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(19) **United States**(12) **Patent Application Publication****Cho et al.**(10) **Pub. No.: US 2006/0015022 A1**(43) **Pub. Date: Jan. 19, 2006**(54) **BLOOD SUGAR LEVEL MEASURING APPARATUS**(22) Filed: **Jun. 30, 2004****Publication Classification**(76) Inventors: **Ok-Kyung Cho**, Schwerte (DE);
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ARLINGTON, VA 22209-3873 (US)(57) **ABSTRACT**

Blood sugar levels are measured non-invasively based on temperature measurement. Non-invasively measured blood sugar level values obtained by a temperature measurement scheme are corrected by blood oxygen saturation and blood flow volume, thereby stabilizing the measurement data.

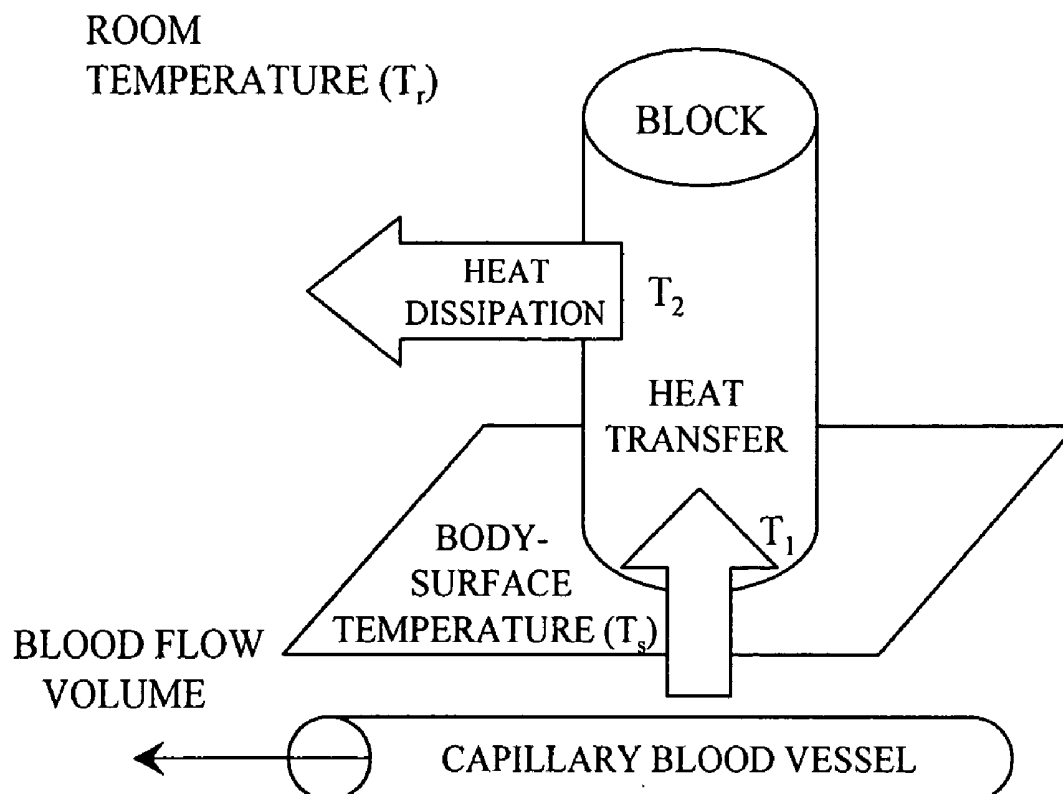
(21) Appl. No.: **10/879,231**

FIG. 1

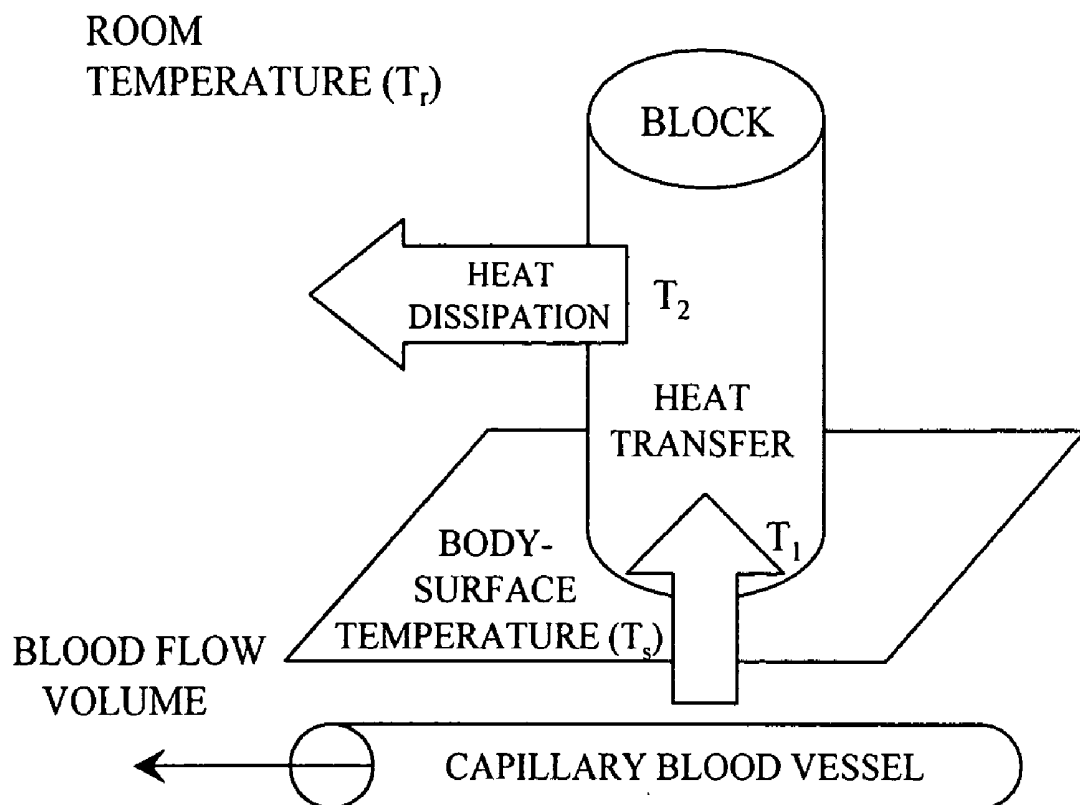


FIG. 2

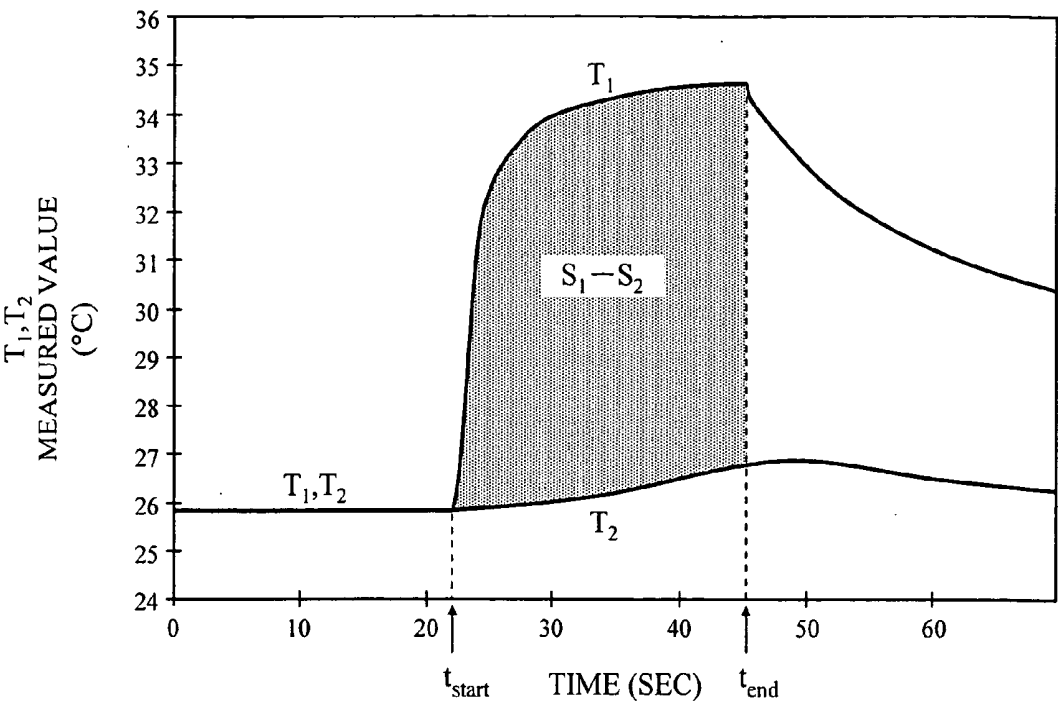


FIG. 3

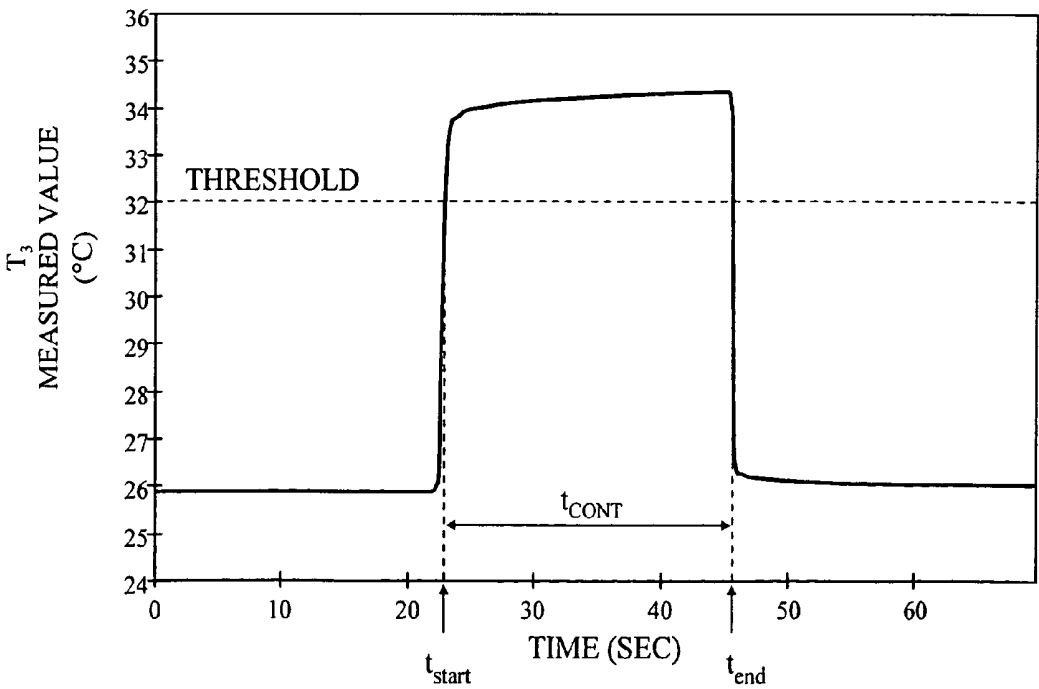


FIG. 4

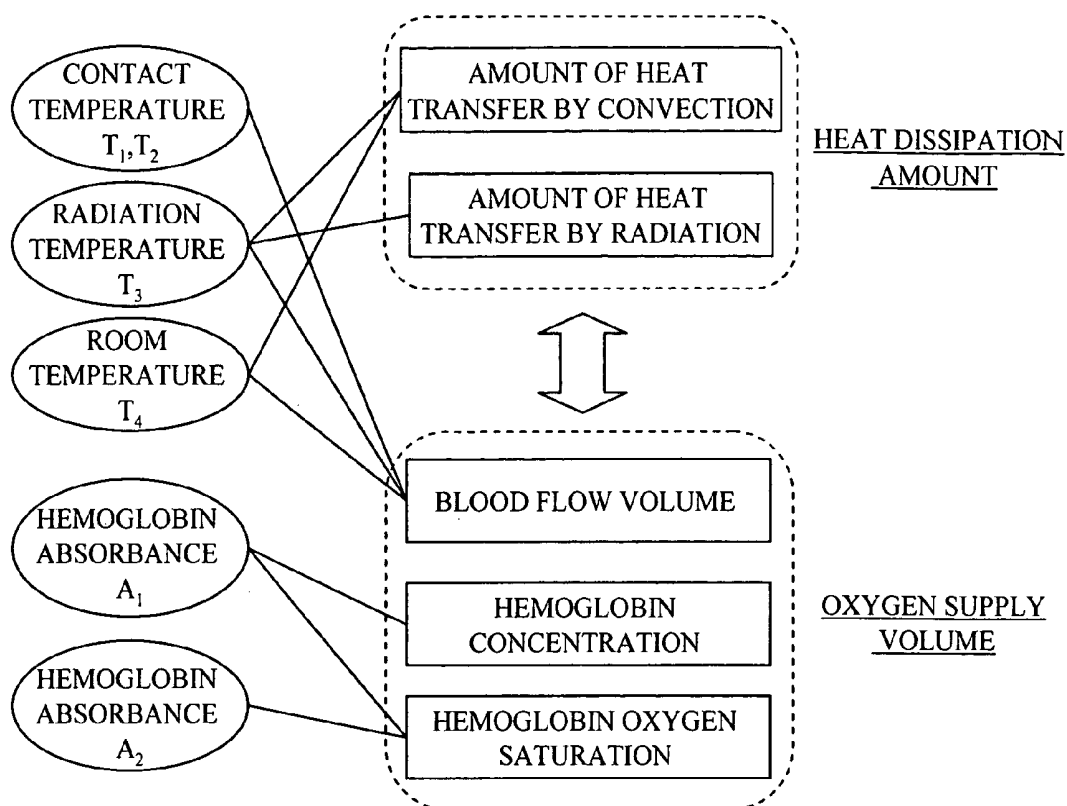


FIG. 5

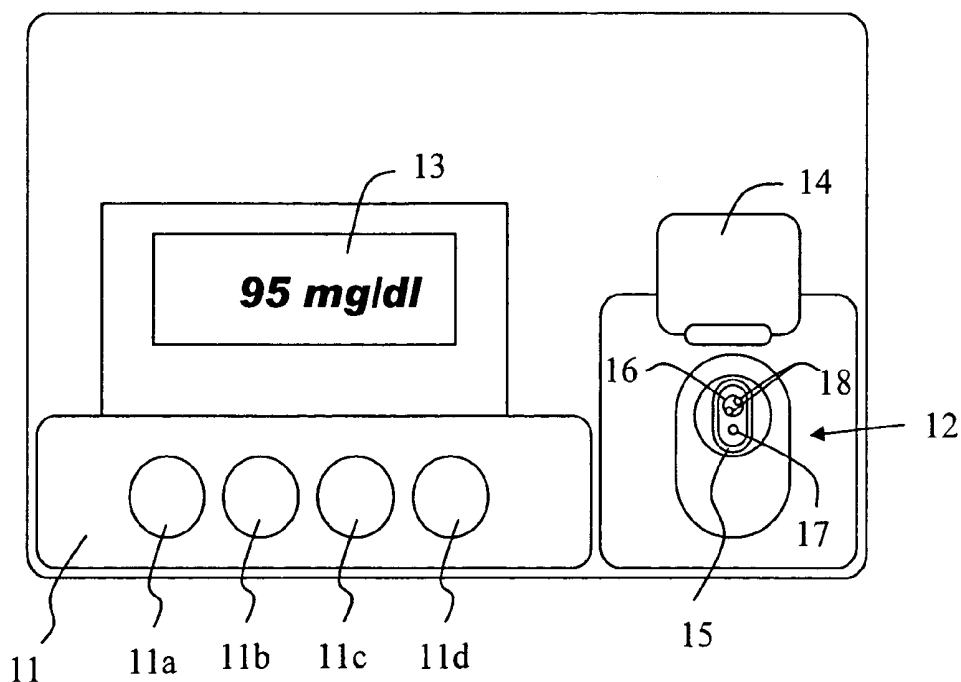


FIG. 6(a)

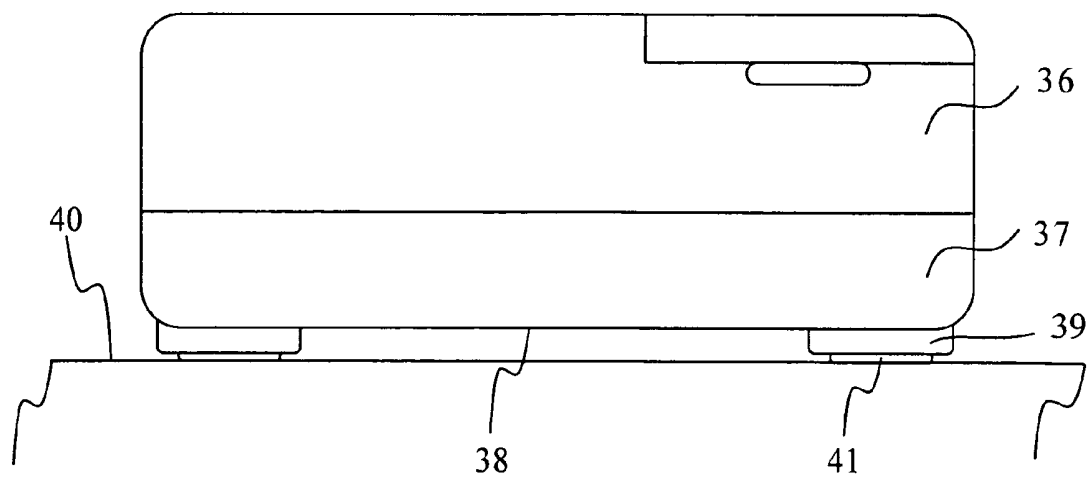


FIG. 6(b)

