to obtain blood pressure data from the inflatable cuff, and a patient monitor configured to receive the blood pressure data from the sensor to determine a blood pressure measurement of the wearer. Moreover, embodiments of a blood pressure monitoring system include an inflatable cuff attachable to a wearer, and a gas reservoir comprising compressed gas and configured to provide the compressed gas to the inflatable cuff via a gas pathway.

For purposes of summarizing the disclosure, certain aspects, advantages and novel features of the inventions have been described herein. It is to be understood that not necessarily all such advantages can be achieved in accordance with any particular embodiment of the inventions disclosed herein. Thus, the inventions disclosed herein can be embodied or carried out in a manner that achieves or optimizes one advantage or group of advantages as taught herein without necessarily achieving other advantages as can be taught or suggested herein.

BRIEF DESCRIPTION OF THE DRAWINGS

Throughout the drawings, reference numbers can be re-used to indicate correspondence between referenced elements. The drawings are provided to illustrate embodiments of the inventions described herein and not to limit the scope thereof.

FIG. 1 illustrates an embodiment of a parameter calculation system that can calculate blood pressure, among other parameters;

FIG. 2 illustrates a plot of example plethysmograph and motion waveforms.

FIG. 3 illustrates an embodiment of a spot-check blood pressure measurement process.

FIG. 4 illustrates an embodiment of a continuous blood pressure measurement process.

FIG. 5 illustrates an embodiment of a system for calculating blood pressure.

FIG. 6 illustrates an embodiment of a motion estimator.

FIG. 7 illustrates a more detailed embodiment of the motion estimator of FIG. 6.

FIGS. 8A and 8B illustrate plots of example blood pressure and motion waveforms being correlated in time.

FIG. 9 illustrates an embodiment of a normalizer.

FIGS. 10 and 11 illustrate embodiments of algorithms for calculating normalized motion ratios.

FIGS. 12 and 13 illustrate example blood pressure calibration curves.

FIG. 14 illustrates an embodiment of a blood pressure calibrator.

FIG. 15 illustrates an embodiment of a system for triggering an occlusive blood pressure measurement.

FIG. 16 illustrates an embodiment of an optical sensor system.

FIGS. 17-19 illustrate example embodiments of blood pressure measurement devices.

FIG. 20 is a block diagram illustrating an embodiment of a blood pressure monitoring system.

FIG. 21 is a system diagram illustrating an embodiment of the blood pressure monitoring system of FIG. 20.

FIG. 22A-22C are plot diagrams illustrating embodiments of pressure variations of an inflatable cuff associated with a wearer during blood pressure measurement.

FIGS. 23A and 23B are flow diagrams illustrating embodiments of a process implemented by a patient monitor for measuring the blood pressure of a wearer.

FIG. 24 is a flow diagram illustrating another embodiment of a process implemented by the patient monitor for measuring blood pressure of a wearer.

FIG. 25 is a flow diagram illustrating yet another embodiment of a process implemented by the patient monitor for measuring blood pressure of a wearer.

DETAILED DESCRIPTION

I. Introduction

Noninvasive optical sensors can use spectrophotometry techniques to measure a variety of blood constituents, including for example, glucose, oxygen saturation, hemoglobin, methemoglobin, carboxyhemoglobin, other hemoglobin species, concentrations of the same, and the like. In addition, noninvasive optical sensors can also be used to measure a variety of other physiological parameters, including pulse rate, perfusion, and the like. An optical sensor can include one or more emitters that shine light through tissue of a living person, such as through a finger, toe, or foot. One or more detectors can receive the transmitted light after attenuation by the tissue and can generate one or more signals responsive to the attenuated light. A processor can process the one or more signals to derive measurements of one or more physiological parameters.

This disclosure describes, among other features, a blood pressure measurement system that non-invasively determines an individual's blood pressure. The blood pressure measurement system can include a noninvasive blood pressure sensor having an optical sensor and a motion sensor. The optical sensor can provide a photoplethysmograph signal obtained from a patient to a processor. The motion sensor can provide a motion signal to the processor responsive to motion of the patient. In one embodiment, the processor calculates or estimates the blood pressure of the patient based on the photoplethysmograph signal and the motion signal. Advantageously, the system can obtain this blood pressure measurement without an occlusive cuff, thereby reducing patient discomfort. In other embodiments, the processor calculates a blood pressure-related parameter from the photoplethysmograph and motion signal. The processor can occasionally trigger an occlusive cuff measurement as this parameter changes, thereby reducing the frequency of occlusive cuff measurements.

Further, this disclosure describes a blood pressure monitoring system that can include a gas reservoir filled with sufficient quantities of compressed gas to inflate an inflatable cuff. The gas reservoir can provide several advantages to the blood pressuring monitoring system, including portability, reusability, disposability, reduction in auditory noise and electrical noise, and/or the ability to measure blood pressure during inflation of the blood pressure cuff.

II. Example Parameter Calculation System

FIG. 1 illustrates an embodiment of a parameter calculation system 100 that can calculate blood pressure, among

other parameters. Advantageously, in certain embodiments, the parameter calculation system 100 noninvasively measures blood pressure of a patient using optical and motion signals. In addition to blood pressure, the parameter calculation system 100 can measure other physiological parameters in some implementations. Some examples of other parameters that may be measured include pulse rate, oxygen saturation (SpO₂), hemoglobin, total hemoglobin, hemoglobin species (e.g., methemoglobin, carboxyhemoglobin, or the like), carbon monoxide or dioxide, perfusion, glucose, and the like.

The parameter calculation system 100 shown includes a noninvasive blood pressure sensor 102. The blood pressure sensor 102 includes an optical sensor 104 and a motion sensor 106. The optical sensor 104 can include one or more emitters configured to irradiate light on a patient's tissue. The optical sensor 104 may further include one or more detectors that detect the light transmitted through the tissue. The optical sensor 104 can generate a photoplethysmograph responsive to this detected light. The photoplethysmograph (often referred to herein as a "plethysmograph" or "pleth") can be a waveform that represents changes in blood volume as measured by the light irradiated at the patient's tissue site. The pleth is caused at least partly by arterial pulsation, and as such, is related to arterial blood pressure. Thus, as will be described in detail herein, the pleth may be used to derive blood pressure measurements noninvasively.

Multiple emitters are included in some embodiments of the optical sensor 104 and may emit light at different wavelengths, as is described in greater detail below with respect to FIG. 16. In addition to being used to derive a pleth, the optical sensor 104 can be used to obtain other physiological parameters, such as any of the blood constituents described above. The optical sensor 104 may be a transmittance sensor or a reflectance sensor.

The motion sensor 106 can be an accelerometer, gyroscope, gradiometer, or any other motion sensing device. The motion detected by the motion sensor 106 can be velocity, position (e.g., displacement), acceleration, or any combination of the above. The motion may be provided as magnitude and/or direction values. For example, acceleration values may be represented with magnitude and direction. The motion sensor 106 can detect a patient's motion in one axis or in multiple axes. A three-axis accelerometer, for instance, may output acceleration magnitudes in x, y, and z coordinates (e.g., relative to a position of the accelerometer).

The noninvasive blood pressure sensor 102 may be placed on a measurement site of a patient, such as a patient's finger, ear, foot, or anywhere where pulsating blood can be detected. Mechanical acceleration or other motion of the measurement site can cause deformation in the pleth. This deformation can be a function, at least in part, of arterial and/or venous blood pressure, as well as the intensity and/or direction of the mechanical acceleration of the measurement site. Advantageously, in certain embodiments, this deformation in the pleth may be measured and used to estimate arterial and/or venous blood pressure noninvasively.

To illustrate motion-induced deformation of the pleth, FIG. 2 depicts a plot 200 of an example pleth waveform 210 and an example motion waveform 220. The pleth waveform 210 may be produced by the optical sensor 104 described above, while the motion waveform 220 may be produced by the motion sensor 106. For ease of illustration, the motion waveform 220 is depicted from a single axis. The example motion pleth and motion waveforms 210, 220 shown are also simplified for illustrative purposes.

As a measurement site is placed into motion, the motion at the measurement site can deform the pleth **210**. Deformation of the pleth **210** may result in the pleth **210** having higher peaks in some places and lower peaks in others, or higher or lower troughs. An example deformed pleth waveform **230** is also shown (not drawn to scale). The deformed pleth **230** reflects changes to the pleth **210** due to the motion **220**. For a first time period **202**, the motion **220** is relatively constant and, in this example, in phase and the same direction as the pleth. The deformed pleth **230** is therefore constructively deformed to be relatively similar to but larger in magnitude than the original pleth **210**. For a second time period **204**, the motion **220** varies, resulting in some destructive deformation of the pleth **210**.

The amount of deformation in the pleth due to the motion can depend on a patient's blood pressure. At higher blood pressures, the arteries or veins are under greater tension than at lower blood pressures. At lower blood pressures, the vessels become more compliant or elastic than at higher blood pressures. Thus, the lower the blood pressure, the greater can be the possible amount of deformation in the pleth due to motion. Conversely, the higher the blood pressure, the lower the possible amount of deformation in the pleth due to motion. As the acceleration increases, the amount of deformation increases. However, the amount of deformation may increase at a slower rate at higher blood pressures than at lower blood pressures.

Thus, the component of the pleth due to motion can be indicative of blood pressure. Deriving this component of the pleth due to motion can allow a processor to calculate blood pressure. Algorithms for deriving this motion component are described in detail below. This component may also be monitored directly without calculating blood pressure, so as to determine whether changes in blood pressure have likely occurred. If changes have likely occurred, an occlusive cuff can be inflated to take a gold-standard blood pressure measurement. Such cuff-measurement embodiments are described in greater detail below with respect to FIG. **15**.

It should be noted that the pleth **210** includes peaks **212** and troughs **214**. The peaks **212** reflect systolic action of the heart, while the troughs **214** reflect diastolic action of the heart. Blood pressure measurements can be correlated in time with the peaks **212** and troughs **214** of the pleth so as to obtain systolic and diastolic blood pressure, respectively. For instance, a second optical sensor may be placed at a second measurement site that is not in motion, while a first optical sensor at a first measurement site is in motion. The motion component of the pleth derived from the first optical sensor can be correlated in time with the peaks and troughs of the second sensor's pleth, which may not be disturbed by motion. The systolic and diastolic pressures can therefore be obtained. In other embodiments, systolic and diastolic pressures are obtained with a single sensor. Alternatively, mean blood pressure is obtained instead of or in addition to systolic and diastolic pressures. For convenience, the remainder of this application will generically refer to obtaining blood pressure measurements without specifying whether the measurements are systolic, diastolic, or mean blood pressure. However, it should be understood that any of these or other types of blood pressure measurements may be obtained by the systems and algorithms described herein.

Referring again to FIG. **1**, also shown is a parameter calculator **110** in communication with the noninvasive blood pressure sensor **102**. The parameter calculator **110** can receive optical sensor data provided by the optical sensor **104** and the motion data provided by the motion sensor **106**. From this data, the parameter calculator **110** can derive the

motion component of a pleth and may use this motion component to calculate blood pressure and/or to trigger a blood pressure cuff.

The parameter calculator **110** can include hardware, such as one or more processors or other circuitry, software, and/or firmware for calculating a physiological parameter such as blood pressure. The parameter calculator **110** can output parameter data **113** indicative of calculated parameters, including blood pressure, for presentation to a user. The parameter data **113** can be displayed on a display device **120**. In another embodiment, the parameter calculator **110** provides parameter values as an output **112** to another device, for example, a device providing an audible response, or over a network to a remote device. For example, a remote device might be a computer located at a nurses' station or a clinician's handheld device.

The parameter calculator **110** can also calculate trend data reflecting trend information for the parameter data **113**. The parameter calculator **110** can also synthesize or scale waveform data. In addition to outputting the parameter data **113**, the parameter calculator **110** can output trend data **114**, synthesized, scaled, or actual waveforms **115**, calibration data **116**, and alarms **117**. The parameter calculator **110** can provide the outputs **113**, **114**, **115**, **116** to the display **120**, to a separate patient monitoring device, or to another device configured to receive physiological parameter information (e.g., to a clinician's device over a network).

In an embodiment, the parameter calculator **110** is implemented in a single monitoring device. In an embodiment, the features of the parameter calculator **110** are distributed among separate devices. In an embodiment, the parameter calculator **110** includes a processor, processor board, or an Original Equipment Manufacture (OEM) board. In an embodiment, the parameter calculator **110** is portable. Data communicated between the various components of the parameter calculation system **100** can be communicated through cables or wirelessly. Other inputs and/or outputs can be included with the system.

III. Example Blood Pressure Measurement Processes

FIGS. **3** and **4** illustrate embodiments of processes for obtaining blood pressure. In particular, FIG. **3** illustrates an embodiment of a spot-check blood pressure measurement process **300**, while FIG. **4** illustrates an embodiment of a continuous blood pressure measurement process **400**. The spot-check measurement process **300** may be used in a home healthcare setting, a doctor's office, or at a hospital to obtain a single instance of a blood pressure measurement at a time. The continuous measurement process **400** may also be used in these settings but for continuous (or periodic) monitoring of patient blood pressure over time. The processes **300**, **400** will be described in the context of the parameter calculation system **100**. However, these processes **300**, **400** can be implemented by any of the systems and algorithms described herein.

Referring specifically to FIG. **3**, the spot-check measurement process **300** begins at block **302**, where a clinician (such as nurse or doctor) places a noninvasive blood pressure sensor on a patient's measurement site. At block **304**, the parameter calculator **110** obtains a baseline pleth during a period of little or no motion from the optical sensor **104**. The clinician may, for instance, instruct the patient not to move for a brief period of time, such as a few seconds. During this time, the parameter calculator **110** can obtain the baseline pleth measurement.

At block 306, the clinician instructs the patient to move the measurement site. If the blood pressure sensor 102 is attached to the patient's finger, for example, the clinician might instruct the patient to gently shake or otherwise move his or her hand. In one embodiment, random motion of the measurement site may enable the signal processing algorithms described below to achieve accurate results in the fastest time. However, periodic motion (such as tapping a finger at a certain frequency) may also be processed to obtain accurate results in some embodiments.

The parameter calculator 110 obtains a pleth during the motion from the optical sensor 104 at block 308. This pleth, unlike the baseline pleth, may be deformed by the motion. As discussed above, the degree to which the pleth is deformed can be indicative of blood pressure. At the same or substantially the same time, the parameter calculator 110 obtains a motion signal from the motion sensor 106. For example, the parameter calculator 110 can obtain acceleration data from an accelerometer. The parameter calculator 110 can calculate one or more blood pressure measurements based on the pleth during motion, the motion signal, and the baseline pleth.

Although the motion component of the deformed pleth may be indicative of blood pressure, the parameter calculator 110 can use the baseline pleth and the motion signal to normalize the motion component with respect to acceleration and perfusion. Normalization can allow deformations in the pleth to be compared across different acceleration and perfusion conditions. Normalization is discussed in greater detail below (see, e.g., FIG. 9).

Referring specifically to FIG. 4, in the continuous measurement process 400, motion is obtained with a motion inducer coupled with the measurement site, rather than by instructing the patient to move the measurement site. The motion inducer may activate periodically or continuously, allowing periodic and/or continuous blood pressure measurements to be calculated.

At block 402, the parameter calculator 110 obtains a baseline pleth during no motion from the optical sensor 104 as described above. At block 404, a motion inducer coupled to the patient is activated, either automatically or with clinician or patient input. The motion inducer may be a motor, vibrator, buzzer, or the like. The motion inducer may be coupled with the patient before the initial pleth is obtained. In some implementations, the motion inducer is part of the sensor 102.

At block 406, the parameter calculator 110 obtains a pleth during motion (caused by the motion inducer) from the optical sensor 104. At the same or substantially same time, the parameter calculator 110 obtains a motion signal from a motion sensor. As described above with respect to FIG. 3, the parameter calculator 110 calculates blood pressure based on the pleth during motion, the motion signal, and the baseline pleth at block 410.