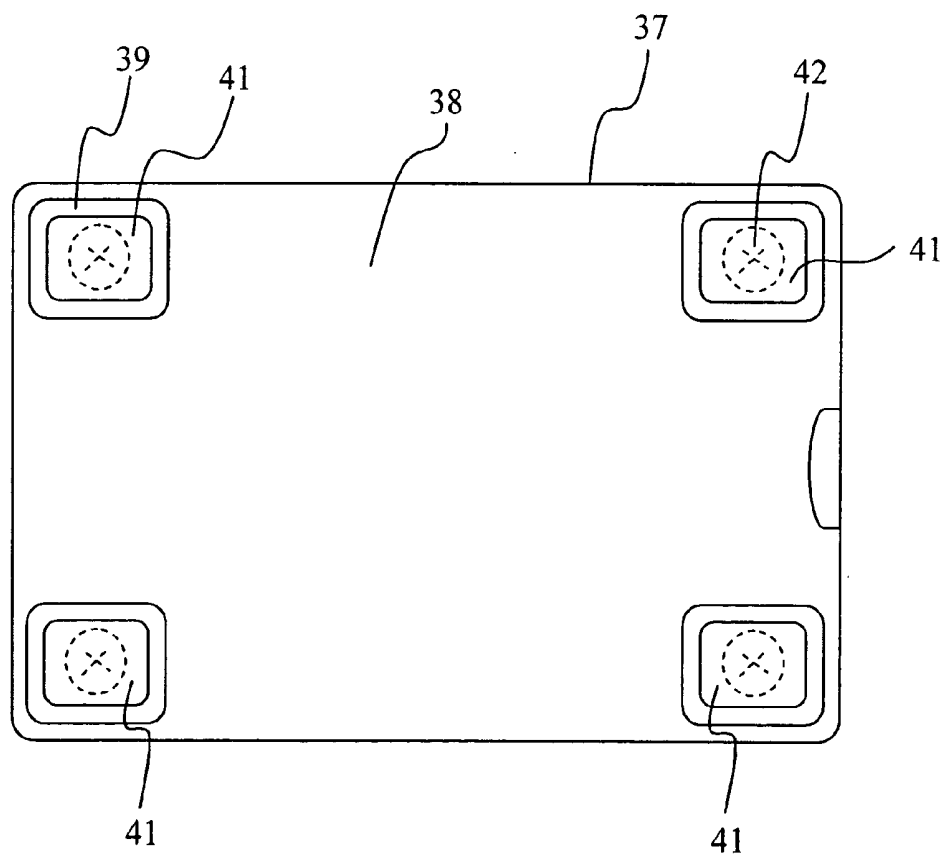


FIG. 7

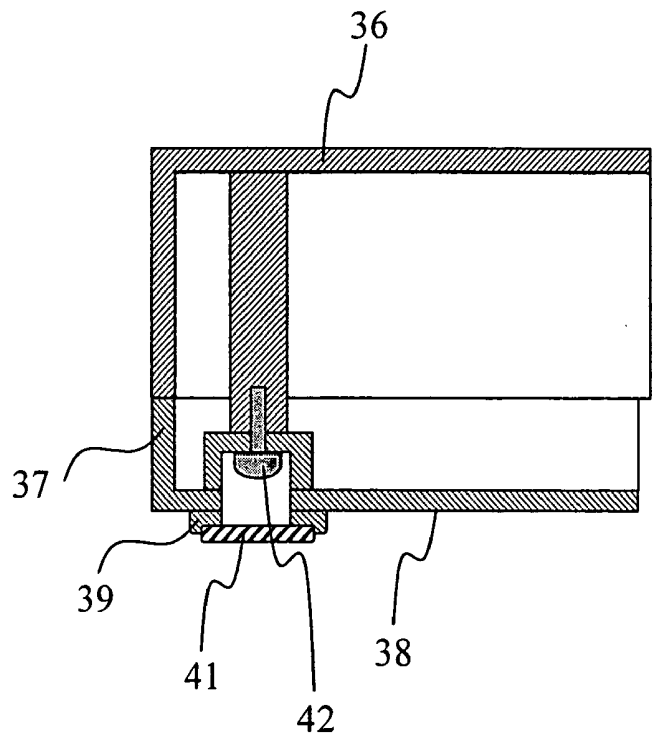


FIG. 8

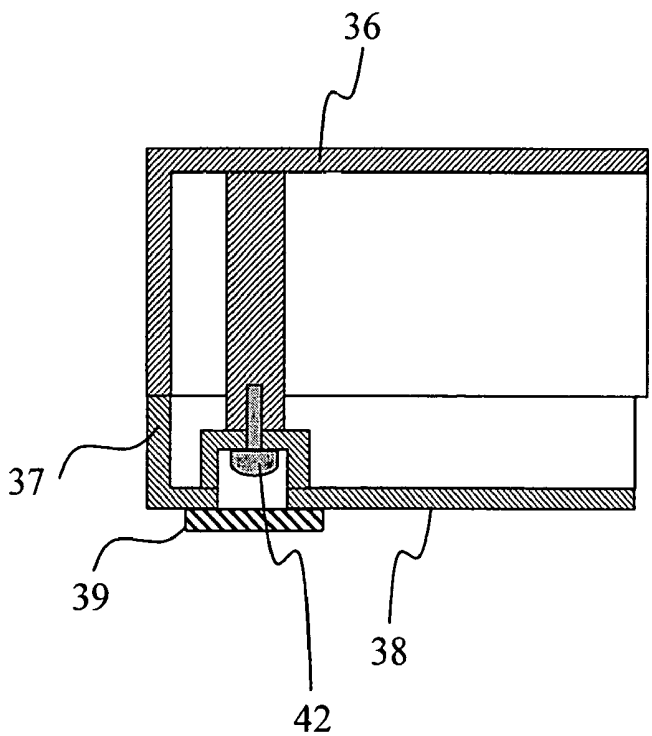


FIG. 9

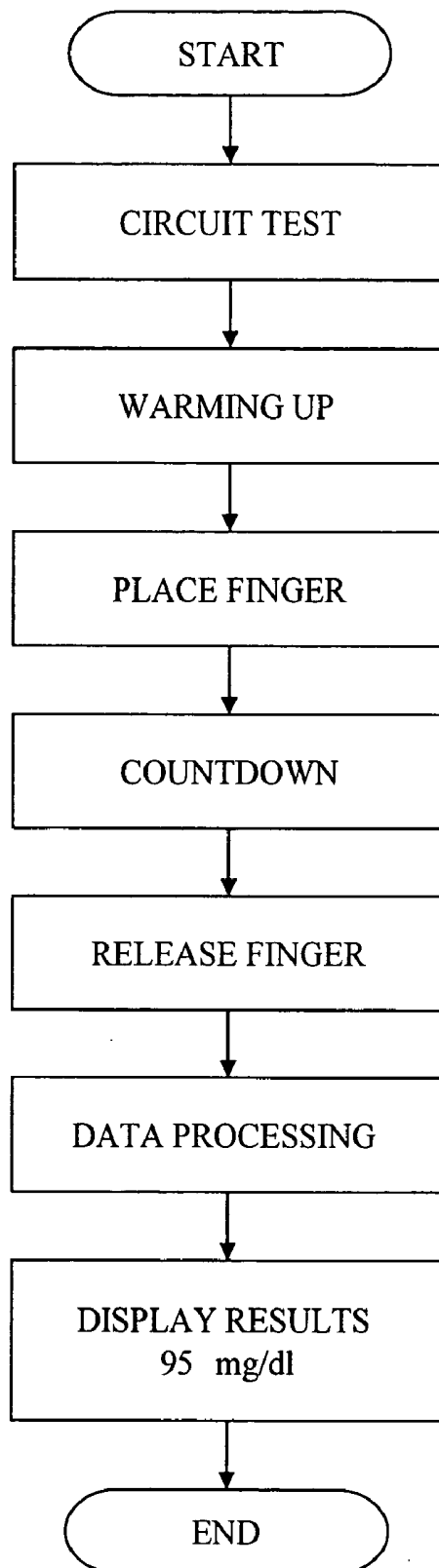


FIG. 10(a)

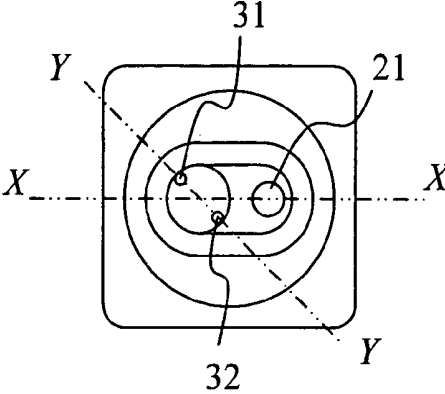


FIG. 10(b)

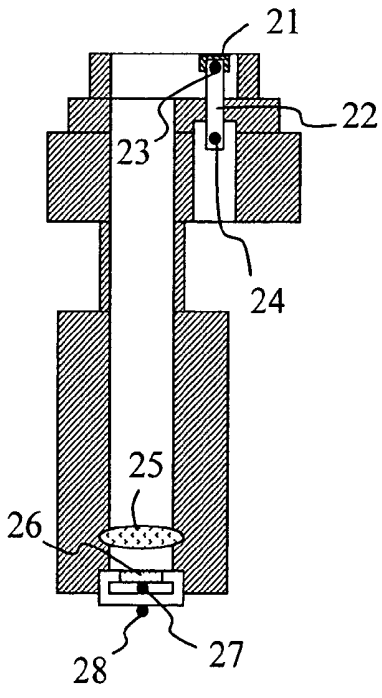


FIG. 10(c)

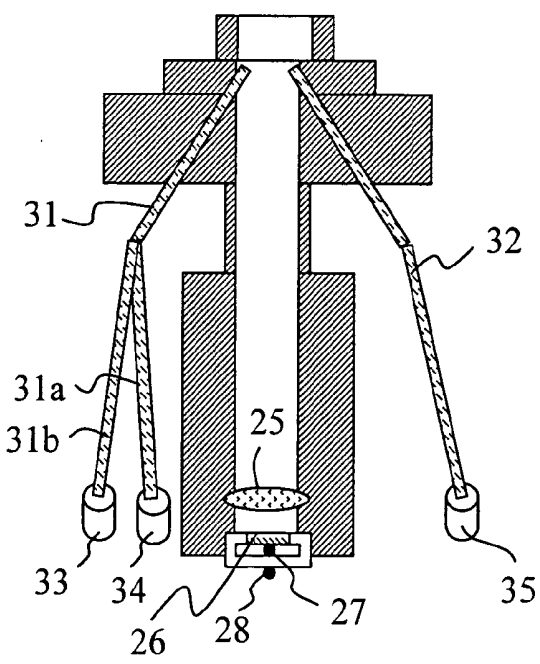


FIG. 11

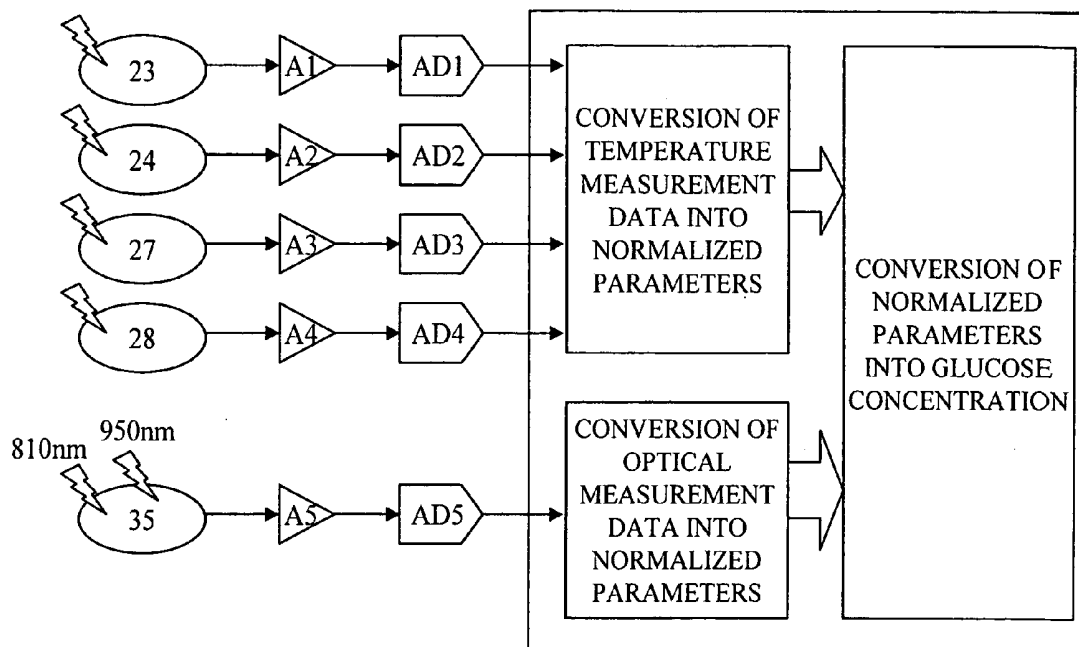


FIG. 12

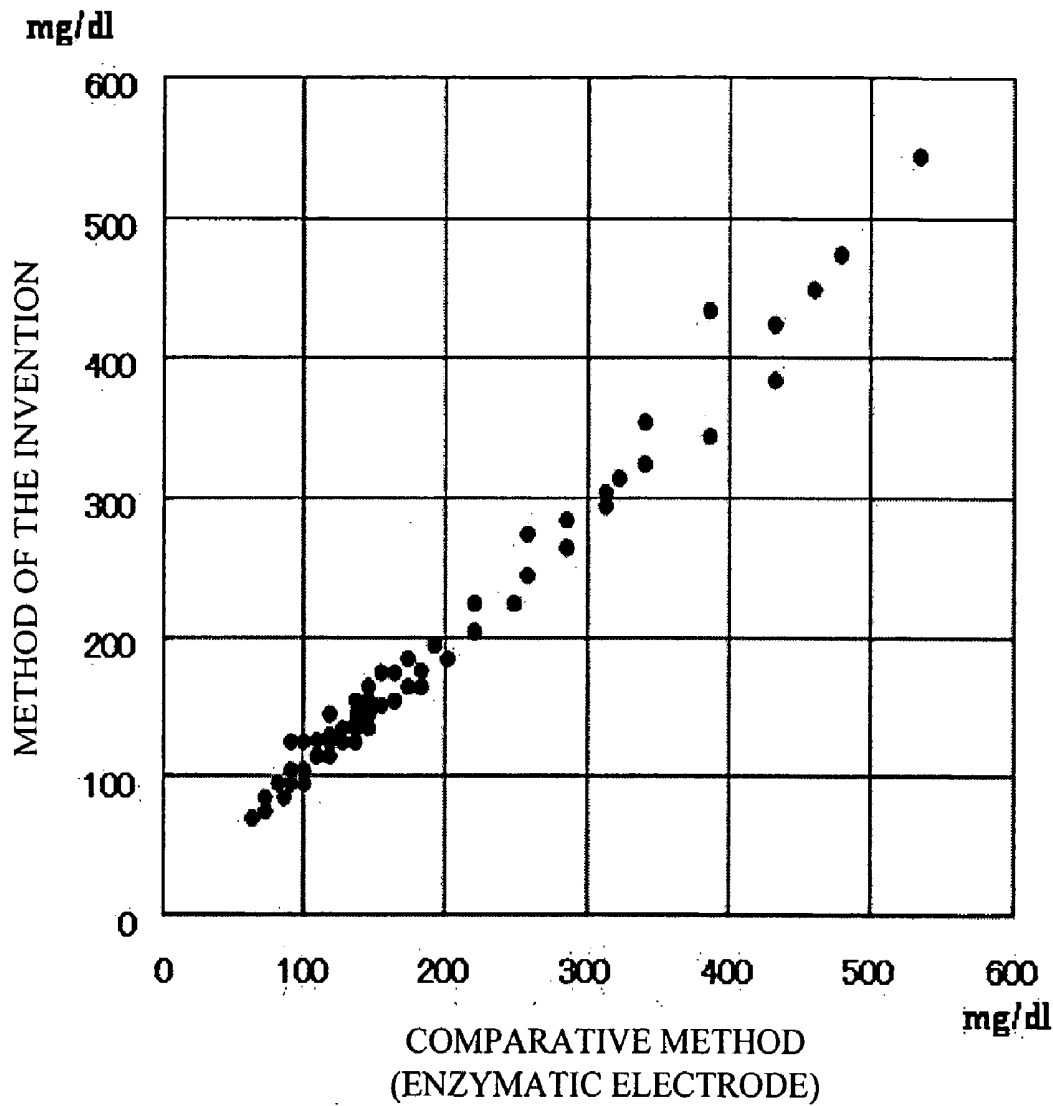


FIG. 13(a)

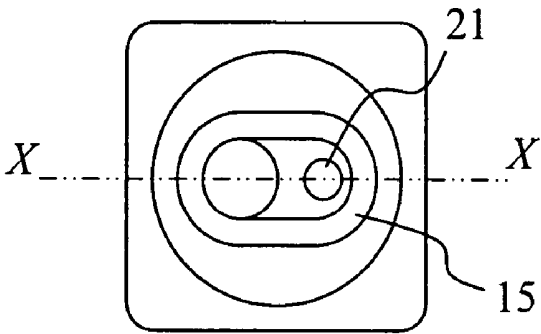


FIG. 13(b)

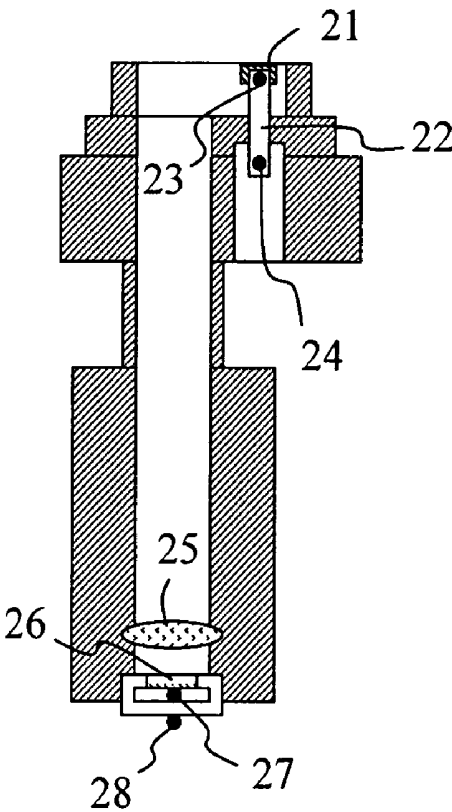


FIG. 14

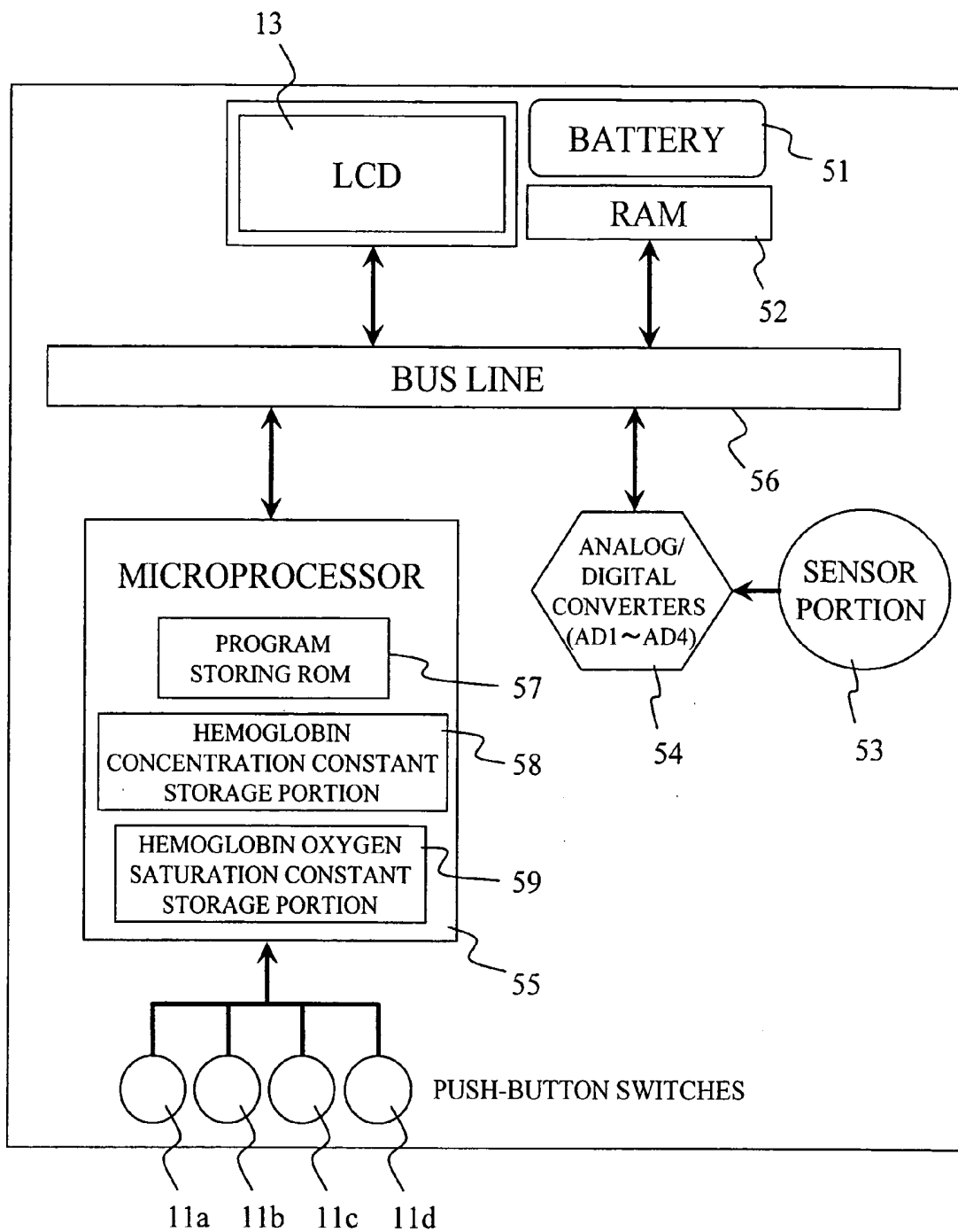
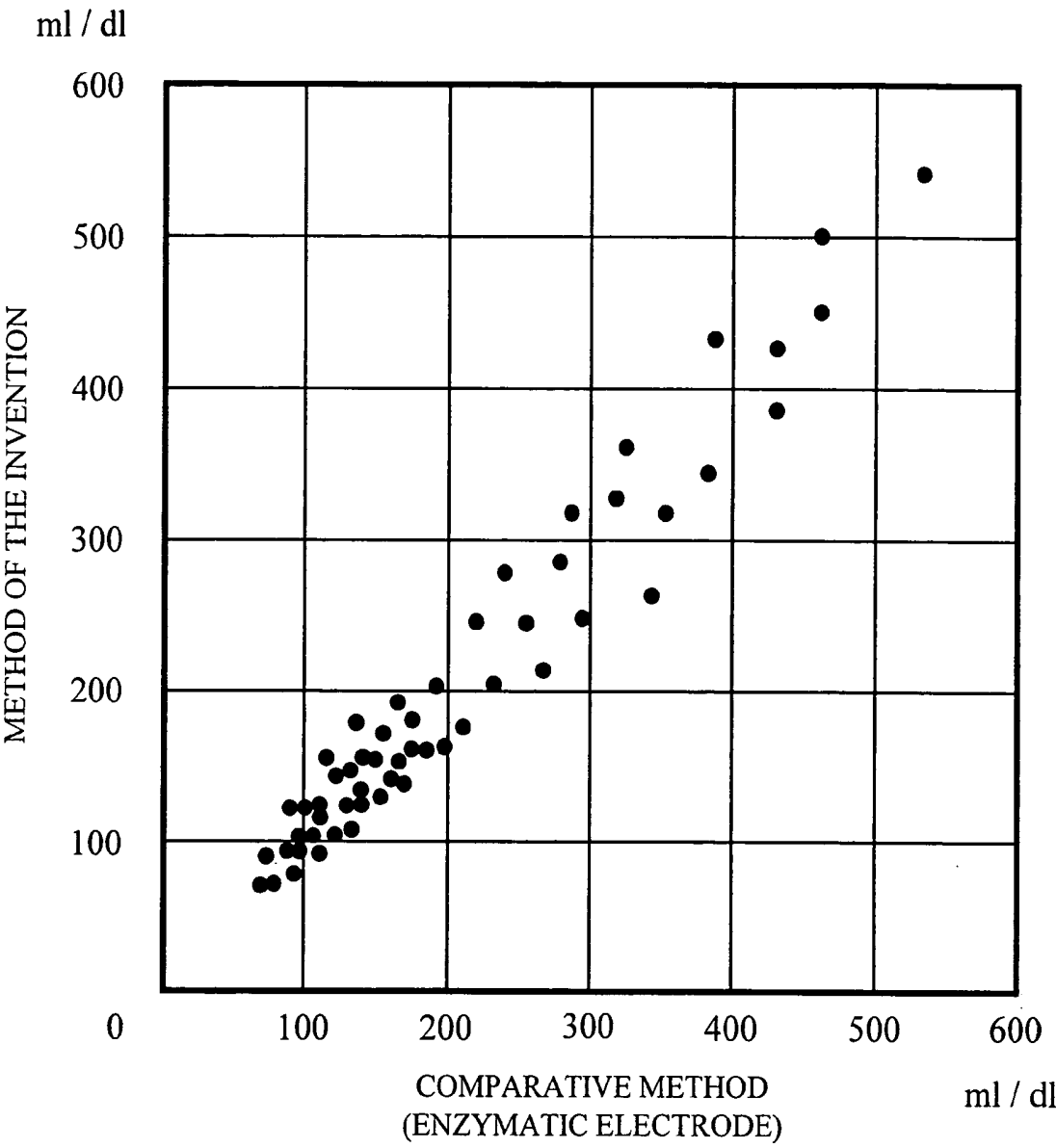


FIG. 15



BLOOD SUGAR LEVEL MEASURING APPARATUS**BACKGROUND OF THE INVENTION**

[0001] 1. Field of the Invention

[0002] The present invention relates to a non-invasive blood sugar level measuring method and apparatus for measuring glucose concentration in a living body without blood sampling.

[0003] 1. Background Art

[0004] Hilson et al. report facial and sublingual temperature changes in diabetics following intravenous glucose injection (Non-Patent Document 1). Scott et al. discuss the issue of diabetics and thermoregulation (Non-Patent Document 2). Based on such researches, Cho et al. suggests a method and apparatus for determining blood glucose concentration by temperature measurement without requiring the collection of a blood sample (Patent Documents 1 and 2).

[0005] Various other attempts have been made to determine glucose concentration without blood sampling. For example, a method has been suggested (Patent Document 3) whereby a measurement site is irradiated with near-infrared light of three wavelengths, and the intensity of transmitted light as well as the temperature of the living body is detected. Then, a representative value of the second-order differentiated value of absorbance is calculated, and the representative value is corrected in accordance with the difference between the living body temperature and a pre-determined reference temperature. A blood sugar level corresponding to the thus corrected representative value is then determined. An apparatus is also provided (Patent Document 4) whereby a measurement site is heated or cooled while monitoring the living body temperature. The degree of attenuation of light based on light irradiation is measured at the moment of temperature change so that the glucose concentration responsible for the temperature-dependency of the degree of light attenuation can be measured. Further, an apparatus is reported (Patent Document 5) whereby an output ratio between reference light and the light transmitted by an irradiated sample is taken, and then a glucose concentration is calculated using a linear expression of the logarithm of the output ratio and the living body temperature.