At block 412, the parameter calculator 110 determines whether to recalibrate. Recalibration can include obtaining a new baseline pleth. As a patient's baseline pleth may change over time, recalibration can increase the accuracy of blood pressure measurements over time. Thus, if recalibration is desired, the parameter calculator 110 (or clinician or patient) deactivates the motion inducer at block 414, and the process 400 loops back to block 402. Otherwise, the parameter calculator 110 determines whether to continue monitoring at block 416. If so, the process loops back to block 406, where the parameter calculator 110 obtains the pleth during motion. If the parameter calculator 110 determines that monitoring is completed, the process 400 ends.

The process 400 may be adapted in certain embodiments to use the natural motion of a patient's body at the tissue site instead of (or in addition to) a motion inducer. Patients typically move periodically. If the pleth is being obtained continuously, periods where the patient moves could be used to obtain a motion-deformed pleth, which can be used to calculate blood pressure as described above. The parameter calculator 110 can, in some embodiments, determine whether the tissue site has reached a threshold amount of movement (based on the motion sensor signal), and in response, calculate a blood pressure measurement. This form of monitoring, although referred to as continuous, may also be considered periodic monitoring. The parameter calculator 110 can also analyze the motion sensor output to determine whether the patient is moving at all. If little or no motion is detected for an extended period, the parameter calculator 110 may output an alarm for clinicians to evaluate whether the patient is in need of medical assistance.

IV. More Detailed Example Blood Pressure Measurement Calculations

FIG. 5 illustrates an overview embodiment of a system 500 for calculating blood pressure. The system 500 may be implemented by the parameter calculation system 100 or by any other system described herein. Components of the system 500 may be implemented in software and/or hardware. These components include a signal conditioning block 510, a motion estimator 520, a normalizer 530, and a calibration curve block 540. More detailed aspects of the motion estimator 520, normalizer 530, and calibration curve block 540 are described in subsequent Figures.

The signal conditioning block 510 receives both pleth and motion signals. The signal conditioning block 510 can include electronic circuitry for front-end signal conditioning, which can include low-noise amplification, transimpedance amplification, analog-to-digital conversion, sampling, combinations of the same, and the like. The signal conditioning block 510 may be implemented in the parameter calculation system 100 or directly in the noninvasive blood pressure sensor 102. The output of the signal conditioning block 510 can include digital pleth and motion signals.

These signals are passed to the motion estimator 520, which can include functionality for estimating the portion of the pleth that is due to motion. Example algorithms for estimating this motion are described in detail below with respect to FIGS. 6 through 8B. The motion portion of the pleth is provided by the motion estimator 520 to the normalizer 530. As described briefly above, the normalizer 530 can use a baseline pleth and the motion signal to normalize the motion component in the pleth with respect to acceleration and perfusion. Normalization can allow deformations in the pleth to be compared across different acceleration and perfusion conditions.

Further, the normalizer 530 can normalize the motion component of a first pleth obtained from a first waveform with a motion component of a second pleth of a second waveform. More than two waveforms may also be used in the normalization process. The normalizer 530 outputs normalized motion components, ratios, or the like (see FIG. 9) to a calibration curve block 540. The calibration curve block 540 can implement a look-up table (LUT) or the like that provides blood pressure values corresponding to the outputs from the normalizer 530. The calibration curve or curves used by the block 540 can be determined experimentally and may vary based on characteristics of the patient. For example, different curves may be used for patients based on

their age (e.g., neonate versus child versus adult), gender, health status, condition, comorbidity, current or past medications, and the like.

FIG. 6 illustrates a more detailed embodiment of a motion estimator 620, which is an example implementation of the motion estimator 520. The motion estimator 620 is shown implemented as an adaptive filter in the depicted embodiment. The motion estimator 620 may be implemented by the parameter calculation system 100 or by any other system described herein.

The motion estimator 620 receives a pleth with motion signal (deformed pleth, P_m) and a motion signal (m). The motion signal is provided to a motion estimation filter 610. As shown, the motion estimation filter 610 is an adaptive filter. This adaptive filter may be a tapped delay line or the like and may be implemented as a finite impulse response (FIR) filter, an infinite impulse response (IIR) filter, or a combination of the same. One embodiment of the motion estimation filter 610 is described in detail below with respect to FIG. 7. The motion estimation filter 610 outputs an estimated motion portion of the pleth (P_m).

The motion portion of the pleth is combined with the pleth plus motion signal, for example, by subtracting the motion portion of the pleth from the pleth plus motion signal. This combination produces an estimated pleth signal with the motion removed, sometimes referred to herein as the clean pleth signal. This clean pleth signal is provided to an adaptive algorithm 630, which uses this signal (or other signals) to adjust weights or coefficients of the adaptive filter 610.

Any of a variety of adaptive algorithms 630 may be used. For instance, the adaptive algorithm 630 could implement one or more of the following: a Wiener filter, gradient search methods, ellipsoid search methods, a least mean squares algorithm (LMS), a least squares algorithm (such as a pseudoinverse), a recursive least squares (RLS) algorithm, a Kalman filter, a joint process estimator, an adaptive joint process estimator, a least-squares lattice joint process estimator, a least-squares lattice predictor, a correlation canceller, a linear predictor, linear programming, an estimator or algorithm using an L_1 , L_2 , or L_∞ norm, optimized or frequency domain implementations of any of the above, combinations of the same, and the like.

As shown, the motion estimator 520 acts like an adaptive noise canceller or adaptive noise filter, removing the noise, or the motion portion of the pleth to produce the clean pleth signal P_{est} . However, this motion noise was intentionally introduced by the patient or a motion inducer (see FIGS. 3 and 4). Unlike a typical adaptive noise filter, in some embodiments we are interested in obtaining the noise instead of the clean pleth signal. Counterintuitively, the noise, or the motion portion of the pleth, is therefore the signal of interest output by the motion estimator 620.

FIG. 7 illustrates a more detailed embodiment of the motion estimator 620 of FIG. 6, namely a motion estimator 720. The motion estimator 720 includes an FIR adaptive filter 710 (corresponding to the filter 610) that takes as inputs the motion signal (m) of FIG. 6. These inputs are represented by the Cartesian coordinates x , y , z in the depicted embodiment, although other coordinate systems or fewer or more coordinates can be used. Each coordinate represents a component of motion output by the motion sensor 106 of FIG. 1, such as acceleration magnitude.

The adaptive filter 710 is a vector FIR filter in the depicted embodiment, composed of three one-dimensional FIR filters 712a, 712b, 712c that combine together in some embodiments to form a single output per sample. Each one-

dimensional FIR filter 712 includes delay blocks 714 and coefficients or taps 716. The number of delay blocks 714 and taps 716 shown are merely illustrative examples, and other numbers of delay blocks 714 and taps 716 may be used in some implementations. The outputs of the taps 716 are combined by a combiner 718. A combiner 718a, 718b, 718c is shown for each one-dimensional FIR filter 712. The outputs of each of the combiners 718 are combined by another combiner 721 to produce an output of the adaptive filter 710.

Each one-dimensional FIR filter 712 can be implemented as a tapped-delay line. The values of the taps 716 in each tapped-delay line may be adjusted to change the phase of the respective motion signal component (x , y , or z). This adjustment in phase can cause the motion signal to be correlated in time with the pleth plus motion signal, so that these two signals can be compared at the same instants in time. Without this phase adjustment, the motion and pleth signals may be out of phase due to dynamic effects, lack of perfect time synchronization between sensors, and the like. This correlation in time is illustrated graphically in FIGS. 8A and 8B, where a pleth signal 810 and motion signal 820 as acquired by the sensor 102 are first out-of-phase in a plot 800A of FIG. 8A, and then subsequently correlated or in-phase in a plot 800B of FIG. 8B.

To illustrate the tapped-delay concept, if the tap w_1 in FIG. 7 is given a weight of 1, and the remaining taps w_i are given a weight of 0, the x coordinate samples will be delayed one sample. If instead the tap w_2 were given a value of 1 and the other taps 0, the x coordinate samples would be delayed by two samples, and so on. The phase of the motion signal may therefore be delayed or phase-shifted to correlate in time with the pleth plus motion signal. The values of the taps 716 may be selected so as to provide a smooth delay, and may or may not actually be 0 or 1. An adaptive algorithm 730 (corresponding to the adaptive algorithm 630 of FIG. 6) can adjust the taps 716 programmatically and continuously to track the motion signal with the pleth. As a result, the output of the combiner 721 can be subtracted from or otherwise combined with the pleth plus motion signal to produce the estimated pleth signal, which is an error signal supplied to the adaptive algorithm 730. The output of the combiner 721 is the motion portion of the pleth, which can be the signal of interest in determining blood pressure.

As described above with respect to FIG. 6, the adaptive algorithm 730 may be implemented in a variety of ways. For example, the adaptive algorithm 730 can use a least squares algorithm based on a block of samples, such as the following:

$$\begin{matrix} x_n & \dots & x_{n-i} & & y_n & \dots & y_{n-i} & & z_n & \dots & z_{n-i} \\ x_{n+1} & \dots & x_{n-i+1} & & y_{n+1} & \dots & y_{n-i+1} & & z_{n+1} & \dots & z_{n-i+1} \\ \vdots & & & & \vdots & & & & \vdots & & \end{matrix} \vec{w} = \vec{P}_m \quad (1)$$

A

where the matrix A includes motion samples x , y , z , where n represents the n th sample, i represents the number of delay blocks 714 (or taps 716), w represents a vector of the weights or taps 716 (and which may include the w_i , u_i , and v_i taps 716 in FIG. 7), and P_m represents a vector of pleth motion component values. Each row in the matrix A represents $3(n+i)$ samples. For example, if the number of delay blocks 714 is 4, there are 5 “ x ” samples, 5 “ y ” samples, and 5 “ z ” samples per row, for a total of 15 samples per row. The samples in the next row are shifted over by one sample in

this example. The matrix can include any number of rows and samples. However, since a larger number of rows than columns can result in a singular matrix “A” that is not invertible, solving for the weights in equation 1 can be performed using a least-squares estimation technique. The least-squares estimation technique can employ the pseudo-inverse as follows:

$$\vec{w}=(A^T A)^{-1} A^T \vec{P}_m \quad (2)$$

where the matrix $(A^T A)^{-1} A^T$ is the Moore-Penrose pseudo-inverse.

The sample values in the motion portion of the pleth (P_m) could be input into the calibration curve lookup table (540) to derive blood pressure values. However, different magnitudes of acceleration or motion could result in different magnitudes of the motion portion of the pleth, even though the blood pressure stays constant. Similarly, different levels of perfusion can result in different magnitudes of the motion component of the pleth, even when the blood pressure stays the same. Moreover, pleth signals obtained from different wavelengths can have different magnitudes than each other and may be affected differently by motion. Thus, instead of directly looking up the motion portion of the pleth in a calibration curve LUT, in some embodiments, the motion portion of the pleth may first be normalized to account for motion, perfusion, and/or wavelength differences.

FIG. 9 illustrates an embodiment of a normalizer 930 that can be used to normalize the motion component of the pleth. The normalizer 930 includes a perfusion normalization component 910, a motion normalization component 920, and a wavelength normalization component 940. Any subset of the normalization components 910, 920, 940 may be used in any given implementation. For convenience, normalization for a single wavelength (“wavelength 1”) is shown in detail. The normalization techniques applied to this wavelength may also be extended to any number of wavelengths (N wavelengths). However, in some embodiments, a single wavelength is used instead of multiple wavelengths, so that wavelength normalization is not employed. The normalizer 930 may be implemented by the parameter calculation system 100 or by any other of the systems described herein.

Inputs to the normalizer 930 include a baseline pleth, motion portion of the pleth, and motion signal for each wavelength. The perfusion normalization component 910 receives the baseline pleth and the motion portion of the pleth. The perfusion normalization component 910 normalizes the motion component of the pleth based on the baseline pleth, to thereby reduce or cancel out the effects of perfusion on the magnitude of the motion component of the pleth. One way to normalize for perfusion is to obtain a first statistical measure of a component of baseline pleth samples and a second statistical measure of a component of motion portion of the pleth samples. A ratio can then be constructed of the two statistical measures, for example, by dividing the second statistical measure by the first statistical measure. One example statistical measure that may be used, among many others, is the root-mean square (RMS). Equation 3 illustrates one possible perfusion normalization:

$$M_{norm} = \frac{\text{RMS}(P_m)}{\text{RMS}(P_{baseline})} \quad (3)$$

where M_{norm} represents a normalized motion ratio, P_m represents a series of pleth motion component values, and $P_{baseline}$ represents a series of baseline pleth values. In

equation 3, as the pleth gets bigger due to higher perfusion or smaller due to lower perfusion, the value of M_{norm} stays the same or about the same for the same value of P_m .

The output of the perfusion normalization component 910 is provided to the motion normalization component 920. As above, a statistical measure of the motion may be used to normalize based on motion. For example, the following equation may be constructed:

$$R_{m1} = \frac{M_{norm}}{\text{RMS}(x, y, z)} \quad (4)$$

where the x, y, z coordinates of an example motion signal m are used, and where R_{m1} represents a normalized motion ratio for wavelength 1. In another embodiment, perfusion normalization is not used. Thus, the normalized motion ratio may instead be:

$$R_{m1} = \frac{\text{RMS}(P_m)}{\text{RMS}(x, y, z)} \quad (5)$$

In either equation 4 or 5, as the motion increases or decreases, the value of R_{m1} stays the same or about the same for the same value of P_m .

The wavelength normalization component 940 may receive normalized motion ratios R_{m1} , for N waveforms. The wavelength normalization component 940 may take ratios of these ratios to produce an overall normalized motion ratio R_m . For example, if there are two wavelengths, the wavelength normalization component 940 can compute R_{m1}/R_{m2} to produce R_m . As with motion and perfusion, it is possible for the normalizer 930 to normalize only for wavelength. Thus, for example, the normalizer 930 can normalize P_{m1}/P_{m2} to produce R_m .

Referring again to FIG. 5, the normalizer 530/930 can provide the normalized motion ratio R_m to the calibration curve lookup table 540, which can lookup a corresponding blood pressure value for a given value of R_m . Although not shown, the R_m values or the blood pressure values (or P_m or other values described herein) may be smoothed or otherwise averaged to reduce variability in the blood pressure measurements.

Up to this point, the framework of FIG. 5 has operated under the assumption that samples in the motion portion of the pleth and blood pressure values share a linear relationship. This may not always be the case. Instead, some aspects of the motion/blood pressure relationship may be linear, while others may be nonlinear. More generally, the blood pressure can be some function of the motion portion of the pleth or of the motion signal itself. This function may itself be a combination of functions. Further, this function may differ for different patients based on their characteristics, conditions, and so forth. Thus, a refinement to the blood pressure calculation framework of FIG. 5 can be to incorporate one or more functions of the motion portion of the pleth or the motion signal itself into the blood pressure calculation.

Doing so may be accomplished in many ways. However, as an example illustration, FIGS. 10 and 11 depict embodiments of algorithms 1000, 1100 that use basis functions as a portion of the blood pressure computation. Referring to FIG. 10, a motion signal (x, y, z) is provided to one or more basis functions 1010 (multiple basis functions 1010 are

shown). The basis functions **1010** can be blending functions or the like. For example, the basis functions can be polynomial functions (such as x , x^2 , $(x_1+x_2)/2$, combinations thereof, and the like), transcendental functions (e.g., $\exp(x)$, $\ln(x)$), trigonometric functions, Fourier basis functions, wavelet basis functions, radial basis functions, combinations of the same, and the like. In the depicted embodiment, a basis function is applied to each coordinate motion input, or in some cases, fewer than all coordinate inputs. The outputs of the basis functions are provided to motion estimation filters **1020**. These motion estimation filters can implement the features of the motion estimation filters **520**, **620**, **720**, except with the basis function inputs instead of the motion signal inputs themselves.

Multiple sets of basis functions **1010** are used in some embodiments to provide several different types of outputs to the motion estimation filters. For any given patient or monitoring scenario, one set of basis functions may result in more accurate blood pressure measurements than another. Although not shown, the outputs of the basis functions may be weighted. These weights may be adapted based on an occlusive cuff measurement (see FIG. **14**). The outputs of the motion estimation filters are provided to a normalizer **1030**, which can implement the features of the normalizers **530**, **930** to produce a single normalized motion ratio. Alternatively, as shown in FIG. **11**, a normalizer **1130** can be provided as the output of each motion estimation filter so as to produce multiple normalized motion ratios. Each of these ratios can be used to calculate blood pressure values.

To save computational complexity and processing resources, the position of the basis functions **1010** and the motion estimation filters **1020** may be reversed. Thus, the motion signal may be instead provided to the motion estimation filters **1020**, and the outputs thereof may be provided to the basis functions **1010**. The basis functions **1010** may then output values to the normalizers **1030** or **1130**.

Each normalized motion ratio can be supplied to the calibration curve lookup table. Simplified examples of calibration curves **1200**, **1300** are illustrated in FIGS. **12** and **13**. In FIG. **12**, the calibration curve **1200** is linear, while in FIG. **13**, the calibration curve **1300** is nonlinear. The type of calibration curve used may depend on the patient or may vary from that shown. The example calibration curves **1200**, **1300** reflect that for increasing values of the normalized motion ratio, the blood pressure decreases and vice versa. More precise calibration curves than those shown can be obtained by comparing occlusive cuff measurements with normalized motion ratios output for several different patients. The particular calibration curve used can be adapted for individual patients.

For scenarios where multiple normalizers are used, such as in FIG. **11**, the calibration curve LUT can output a separate blood pressure value for each normalizer. Similarly, if multiple wavelengths of light are used to obtain multiple plethysmographs, multiple blood pressure estimates may be obtained. For example, wavelength normalization in FIG. **9** may be avoided, or pairs of wavelengths may be normalized together to form ratios that are supplied to the calibration curve LUT. Many different algorithms can be used to select from or combine the multiple blood pressure estimates to produce an overall blood pressure value.

One example of such an algorithm **1400** is illustrated in FIG. **14**. In this algorithm **1400**, candidate blood pressure estimates are provided to a selector **1410**. The selector includes a plurality of gain blocks **1412** that have adjustable weights. The candidate blood pressure estimates are also provided to a calibration module **1420**. This calibration

module **1420** also receives as an input a blood pressure measurement from a blood pressure cuff (BP_{CUFF}). Based on differences between the cuff-based measurement and the candidate measurements, the calibration module **1420** can adjust the weights. For instance, the calibration module **1420** can apply relatively greater weight to blood pressure values that are closer to the cuff measurement and relatively lower weights to values that are farther from the cuff measurement. A combiner block **1414** can combine the outputs of the gain blocks **1412** together to produce an overall blood pressure ($BP_{OVERALL}$).

In another embodiment, the selector **1410** applies a weight of 1 to the gain block **1412** corresponding to the closest blood pressure value to the cuff measurement, effectively selecting this measurement over the others, rather than combining the measurements together. In yet another embodiment, the weights **1412** are applied to the output of the basis functions, motion estimation filter, or normalizer of FIG. **10** or **11** in addition to or instead of the blood pressure values (BP_{est}).

V. Occlusive Cuff Triggering

FIG. **15** illustrates an embodiment of a system **1500** for triggering an occlusive blood pressure measurement. The system **1500** may be implemented by the parameter calculation system **100** or by any other system described herein.

The system **1500** includes several components from the system **500** of FIG. **5**, including the signal conditioning block **510**, the motion estimator **520**, and the normalizer **530**. However, instead of computing blood pressure values, the system **1500** enables a blood pressure cuff to be triggered. To that end, the output of the normalizer **530** is provided to a cuff trigger module **1540**. The cuff trigger module **1540** determines whether an output of the normalizer **530**, such as a normalized motion ratio, has changed significantly over a period of time. If the output has changed significantly, then the patient's blood pressure may also have changed significantly. The cuff trigger module **1540** can therefore send a triggering signal to a blood pressure cuff **1550** to take an occlusive cuff measurement. Taking occlusive cuff measurements in response to a significant change in a noninvasive measured parameter (such as a normalized motion ratio) can reduce the frequency that occlusive cuff measurements are taken, improving patient comfort.

The cuff trigger module **1540** can use a different parameter than that output by the normalizer **530** to determine whether to trigger the blood pressure cuff. In fact, the cuff trigger module **1540** can evaluate changes in any of the measured parameters described herein, such as the motion portion of the pleth (P_m), any of the normalized ratios, the outputs of a basis function, or combinations of the same, including averaged or smoothed versions of the same.

VI. More Detailed Example Patient Monitoring Systems

FIG. **16** illustrates an example of a data collection system **1600**. In certain embodiments, the data collection system **1600** noninvasively measures blood pressure, as described above. In addition, the data collection system **1600** can noninvasively measure a blood analyte, such as oxygen, carbon monoxide, methemoglobin, total hemoglobin, glucose, proteins, lipids, a percentage thereof (e.g., saturation) or one or more other physiologically relevant patient characteristics. The system **1600** can also measure

additional blood constituents or analytes and/or other physiological parameters useful in determining a state or trend of wellness of a patient.

The data collection system **1600** can be capable of measuring optical radiation from the measurement site. For example, in some embodiments, the data collection system **1600** can employ one or more photodiodes. In an embodiment, the photodiodes have an area from about 1 mm²-5 mm² (or higher) and are capable of detecting about 100 nanoamps (nA) or less of current resulting from measured light at full scale. In addition to having its ordinary meaning, the phrase “at full scale” can mean light saturation of a photodiode amplifier (not shown). Of course, other sizes and types of photodiodes can be used in various embodiments.

The data collection system **1600** can measure a range of approximately about 2 nA to about 100 nA or more full scale. The data collection system **1600** can also include sensor front-ends that are capable of processing and amplifying current from the detector(s) at signal-to-noise ratios (SNRs) of about 100 decibels (dB) or more, such as about 120 dB in order to measure various desired analytes. The data collection system **1600** can operate with a lower SNR if less accuracy is desired for an analyte like glucose.

The data collection system **1600** can measure analyte concentrations at least in part by detecting light attenuated by a measurement site **1602**. The measurement site **1602** can be any location on a patient’s body, such as a finger, foot, ear lobe, or the like. For convenience, this disclosure is described primarily in the context of a finger measurement site **1602**. However, the features of the embodiments disclosed herein can be used with other measurement sites **1602**.

In the depicted embodiment, the system **1600** includes an optional tissue thickness adjuster or tissue shaper **1605**, which can include one or more protrusions, bumps, lenses, or other suitable tissue-shaping mechanisms. In certain embodiments, the tissue shaper **1605** is a flat or substantially flat surface that can be positioned proximate the measurement site **1602** and that can apply sufficient pressure to cause the tissue of the measurement site **1602** to be flat or substantially flat. In other embodiments, the tissue shaper **1605** is a convex or substantially convex surface with respect to the measurement site **1602**. Many other configurations of the tissue shaper **1605** are possible. Advantageously, in certain embodiments, the tissue shaper **1605** reduces thickness of the measurement site **1602** while preventing or reducing occlusion at the measurement site **1602**. Reducing thickness of the site can advantageously reduce the amount of attenuation of the light because there is less tissue through which the light must travel. Shaping the tissue into a convex (or alternatively concave) surface can also provide more surface area from which light can be detected.

The embodiment of the data collection system **1600** shown also includes an optional noise shield **1603**. In an embodiment, the noise shield **1603** can be advantageously adapted to reduce electromagnetic noise while increasing the transmittance of light from the measurement site **1602** to one or more detectors **1606** (described below). For example, the noise shield **1603** can advantageously include one or more layers of conductive coated glass or a metal grid electrically communicating with one or more other shields of the sensor **1601** or electrically grounded. In an embodiment where the noise shield **1603** includes conductive coated glass, the coating can advantageously include indium tin oxide. In an embodiment, the indium tin oxide includes a surface resistivity ranging from approximately 30 ohms per square inch to about 500 ohms per square inch. In an embodiment, the

resistivity is approximately 30, 200, or 500 ohms per square inch. Other resistivities can also be used which are less than about 30 ohms or more than about 500 ohms. Other conductive materials that are transparent or substantially transparent to light can be used instead.

In some embodiments, the measurement site **1602** is located somewhere along a non-dominant arm or a non-dominant hand, e.g., a right-handed person’s left arm or left hand. In some patients, the non-dominant arm or hand can have less musculature and higher fat content, which can result in less water content in that tissue of the patient. Tissue having less water content can provide less interference with the particular wavelengths that are absorbed in a useful manner by blood analytes like glucose. Accordingly, in some embodiments, the data collection system **1600** can be used on a person’s non-dominant hand or arm.

The data collection system **1600** can include a sensor **1601** (or multiple sensors) that is coupled to a processing device or physiological monitor **1609**. In an embodiment, the sensor **1601** and the monitor **1609** are integrated together into a single unit. In another embodiment, the sensor **1601** and the monitor **1609** are separate from each other and communicate one with another in any suitable manner, such as via a wired or wireless connection. The sensor **1601** and monitor **1609** can be attachable and detachable from each other for the convenience of the user or caregiver, for ease of storage, sterility issues, or the like. The sensor **1601** and the monitor **1609** will now be further described.

In the depicted embodiment shown in FIG. **16**, the sensor **1601** includes an emitter **1604**, an optional tissue shaper **1605**, a set of detectors **1606**, and a front-end interface **1608**. The emitter **1604** can serve as the source of optical radiation transmitted towards measurement site **1602**. As will be described in further detail below, the emitter **1604** can include one or more sources of optical radiation, such as LEDs, laser diodes, incandescent bulbs with appropriate frequency-selective filters, combinations of the same, or the like. In an embodiment, the emitter **1604** includes sets of optical sources that are capable of emitting visible and near-infrared optical radiation.

In some embodiments, the emitter **1604** is used as a point optical source, and thus, the one or more optical sources of the emitter **1604** can be located within a close distance to each other, such as within about a 2 mm to about 4 mm. The emitters **1604** can be arranged in an array, such as is described in U.S. Publication No. 2006/0211924, filed Sep. 21, 2006, titled “Multiple Wavelength Sensor Emitters,” the disclosure of which is hereby incorporated by reference in its entirety. In particular, the emitters **1604** can be arranged at least in part as described in paragraphs [0061] through [0068] of the aforementioned publication, which paragraphs are hereby incorporated specifically by reference. Other relative spatial relationships can be used to arrange the emitters **1604**.

For analytes like glucose, currently available non-invasive techniques often attempt to employ light near the water absorbance minima at or about 1600 nm. Typically, these devices and methods employ a single wavelength or single band of wavelengths at or about 1600 nm. However, to date, these techniques have been unable to adequately consistently measure analytes like glucose based on spectroscopy.

In contrast, the emitter **1604** of the data collection system **1600** can emit, in certain embodiments, combinations of optical radiation in various bands of interest. For example, in some embodiments, for analytes like glucose, the emitter **1604** can emit optical radiation at three (3) or more wavelengths between about 1600 nm to about 1700 nm. In

particular, the emitter **1604** can emit optical radiation at or about 1610 nm, about 1640 nm, and about 1665 nm. In some circumstances, the use of three wavelengths within about 1600 nm to about 1700 nm enable sufficient SNRs of about 100 dB, which can result in a measurement accuracy of about 20 mg/dL or better for analytes like glucose.

In other embodiments, the emitter **1604** can use two (2) wavelengths within about 1600 nm to about 1700 nm to advantageously enable SNRs of about 85 dB, which can result in a measurement accuracy of about 25-30 mg/dL or better for analytes like glucose. Furthermore, in some embodiments, the emitter **1604** can emit light at wavelengths above about 1670 nm. Measurements at these wavelengths can be advantageously used to compensate or confirm the contribution of protein, water, and other non-hemoglobin species exhibited in measurements for analytes like glucose conducted between about 1600 nm and about 1700 nm. Of course, other wavelengths and combinations of wavelengths can be used to measure analytes and/or to distinguish other types of tissue, fluids, tissue properties, fluid properties, combinations of the same or the like.

For example, the emitter **1604** can emit optical radiation across other spectra for other analytes. In particular, the emitter **1604** can employ light wavelengths to measure various blood analytes or percentages (e.g., saturation) thereof. For example, in one embodiment, the emitter **1604** can emit optical radiation in the form of pulses at wavelengths of about 905 nm, about 1050 nm, about 1200 nm, about 1300 nm, about 1330 nm, about 1610 nm, about 1640 nm, and/or about 1665 nm. In another embodiment, the emitter **1604** can emit optical radiation ranging from about 860 nm to about 950 nm, about 950 nm to about 1100 nm, about 1100 nm to about 1270 nm, about 1250 nm to about 1350 nm, about 1300 nm to about 1360 nm, and/or about 1590 nm to about 1700 nm. Of course, the emitter **1604** can transmit any of a variety of wavelengths of visible or near-infrared optical radiation.

Due to the different responses of analytes to the different wavelengths, certain embodiments of the data collection system **1600** can advantageously use the measurements at these different wavelengths to improve the accuracy of measurements. For example, the measurements of water from visible and infrared light can be used to compensate for water absorbance that is exhibited in the near-infrared wavelengths.

As briefly described above, the emitter **1604** can include sets of light-emitting diodes (LEDs) as its optical source. The emitter **1604** can use one or more top-emitting LEDs. In particular, in some embodiments, the emitter **1604** can include top-emitting LEDs emitting light at about 850 nm to 1350 nm.

The emitter **1604** can also use super luminescent LEDs (SLEDs) or side-emitting LEDs. In some embodiments, the emitter **1604** can employ SLEDs or side-emitting LEDs to emit optical radiation at about 1600 nm to about 1800 nm. Emitter **1604** can use SLEDs or side-emitting LEDs to transmit near infrared optical radiation because these types of sources can transmit at high power or relatively high power, e.g., about 40 mW to about 100 mW. This higher power capability can be useful to compensate or overcome the greater attenuation of these wavelengths of light in tissue and water. For example, the higher power emission can effectively compensate and/or normalize the absorption signal for light in the mentioned wavelengths to be similar in amplitude and/or effect as other wavelengths that can be detected by one or more photodetectors after absorption. However, certain the embodiments do not necessarily

require the use of high power optical sources. For example, some embodiments may be configured to measure analytes, such as total hemoglobin (tHb), oxygen saturation (SpO₂), carboxyhemoglobin, methemoglobin, etc., without the use of high power optical sources like side emitting LEDs. Instead, such embodiments may employ other types of optical sources, such as top emitting LEDs. Alternatively, the emitter **1604** can use other types of sources of optical radiation, such as a laser diode, to emit near-infrared light into the measurement site **1602**.

In addition, in some embodiments, in order to assist in achieving a comparative balance of desired power output between the LEDs, some of the LEDs in the emitter **1604** can have a filter or covering that reduces and/or cleans the optical radiation from particular LEDs or groups of LEDs. For example, since some wavelengths of light can penetrate through tissue relatively well, LEDs, such as some or all of the top-emitting LEDs can use a filter or covering, such as a cap or painted dye. This can be useful in allowing the emitter **1604** to use LEDs with a higher output and/or to equalize intensity of LEDs.

The data collection system **1600** also includes a driver **1611** that drives the emitter **1604**. The driver **1611** can be a circuit or the like that is controlled by the monitor **1609**. For example, the driver **1611** can provide pulses of current to the emitter **1604**. In an embodiment, the driver **1611** drives the emitter **1604** in a progressive fashion, such as in an alternating manner. The driver **1611** can drive the emitter **1604** with a series of pulses of about 1 milliwatt (mW) for some wavelengths that can penetrate tissue relatively well and from about 40 mW to about 100 mW for other wavelengths that tend to be significantly absorbed in tissue. A wide variety of other driving powers and driving methodologies can be used in various embodiments.