[0006] [Non-Patent Document 1] R. M. Hilson and T. D. R. Hockaday, "Facial and sublingual temperature changes following intravenous glucose injection in diabetics," *Diabete & Metabolisme*, 1982, 8, 15-19

[0007] [Non-Patent Document 2] A. R. Scott, T. Bennett, I. A. MacDonald, "Diabetes mellitus and thermoregulation," *Can. J. Physiol. Pharmacol.*, 1987, 65, 1365-1376

[0008] [Patent Document 1] U.S. Pat. No. 5,924,996

[0009] [Patent Document 2] U.S. Pat. No. 5,795,305

[0010] [Patent Document 3] JP Patent Publication (Kokai) No. 2000-258343 A

[0011] [Patent Document 4] JP Patent Publication (Kokai) No. 10-33512 A (1998)

[0012] [Patent Document 5] JP Patent Publication (Kokai) No. 10-108857 A (1998)

SUMMARY OF THE INVENTION

[0013] Glucose (blood sugar) in blood is used for glucose oxidation reaction in cells to produce necessary energy for the maintenance of a living body. In the basal metabolism state, in particular, most of the produced energy is converted into heat energy for the maintenance of body temperature. Thus, it can be expected that there is some relationship between blood glucose concentration and body temperature. However, as is evident from the way sicknesses cause fever, the body temperature also varies due to factors other than blood glucose concentration. While methods have been proposed to determine blood glucose concentration by temperature measurement without blood sampling, they lack sufficient accuracy.

[0014] It is the object of the invention to provide a method and apparatus for determining blood glucose concentration with high accuracy based on temperature data of a subject without blood sampling.

[0015] Blood sugar is delivered to the cells throughout the human body via the blood vessel system, particularly the capillary blood vessels. In the human body, complex metabolic pathways exist. Glucose oxidation is a reaction in which, fundamentally, blood sugar reacts with oxygen to produce water, carbon dioxide, and energy. Oxygen herein refers to the oxygen delivered to the cells via blood. The amount of oxygen supply is determined by the blood hemoglobin concentration, the hemoglobin oxygen saturation, and the volume of blood flow. On the other hand, the heat produced in the body by glucose oxidation is dissipated from the body by convection, heat radiation, conduction, and so on. On the assumption that the body temperature is determined by the balance between the amount of energy produced in the body by glucose burning, namely heat production, and heat dissipation such as mentioned above, we set up the following model:

[0016] (1) The amount of heat production and the amount of heat dissipation are considered equal.

[0017] (2) The amount of heat production is a function of the blood glucose concentration and the amount of oxygen supply.

[0018] (3) The amount of oxygen supply is determined by the blood hemoglobin concentration, the blood hemoglobin oxygen saturation, and the volume of blood flow in the capillary blood vessels.

[0019] (4) The amount of heat dissipation is mainly determined by heat convection and heat radiation.

[0020] The inventors have achieved the present invention after realizing that blood sugar levels can be accurately determined on the basis of the results of measuring the temperature of the body surface and parameters relating to oxygen concentration in blood and blood flow volume, in accordance with the aforementioned model. The parameters can be measured from a part of the human body, such as the fingertip. Parameters relating to convection and radiation can be determined by carrying out thermal measurements on the fingertip. Parameters relating to blood hemoglobin concentration and blood hemoglobin oxygen saturation can be obtained by spectroscopically measuring blood hemoglobin and determining the ratio of hemoglobin bound with oxygen to hemoglobin not bound with oxygen. With regard to the

parameters relating to blood hemoglobin concentration and blood hemoglobin oxygen saturation, measurement accuracy would not be significantly lowered if pre-stored constants are employed rather than taking measurements. A parameter relating to the volume of blood flow can be determined by measuring the amount of heat transfer from the skin.

[0021] In one aspect, the invention provides a blood sugar level measuring apparatus comprising:

[0022] a heat amount measurement portion for measuring a plurality of temperatures derived from a body surface and obtaining information used for calculating the amount of heat transferred by convection and the amount of heat transferred by radiation, both related to the dissipation of heat from said body surface;

[0023] an oxygen amount measuring portion for obtaining information about blood oxygen amount;

[0024] a storage portion for storing a relationship between parameters individually corresponding to said plurality of temperatures and blood oxygen amount and blood sugar levels;

[0025] a calculating portion which converts a plurality of measurement values fed from said heat amount measuring portion and said oxygen amount measurement portion into said parameters, and which computes a blood sugar level by applying said parameters to said relationship stored in said storage portion;

[0026] a display portion for displaying the blood sugar level calculated by said calculating portion; and

[0027] an apparatus chassis, wherein

[0028] said oxygen amount measuring portion comprises a blood flow volume measuring portion for obtaining information about the blood flow volume and an optical measuring portion for obtaining the hemoglobin concentration and hemoglobin oxygen saturation in blood, wherein the blood flow volume measuring portion comprises a body-surface contact portion, an adjacent-temperature detector disposed adjacent to the body-surface contact portion, an indirect-temperature detector for detecting the temperature at a position spaced apart from the body-surface contact portion, and a heat conducting member connecting the body-surface contact portion and the indirect temperature detector, and wherein the chassis comprises a plurality of legs at a bottom surface thereof for supporting the chassis.

[0029] In another aspect, the invention provides a blood sugar level measuring apparatus comprising:

[0030] an ambient temperature measuring device for measuring ambient temperature;

[0031] a body-surface contact portion to which a body surface is brought into contact;

[0032] an adjacent-temperature detector disposed adjacent to said body-surface contact portion;

[0033] a radiant heat detector for measuring radiant heat from said body surface;

[0034] a heat conducting member disposed in contact with said body-surface contact portion;

[0035] an indirect-temperature detector disposed at a position that is adjacent to said heat conducting member and that is spaced apart from said body-surface contact portion, said indirect-temperature detector measuring temperature at the position spaced apart from said body-surface contact portion;

[0036] a light source for irradiating said body-surface contact portion with light of at least two different wavelengths;

[0037] a photodetector for detecting reflected light that is produced as the light is reflected by the body surface;

[0038] a calculating portion including a converting portion for converting outputs from said adjacent-temperature detector, said indirect-temperature detector, said ambient temperature detector, said radiant temperature detector and said photodetector, into individual parameters, and a processing portion in which a relationship between said parameters and blood sugar levels is stored in advance and which calculates a blood sugar level by applying said parameters to said relationship;

[0039] a display for displaying the blood sugar level outputted from said calculating portion; and

[0040] an apparatus chassis, wherein the chassis comprises a plurality of legs at a bottom surface thereof for supporting the chassis.

[0041] In yet another aspect, the invention provides a blood sugar level measuring apparatus comprising:

[0042] an ambient temperature measuring device for measuring ambient temperature;

[0043] a body-surface contact portion to which a body surface is brought into contact;

[0044] an adjacent-temperature detector disposed adjacent to said body-surface contact portion;

[0045] a radiant heat detector for measuring radiant heat from said body surface;

[0046] a heat conducting member disposed in contact with said body-surface contact portion;

[0047] an indirect-temperature detector disposed at a position that is adjacent to said heat conducting member and that is spaced apart from said body-surface contact portion, said indirect-temperature detector measuring temperature at the position spaced apart from said body-surface contact portion;

[0048] a storage portion where information about blood hemoglobin concentration and blood hemoglobin oxygen saturation is stored;

[0049] a calculating portion including a converting portion for converting outputs from said adjacent-temperature detector, said indirect-temperature detector, said ambient temperature measuring device and said radiant heat detector, into a plurality of parameters, and a processing portion in which a relationship between said parameters and blood sugar levels is stored in advance and which calculates a blood sugar level by applying said parameters to said relationship;

[0050] a display for displaying the blood sugar level outputted from said calculating portion; and

[0051] an apparatus chassis, wherein the chassis comprises a plurality of legs at a bottom surface thereof for supporting the chassis.

[0052] The legs mounted on the bottom surface of the chassis are made from a heat insulating material with a smaller heat conductivity than that of the chassis.

[0053] The invention makes it possible to non-invasively determine blood sugar levels with the same level of accuracy as that achieved by the conventional invasive method.

BRIEF DESCRIPTION OF THE DRAWINGS

[0054] FIG. 1 shows a model of the transfer of heat from a body surface to a block.

[0055] FIG. 2 shows changes in measurement values of temperatures T_1 and T_2 with time.

[0056] FIG. 3 shows an example of the measurement of a change in temperature T_3 with time.

[0057] FIG. 4 shows the relationships between measurement values obtained by various sensors and parameters derived therefrom.

[0058] FIG. 5 shows a top plan view of a non-invasive blood sugar level measuring apparatus according to the present invention.

[0059] FIG. 6 shows an external view of the blood sugar level measuring apparatus.

[0060] FIG. 7 shows a lateral cross section of a leg portion.

[0061] FIG. 8 shows a lateral cross section of a leg portion according to another embodiment.

[0062] FIG. 9 shows an operating procedure of the apparatus.

[0063] FIG. 10 shows a measuring portion in detail.

[0064] FIG. 11 shows a conceptual chart of the flow of data processes in the apparatus.

[0065] FIG. 12 shows a graph plotting the values of glucose concentration calculated according to the invention and the values of glucose concentration measured according to the enzymatic electrode method.

[0066] FIG. 13 shows another example of the measuring portion in detail.

[0067] FIG. 14 shows a conceptual chart illustrating data storage locations in the apparatus.

[0068] FIG. 15 shows a graph plotting the values of glucose concentration calculated according to the invention and the values of glucose concentration measured according to the enzymatic electrode method.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0069] The invention will now be described by way of preferred embodiments thereof with reference made to the drawings.

[0070] Initially, the above-mentioned model will be described in more specific terms. Regarding the amount of heat dissipation, convective heat transfer, which is one of the

main causes of heat dissipation, is related to the temperature difference between the ambient (room) temperature and the body-surface temperature. The amount of heat dissipation due to radiation, another main cause of dissipation, is proportional to the fourth power of the body-surface temperature according to the Stefan-Boltzmann law. Thus, it can be seen that the amount of heat dissipation from the human body is related to the room temperature and the body-surface temperature. Another major factor related to the amount of heat production, the oxygen supply amount, is expressed as the product of hemoglobin concentration, hemoglobin oxygen saturation, and blood flow volume.

[0071] The hemoglobin concentration can be measured based on the absorbance of light at the wavelength (isoabsorption wavelength) at which the molar absorption coefficient of theoxyhemoglobin and that of the reduced hemoglobin (deoxyhemoglobin) are equal. The hemoglobin oxygen saturation can be measured by measuring the absorbance at the isoabsorption wavelength and the absorbance at at least one other wavelength at which the ratio of the molar absorption coefficient of the oxyhemoglobin to that of the reduced hemoglobin (deoxyhemoglobin) is known, and then solving simultaneous equations. Thus, the hemoglobin concentration and the hemoglobin oxygen saturation can be obtained by measuring absorbance at at least two wavelengths.

[0072] The rest is the blood flow volume, which can be measured by various methods. One example will be described below.

[0073] FIG. 1 shows a model for the description of the transfer of heat from the body surface to a solid block with a certain heat capacity as the block is brought into contact with the body surface for a certain time and then separated. The block may be made of resin such as plastic or vinyl chloride. In the illustrated example, attention will be focused on the chronological variation of a temperature T_1 of a portion of the block in contact with the body surface, and the chronological variation of a temperature T_2 at a point on the block away from the body surface. The blood flow volume can be estimated by monitoring mainly the chronological variation of the temperature T_2 (at the spatially distant point on the block). The details will be described below.

[0074] Before the block comes into contact with the body surface, the temperatures T_1 and T_2 at the two points of the block are equal to the room temperature T_r . When a body-surface temperature T_s is higher than the room temperature T_r , the temperature T_1 swiftly rises as the block comes into contact with the body surface, due to the transfer of heat from the skin, and it approaches the body-surface temperature T_s . On the other hand, the temperature T_2 , which is lower than the temperature T_1 due to the dissipation of the heat conducted through the block from its surface, rises more gradually than the temperature T_1 . The chronological variation of the temperatures T_1 and T_2 depends on the amount of heat transferred from the body surface to the block, which in turn depends on the blood flow volume in the capillary blood vessels under the skin. If the capillary blood vessels are regarded as a heat exchanger, the coefficient of heat transfer from the capillary blood vessels to the surrounding cell tissue is given as a function of the blood flow volume. Thus, by measuring the amount of heat transfer from the body surface to the block by monitoring the

chronological variation of the temperatures T_1 and T_2 , the amount of heat transmitted from the capillary blood vessels to the cell tissue can be estimated, which in turn makes it possible to estimate the blood flow volume.