The driver **1611** can be synchronized with other parts of the sensor **1601** and can minimize or reduce jitter in the timing of pulses of optical radiation emitted from the emitter **1604**. In some embodiments, the driver **1611** is capable of driving the emitter **1604** to emit optical radiation in a pattern that varies by less than about 10 parts-per-million.

The detectors **1606** capture and measure light from the measurement site **1602**. For example, the detectors **1606** can capture and measure light transmitted from the emitter **1604** that has been attenuated or reflected from the tissue in the measurement site **1602**. The detectors **1606** can output a detector signal **1607** responsive to the light captured or measured. The detectors **1606** can be implemented using one or more photodiodes, phototransistors, or the like.

In addition, the detectors **1606** can be arranged with a spatial configuration to provide a variation of path lengths among at least some of the detectors **1606**. That is, some of the detectors **1606** can have the substantially, or from the perspective of the processing algorithm, effectively, the same path length from the emitter **1604**. However, according to an embodiment, at least some of the detectors **1606** can have a different path length from the emitter **1604** relative to other of the detectors **1606**. Variations in path lengths can be helpful in allowing the use of a bulk signal stream from the detectors **1606**. In some embodiments, the detectors **1606** may employ a linear spacing, a logarithmic spacing, or a two or three dimensional matrix of spacing, or any other spacing scheme in order to provide an appropriate variation in path lengths.

The front end interface **1608** provides an interface that adapts the output of the detectors **1606**, which is responsive to desired physiological parameters. For example, the front end interface **1608** can adapt a signal **1607** received from

one or more of the detectors **1606** into a form that can be processed by the monitor **1609**, for example, by a signal processor **1610** in the monitor **1609**. The front end interface **1608** can have its components assembled in the sensor **1601**, in the monitor **1609**, in connecting cabling (if used), combinations of the same, or the like. The location of the front end interface **1608** can be chosen based on various factors including space desired for components, desired noise reductions or limits, desired heat reductions or limits, and the like.

The front end interface **1608** can be coupled to the detectors **1606** and to the signal processor **1610** using a bus, wire, electrical or optical cable, flex circuit, or some other form of signal connection. The front end interface **1608** can also be at least partially integrated with various components, such as the detectors **1606**. For example, the front end interface **1608** can include one or more integrated circuits that are on the same circuit board as the detectors **1606**. Other configurations can also be used.

The front end interface **1608** can be implemented using one or more amplifiers, such as transimpedance amplifiers, that are coupled to one or more analog to digital converters (ADCs) (which can be in the monitor **1609**), such as a sigma-delta ADC. A transimpedance-based front end interface **1608** can employ single-ended circuitry, differential circuitry, and/or a hybrid configuration. A transimpedance-based front end interface **1608** can be useful for its sampling rate capability and freedom in modulation/demodulation algorithms. For example, this type of front end interface **1608** can advantageously facilitate the sampling of the ADCs being synchronized with the pulses emitted from the emitter **1604**.

The ADC or ADCs can provide one or more outputs into multiple channels of digital information for processing by the signal processor **1610** of the monitor **1609**. Each channel can correspond to a signal output from a detector **1606**.

In some embodiments, a programmable gain amplifier (PGA) can be used in combination with a transimpedance-based front end interface **1608**. For example, the output of a transimpedance-based front end interface **1608** can be output to a PGA that is coupled with an ADC in the monitor **1609**. A PGA can be useful in order to provide another level of amplification and control of the stream of signals from the detectors **1606**. Alternatively, the PGA and ADC components can be integrated with the transimpedance-based front end interface **1608** in the sensor **1601**.

In another embodiment, the front end interface **1608** can be implemented using switched-capacitor circuits. A switched-capacitor-based front end interface **1608** can be useful for, in certain embodiments, its resistor-free design and analog averaging properties. In addition, a switched-capacitor-based front end interface **1608** can be useful because it can provide a digital signal to the signal processor **1610** in the monitor **1609**.

As shown in FIG. **16**, the monitor **1609** can include the signal processor **1610** and a user interface, such as a display **1612**. The monitor **1609** can also include optional outputs alone or in combination with the display **1612**, such as a storage device **1614** and a network interface **1616**. In an embodiment, the signal processor **1610** includes processing logic that determines measurements for desired analytes, such as glucose, based on the signals received from the detectors **1606**. The signal processor **1610** can be implemented using one or more microprocessors or subprocessors (e.g., cores), digital signal processors, application specific integrated circuits (ASICs), field programmable gate arrays (FPGAs), combinations of the same, and the like.

The signal processor **1610** can provide various signals that control the operation of the sensor **1601**. For example, the signal processor **1610** can provide an emitter control signal to the driver **1611**. This control signal can be useful in order to synchronize, minimize, or reduce jitter in the timing of pulses emitted from the emitter **1604**. Accordingly, this control signal can be useful in order to cause optical radiation pulses emitted from the emitter **1604** to follow a precise timing and consistent pattern. For example, when a transimpedance-based front end interface **1608** is used, the control signal from the signal processor **1610** can provide synchronization with the ADC in order to avoid aliasing, cross-talk, and the like. As also shown, an optional memory **1613** can be included in the front-end interface **1608** and/or in the signal processor **1610**. This memory **1613** can serve as a buffer or storage location for the front-end interface **1608** and/or the signal processor **1610**, among other uses. Further, a motion sensor **1615** is included, as described above, for providing a motion signal used for calculating blood pressure.

The user interface **1612** can provide an output, e.g., on a display, for presentation to a user of the data collection system **1600**. The user interface **1612** can be implemented as a touch-screen display, an LCD display, an organic LED display, or the like. In addition, the user interface **1612** can be manipulated to allow for measurement on the non-dominant side of patient. For example, the user interface **1612** can include a flip screen, a screen that can be moved from one side to another on the monitor **1609**, or can include an ability to reorient its display indicia responsive to user input or device orientation. In alternative embodiments, the data collection system **1600** can be provided without a user interface **1612** and can simply provide an output signal to a separate display or system.

A storage device **1614** and a network interface **1616** represent other optional output connections that can be included in the monitor **1609**. The storage device **1614** can include any computer-readable medium, such as a memory device, hard disk storage, EEPROM, flash drive, or the like. The various software and/or firmware applications can be stored in the storage device **1614**, which can be executed by the signal processor **1610** or another processor of the monitor **1609**. The network interface **1616** can be a serial bus port (RS-232/RS-485), a Universal Serial Bus (USB) port, an Ethernet port, a wireless interface (e.g., WiFi such as any 802.1x interface, including an internal wireless card), or other suitable communication device(s) that allows the monitor **1609** to communicate and share data with other devices. The monitor **1609** can also include various other components not shown, such as a microprocessor, graphics processor, or controller to output the user interface **1612**, to control data communications, to compute data trending, or to perform other operations.

Although not shown in the depicted embodiment, the data collection system **1600** can include various other components or can be configured in different ways. For example, the sensor **1601** can have both the emitter **1604** and detectors **1606** on the same side of the measurement site **1602** and use reflectance to measure analytes. The data collection system **1600** can also include a sensor that measures the power of light emitted from the emitter **1604**.

FIGS. **17** through **19** illustrate example embodiments of blood pressure measurement devices **1700**, **1800**, and **1900**. Referring to FIG. **17**, an example monitoring system **1700** is shown that can implement the parameter calculation system **100** or any of the other systems and algorithms described herein. The monitoring system **1700** includes a noninvasive

monitor **1710**, which is coupled to an individual **1702** via a sensor **1701**. The sensor **1701** can include a noninvasive optical sensor and a motion sensor in a single housing. In alternative embodiments, the optical and motion sensors are provided in separate housings.

The sensor **1701** can provide photoplethysmograph and motion data to the noninvasive monitor **1710**. The noninvasive monitor **1710** can calculate blood pressure (among other parameters) based at least in part on the photoplethysmograph and motion data. The noninvasive monitor **1710** can display blood pressure values, waveforms, alarms, and the like. The noninvasive monitor **1710** can measure blood pressure continuously and/or can be used for spot-check measurements.

Referring to FIG. **18**, another example monitoring system **1800** is shown that can implement the parameter calculation system **100** or any of the other systems and algorithms described herein. The monitoring system **1800** includes a monitor **1810** that obtains blood pressure measurements noninvasively from a sensor **201** coupled to an individual **202**. Additionally, the monitoring system **1800** includes an alternative blood pressure measurement device **1820**.

In the depicted embodiment, the alternative blood pressure measurement device **1820** is an oscillometric cuff **1820**. The oscillometric cuff **1820** can automatically inflate and occlude blood vessels using intelligent cuff inflation (ICI) techniques, thereby generating blood pressure signals that can be output to the monitor **1810**. In other embodiments, the alternative blood pressure measurement device used can be a manually-operated cuff and stethoscope. In some embodiments, the alternative blood pressure measurement device can be an invasive pressure transducer.

In many care settings, oscillometric cuffs are used as the gold standard for periodically obtaining blood pressure readings from patients. Because cuffs occlude blood vessels, however, too-frequent blood pressure readings can damage blood vessels and possibly cause nerve damage. On the other hand, if blood pressure readings are not taken frequently enough, significant changes in blood pressure can be missed, potentially resulting in harm to a patient. Thus, in certain embodiments, the monitor **1810** can obtain noninvasive blood pressure measurements using the sensor **201**. If the noninvasive blood pressure measurements deviate from a threshold, the monitor **1810** can trigger the occlusive cuff **1820** (or other alternative device) to obtain an occlusive (or other alternative) blood pressure measurement. As a result, occlusive, gold-standard measurements can be taken less frequently when noninvasive measurements are within a threshold range, potentially reducing damage to blood vessels.

FIG. **19** illustrates another example monitoring device **1900** in which the parameter calculation system **100** or any of the other systems and algorithms described herein can be implemented for measuring blood pressure and other physiological parameters. Advantageously, in certain embodiments, the example monitoring device **1900** shown can have a shape and size that allows a user to operate it with a single hand or attach it, for example, to a user's body or limb. The features of the monitoring device **1900** can also be included in the monitoring systems **1700**, **1800** described above.

In the depicted embodiment, the monitoring device **1900** includes a finger clip sensor **1901** connected to a monitor **1910** via a cable **1916**. In the embodiment shown, the monitor **1910** includes a display **1912**, control buttons **1914** and a power button. Moreover, the monitor **1910** can advantageously include electronic processing, signal processing, and data storage devices capable of receiving signal data

from the sensor **1901**, processing the signal data to determine one or more output measurement values indicative of one or more physiological parameters of a user, and displaying the measurement values, trends of the measurement values, combinations of measurement values, and the like.

The cable **1916** connecting the sensor **1901** and the monitor **1910** can be implemented using one or more wires, optical fiber, flex circuits, or the like. In some embodiments, the cable **1916** can employ twisted pairs of conductors in order to minimize or reduce cross-talk of data transmitted from the sensor **1901** to the monitor **1910**. Various lengths of the cable **1916** can be employed to allow for separation between the sensor **1901** and the monitor **1910**. The cable **1916** can be fitted with a connector (male or female) on either end of the cable **1916** so that the sensor **1901** and the monitor **1910** can be connected and disconnected from each other. Alternatively, the sensor **1901** and the monitor **1910** can be coupled together via a wireless communication link, such as an infrared link, a radio frequency channel, or any other wireless communication protocol and channel. The sensor **1901** could also be integrated with a monitor **1910** in other embodiments.

The monitor **1910** can be attached to the patient. For example, the monitor **1910** can include a belt clip or straps (not shown) that facilitate attachment to a patient's belt, arm, leg, or the like. The monitor **1910** can also include a fitting, slot, magnet, LEMO snap-click connector, or other connecting mechanism to allow the cable **1916** and sensor **1901** to be attached to the monitor **1910**.

The monitor **1909** can also include other components, such as a speaker, power button, removable storage or memory (e.g., a flash card slot), an AC power port, and one or more network interfaces, such as a universal serial bus interface or an Ethernet port. For example, the monitor **1910** can include a display **1912** that can indicate a measurement for blood pressure, for example, a measurement of the systolic and diastolic blood pressure in mmHg. Other physiological parameter values, waveforms, and the like can also be output on the display **1912**.

The sensor **1901** can measure various blood constituents or analytes noninvasively using multi-stream spectroscopy. In an embodiment, the multi-stream spectroscopy can employ visible, infrared and near infrared wavelengths. The sensor **1901** can include photocommunicative components, such as an emitter, a detector, and other components (not shown). The emitter can include a plurality of sets of optical sources that, in an embodiment, are arranged together as a point source. The various optical sources can emit a sequence of optical radiation pulses at different wavelengths towards a measurement site, such as a patient's finger. Detectors can then detect optical radiation from the measurement site. The optical sources and optical radiation detectors can operate at any appropriate wavelength, including, for example, infrared, near infrared, visible light, and ultraviolet. In addition, the optical sources and optical radiation detectors can operate at any appropriate wavelength, and modifications to the embodiments desirable to operate at any such wavelength can be used in certain embodiments.

The sensor **1901** can also include a motion sensor, such as an accelerometer, a gyroscope, or the like. The accelerometer can be a one-axis, two-axis, three-axis, or higher-axis accelerometer, such as a six-axis accelerometer. The sensor **1901** can also include multiple motion sensors, including different types of motion sensors.

The sensor **1901** or the monitor **1910** can also provide outputs to a storage device or network interface. In addition,

although a single sensor **1901** with a single monitor **1910** is shown, different combinations of sensors and device pairings can be implemented. For example, multiple sensors can be provided for a plurality of differing patient types or measurement sites.

VII. Blood Pressure Measurement System with Gas Reservoir

As described above, blood pressure (which can refer to diastolic pressure, systolic pressure, or some combination or mathematical representation of same), considered one of the principal vital signs, is one example of a physiological parameter that can be monitored. Blood pressure monitoring can be an important indicator of a wearer's cardiovascular status. Many devices allow blood pressure to be measured by manual or digital sphygmomanometer systems that utilize an inflatable cuff applied to a person's arm. These devices typically measure diastolic pressure and systolic pressure during deflation of the inflatable cuff.

For example, the inflatable cuff is inflated to a pressure level at or above the expected systolic pressure of the wearer and high enough to occlude an artery. Automated or motorized blood pressure monitoring systems use a motor or pump to inflate the inflatable cuff, while manual blood pressure monitors typically use an inflation bulb. As the air from the inflatable cuff slowly exits, the wearer's blood pressure can be determined by detecting Korotkoff sounds using a stethoscope or other detection means placed over the artery.

Alternatively, digital sphygmomanometers compute diastolic and systolic pressure as the inflatable cuff deflates based on the oscillations observed by a pressure sensor on the cuff. For example, some digital sphygmomanometers calculate the systolic blood pressure as the pressure at which the oscillations become detectable and the diastolic pressure as the pressure at which the oscillations are no longer detectable. Other digital sphygmomanometers calculate the mean arterial pressure first (the pressure on the cuff at which the oscillations have the maximum amplitude). The diastolic and systolic pressures are then calculated based on their fractional relationship with the mean arterial pressure. Other algorithms are used, such as identifying the change in slope of the amplitude of the pressure fluctuations to calculate the diastolic pressure.

As mentioned above, both methods of determining blood pressure include inflating the cuff to a pressure high enough to occlude an artery and then determining blood pressure during deflation of the inflatable cuff. Occluding the artery and then determining blood pressure during deflation can have a number of drawbacks. For example, inflating the inflatable cuff to a pressure higher than systolic pressure can cause pain and discomfort to the wearer. Other adverse effects can include limb edema, venous stasis, peripheral neuropathy, etc, or simply wearer interruption. In addition, as the artery is completely occluded prior to each measurement, sufficient time must elapse between measurements to ensure accurate results. Furthermore, manual systems make it difficult to measure blood pressure during inflation of the inflatable cuff due to the difficulty of inflating the inflatable cuff at an approximately constant rate using an inflation bulb.

Digital blood pressure monitors can have additional drawbacks. The motors used to pump gas into the cuff are often noisy and can disturb wearers at rest. In addition to auditory noise, in automated or motorized systems, the motors can cause electrical noise in sensor signals making the signal processing attempting to identify reference points for blood

pressure detection unreliable and difficult. Furthermore, portable motorized blood pressure monitors require a significant amount of power to produce the air pressure required to inflate the cuff. To provide the power levels required by the pump, a large battery is often used. The large battery makes the portable blood pressure monitor more cumbersome and less convenient. Furthermore, the large battery frequently needs to be recharged or replaced.

Advantageously, in certain embodiments, a blood pressure monitoring system can include a gas reservoir filled with sufficient quantities of compressed gas to inflate an inflatable cuff. The gas reservoir provides several advantages to the blood pressuring monitoring system, including portability, reusability, disposability, reduction in auditory noise and electrical noise, and the ability to measure blood pressure during inflation of the blood pressure cuff.

The addition of a gas reservoir to a blood pressure monitoring system makes it possible to inflate the inflatable cuff at an approximately constant rate with less auditory noise. By providing a quieter environment, the blood pressure monitoring system is capable of taking blood pressure measurements without disturbing the wearer. In addition, the use of the gas reservoir can significantly reduce the amount of electrical noise on the sensor signal. Furthermore, the addition of the gas reservoir allows the patient monitor to take blood pressure measurements during inflation of the inflatable cuff.

Measuring blood pressure during inflation can reduce the time required for blood pressure measurements and the amount of pressure used. Furthermore, measuring blood pressure during inflation can eliminate the need to occlude a wearer's artery.

In addition, the gas reservoir enables the manufacture of a smaller portable patient monitor. The gas reservoir can eliminate the need for a pump and/or motor in the portable patient monitor, thereby reducing its size. Furthermore, the gas in the gas reservoir can be used to generate electricity for the portable patient monitor, thereby eliminating the need for a battery and further reducing the size of the portable patient monitor.

FIG. 20 is a block diagram illustrating an embodiment of a blood pressure monitoring system **2100** for measuring blood pressure of a wearer, which may also be referred to as taking blood pressure measurements, using an inflatable cuff **2104**. The blood pressure monitoring system **2100** can be used to measure the blood pressure of a wearer during inflation, deflation or both. In an embodiment, the blood pressure monitoring system **2100** includes a gas reservoir **2102**, an inflatable cuff **2104** and a patient monitor **2106**.

The gas reservoir **2102** contains compressed gas and includes a regulator **2103** and is operatively connected to the inflatable cuff **2104** via a gas pathway, which allows gas to flow from the gas reservoir **2102** to the bladder of the inflatable cuff **2104**. In one embodiment, the gas pathway is an airtight pathway constructed of any number of materials including, but not limited to, metal, plastic, cloth, or some other airtight material.

The gas reservoir **2102** can be implemented using one or more disposable or reusable gas tanks, cylinders, bottles, canisters, or cartridges, of any number of shapes or sizes, and can be located in the same room as the wearer, or can be remotely located from the wearer, such as in a different room or even in a different building. For example, the gas reservoir **2102** can include a large gas tank that remains in a stationary location. The gas reservoir **2102** can be large enough to contain sufficient gas for a large number of blood pressure readings (e.g. more than 100). Furthermore, The

gas reservoir **2102** can store compressed gas at any number of PSI levels. For example, the gas reservoir can store compressed gas up to 6000 PSI or more, depending on the safety conditions of the environment. Furthermore, the gas tank can be configured to supply gas to multiple inflatable cuffs **2104**, thereby limiting the number of gas tanks used for multiple wearers. When the pressure levels in the gas tank reach a threshold, the gas tank can either be refilled, replaced or a combination of both. For example a rotating cache of gas tanks can be used as the gas reservoir **2102**.

Alternatively, the gas reservoir **2102** can be implemented using a small gas tank of any number of sizes. For example, the gas reservoir **2102** can be implemented using a gas tank that is small enough to fit in the palm of a hand, such as a carbon dioxide (CO₂) cartridge used for paint ball guns or tire inflation. CO₂ cartridges are available from a number of different manufacturers and distributors, such as the Air-Source 88 Gram Pre-filled Disposable CO₂ cartridge available from Crosman (Product Code: CRO-88-GRAM). The PSI levels for smaller gas tanks can also differ greatly and can store compressed gas up to 2000 PSI or more. In one embodiment, the gas reservoir **2102** is implemented using a gas tank containing compressed gas at 1000 PSI. The small gas reservoir **2102** can be used where mobility is important. For example, paramedics or first responders can carry a small gas reservoir **2102** for measuring blood pressure of persons needing emergency medical care. Using the gas reservoir **2102**, the emergency personnel (or some other user) can measure the blood pressure of the wearer during inflation of the inflatable cuff, deflation, or a combination of the two. The measurements can be taken using a patient monitor **2106** or manually using a stethoscope.

In one embodiment, a pressure regulator, or regulator **2103**, placed at an opening of the gas reservoir **2102** controls whether gas can exit the gas reservoir and the amount of gas allowed to exit. In one embodiment, the regulator is a valve. The regulator **2103** can also be configured to control the rate at which gas flows to the inflatable cuff **2104**, as well as the pressure of the gas or PSI. The regulator **2103** can include a second regulator near the opening of the gas reservoir **2102** or in the gas pathway to form a two-stage pressure regulator. Additional regulators can be added as desired. The regulator **2103** and/or valve can be implemented using any number of different valves, such as a globe valve, butterfly valve, poppet valve, needle valve, etc., or any other type of valve capable of operating as a variable restriction to the gas flow. Furthermore, the regulator **2103** can include a pressure gauge to identify the pressure levels of the gas exiting the gas reservoir **2102** and/or in the gas pathway.

Using the regulator **2103**, the inflatable cuff **2104** can be inflated at a controlled rate, such as, for example, an approximately constant rate. By inflating the inflatable cuff at a controlled rate, such as an approximately constant rate, the wearer's blood pressure can be measured during inflation and without occluding the artery. The regulator **2103** can further include a wireless transmitter for communication with the patient monitor **2106**. Alternatively, the regulator **2103** can communicate with the patient monitor via wired communication. Additionally, the gas reservoir **2102** can include a pressure gauge to monitor the remaining pressure and/or the amount of compressed gas remaining in the gas reservoir **2102**. The pressure gauge can communicate the pressure levels to the patient monitor **2106** via wired or wireless communication, similar to the regulator **2103**. Once the pressure gauge indicates a threshold pressure level or gas level has been reached, the patient monitor **2106** can indicate that the gas reservoir **2102** should be replaced or refilled.

The gas reservoir **2102** can contain any number of compressed gases to inflate the inflatable cuff **2104**. For example, the gas reservoir **2102** can contain compressed air, carbon dioxide, nitrogen, oxygen, helium, hydrogen, etc. Any number of other gases can be used to inflate the inflatable cuff **2104**. Furthermore, the gas reservoir **2102** can contain enough gas to inflate the inflatable cuff **2104** without the use of a motor or pump during the inflation. The gas reservoir **2102** can be pre-filled with gas near the wearer or at a remote site away from the wearer. In one embodiment, the gas reservoir **2102** is filled with gas prior to being associated with the inflatable cuff **2104**. Pre-filling the gas reservoir **2102** prior to use can significantly reduce the ambient noise caused during inflation of the inflatable cuff **2104**. In addition, by using the gas reservoir **2102**, the electrical noise from a motor can be removed. The reduction in ambient and electrical noise and the approximately constant rate of inflation of the inflatable cuff **2104** allows the patient monitor **2106** to measure the wearer's blood pressure while the inflatable cuff **2104** is inflating. In addition, the gas reservoir **2102** can be used to quickly inflate the inflatable cuff **2104** for blood pressure measurements taken during deflation of the inflatable cuff **2104**.

It is to be understood that other techniques exist for implementing the gas reservoir **2102** without departing from the spirit and scope of the description. For example, the gas reservoir **2102** can be implemented using the central gas line of a building, such as a hospital or other healthcare facility. Alternatively, the gas reservoir **2102** can be implemented using a bulb, bladder, pump, or the like.

The inflatable cuff **2104** includes a bladder and fills with gas in a manner controlled by the patient monitor **2106** or manually, and is used to at least partially obstruct the flow of blood through a wearer's artery in order to measure the wearer's blood pressure. The inflatable cuff **2104** can be attached to a wearer's arm or other location, and can be inflated electronically (e.g., via intelligent cuff inflation) or manually using an inflation bulb to obtain blood pressure data. Blood pressure data can include any type of signal received from a sensor used to identify blood pressure. Blood pressure data can be in the form of pressure sensor data, auditory sensor data, and the like. The inflatable cuff **2104** can further include a wireless transmitter for wireless communication with the patient monitor **2106**. Alternatively, the inflatable cuff can include cables for sending and receiving information to and from the patient monitor **2106**. The inflatable cuff can receive gas from a gas reservoir **2102** via a gas pathway. Furthermore, the inflatable cuff can include a release valve for releasing the gas stored in the inflatable cuff once inflated. The release valve can be actuated electronically by the patient monitor **2106** or manually by a user. In one embodiment, the release valve can be used when the pressure in the inflatable cuff **2104** reaches unsafe levels or when the inflatable cuff **2104** has been inflated beyond a threshold period of time.

A sensor **2108** can be placed in close proximity to the inflatable cuff **2104** to monitor the inflatable cuff **2104** during inflation and deflation. Alternatively, the sensor **2108** can be located in the patient monitor **2106** along a gas pathway between the gas reservoir **2102** and inflatable cuff **2104**, or at some other location where it is able to collect sufficient data for the patient monitor **2106** to determine the blood pressure of the wearer.

The sensor **2108** can be a pressure sensor or an auditory sensor. In one embodiment, the sensor **2108** communicates the pressure measurements of the inflatable cuff **2104** to the patient monitor **2106** via wired or wireless communication.

The pressure measurements can include blood pressure data of the wearer and can be used by the patient monitor to determine a blood pressure measurement of the wearer. The patient monitor **2106** can additionally use the pressure measurements to determine if the pressure in the inflatable cuff **2104** is above a threshold or is at an unsafe level. If the pressure in the inflatable cuff **2104** is above a threshold or is at an unsafe level, the patient monitor **2106** can actuate an emergency release valve to deflate the inflatable cuff **2104**. In an embodiment where the sensor **2108** is an auditory sensor, the sensor **2108** can be used to detect Korotkoff sounds. In one embodiment, the sensor **2108** is a stethoscope.

In an embodiment, the patient monitor **2106** includes a display device **2110**, a user interface **2112**, and a microprocessor or microcontroller or combination thereof **2114**. The patient monitor **2106** can further include a number of components implemented by the microprocessor **2114** for filtering the blood pressure data received from the sensor **2108** and determining the blood pressure of the wearer. The patient monitor **2106** can be a dedicated device for determining blood pressure, or can be part of a larger patient monitoring device capable of measuring additional physiological parameters as described in greater detail in U.S. application Ser. No. 10/153,263, entitled System and Method for Altering a Display Mode Based on a Gravity-Responsive Sensor, filed May 21, 2002, herein incorporated by reference in its entirety.

In some embodiments, the patient monitor **2106** is configured to communicate with the inflatable cuff **2104** and the gas reservoir **2102** via wired or wireless communication, such as LAN, WAN, WiFi, infra-red, Bluetooth, radio wave, cellular, or the like, using any number of communication protocols. The patient monitor **2106** can further be configured to determine blood pressure measurements of a wearer when the inflatable cuff **2104** is being inflated with gas from the gas reservoir **2102**, during deflation of the inflatable cuff **2104**, or a combination of both. The patient monitor **2106** can use the microprocessor **2114**, the filtering component, and blood pressure monitoring component to determine the blood pressure measurements. The blood pressure measurements determined by the patient monitor **2106** can be displayed on the display **2110**. In addition, the display **2110** can display blood pressure data and filtered blood pressure data in the form of plots of the pressure of the inflatable cuff and plots of the pressure oscillations in the inflatable cuff **2104** caused by blood flowing through an artery of the wearer. Furthermore, the display **2110** can display additional physiological parameters, such as heart rate, perfusion, oxygen saturation and the like.

The user interface **2112** can be used to allow a user to easily operate the patient monitor **2106** and obtain the blood pressure measurements. Furthermore, the user interface **2112** can allow a user to set or change any number of configuration parameters. For example, using the user interface **2112**, a user can determine what is displayed on the display **2110**, such as the blood pressure measurements during inflation and/or deflation, additional physiological parameters, and/or the pressure plots. Furthermore, the user interface **2112** can allow a user to set what measurements the patient monitor **2106** should take. For example, the user can set the configuration parameters to take blood pressure measurements only during inflation or deflation. Alternatively, the user can use the user interface **2112** to set the configuration parameters to take blood pressure measurements during inflation and deflation and then use both measurements to determine an appropriate blood pressure.

In addition, using the user interface **2122**, the user can determine how often the patient monitor **2106** takes blood pressure measurements. The user interface **2112** can further be used for any other type of configuration parameters that can be set or changed by a user.

FIG. **21** illustrates a blood pressure monitoring system **2200** similar to the blood pressure monitoring system **2100** of FIG. **20**. Similar to the blood pressure monitoring system **2100** of FIG. **20**, the blood pressure monitoring system **2200** of FIG. **21** includes a gas reservoir **2202**, an inflatable cuff **2204**, a patient monitor **2206**, and a sensor **2226**. In addition, the blood pressure monitoring system **2200** includes a gas pathway having a number of gas pathway segments **2210**, **2214**, **2218** and valves **2212**, **2216**, **2222** facilitating the movement of gas throughout the system. The gas reservoir **2202**, the inflatable cuff **2204**, the patient monitor **2206**, the valve **2216**, and the sensor **2226** can communicate using wired or wireless communication. Cables **2228** can be used to facilitate communication between the various components of the blood pressure monitoring system **2200**. The various components can all be connected directly to each other or can all connect to a central location, such as the patient monitor **2206**. Alternatively, the cables **2228** can be removed and the patient monitor **2202** can communicate with the other components of the blood pressure monitoring system via wireless communication.

As mentioned previously with reference to FIG. **20**, the gas reservoir **2202** can be implemented using one or more gas tanks of any number of different sizes. In addition, the gas reservoir **2202** can be located in the same room as the wearer or can be located at a remote location, such as in a different room or different building from the wearer. In such an embodiment, the gas pathway runs from the wearer to the remote location where the gas reservoir **2202** is located. In addition, the gas reservoir **2202** can be filled with any number of different gases prior to use with the wearer **2218**. In other words, the gas reservoir **2202** can be filled with gas prior to installation with the other components of the blood pressure monitoring system **2200**. In one embodiment, the gas reservoir **2202** is filled with a compressed gas.

Furthermore, the gas from the gas reservoir **2202** can be used to generate electricity for the blood pressure monitoring system **2200**. A small turbine can be located near the opening of the gas reservoir **2202**, along the gas pathway, or near an opening of the inflatable cuff **2204**. As the gas flows by the turbine and into the inflatable cuff **2202**, the turbine rotates. The rotation of the turbine can be used to generate electricity for the blood pressure monitoring system **2200**. The electricity can be fed to the patient monitor **2206** so that the patient monitor **2206** can measure the blood pressure of the wearer as the inflatable cuff inflates. Another turbine can be located near the release valve **2224** of the inflatable cuff **2204** or the gas pathway segment **2220**. When the release valve **2224** of the inflatable cuff **2204** is opened or the valve **2216** is actuated, the exiting gas causes the turbine to rotate, thereby generating electricity. The generated electricity can be fed to the patient monitor **2206**, allowing the patient monitor to measure the blood pressure of the wearer as the inflatable cuff **2204** deflates.