[0075] FIG. 2 shows the chronological variation of the measured values of the temperature T_1 at the portion of the block in contact with the body surface and the temperature T_2 at the point on the block away from the body-surface contact position. As the block comes into contact with the body surface, T_1 swiftly rises, and it gradually drops as the block is brought out of contact.

[0076] FIG. 3 shows the chronological variation of the measured value of a temperature T_3 measured by a radiation temperature detector. As the temperature T_3 measured is that due to the radiation from the body surface, this sensor can more sensitively react to temperature changes than other sensors. Because radiation heat propagates as an electromagnetic wave, it can transmit temperature changes instantaneously. Thus, as shown in FIG. 7, reference to which will be made below, by providing the radiation temperature detector near the position where the block is in contact with the body surface in order to detect the radiant heat from the body surface, contact start time t_{start} and contact end time t_{end} of contact between the block and body surface can be detected based on a change in temperature T_3 . For example, when a temperature threshold value is set as shown in FIG. 3, it can be determined that contact start time t_{start} is when the temperature threshold value is exceeded, and contact end time t_{end} is when the measured temperature drops below the temperature threshold value. The temperature threshold value may be set at 32° C., for example.

[0077] Then, the T_1 measured value between t_{start} and t_{end} is approximated by an S curve, such as a logistic curve. A logistic curve is expressed by the following equation:

$$T = \frac{b}{1 + c \times \exp(-a \times t)} + d$$

where T is temperature, and t is time.

[0078] The measured value can be approximated by determining factors a , b , c , and d by the non-linear least-squares method. For the resultant approximate expression, T is integrated between time t_{start} and time t_{end} to obtain a value S_1 .

[0079] Similarly, an integrated value S_2 is calculated from the T_2 measured value. The smaller the $(S_1 - S_2)$ is, the larger the amount of transfer of heat from the finger surface to the position of T_2 . $(S_1 - S_2)$ becomes larger with increasing finger contact time t_{CONT} ($=t_{\text{end}} - t_{\text{start}}$). Thus, $a_5/(t_{\text{CONT}} \times (S_1 - S_2))$ is designated as a parameter X_5 indicating the volume of blood flow, where a_5 is a proportionality coefficient.

[0080] It will be seen from the above description that the measured quantities necessary for the determination of blood glucose concentration by the aforementioned model are the room temperature (ambient temperature), body surface temperature, temperature changes in the block in contact with the body surface, the temperature due to radiation from the body surface, and the absorbance of at least two wavelengths.

[0081] FIG. 4 shows the relationships between the measured values provided by various sensors and the parameters derived therefrom. A block is brought into contact with the body surface, and chronological changes in the two kinds of temperatures T_1 and T_2 are measured by two temperature sensors provided at two locations of the block. Separately, the radiation temperature T_3 on the body surface and the room temperature T_4 are measured. Absorbance A_1 and A_2 are measured at at least two wavelengths related to the absorption of hemoglobin. The temperatures T_1 , T_2 , T_3 , and T_4 provide parameters related to the volume of blood flow. The temperature T_3 provides a parameter related to the amount of heat transferred by radiation. The temperatures T_3 and T_4 provide parameters related to the amount of heat transferred by convection. Absorbance A_1 provides a parameter relating to hemoglobin concentration. Absorbance A_1 and A_2 provide parameters relating to hemoglobin oxygen saturation.

[0082] Hereafter, an example of the apparatus for non-invasively measuring blood sugar levels according to the principle of the invention will be described.

[0083] FIG. 5 shows a top plan view of the non-invasive blood sugar level measuring apparatus according to the invention. While in this example the skin on the ball of the fingertip is used as the body surface, other parts of the body surface may be used.

[0084] On the upper surface of the apparatus are provided an operating portion 11, a measurement portion 12 where the finger to be measured is to be placed, and a display portion 13 for displaying the result of measurement, the state of the apparatus, measured values, and so on. The operating portion 11 includes four push buttons 11a to 11d for operating the apparatus. The measurement portion 12 has a cover 14 which, when opened (as shown), reveals a finger rest portion 15 with an oval periphery. The finger rest portion 15 accommodates an open end 16 of a radiation temperature sensor portion, a contact temperature sensor portion 17, and an optical sensor portion 18.

[0085] FIG. 6 shows an external view of the blood sugar level measuring apparatus, FIG. 6(a) showing a front view, and FIG. 6(b) a bottom view. The chassis of the apparatus comprises an upper case 36 and a lower case 37. A plurality of legs 39 are integrally provided on a bottom surface 38 of the lower case 37. In order to prevent the conduction of heat from the base or the like on which the apparatus is placed, the sum of the cross-sectional areas of the plural legs 39 on the bottom surface 38 of the lower case 37, or a sum cross-sectional area, should preferably be less than one tenth the bottom area of the lower case 37 (including the areas of the legs 39). A distance of at least 1 mm is provided between the bottom surface 38 of the lower case and a mount surface 40 on which the apparatus is mounted so that the bottom surface 38 would not come into contact with the mount surface 40 in case the bottom surface 38 and the mount surface 40 should be deformed. Moreover, an antislip sheet 41 is affixed to each of the plurality of legs 39. The antislip sheets 41 are designed to maintain a thickness of at least 0.5 mm when deformed by the mass of the apparatus and the pressing force exerted by the user's fingers during measurement, thus preventing the legs 39 from coming into contact with the mount surface 40. The antislip sheets 41 are made of a material with a lower heat conductivity than that of the

lower case 37, such as urethane rubber. The heat conductivity of the lower case 37 should preferably be of the order of 0.4 kcal/m.hr. $^{\circ}$ C., for example. The heat conductivity of the antislip sheets 41 should preferably be of the order of 0.01 to 0.3 kcal/m.hr. $^{\circ}$ C. The material of the legs 39 integrated with the lower case 37 may be a plastic resin, such as ABS resin.

[0086] FIG. 7 shows a lateral cross section of a leg portion. The upper case 36 and the lower case 37 are fastened using a plurality of screws 42. The screws 42 are disposed within the legs 39 on the lower case 37 and are sealed by the antislip seats 41, such that they are invisible from the outside.

[0087] FIG. 8 shows a lateral cross section of another embodiment of the leg portion. The legs 39 are independent of the lower case 37 and are made of a material with a lower heat conductivity than that of the lower case 37, such as urethane rubber. The heat conductivity of the multiple legs 39 independent of the lower case 37 should preferably be of the order of 0.01 to 0.3 kcal/m.hr. $^{\circ}$ C., for example.

[0088] These legs block the transfer of heat from the apparatus-mount surface to the non-invasive blood sugar level measuring apparatus during the measurement of blood sugar levels, thereby improving the accuracy of measurement of blood sugar levels.

[0089] FIG. 9 shows the operation procedure for the apparatus. As a button in the operating portion is pressed and the apparatus is turned on, the message "WARMING UP" is displayed on the LCD, and the electronic circuitry in the apparatus is warmed up. Simultaneously, a checking program is activated, whereby the electronic circuitry is automatically checked. When the warm-up is completed, a message "PLACE FINGER" is displayed on the LCD. As the user places his or her finger on the finger rest portion, a countdown is displayed on the LCD. When the countdown is over, the LCD displays "LIFT FINGER." As the user lifts his or her finger from the finger rest portion, the LCD displays "DATA PROCESSING." Thereafter, a blood sugar level is displayed on the LCD, and the blood sugar level is stored in an IC card, together with the date and time. The user reads the blood sugar level that is being displayed and then presses a button in the operating portion. This causes the message "PLACE FINGER" to appear on the LCD approximately one minute later, indicating that the apparatus is ready for the next measurement.

[0090] FIG. 10 shows the details of the measurement portion. FIG. 10(a) is a top plan view, FIG. 10(b) is a cross section taken along line X-X of FIG. 10(a), and FIG. 10(c) is a cross section taken along Y-Y of FIG. 10(a).

[0091] First, temperature measurement by the non-invasive blood sugar level measuring apparatus according to the invention will be described. A thin plate 21 of a highly heat-conductive material, such as gold, is disposed on a portion where a measured portion (ball of the finger) is to come into contact. A bar-shaped heat-conductive member 22 made of a material with a heat conductivity lower than that of the plate 21, such as polyvinylchloride, is thermally connected to the plate 21 and extends into the apparatus. The temperature sensors include a thermistor 23, which is an adjacent-temperature detector with respect to the measured portion for measuring the temperature of the plate 21. There

is also a thermistor 24, which is an indirect-temperature detector with respect to the measured portion for measuring the temperature of a portion of the heat-conducting member away from the plate 21 by a certain distance. An infrared lens 25 is disposed inside the apparatus at such a position that the measured portion (ball of the finger) placed on the finger rest portion 15 can be seen through the lens. Below the infrared lens 25, there is disposed a pyroelectric detector 27 via an infrared radiation-transmitting window 26. Another thermistor 28 is disposed near the pyroelectric detector 27.

[0092] Thus, the temperature sensor portion of the measurement portion has four temperature sensors, and they measure four kinds of temperatures as follows:

[0093] (1) Temperature on the finger surface (thermistor 23): T_1 .

[0094] (2) Temperature of the heat-conducting member (thermistor 24): T_2 .

[0095] (3) Temperature of radiation from the finger (pyroelectric detector 27): T_3 .

[0096] (4) Room temperature (thermistor 28): T_4 .

[0097] The optical sensor portion 18 will be described. The optical sensor portion measures the hemoglobin concentration and hemoglobin oxygen saturation for obtaining the oxygen supply amount. For measuring the hemoglobin concentration and hemoglobin oxygen saturation, absorbance must be measured at at least two wavelengths. FIG. 10(c) shows an example of an arrangement for performing the two-wavelength measurement using two light sources 33 and 34 and one detector 35.

[0098] Inside the optical sensor portion 18, there are disposed the end portions of two optical fibers 31 and 32. The optical fiber 31 is for irradiating light, and the optical fiber 32 is for receiving light. As shown in FIG. 10(c), the optical fiber 31 is connected to branch fibers 31a and 31b at the ends of which light-emitting diodes 33 and 34 with two different wavelengths are provided. At the end of the optical fiber 32, there is provided a photodiode 35. The light-emitting diode 33 emits light of a wavelength 810 nm. The light-emitting diode 34 emits light of a wavelength 950 nm. The wavelength 810 nm is the isoabsorption wavelength at which the molar absorption coefficients of oxyhemoglobin and reduced hemoglobin (deoxyhemoglobin) are equal. The wavelength 950 nm is the wavelength at which the difference in molar absorption coefficients between theoxyhemoglobin and the reduced hemoglobin is large.

[0099] The two light-emitting diodes 33 and 34 emit light in a time-divided manner. The light emitted by the light-emitting diodes 33 and 34 is irradiated via the light-emitting optical fiber 31 onto the finger of the subject. The light with which the finger is irradiated is reflected by the finger skin, incident on the light-receiving optical fiber 32, and then detected by the photodiode 35. When the light with which the finger is irradiated is reflected by the finger skin, some of the light penetrates through the skin and into the tissue, and is then absorbed by the hemoglobin in the blood flowing in the capillary blood vessels. The measurement data obtained by the photodiode 35 is reflectance R, and the absorbance is approximated by $\log(1/R)$. Irradiation is conducted with light of the wavelengths 810 nm and 950 nm, and R is measured for each, and then $\log(1/R)$ is

calculated, thereby measuring absorbance A_1 for wavelength 810 nm and absorbance A_2 for wavelength 950 nm.