Using the gas reservoir **2202** to inflate the inflatable cuff **2204** can significantly reduce the ambient noise caused by the blood pressure monitoring system, resulting in a quieter environment for the wearer. In addition, the gas reservoir **2202** can supply gas at an approximately constant pressure and rate. Thus, the blood pressure monitoring system **2200** can inflate the inflatable cuff at an approximately constant rate without the auditory and electrical noise of a motor or

pump, resulting in a cleaner signal for the patient monitor **2206**. Furthermore, by using the gas reservoir **2202**, the patient monitor can measure the wearer's blood pressure during inflation of the inflatable cuff **2204**.

By measuring the blood pressure during inflation of the inflatable cuff, the blood pressure monitoring system **2200** can measure the blood pressure in less time and using less pressure. Furthermore, measuring blood pressure during inflation of the inflatable cuff can reduce, and in some embodiments completely remove, the amount of time that the artery is occluded, allowing for more frequent blood pressure readings.

The gas reservoir **2202** is operatively connected with the inflatable cuff **2204** via the regulator **2208**, gas pathway segments **2210**, **2214**, **2218** and valves **2212**, **2216**. The gas pathway and gas pathway segments **2210**, **2214**, **2218** can be made of any air-tight material, such as a plastic tube, metal, cloth, or the like. Gas from the gas reservoir **2202** flows through the gas pathway segments **2210**, **2214**, **2218** to inflate the inflatable cuff **2204**. In an embodiment, the regulator **2208**, the gas pathway segments **2210**, **2214**, **2218** and the valves **2212**, **2216**, **2222** control the direction and rate of gas flow throughout the blood pressure monitoring system **2200**. The regulator **2208**, which can also be a valve, located near the opening of the gas reservoir **2202**, controls the pressure of the gas exiting the gas reservoir **2202** and along the gas pathway segment **2210**. The valve **2212** controls the pressure of the gas exiting gas pathway segment **2210** and along gas pathway segments **2214**, **2218** to the inflatable cuff **2204**. The regulator **2208** and valve **2212** can be configured as a two-stage pressure regulator and used to maintain an approximately constant pressure of gas entering the inflatable cuff **2204**. The approximately constant pressure of gas leads to an approximately constant rate of inflation of the inflatable cuff **2204**. The regulator **2208** and valve **2212** can be configured to maintain any number of pressure levels in the gas pathway segments **2210**, **2214**, **2218**. In one embodiment, the regulator **2208** and valve **2212** are configured to maintain a pressure of approximately 6 PSI (pounds per square inch) along the gas pathway segment **2214** and gas pathway segment **2218**.

The valve **2216** located along the gas pathway segments **2210**, **2214**, **2218** can be used to control the direction of the gas flow throughout the blood pressure monitoring system **2200**. In an "on" configuration, the valve **2216** allows the gas to pass from the gas pathway segment **2214** to the gas pathway segment **2218** into the inflatable cuff **2204**. In an "off" configuration, the valve **2216** closes the gas pathway between the gas reservoir **2202** and the inflatable cuff **2204** and opens a gas pathway from the inflatable cuff **2204** and gas pathway segment **2218** to the gas pathway segment **2220** and through valve **2222**. The valve **2216** can be actuated electronically using the patient monitor **2206** or manually by a user. For safety, the default position for the valve **2216** can be the "off" configuration. In this way, should there be any malfunctions, the inflatable cuff **2204** can deflate. In an embodiment, the valve **2216** is a three-way valve. The valve **2216** can be implemented in a number of different ways without departing from the spirit and scope of the description.

The valve **2222** is similar in most respects to the valve **2212** and can control the rate at which gas is allowed to exit the inflatable cuff **2204**. The valves **2212**, **2222** can be implemented as any number of different valves, such as globe valve, butterfly valves, poppet valves, needle valves, proportional valves, etc., or any other type of valve capable of operating as a variable restriction to the gas flow. Fur-

thermore, the valves **2212**, **2222** can be actuated manually by a user or electronically by the patient monitor **2206**.

A number of alternative embodiments exist for implementing the blood pressure monitoring system **2200** without departing from the spirit and scope of the description. For example, the valve **2216** can be located in the inflatable cuff **2204** or nearby. In addition, the valves **2216**, **2222** can be removed completely. In this embodiment, the patient monitor **2206** can actuate the regulator **2208** and/or valve **2212** to inflate the inflatable cuff **2204**. When the inflatable cuff **2204** is to be deflated, the patient monitor **2206** can actuate the regulator **2208** and/or valve **2212** a second time, as well as actuate the release valve **2224**. Alternatively, two valves can be used in place of the valve **2216**. One valve can be used to allow gas to flow from the gas reservoir to the inflatable cuff. The second valve can be used to release gas from the inflatable cuff. The two valves can be actuated independently or at the same time. Furthermore, the two valves can be actuated electronically using the patient monitor **2206** or manually by a user.

In addition, the regulator **2208** and valve **2212** can be implemented using any number of different configurations. For example, regulator **2208** and valve **2212** can be implemented as two separate devices as shown or as one single device. Alternatively, the blood pressure monitoring system **2200** can be implemented using only the regulator **2208** and/or the valve **2212**. In addition, the regulator **2208** or any of the valves **2212**, **2216**, **2222** can further include a pressure gauge to identify the pressure levels of the gas. In addition, the regulator **2208** and each valve **2212**, **2216**, **2222** can communicate with the patient monitor **2206** via wired or wireless communication.

As mentioned previously, the inflatable cuff **2204** is used to at least partially obstruct an artery of a wearer to measure the wearer's blood pressure. In an embodiment, the inflatable cuff **2204** partially obstructs the wearer's artery without occluding, or completely closing, the artery to determine a blood pressure measurement of the wearer.

In one embodiment, the inflatable cuff **2204** includes a bladder, a release valve **2224** and an attachment mechanism. The bladder contains the gas received from the gas reservoir **2202**, via the gas pathway and can be made of any material capable of holding gas. For example, the bladder can be made of plastic, cloth, or some other airtight material. Furthermore, the bladder can be configured to hold gas at any number of PSI levels. In one embodiment, the bladder is capable of holding gas at 4 PSI. However, it is to be understood that the bladder can hold gas at greater than or less than 4 PSI. An opening in the bladder allows the gas from the gas reservoir to enter exit.

The attachment mechanism allows the inflatable cuff **2204** to be attached to a wearer. The attachment mechanism can be made of Velcro, cloth, a clip, or other material that allows the inflatable cuff **2204** to attach to a wearer. The release valve **2224** can be actuated manually by a user, electronically by the patient monitor **2206**, or automatically based on a predefined threshold pressure level. The release valve **2224** can be used to release the gas from the inflatable cuff **2204** when the pressure reaches a predetermined threshold or unsafe level, or when the inflatable cuff **2204** has been inflated above a threshold pressure for a predetermined amount of time.

The sensor **2226** can be located on the inside of the inflatable cuff **2204**, at the patient monitor **2206**, along the gas pathway segments **2210**, **2214**, **2218** or along a separate gas pathway segment, as illustrated in FIG. 21. Alternatively, the sensor **2226** can be located at the wearer's ear,

wrist, finger, or other location. When obtaining blood pressure data from the finger, wrist, or ear less pressure is needed to identify the blood pressure of a wearer, which increases the amount of blood pressure measurements that can be taken by the gas reservoir **2202**. As mentioned previously, the sensor **2226** can be used to collect blood pressure data from the wearer. In an embodiment, the sensor **2226** is a pressure sensor capable of measuring the pressure of the inflatable cuff **2204** as the inflatable cuff **2204** inflates and/or deflates. In another embodiment, the sensor **2226** is an auditory sensor used to identify Korotkoff sounds as the inflatable cuff **2204** inflates and/or deflates. The cables **2228** can be used to communicate the information from the sensor **2226** to the patient monitor **2206**. Alternatively, the sensor **2226** can use a wireless transmitter to communicate the blood pressure data to the patient monitor **2206**.

As mentioned previously, the patient monitor **2206** includes a display **2230** capable of displaying the diastolic and systolic pressure **2232** of the wearer as determined by the patient monitor **2206** during inflation and/or deflation. Furthermore, the patient monitor **2206** can display the blood pressure measured during inflation and deflation at the same time or simultaneously, thereby allowing the user to compare the values. The display **2230** of the patient monitor **2206** can further be configured to display pressure plots, which can include plots of the blood pressure data **2236A** and filtered blood pressure data **2236B**. The plots of the blood pressure data **2236A** can include the pressure of the inflatable cuff **2204** over time, and the plots of the filtered blood pressure data **2236B** can include the pressure oscillations observed by the sensor, as will be described in greater detail below with reference to FIGS. **22A-22C**. In addition, the patient monitor **2206** can be configured to display additional physiological parameters **2234** as further illustrated on the display device **2208**. These physiological parameters can include, but are not limited to, heart rate, oxygen saturation, perfusion, glucose measurements, and the like. In addition, the patient monitor **2206** can include configuration parameters to control the display **2230**, as well as the patient monitor **2206**. Using the configuration parameters, a user can initiate blood pressure measurements of the wearer **2218** to control the patient monitor **2206**.

The patient monitor can also include a user interface for setting or changing the configuration parameters. The configuration parameters can be used to set the frequency and type of blood pressure measurements taken as well as the manner in which to display the measurements. For example, the configuration parameters can determine how often a blood pressure measurement should be taken, whether it should be taken during inflation, deflation or both. Furthermore, the configuration parameters can determine how the patient monitor calculates the blood pressure measurements, such as using the inflationary blood pressure measurements, the deflationary blood pressure measurements, arbitrating between the two, or using a combination of the two. Furthermore, the configuration parameters can determine how the blood pressure measurements should be displayed. For example, the configuration parameters can dictate that only inflationary blood pressure measurements, deflationary blood pressure measurements, or a combination are to be displayed. Furthermore, the configuration parameters can determine if and how the pressure plots, and other physiological parameters are to be displayed.

In addition, the patient monitor **2206** can be configured to determine blood pressure measurements while the inflatable cuff **2204** is inflating and without occluding the wearer's artery. The patient monitor **2206** can be configured to actuate

a valve connected to the gas reservoir **2202**, causing gas to flow from the gas reservoir **2202** to the inflatable cuff **2204**. As the inflatable cuff **2204** inflates, the patient monitor **2206** can calculate the diastolic pressure and systolic pressure of the wearer **2218** using any number of techniques, as described in greater detail below with reference to FIGS. **23A** and **23B**. For example, the patient monitor **2206** can calculate the diastolic pressure and systolic pressure by measuring oscillations of blood flow in an artery or auditory cues as the inflatable cuff **2204** inflates. By measuring the wearer's blood pressure during inflation of the inflatable cuff, both the diastolic and systolic pressure can be determined by partially obstructing the wearer's artery and without occluding it. Once the systolic pressure is measured, the patient monitor can actuate the valve **2216** or a release valve **2224** on the inflatable cuff **2204** to release the gas within the inflatable cuff **2204**.

As mentioned previously, the display **2230** can be configured to display additional information regarding the wearer. FIGS. **22A-22C** are plot diagrams illustrating embodiments of various plots that can be displayed by the display **2230**. The plots in FIGS. **22A-22C** are plot diagrams illustrating some embodiments of the pressure at the inflatable cuff **2204**, including the oscillations of pressure, observed by the sensor **2226** during inflation and deflation.

Plot **2301A** is a plot diagram illustrating an embodiment of the pressure of the inflatable cuff **2204** during inflation and deflation, which can also be referred to as blood pressure data. The x-axis of plot **2301A** represents the number of samples taken by the patient monitor **2206** over time. The patient monitor **2206** can be configured to take samples at any number of increments to achieve a desired data resolution. For example, the patient monitor **2206** can sample the inflatable cuff every second, millisecond, microsecond, etc. Although illustrated in increments of samples, time can also be used for the x-axis **2302**. The y-axis **2304A** of plot **2301A** represents the pressure level, in mmHg, of the inflatable cuff **2204**. The line **2312** represents the pressure level of the inflatable cuff **2204** over time.

Prior to point **2308**, signals on the line **2312** represent electronic noise caused by the environment or blood pressure monitoring system **2200**. At point **2308**, the valve **2216** is actuated. The valve **2216** can be actuated electronically by the patient monitor **2206** or manually by a user. Once actuated, gas from the gas reservoir **2202** begins to inflate the inflatable cuff **2204** at a rate determined by a user electronically using the patient monitor **2206** or manually using the regulator **2208** and/or valve **2212**. In one embodiment, the inflation rate is an approximately constant rate, which leads to an approximately constant increase in pressure in the inflatable cuff. The sensor **2226** reads the rise in pressure in the inflatable cuff **2204**, as indicated by the rise in line **2312** of the plot **2301A**. Thus, from point **2308** to point **2310**, the inflatable cuff is in an inflation mode and is inflating.

At point **2310**, the valve **2216** is actuated again, ending the inflation of the inflatable cuff **2204**. Although illustrated at 200 mmHg, the point **2310** can be located at any desired pressure level. In one embodiment, the **2216** valve is actuated when the measured pressure level within the inflatable cuff **2204** is greater than the expected systolic pressure of the wearer. The expected systolic pressure of the wearer can be determined by previous blood pressure measurements, historical information, clinical data from one or more wearers, or the like. In one embodiment, the point **2310** changes between blood pressure measurements. For example, the inflatable cuff can be configured to inflate to 200 mmHg for

the first measurement. If it is determined during the first measurement that the wearer's systolic pressure is measurably less than 200, then during the proximate measurement, the inflatable cuff **2204** can be inflated to a lower pressure. Varying the pressure level to which the inflatable cuff **2204** inflates can conserve gas. Likewise, if the wearer's measured systolic pressure is greater than the expected systolic pressure, the inflatable cuff **2204** can be inflated to a greater pressure during the proximate measurement. Alternatively, the valve **2216** can be actuated once the inflatable cuff **2204** reaches any desired or predefined pressure level, such as 160 mmHg, 200 mmHg, 300 mmHg, etc.

In one embodiment, in addition to ending the inflation of the inflatable cuff, actuating the valve **2216** also begins a deflation mode of the inflatable cuff. For example, actuating the valve **2216** can close the gas pathway between the gas reservoir **2202** and the inflatable cuff **2204** and open the gas pathway between the inflatable cuff **2204** and ambient air, allowing the gas to exit the inflatable cuff **2204**. Once the valve **2216** is actuated, the inflatable cuff **2204** deflates leading to a decrease in pressure within the inflatable cuff **2204**. Actuating the valve **2216**, as well as the valve **2222** can be configured so that the pressure within the inflatable cuff **2204** decreases at any desired rate. In one embodiment, the pressure within the inflatable cuff **2204** decreases at an approximately constant rate. Additional blood pressure measurements can be taken during the deflation of the inflatable cuff **2204**, as described in greater detail below with reference to FIGS. **23A** and **23B**. The patient monitor **2206** can calculate the blood pressure of the wearer at any time during inflation and/or deflation, once it has received sufficient blood pressure data. For example, the patient monitor **2206** can calculate the diastolic pressure followed by the systolic pressure during inflation of the inflatable cuff **2204**. Alternatively, the patient monitor can calculate both diastolic and systolic pressure simultaneously once the valve **2216** is actuated or during inflation, once the patient monitor **2206** has sufficient blood pressure data. The patient monitor **2206** can alternatively wait until additional measurements are taken during the deflation of the inflatable cuff **2204** before calculating the diastolic and systolic pressure. In this way, the patient monitor can compare or arbitrate the diastolic and systolic measurements during inflation and deflation of the inflatable cuff **2204** to achieve greater reliability in the measurements.

With continued reference to FIG. **22A**, the plot **2301B** is a plot diagram illustrating an embodiment of the change in pressure in the inflatable cuff **2204** due to blood flow in the artery during inflation and deflation of the inflatable cuff **2204**. In one embodiment, the line **2314** is obtained by filtering the plot **2301A** and normalizing the data based on the change in pressure due to the inflation and deflation of the inflatable cuff **2204** and can be referred to as filtered blood pressure data. The plot **2301B** of the pressure oscillations due to the blood flow in the artery of the wearer, or filtered blood pressure data, can be displayed on the display **2230** along with the plot **2301A**, the blood pressure readings, and/or other physiological parameters. Similar to plot **2301A**, the x-axis **2302** of plot **2301B** represents the number of samples taken by the patient monitor **2206** over time. The y-axis **2304B** of plot **2301B** represents normalized changes in pressure in the inflatable cuff **2204**.

As illustrated in the plot **2301B**, when the valve **2216** is actuated at point **2308**, the inflatable cuff **2204** inflates and exerts pressure against the wearer's artery. As the inflatable cuff **2204** exerts pressure against the wearer's artery, the sensor **2226** is able to detect the variations in pressure in the

inflatable cuff **2204** due to blood flow within the artery, which are also referred to as pressure variations or pressure oscillations. The pressure oscillations are illustrated in plot **2301A** as small deviations or bumps in the line **2312**.

As further illustrated by the plot **2301B**, as the inflatable cuff **2204** continues to inflate, the artery becomes increasingly obstructed, leading to greater pressure variations observed by the pressure sensor, which leads to greater oscillations in the line **2314**. With continued inflation of the inflatable cuff, the variations in pressure eventually begin to decrease as the blood flow becomes occluded. At point **2310**, the pressure exerted by the inflatable cuff completely occludes the artery. As mentioned previously, in one embodiment, once the artery is occluded, the valve **2216** is actuated allowing the gas to exit the inflatable cuff **2204** and the inflatable cuff **2204** to deflate. In another embodiment, the valve **2216** is actuated prior to the occlusion of the artery.

As further illustrated by the plot **2301**, as the inflatable cuff **2204** begins to deflate, the oscillations of the pressure observed by the pressure sensor **2226** again begin to increase significantly as blood flow in the artery increases. As the inflatable cuff **2204** further deflates, the pressure exerted on the artery decreases leading to a decrease in pressure variation observed by the pressure sensor **2226**. Eventually, the inflatable cuff **2204** exerts little to no pressure on the artery, and the blood flow in the artery has little to no effect on the pressure in the inflatable cuff **2226**. The patient monitor **2206** uses the characteristics of the oscillations of pressure due to blood flow through an artery of the wearer, such as the slope of the oscillations and/or the magnitude or amplitude of the oscillations, to determine the blood pressure. The patient monitor **2206** can use the blood pressure data obtained during inflation and/or deflation of the inflatable cuff to determine the blood pressure.

In one embodiment, to determine the blood pressure during inflation, the patient monitor identifies the pressure in the inflatable cuff at which the largest magnitude oscillation, also referred to as the maximum deflection point or largest amplitude oscillation, during inflation is detected. The pressure in the inflatable cuff at which the largest magnitude oscillation during inflation is detected coincides with the systolic blood pressure of the wearer. In one embodiment, the patient monitor also identifies the pressure in the inflatable cuff at which the largest slope in the oscillations prior to the largest magnitude oscillation during inflation is detected. The largest slope in the oscillations prior to the largest magnitude oscillation during inflation coincides with the diastolic pressure of the wearer.

In addition, the patient monitor can determine the blood pressure of the wearer during deflation. In one embodiment, to determine the blood pressure during deflation, the patient monitor identifies the largest magnitude oscillation during deflation. The patient monitor further identifies the pressure in the inflatable cuff at which the largest slope in the oscillations prior to the largest magnitude oscillation during deflation is detected. The largest slope in the oscillations prior to the largest magnitude oscillation during deflation coincides with the systolic pressure of the wearer. The patient monitor also identifies the pressure in the inflatable cuff at which the largest slope in the oscillations after the largest magnitude oscillation during deflation is detected. The largest slope in the oscillations after the largest magnitude oscillation during deflation coincides with the diastolic pressure of the wearer.

A number of alternate methods exist for determining blood pressure during inflation and deflation of the inflatable cuff. For example, during deflation the patient monitor can

calculate the systolic blood pressure as the pressure at which the oscillations become detectable and the diastolic pressure as the pressure at which the oscillations are no longer detectable. Alternatively, the patient monitor can calculate the mean arterial pressure first (the pressure on the cuff at which the oscillations have the maximum amplitude). The patient monitor can then calculate the diastolic and systolic pressures based on their relationship with the mean arterial pressure. Additional methods can be used without departing from the spirit and scope of the description. For example, pressure values at locations other than the largest magnitude oscillation or maximum deflection point and largest slope can also be used.

Plots **2301A** and **2301B** further illustrate the potentially adverse effect signal noise can have on the blood pressure measurements. As illustrated, signal noise is detected at least twice in line **2314** prior to inflation. The detected signal noise in at least one instance exceeds the maximum deflection point during inflation. In addition, the signal noise may also contain the largest slope prior to the maximum deflection. In either event, if the signal noise is not accounted for, the patient monitor **2206** can erroneously detect the diastolic and systolic pressure of the wearer. In some embodiments, based on the amount and magnitude of signal noise detected, the patient monitor can assign confidence levels to the blood pressure measurements. Based on line **2314**, the patient monitor **2206** can place a lower confidence level in the blood pressure measurement during inflation due to the observed signal noise.

As mentioned above, the plots **2301A**, **2301B** can both be displayed on the display **2230** of the patient monitor **2206**. The plots **2301A**, **2301B** can be displayed simultaneously or consecutively. In addition the plots **2301A**, **2301B** can be displayed along with the diastolic pressure and systolic pressure as measured by the patient monitor **2206**. Furthermore, the measured diastolic pressure and systolic pressure during inflation can be displayed along with the measured diastolic pressure and systolic pressure during deflation. In addition, the patient monitor **2206** can further display additional physiological parameters measured by the patient monitor **2206**.

FIGS. **22B** and **22C** include plot diagrams illustrating additional embodiments of the pressure of the inflatable cuff **2204** during inflation and deflation. Plots **2303A** and **2305A** correspond to plot **2301A**, and plots **2303B** and **2305B** correspond to plot **2301B**. Similar to plots **2301A** and **2301B**, plots **2303A**, **2303B**, **2305A**, and **2305B** illustrate the inflation of the inflatable cuff **2204** beginning at point **2308** and ending at point **2310**. In addition the deflation of the inflatable cuff begins at point **2310** in plots **2303A**, **2303B**, **2305A**, and **2305B**.

Plots **2303A** and **2303B** further illustrate signal noise being exhibited at different points throughout the lines **2316** and **2318**. The first observed signal noise occurs near the beginning of the lines **2318** and another occurs near the end. Similar to the oscillations due to blood flow in the artery, signal noise is exhibited as small displacements on the line **2316** and oscillations in the line **2318**. As illustrated, unless accounted for, the signal noise occurring in plots **2303A** and **2303B** can have an adverse affect on blood pressure measurements due to their magnitude. The first detected signal noise results in the maximum deflection point prior to deflation and the last detected signal noise results in the maximum deflection point after deflation. In embodiments, where maximum deflection points are used, if inflation and deflation are not demarcated appropriately or if signal noise

is not accounted for, the patient monitor **2206** can erroneously determine the blood pressure measurements based on the signal noise.

The plot **2303B** further illustrates an example where a blood pressure measurement taken during inflation can in some instance have a higher confidence level than the blood pressure measurement taken during deflation. As mentioned previously, during inflation, the diastolic pressure can be determined as the pressure at which the largest slope in line **2318** prior to the maximum deflection point during inflation occurs. The systolic pressure can be calculated as the pressure at which the maximum deflection point of line **2318** occurs during inflation. Upon deflation, the systolic pressure is calculated as the pressure at which the largest slope in line **2318** prior to the maximum deflection point during deflation occurs. Similarly, the diastolic pressure is calculated as the pressure at which the largest slope in line **2318** after the maximum deflection point during deflation occurs. As illustrated in plot **2303B**, the maximum deflection point during deflation can be difficult to identify, which can make it difficult to calculate the diastolic and systolic pressure of the wearer accurately. Accordingly, the confidence placed in the blood pressure measurement during deflation can be relatively low compared to the confidence level placed in the blood pressure measurement during inflation. Accordingly, the patient monitor **2204** can determine that the blood pressure measurement taken during inflation is likely more accurate. In addition, depending on the amount and magnitude of the signal noise detected, the patient monitor **2206** can determine that neither blood pressure measurement reaches a threshold and that blood pressure measurements should be retaken.

Plots **2305A** and **2305B** illustrate yet another example of blood pressure measurements taken during inflation and deflation of the inflatable cuff **2204**. As illustrated, signal noise is detected near the beginning of lines **2320** and **2322**, resulting in oscillations observed in line **2322**. As mentioned previously, if not accounted for, the signal noise can adversely affect the blood pressure measurements during inflation. However, in the line **2322**, the maximum deflection point prior to deflation occurs during inflation. Thus, the signal noise at the beginning of the line **2322** should not affect the blood pressure measurements. Plots **2305A** and **2305B** further illustrate an example where the blood pressure measurement taken during inflation can have a similar confidence level as the confidence level of the blood pressure measurement taken during deflation. As illustrated, the line **2318** exhibits a distinctive maximum amplitude during inflation and during deflation.

FIG. **23A** is a flow diagram illustrating an embodiment of a process **2400A** for measuring blood pressure during inflation of an inflatable cuff **2204**. As illustrated in FIG. **23A**, the process **2400A** begins at block **2402** by actuating a valve, which allows gas to flow from a gas reservoir **2202** to the inflatable cuff **2204**, causing the inflatable cuff **2204** to inflate. The valve can be located near an opening of the gas reservoir **2202**, at some point along the gas pathway or at the inflatable cuff **2204**. In one embodiment, multiple valves **2212**, **2216** and/or regulators **2208** can be included between the gas reservoir **2202** and the inflatable cuff **2204**. Each valve and/or regulator can be actuated prior to inflating the inflatable cuff **2204**. The valve(s) can be actuated manually by a user or electronically by a patient monitor **2206**. For example, a user can manually open the valve **2216** to allow gas to flow from the gas reservoir **2202** to the inflatable cuff **2204**. The user can open the valve in a way that allows for the inflation of the inflatable cuff **2204** at an approximately

constant rate of inflation. A regulator **2208** can also be used to achieve the approximately constant rate of inflation. Alternatively, a patient monitor **2206** in communication with the gas reservoir can actuate the valve **2216**, allowing the gas to flow from the gas reservoir **2202** to the inflatable cuff **2206**. Communication from the patient monitor **2206** can occur by wired or wireless communication, such as a LAN, WAN, Wi-Fi, infra-red, Bluetooth, radio wave, cellular, or the like, using any number of communication protocols.

To actuate the valve, an input to the patient monitor **2206** such as a button can be used. Alternatively, the patient monitor can automatically actuate the valve once the patient monitor is turned on or based on one or more configuration parameters. For example, the patient monitor can be configured to determine the blood pressure of a wearer once every time period. The timer period can be configured as any period of time, such as 5 minutes, 15 minutes, 50 minutes, etc. In yet another embodiment, the patient monitor **2206** determines if the inflatable cuff is attached to a wearer. If the patient monitor **2206** determines that the inflatable cuff is attached to a wearer, the patient monitor **2206** can actuate the valve at predefined time intervals. Any number of methods can be used to determine if the inflatable cuff is attached to a wearer. For example, the patient monitor **2206** can determine whether the inflatable cuff is attached to a wearer using infra-red sensors, pressure sensors, capacitive touch, skin resistance, and the like.

Once the inflatable cuff **2204** is inflating, the patient monitor **2206** receives blood pressure data from the sensors, as illustrated in block **2404**. The blood pressure data can be obtained at the inflatable cuff **2204** using any number of different sensors or methods. For example, a pressure sensor can be used to identify the air pressure due to the inflation and deflation of the inflatable cuff **2204**. The pressure sensor can be located at the inflatable cuff, the patient monitor **2206**, at some point along the gas pathway, or some other location where it is capable of measuring the pressure of the inflatable cuff **2204**. Alternatively, an auditory sensor communicatively coupled to the patient monitor **2206** can be used to detect Korotkoff sounds, similar to the method used for manual determination of blood pressure using a stethoscope.

At block **2406**, the patient monitor **2206** filters the blood pressure data. Filtering the blood pressure data can reduce the effects of, or completely remove, environmental noise and/or the electrical noise found within the blood pressure monitoring system. Furthermore, during filtering, the patient monitor **2206** can normalize the blood pressure data to account for the changes in pressure due to the inflation and deflation of the inflatable cuff. In one embodiment, after filtering the blood pressure data, only the pressure oscillations in the inflatable cuff **2204** due to blood flow in an artery of the wearer remain, and in some instances signal noise. Upon filtering the blood pressure data, the patient monitor **2206** can determine the blood pressure of the wearer, as illustrated in block **2408**.

The patient monitor **2206** can determine the blood pressure using any number of different methods as described above with reference to FIGS. **22A-22C**. For example, the patient monitor **2206** can determine the blood pressure of the wearer using the slopes and/or amplitude of the pressure oscillations, the mean arterial pressure, and/or the Korotkoff sounds.

Once the patient monitor **2206** determines the blood pressure of the wearer, the patient monitor **2206** can actuate a valve to stop gases from flowing from the gas reservoir to the inflatable cuff, as illustrated in block **2410**. In one

embodiment, the valve is a three-way valve **2216** and actuating the valve to stop the gases from flowing from the gas reservoir to the inflatable cuff also opens the gas pathway segment **2220** to release the gas from the inflatable cuff.

Fewer, more, or different blocks can be added to the process **2400A** without departing from the spirit and scope of the description. For example, the patient monitor **2206** can filter the blood pressure data to determine the diastolic pressure first. As the diastolic pressure is being calculated, the patient monitor **2206** can continue receiving and filtering the blood pressure data to determine the systolic pressure. In an embodiment, the patient monitor can determine the blood pressure without filtering the blood pressure data. In addition, a user can determine the blood pressure measurements without the use of the patient monitor **2206**. In an embodiment, a user using a stethoscope can determine the diastolic and systolic pressure during inflation of the inflatable cuff without filtering the blood pressure data.

As mentioned previously, by measuring the blood pressure during inflation of the inflatable cuff **2204**, the blood pressure of the wearer can be measured in less time and using less pressure. Furthermore, because the artery is occluded for less time, or not occluded at all, the blood pressure can be measured more frequently.

FIG. **23B** illustrates a flow diagram of a process **2400B** for measuring blood pressure during deflation of an inflatable cuff. At block **2450**, the inflatable cuff **2204** is inflated. In one embodiment, the inflatable cuff **2204** is inflated using gas from a gas reservoir **2202**. Using the gas from the gas reservoir **2202**, the inflatable cuff **2204** can be inflated very quickly leading to a relatively short wait time before blood pressure measurements can be taken.

As the inflatable cuff **2204** inflates, the patient monitor determines whether a threshold pressure has been reached, as illustrated in block **2452**. The threshold pressure can be any pressure level and can vary between blood pressure measurements. Furthermore, the threshold pressure can be determined based on previous blood pressure measurements, historical information, clinical data from one or more wearers, or the like. In one embodiment, the threshold pressure is above an expected systolic pressure of the wearer. In another embodiment, the threshold pressure is above an expected occlusion pressure or the pressure at which the artery is occluded. The inflation can be initiated in a manner similar to that described above with reference to FIG. **23A**. If the patient monitor **2206** determines that the threshold pressure has not been reached, the inflatable cuff **2204** continues to inflate. However, if the patient monitor **2206** determines that the threshold pressure has been reached, the process moves to block **2454**.