[0100] When the reduced hemoglobin concentration is $[Hb]$, and the oxyhemoglobin concentration is $[HbO_2]$, absorbance A_1 and A_2 are expressed by the following equations:

$$\begin{aligned} A_1 &= a \times ([Hb] \times A_{Hb}(810 \text{ nm}) + [HbO_2] \times A_{HbO_2}(810 \text{ nm})) \\ &= a \times ([Hb] \times HbO_2) \times A_{HbO_2}(810 \text{ nm}) \end{aligned}$$

$$\begin{aligned} A_2 &= a \times ([Hb] \times A_{Hb}(950 \text{ nm}) + [HbO_2] \times A_{HbO_2}(950 \text{ nm})) \\ &= a \times ([Hb] + [HbO_2]) \times \left(\left(1 - \frac{[HbO_2]}{[Hb] + [HbO_2]} \right) \times A_{Hb}(950 \text{ nm}) + \right. \\ &\quad \left. \frac{[HbO_2]}{[Hb] + [HbO_2]} \times A_{HbO_2}(950 \text{ nm}) \right) \end{aligned}$$

[0101] A_{Hb} (810 nm) and A_{Hb} (950 nm), and A_{HbO_2} (810 nm) and A_{HbO_2} (950 nm) are molar absorption coefficients of reduced hemoglobin and oxyhemoglobin, respectively, and are known at the respective wavelengths. Sign a is a proportional coefficient. Based on the above equations, the hemoglobin concentration $\{[Hb] + [HbO_2]\}$ and the hemoglobin oxygen saturation $\{[HbO_2]/([Hb] + [HbO_2])\}$ can be determined as follows:

$$\begin{aligned} [Hb] + [HbO_2] &= \frac{A_1}{a \times A_{HbO_2}(810 \text{ nm})} \\ \frac{[HbO_2]}{[Hb] + [HbO_2]} &= \frac{A_2 \times A_{HbO_2}(810 \text{ nm}) - A_1 \times A_{Hb}(950 \text{ nm})}{A_1 \times (A_{HbO_2}(950 \text{ nm}) - A_{Hb}(950 \text{ nm}))} \end{aligned}$$

[0102] While in the above example the hemoglobin concentration and hemoglobin oxygen saturation are measured by measuring absorbance at two wavelengths, it is possible to reduce the influence of interfering components and increase measurement accuracy by measuring at three or more wavelengths.

[0103] FIG. 11 is a conceptual chart illustrating the flow of data processing in the apparatus. The apparatus according to the present example is equipped with five sensors, namely thermistor 23, thermistor 24, pyroelectric detector 27, thermistor 28 and photodiode 35. The photodiode 35 measures the absorbance at wavelength 810 nm and the absorbance at wavelength 950 nm. Thus, six kinds of measurement values are fed to the apparatus.

[0104] Five kinds of analog signals are supplied via amplifiers A1 to A5 and digitally converted by analog/digital converters AD1 to AD5. Based on the digitally converted values, parameters x_i ($i=1, 2, 3, 4, 5$) are calculated. The following are specific descriptions of x_i (where a_1 to a_5 are proportionality coefficients):

[0105] Parameter proportional to heat radiation

$$x_1 = a_1 \times (T_3)^4$$

[0106] Parameter proportional to heat convection

$$x_2 = a_2 \times (T_4 - T_3)$$

[0107] Parameter proportional to hemoglobin concentration

$$x_3 = a_3 \left(\frac{A_1}{a \times A_{HbO_2}(810 \text{ nm})} \right)$$

[0108] Parameter proportional to hemoglobin oxygen saturation

$$x_4 = a_4 \times \left(\frac{A_2 \times A_{HbO_2}(810 \text{ nm}) - A_1 \times A_{Hb}(950 \text{ nm})}{A_1 \times (A_{HbO_2}(950 \text{ nm}) - A_{Hb}(950 \text{ nm}))} \right)$$

[0109] Parameter proportional to blood supply volume

$$x_5 = a_5 \times \left(\frac{1}{I_{CONT} \times (S_1 - S_2)} \right)$$

[0110] Then, normalized parameters are calculated from mean values and standard deviations of parameters x_i based on actual data from large numbers of able-bodied people and diabetic patients. A normalized parameter X_i (where $i=1, 2, 3, 4, 5$) is calculated from each parameter x_i according to the following equation:

$$X_i = \frac{x_i - \bar{x}_i}{SD(x_i)}$$

where

[0111] x_i : parameter

[0112] \bar{x}_i : mean value of the parameter

[0113] $SD(x_i)$: standard deviation of the parameter

[0114] Calculations are conducted to convert the above five normalized parameters into a glucose concentration to be eventually displayed. Programs necessary for computations are stored in the ROM built inside the microprocessor in the apparatus. Memory areas necessary for computations are ensured in a RAM built inside the apparatus. The results of the calculations are displayed on the LCD portion.

[0115] The ROM stores, as a constituent element of the program necessary for the computations, a function for determining glucose concentration C in particular. The function is defined as follows. C is expressed by a below-indicated equation (1), where a_i ($i=0, 1, 2, 3, 4, 5$) is determined from a plurality of pieces of measurement data in advance according to the following procedure:

[0116] (1) A multiple regression equation is created that indicates the relationship between the normalized parameter and the glucose concentration C .

[0117] (2) Normalized equations (simultaneous equations) relating to the normalized parameter are obtained from an equation obtained by the least-squares method.

[0118] (3) Values of coefficient a_i ($i=0, 1, 2, 3, 4, 5$) are determined from the normalized equation and then substituted into the multiple regression equation.

[0119] Initially, the regression equation (1) indicating the relationship between the glucose concentration C and the normalized parameters X_1, X_2, X_3, X_4 and X_5 is formulated.

$$C = f(X_1, X_2, X_3, X_4, X_5) \quad (1)$$

$$= a_0 + a_1 X_1 + a_2 X_2 + a_3 X_3 + a_4 X_4 + a_5 X_5$$

[0120] Then, the least-squares method is employed to obtain a multiple regression equation that would minimize the error with respect to a measured value C_i of glucose concentration according to an enzyme electrode method. When the sum of squares of the residual is D, D is expressed by the following equation (2):

$$D = \sum_{i=1}^n d_i^2 \quad (2)$$

$$= \sum_{i=1}^n (C_i - f(X_{i1}, X_{i2}, X_{i3}, X_{i4}, X_{i5}))^2$$

$$= \sum_{i=1}^n \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\}^2$$

[0121] The sum of squares of the residual D becomes minimum when partial differentiation of equation (2) with respect to a_0, a_2, \dots, a_5 gives zero. Thus, we have the following equations:

$$\frac{\partial D}{\partial a_0} = -2 \sum_{i=1}^n \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\} = 0 \quad (3)$$

$$\frac{\partial D}{\partial a_1} = -2 \sum_{i=1}^n X_{i1} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\} = 0$$

$$\frac{\partial D}{\partial a_2} = -2 \sum_{i=1}^n X_{i2} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\} = 0$$

$$\frac{\partial D}{\partial a_3} = -2 \sum_{i=1}^n X_{i3} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\} = 0$$

$$\frac{\partial D}{\partial a_4} = -2 \sum_{i=1}^n X_{i4} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\} = 0$$

$$\frac{\partial D}{\partial a_5} = -2 \sum_{i=1}^n X_{i5} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3} + a_4 X_{i4} + a_5 X_{i5})\} = 0$$

[0122] When the mean values of C and X_1 to X_5 are C_{mean} and $X_{1\text{mean}}$ to $X_{5\text{mean}}$, respectively, since $X_{i\text{mean}}=0$ ($i=1$ to 5), equation (1) yields equation (4) thus:

$$a_0 = C_{\text{mean}} - a_1 X_{1\text{mean}} - a_2 X_{2\text{mean}} - a_3 X_{3\text{mean}} - a_4 X_{4\text{mean}} - a_5 X_{5\text{mean}} \quad (4)$$

$$= C_{\text{mean}}$$

[0123] The variation and covariation between the normalized parameters are expressed by equation (5). Covariation between the normalized parameter X_i ($i=1$ to 5) and C is expressed by equation (6).

$$S_{ij} = \sum_{k=1}^n (X_{ki} - X_{i\text{mean}})(X_{kj} - X_{j\text{mean}}) = \sum_{k=1}^n X_{ki} X_{kj} \quad (5)$$

$(i, j = 1, 2, \dots, 5)$

$$S_{iC} = \sum_{k=1}^n (X_{ki} - X_{i\text{mean}})(C_k - C_{\text{mean}}) = \sum_{k=1}^n X_{ki} (C_k - C_{\text{mean}}) \quad (6)$$

$(i = 1, 2, \dots, 5)$

[0124] Substituting equations (4), (5), and (6) into equation (3) and rearranging yields simultaneous equations (normalized equations) (7). Solving equations (7) yields a_1 to a_5 .

$$a_1 S_{11} + a_2 S_{12} + a_3 S_{13} + a_4 S_{14} + a_5 S_{15} = S_{1C}$$

$$a_1 S_{21} + a_2 S_{22} + a_3 S_{23} + a_4 S_{24} + a_5 S_{25} = S_{2C}$$

$$a_1 S_{31} + a_2 S_{32} + a_3 S_{33} + a_4 S_{34} + a_5 S_{35} = S_{3C}$$

$$a_1 S_{41} + a_2 S_{42} + a_3 S_{43} + a_4 S_{44} + a_5 S_{45} = S_{4C}$$

$$a_1 S_{51} + a_2 S_{52} + a_3 S_{53} + a_4 S_{54} + a_5 S_{55} = S_{5C} \quad (7)$$

[0125] Constant term a_0 is obtained by means of equation (4). The thus obtained a_i ($i=0, 1, 2, 3, 4, 5$) is stored in ROM at the time of manufacture of the apparatus. In actual measurement using the apparatus, the normalized parameters X_1 to X_5 obtained from the measured values are substituted into regression equation (1) to calculate the glucose concentration C.

[0126] Hereafter, an example of the process of calculating the glucose concentration will be described. The coefficients in equation (1) are determined in advance based on a large quantity of data obtained from able-bodied persons and diabetic patients. The ROM in the microprocessor stores the following formula for the calculation of glucose concentration:

$$C = 99.4 + 18.3 \times X_1 - 20.2 \times X_2 - 23.7 \times X_3 - 22.0 \times X_4 - 25.9 \times X_5$$

[0127] X_1 to X_5 are the results of normalization of parameters x_1 to x_5 . Assuming the distribution of the parameters is normal, 95% of the normalized parameters take on values between -2 and +2.

[0128] In an example of measured values for an able-bodied person, substituting normalized parameters $X_1=-0.06$, $X_2=+0.04$ and $X_3=+0.05$, $X_4=-0.12$ and $X_5=+0.10$ in the above equation yields $C=96$ mg/dL. In an example of measured values for a diabetic patient, substituting normal-

ized parameters $X_1=+1.15$, $X_2=-0.02$, $X_3=-0.83$, $X_4=-0.91$ and $X_5=-1.24$ in the equation yields $C=213$ mg/dL.