At block **2454**, the patient monitor **2206** actuates the valve to initiate deflation of the inflatable cuff **2206**. In one embodiment, the valve is a three-way valve similar to valve **2216** of FIG. **21**, such that the inflation of the inflatable cuff **2204** ends at the same time deflation begins. Once the deflation of the inflatable cuff **2204** begins, the process moves to block **2456** and the patient monitor receives blood pressure data, filters the blood pressure data **2458**, and determines blood pressure **2460**. Greater detail regarding receiving blood pressure data **2456**, filtering the blood pressure data **2458** and determining blood pressure is described above with reference to blocks **2404-2408** of FIG. **23A**.

Fewer, more, or different blocks can be added to the process **2400B** without departing from the spirit and scope of the description. For example, the patient monitor **2206**

can determine the systolic pressure prior to receiving the blood pressure data or filtering the blood pressure data to determine the diastolic pressure. In addition, the process **2400B** can be implemented without the use of the patient monitor **2206**. For example, a user can receive blood pressure data via a stethoscope. The user can determine the blood pressure of the wearer using Korotkoff sounds, and can also determine the blood pressure of the wearer without filtering the blood pressure data. Furthermore, process **2400A** and **2400B** can be combined and measurements taken during inflation and deflation of the inflatable cuff. Furthermore, the measurements taken during deflation of the inflatable cuff can be used to verify the blood pressure readings taken during inflation of the inflatable cuff **2204**.

FIG. **24** is a flow diagram illustrating another embodiment of a process **2500** implemented by the patient monitor for measuring blood pressure of a wearer. FIG. **24** is similar in many respects to FIGS. **23A** and **23B**. For example, blocks **2502-2508** of FIG. **24** correspond to blocks **2402-2408** of FIG. **23A**, respectively. Furthermore, blocks **2514-2520** correspond to blocks **2454-2460** of FIG. **23B**, respectively.

As described above with reference to FIG. **23A** and illustrated in blocks **2502-2508**, the patient monitor **2206** actuates a valve to initiate inflation, receives blood pressure data during inflation, filters the blood pressure data, and determines the blood pressure of the wearer. Upon determining the blood pressure of the wearer, the patient monitor assigns a confidence level to the blood pressure measurements, as illustrated in block **2510**. The confidence level assigned can be determined in any number of ways. For example, based on the amount and magnitude of the noise observed in the blood pressure data, the patient monitor can assign the confidence level. Alternatively, if an anomaly in the blood pressure data is detected or if the blood pressure data deviates beyond a threshold level a lower confidence level can be assigned to the blood pressure measurements.

At determination block **2512**, the patient monitor **2206** determines if the confidence level assigned to the inflationary blood pressure measurements are above a threshold confidence level. The threshold confidence level can be determined based on previous blood pressure measurements, historical information, clinical data from one or more wearers, or the like. If the confidence level assigned to the blood pressure measurements during inflation exceeds the threshold confidence level, the patient monitor **2206** outputs the inflationary blood pressure measurements, as illustrated in block **2528**. The inflationary blood pressure measurements can be output to a display, a printer, another patient monitor, etc. Once output, the patient monitor **2206** can actuate a valve to deflate the inflatable cuff **2204** at a rate greater than would be used if the blood pressure measurements were taken during deflation. Alternatively, the patient monitor **2206** can deflate the inflatable cuff **2204** at the same rate as when blood pressure measurements taken during deflation.

If on the other hand, the confidence level assigned to the inflationary blood pressure measurements is less than the threshold confidence level, then the patient monitor can actuate the valve to initiate deflation of the inflatable cuff, as illustrated in block **2514**. As blocks **2514-2520** correspond to blocks **2454-2460** of FIG. **23B**, additional details with respect to blocks **2514-2520** are provided above with reference to FIG. **23B**.

Upon determining the blood pressure during deflation, the patient monitor **2206** can assign a confidence level to the deflationary blood pressure measurements, as illustrated in block **2522** and described in greater detail above with reference to block **2510**. Upon assigning the confidence

level to the deflationary blood pressure measurements, the patient monitor **2206** determines if the confidence level exceeds a threshold confidence, as illustrated in determination block **2524**, similar to the determination made in block **2512**. If the patient monitor **2206** determines that the confidence level assigned to the deflationary blood pressure measurements does not exceed the confidence threshold, the patient monitor **2206** can output an error, as illustrated in block **2526**. The error can indicate that neither the inflationary blood pressure measurements nor the deflationary blood pressure measurements exceeded the confidence threshold. In addition, the patient monitor **2206** can recommend that additional blood pressure measurements be taken.

If on the other hand, the patient monitor determines that the confidence level assigned to the deflationary blood pressure measurements exceeds the confidence threshold, the patient monitor outputs the deflationary blood pressure measurements, as shown in block **2528**.

Fewer, more, or different blocks can be added to the process **2500** without departing from the spirit and scope of the description. For example, in an embodiment, the patient monitor **2206** automatically returns to step **2502** upon outputting the error or determining that the confidence level did not exceed the confidence threshold, and repeats the process **2500**. In yet another embodiment, the patient monitor **2206** outputs the error as well as the blood pressure measurements having the highest confidence level.

FIG. **25** is a flow diagram illustrating yet another embodiment of a process **2600** implemented by the patient monitor **2206** for measuring blood pressure of a wearer. At block **2602**, the patient monitor **2206** receives configuration parameters. The configuration parameters can be set by a user, another patient monitor, or preset. The configuration parameters can include when to measure blood pressure, how to calculate the diastolic and systolic blood pressure, what measurements to display, confidence thresholds, etc. For example the configuration parameters can include whether to take blood pressure measurements during inflation, deflation, or both. In addition, the configuration parameters can include information regarding what process to use to determine the blood pressure measurements. For example, the patient monitor can determine the blood pressure measurements using the measured arterial pressure, the slopes of the pressure oscillations, maximum deflection points of the filtered blood pressure data, or other criteria. The configuration parameters can also include the confidence level to be used in determining whether the blood pressure measurements should be accepted. Furthermore, the configuration parameters can include what blood pressure measurements are to be output and how to determine which blood pressure measurements to output. For example, the configuration parameters can dictate that only blood pressure measurements having a confidence level greater than a threshold are to be output, or that the blood pressure measurements having the highest threshold are to be output. Additionally, the configuration parameters can dictate that both blood pressure measurements, average blood pressure measurements, and the like are to be output. Furthermore, the configuration parameters can include the frequency with which the blood pressure measurements are to be taken.

At block **2604**, the patient monitor initiates inflation based on the received configuration parameters. For example, the configuration parameters can dictate the rate at which the inflatable cuff **2204** is to be inflated using the gas reservoir **2202**. In an embodiment, the inflatable cuff **2204** is inflated at an approximately constant rate. In another embodiment, the inflatable cuff is not inflated at an approximately constant

rate. In an embodiment, the inflatable cuff **2204** is inflated in a relatively short amount of time or at a very high rate of inflation. In another embodiment, the inflatable cuff **2204** is inflated more slowly.

At block **2606** the inflationary blood pressure measurements are determined by the patient monitor **2606** based on the configuration parameters. The configuration parameters can dictate whether and what method to use in determining the inflationary blood pressure measurements. Furthermore, the configuration parameters can dictate whether the blood pressure data is filtered and how. In an embodiment, the configuration parameters dictate that the inflationary blood pressure measurements are not to be taken based on the inflation rate. In another embodiment, the patient monitor determines the inflationary blood pressure measurements based on the slope and magnitude of the oscillations of the filtered blood pressure data during inflation based on the configuration parameters. In addition, the patient monitor can set confidence levels and perform other operations based on the configuration parameters.

Upon determining the inflationary blood pressure measurements, the patient monitor initiates deflation of the inflatable cuff **2204** based on the configuration parameters. The configuration parameters can dictate the time and rate at which the inflatable cuff **2204** deflates. For example, the configuration parameters can dictate a threshold pressure that when reached initiates the deflation. The threshold pressure can be based on personal information of the wearer or general safety levels. In an embodiment, the patient monitor initiates deflation based on a threshold pressure being reached for a predefined period of time based on the configuration parameters. In another embodiment, the patient monitor initiates deflation once the inflationary blood pressure measurements are taken.

Upon initiating deflation, the patient monitor determines deflationary blood pressure measurements based on one or more configuration parameters, as illustrated in block **2610**. As discussed previously, with reference to block **2606** the configuration parameters can include any number of parameters that determine if and how the deflationary blood pressure measurements are taken, as well as if and how the blood pressure data is filtered. In addition, the patient monitor can set confidence levels and perform other operations based on the configuration parameters.

Upon determining the deflationary blood pressure measurements, the patient monitor arbitrates blood pressure measurements based on the configuration parameters. The patient monitor can arbitrate the blood pressure measurements based on any number of configuration parameters. For example, the patient monitor can arbitrate the blood pressure measurements based on the highest confidence level or whether a threshold confidence level was reached. Furthermore, the patient monitor can arbitrate based on expected values, previous values, averages or the like. Alternatively, the patient monitor can select both the inflationary and deflationary blood pressure measurements.

At block **2614**, the patient monitor outputs the results of the arbitration based on the configuration parameters. The output can include the inflationary blood pressure measurements, the deflationary blood pressure measurements, both or a combination of the two. The output can further include additional information, such as inflation rate, deflation rate, average blood pressure measurements depending on whether they were determined during inflation or deflation, etc.

VIII. Terminology

Many other variations than those described herein will be apparent from this disclosure. For example, depending on

the embodiment, certain acts, events, or functions of any of the algorithms described herein can be performed in a different sequence, can be added, merged, or left out all together (e.g., not all described acts or events are necessary for the practice of the algorithms). Moreover, in certain embodiments, acts or events can be performed concurrently, e.g., through multi-threaded processing, interrupt processing, or multiple processors or processor cores or on other parallel architectures, rather than sequentially. In addition, different tasks or processes can be performed by different machines and/or computing systems that can function together.

The various illustrative logical blocks, modules, and algorithm steps described in connection with the embodiments disclosed herein can be implemented as electronic hardware, computer software, or combinations of both. To clearly illustrate this interchangeability of hardware and software, various illustrative components, blocks, modules, and steps have been described above generally in terms of their functionality. Whether such functionality is implemented as hardware or software depends upon the particular application and design constraints imposed on the overall system. The described functionality can be implemented in varying ways for each particular application, but such implementation decisions should not be interpreted as causing a departure from the scope of the disclosure.

The various illustrative logical blocks and modules described in connection with the embodiments disclosed herein can be implemented or performed by a machine, such as a general purpose processor, a digital signal processor (DSP), an application specific integrated circuit (ASIC), a field programmable gate array (FPGA) or other programmable logic device, discrete gate or transistor logic, discrete hardware components, or any combination thereof designed to perform the functions described herein. A general purpose processor can be a microprocessor, but in the alternative, the processor can be a controller, microcontroller, or state machine, combinations of the same, or the like. A processor can also be implemented as a combination of computing devices, e.g., a combination of a DSP and a microprocessor, a plurality of microprocessors, one or more microprocessors in conjunction with a DSP core, or any other such configuration. Although described herein primarily with respect to digital technology, a processor may also include primarily analog components. For example, any of the signal processing algorithms described herein may be implemented in analog circuitry. A computing environment can include any type of computer system, including, but not limited to, a computer system based on a microprocessor, a mainframe computer, a digital signal processor, a portable computing device, a personal organizer, a device controller, and a computational engine within an appliance, to name a few.

The steps of a method, process, or algorithm described in connection with the embodiments disclosed herein can be embodied directly in hardware, in a software module executed by a processor, or in a combination of the two. A software module can reside in RAM memory, flash memory, ROM memory, EPROM memory, EEPROM memory, registers, hard disk, a removable disk, a CD-ROM, or any other form of non-transitory computer-readable storage medium, media, or physical computer storage known in the art. An exemplary storage medium can be coupled to the processor such that the processor can read information from, and write information to, the storage medium. In the alternative, the storage medium can be integral to the processor. The processor and the storage medium can reside in an ASIC. The ASIC can reside in a user terminal. In the alternative, the

processor and the storage medium can reside as discrete components in a user terminal.

Conditional language used herein, such as, among others, “can,” “might,” “may,” “e.g.,” and the like, unless specifically stated otherwise, or otherwise understood within the context as used, is generally intended to convey that certain embodiments include, while other embodiments do not include, certain features, elements and/or states. Thus, such conditional language is not generally intended to imply that features, elements and/or states are in any way required for one or more embodiments or that one or more embodiments necessarily include logic for deciding, with or without author input or prompting, whether these features, elements and/or states are included or are to be performed in any particular embodiment. The terms “comprising,” “including,” “having,” and the like are synonymous and are used inclusively, in an open-ended fashion, and do not exclude additional elements, features, acts, operations, and so forth. Also, the term “or” is used in its inclusive sense (and not in its exclusive sense) so that when used, for example, to connect a list of elements, the term “or” means one, some, or all of the elements in the list.

While the above detailed description has shown, described, and pointed out novel features as applied to various embodiments, it will be understood that various omissions, substitutions, and changes in the form and details of the devices or algorithms illustrated can be made without departing from the spirit of the disclosure. As will be recognized, certain embodiments of the inventions described herein can be embodied within a form that does not provide all of the features and benefits set forth herein, as some features can be used or practiced separately from others.

What is claimed is:

1. A method of measuring blood pressure, the method comprising:

obtaining a baseline photoplethysmograph signal from an optical sensor coupled to a measurement site of the patient before a deliberate movement of the measurement site;

obtaining a motion induced photoplethysmograph signal from the optical sensor coupled with the patient at the measurement site that is in motion;

obtaining a motion signal from a motion sensor coupled with the measurement site;

estimating a motion component of the motion induced photoplethysmograph signal responsive to the deliberate movement based at least on the motion signal and the baseline photoplethysmograph signal;

normalizing the motion portion with respect to acceleration and perfusion to generate an output normalized signal;

supplying the output normalized signal into a cuff trigger module to determine whether the output normalized signal exceeds a threshold;

generating a triggering signal to a blood pressure cuff based on the output normalized signal exceeding the threshold;

controlling an operation of the blood pressure cuff in response to the triggering signal; and

calculating, by a hardware processor, a blood pressure based on the normalized motion portion instead of deriving the blood pressure from an estimated plethysmograph portion of the motion induced photoplethysmograph signal and based on the operation of the blood pressure cuff.

2. The method of claim 1, wherein the motion sensor comprises an accelerometer.

3. The method of claim 1, further comprising inducing the motion at the measurement site with a motion inducer.

4. The method of claim 3, wherein the motion inducer comprises a motor.

5. The method of claim 1, further comprising one or more basis functions to values of the motion portion prior to normalizing the motion portion.

6. The method of claim 5, further comprising determining weights associated with the one or more basis functions based on a measurement from the blood pressure cuff.

7. The method of claim 6, where the one or more basis functions comprise both linear and non-linear functions.

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专利名称(译)	血压测量方法		
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[标]申请(专利权)人(译)	梅西莫股份有限公司		
申请(专利权)人(译)	Masimo公司		
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摘要(译)

非侵入性地确定个体血压的血压测量系统可包括具有光学传感器和运动传感器的非侵入式血压传感器。光学传感器可以将从患者获得的光电容积描记器信号提供给处理器。运动传感器可响应于患者的运动向处理器提供运动信号。在一个实施例中，处理器基于光电容积描记器信号和运动信号计算或估计患者的血压。有利地，该系统可以在没有闭塞箍的情况下获得该血压测量值，从而减少患者的不适。在其他实施方式中，处理器根据光电容积描记器和运动信号计算血压相关参数。当该参数改变时，处理器偶尔可以触发闭塞袖带测量，从而减少闭塞袖带测量的频率。