[0129] Hereafter, the results of measurement by the conventional enzymatic electrode method and those by the embodiment of the invention will be described. In the enzymatic electrode method, a blood sample is reacted with a reagent and the amount of resultant electrons is measured to determine blood sugar level. When the glucose concentration was 89 mg/dL according to the enzymatic electrode method in an example of measured values for an able-bodied person, substituting the normalized parameters $X_1=-0.06$, $X_2=+0.04$, $X_3=+0.05$, $X_4=-0.12$ and $X_5=+0.10$ obtained by measurement at the same time according to the inventive method into the above equation yielded $C=96$ mg/dL. Further, when the glucose concentration was 238 mg/dL according to the enzymatic electrode method in an example of measurement values for a diabetic patient, substituting the normalized parameters $X_1=+1.15$, $X_2=-1.02$, $X_3=-0.83$, $X_4=-0.91$ and $X_5=-1.24$ obtained by measurement at the same time according to the inventive method into the above equation yielded $C=213$ mg/dL. From the above results, it has been confirmed that the glucose concentration can be accurately determined using the method of the invention.

[0130] FIG. 12 shows a chart plotting on the vertical axis the values of glucose concentration calculated by the inventive method and on the horizontal axis the values of glucose concentration measured by the enzymatic electrode method, based on measurement values obtained from a plurality of patients. A good correlation is obtained by measuring the oxygen supply amount and blood flow volume according to the invention (correlation coefficient=0.9324).

[0131] In the above-described embodiment, the parameters relating to blood hemoglobin concentration and blood hemoglobin oxygen saturation are obtained by spectroscopically measuring the hemoglobin in blood. However, the hemoglobin concentration is stable in persons without such symptoms as anemia, bleeding or erythrocytosis. The hemoglobin concentration is normally in the range between 13 and 18 g/dL for males and between 12 and 17 g/dL for females, and the range of variation of hemoglobin concentration from the normal values is 5 to 6%. Further, the weight of the term relating to the blood flow volume in the aforementioned formula for calculating blood sugar level is smaller than the other terms. Therefore, the hemoglobin concentration can be treated as a constant without greatly lowering the measurement accuracy. Similarly, the hemoglobin oxygen saturation is stable between 97 to 98% if the person is undergoing aerial respiration at atmospheric pressure, at rest and in a relaxed state. Thus the hemoglobin concentration and the hemoglobin oxygen saturation can be treated as constants, and the oxygen supply amount can be determined from the product of the hemoglobin concentration constant, the hemoglobin oxygen saturation constant and the blood flow volume.

[0132] By treating the hemoglobin concentration and hemoglobin oxygen saturation as constants, the sensor arrangement for measuring blood sugar level can be simplified by removing the optical sensors, for example. Further, by eliminating the time necessary for optical measurement and the processing thereof, the procedure for blood sugar level measurement can be accomplished in less time.

[0133] Because the hemoglobin oxygen saturation takes on a stable value when at rest, in particular, by treating the

hemoglobin concentration and hemoglobin oxygen saturation as constants, the measurement accuracy for blood sugar level measurement when at rest can be increased, and the procedure of blood sugar level measurement can be accomplished in less time. By "when at rest" herein is meant the state in which the test subject has been either sitting on a chair or lying and thus moving little for approximately five minutes.

[0134] Hereafter, an embodiment will be described in which the blood hemoglobin concentration and blood hemoglobin oxygen saturation are treated as constants. This embodiment is similar to the above-described embodiment except that the blood hemoglobin concentration and blood hemoglobin oxygen saturation are treated as constants, and therefore the following description mainly concerns the differences from the earlier embodiment.

[0135] In the present embodiment, the hemoglobin concentration and hemoglobin oxygen saturation shown in FIG. 4 are not measured but treated as constants. Therefore, as shown in FIG. 13, the measurement portion of the present embodiment has the structure of the measurement portion of the earlier embodiment shown in FIG. 10 from which the light sources 33 and 34, photodiode 35 and optical fibers 31 and 32 have been removed. The apparatus chassis comprises a structure on the bottom surface thereof for blocking the transfer of heat from the apparatus mount surface to the apparatus, similar to the one described with reference to FIGS. 6 to 8. The parameters used in the present embodiment are parameter x_1 proportional to heat radiation, parameter x_2 proportional to heat convection, and parameter x_3 proportional to the oxygen supply amount (hereafter, parameter proportional to oxygen supply amount will be indicated as x_3). From these parameters, normalized parameters are calculated in the manner described above, and a glucose concentration is calculated based on the three normalized parameters X_i ($i=1, 2, 3$). During data processing, the step "CONVERSION OF OPTICAL MEASUREMENT DATA INTO NORMALIZED PARAMETERS" (see FIG. 11), which is necessary in the previous embodiment, can be omitted.

[0136] FIG. 14 shows a functional block diagram of the apparatus according to the embodiment. The apparatus runs on battery 51. Signals measured by sensor portion 53 including a temperature sensor are fed to analog/digital converters 54 (AD1 to AD4) provided for individual signals and are converted into digital signals. Analog/digital converters AD1 to AD4, LCD 13 and RAM 52 are peripheral circuits for microprocessor 55. They are accessed by the microprocessor 55 via bus line 56. The push buttons 11a to 11d are connected to the microprocessor 55. The microprocessor 55 includes a ROM for storing software. By pressing the buttons 11a to 11d, external instructions can be entered into the microprocessor 55.

[0137] The ROM 57 included in the microprocessor 55 stores a program necessary for computations, i.e., it has the function of an arithmetic or calculating unit. The microprocessor 55 further includes a hemoglobin concentration constant storage portion 58 for storing hemoglobin concentration constants, and a hemoglobin oxygen saturation constant storage portion 59 for storing hemoglobin oxygen saturation constants. After the measurement of the finger is finished, the computing program calls optimum constants from the

hemoglobin concentration storage portion **58** and hemoglobin oxygen saturation constant storage portion **59** and perform calculations. A memory area necessary for computations is ensured in the RAM **52** similarly incorporated into the apparatus. The result of computations is displayed on the LCD portion.

[0138] The ROM stores, as a constituent element of the program necessary for the computations, a function for determining glucose concentration C in particular. The function is defined as follows. C is expressed by a below-indicated equation (8), where as (i=0, 1, 2, 3) is determined from a plurality of pieces of measurement data in advance according to the following procedure:

[0139] (1) A multiple regression equation is created that indicates the relationship between the normalized parameter and the glucose concentration C.

[0140] (2) Normalized equations (simultaneous equations) relating to the normalized parameter are obtained from an equation obtained by the least-squares method.

[0141] (3) Values of coefficient a_i (i=0, 1, 2, 3) are determined from the normalized equation and then substituted into the multiple regression equation.

[0142] Initially, the regression equation (8) indicating the relationship between the glucose concentration C and the normalized parameters X_1 , X_2 and X_3 is formulated.

$$\begin{aligned} C &= f(X_1, X_2, X_3) \\ &= a_0 + a_1 X_1 + a_2 X_2 + a_3 X_3 \end{aligned} \quad (8)$$

[0143] Then, the least-squares method is employed to obtain a multiple regression equation that would minimize the error with respect to a measured value C_i of glucose concentration according to an enzyme electrode method. When the sum of squares of the residual is D, D is expressed by the following equation (9):

$$\begin{aligned} D &= \sum_{i=1}^n d_i^2 \\ &= \sum_{i=1}^n (C_i - f(X_{i1}, X_{i2}, X_{i3}))^2 \\ &= \sum_{i=1}^n \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3})\}^2 \end{aligned} \quad (9)$$

[0144] The sum of squares of the residual D becomes minimum when partial differentiation of equation (9) with respect to a_0 to a_3 gives zero. Thus, we have the following equations:

$$\frac{\partial D}{\partial a_0} = -2 \sum_{i=1}^n \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3})\} = 0 \quad (10)$$

-continued

$$\frac{\partial D}{\partial a_1} = -2 \sum_{i=1}^n X_{i1} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3})\} = 0$$

$$\frac{\partial D}{\partial a_2} = -2 \sum_{i=1}^n X_{i2} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3})\} = 0$$

$$\frac{\partial D}{\partial a_3} = -2 \sum_{i=1}^n X_{i3} \{C_i - (a_0 + a_1 X_{i1} + a_2 X_{i2} + a_3 X_{i3})\} = 0$$

[0145] When the mean values of C and X_1 to X_3 are C_{mean} and $X_{1\text{mean}}$ to $X_{3\text{mean}}$, respectively, since $X_{i\text{mean}}=0$ (i=1 to 3), equation (8) yields equation (11) thus:

$$a_0 = C_{\text{mean}} - a_1 X_{1\text{mean}} - a_2 X_{2\text{mean}} - a_3 X_{3\text{mean}} = C_{\text{mean}} \quad (11)$$

[0146] The variation and covariation between the normalized parameters are expressed by equation (12). Covariation between the normalized parameter X_i (i=1 to 3) and C is expressed by equation (13).

$$S_{ij} = \sum_{k=1}^n (X_{ki} - X_{i\text{mean}})(X_{kj} - X_{j\text{mean}}) = \sum_{k=1}^n X_{ki} X_{kj} \quad (12)$$

$$(i, j = 1, 2, 3)$$

$$S_{iC} = \sum_{k=1}^n (X_{ki} - X_{i\text{mean}})(C_k - C_{\text{mean}}) = \sum_{k=1}^n X_{ki}(C_k - C_{\text{mean}}) \quad (13)$$

$$(i = 1, 2, 3)$$

[0147] Substituting equations (11), (12), and (13) into equation (10) and rearranging yields simultaneous equations (normalized equations) (14). Solving equations (14) yields a_1 to a_3 .

$$\begin{aligned} a_1 S_{11} + a_2 S_{12} + a_3 S_{13} &= S_{1C} \\ a_1 S_{21} + a_2 S_{22} + a_3 S_{23} &= S_{2C} \\ a_1 S_{31} + a_2 S_{32} + a_3 S_{33} &= S_{3C} \end{aligned} \quad (14)$$

[0148] Constant term a_0 is obtained by means of equation (11). The thus obtained a_i (i=0, 1, 2, 3) is stored in ROM at the time of manufacture of the apparatus. In actual measurement using the apparatus, the normalized parameters X_1 to X_3 obtained from the measured values are substituted into regression equation (8) to calculate the glucose concentration C.

[0149] Hereafter, an example of the process of calculating the glucose concentration will be described. The coefficients in equation (8) are determined in advance based on a large quantity of data obtained from able-bodied persons and diabetic patients. The ROM in the microprocessor stores the following formula for the calculation of glucose concentration:

$$C = 101.7 + 25.8 \times X_1 - 23.2 \times X_2 - 12.9 \times X_3$$

[0150] X_1 to X_3 are the results of normalization of parameters x_1 to x_3 . Assuming the distribution of the parameters is normal, 95% of the normalized parameters take on values between -2 and +2.

[0151] In an example of measured values for an able-bodied person, substituting normalized parameters $X_1 = -0.06$, $X_2 = +0.04$ and $X_3 = +0.10$ in the above equation yields $C = 101$ mg/dL. In an example of measured values for a diabetic patient, substituting normalized parameters $X_1 = +1.35$, $X_2 = -1.22$ and $X_3 = -1.24$ in the equation yields $C = 181$ mg/dL. In the above equation, the hemoglobin concentration and hemoglobin oxygen saturation are rendered into constants of 15 g/dL and 97%, respectively.

[0152] Hereafter, the results of measurement by the conventional enzymatic electrode method and those by the embodiment of the invention will be described. In the enzymatic electrode method, a blood sample is reacted with a reagent and the amount of resultant electrons is measured to determine the blood sugar level. When the glucose concentration was 93 mg/dL according to the enzymatic electrode method in an example of measured values for an able-bodied person, substituting normalized parameters $X_1 = -0.06$, $X_2 = +0.04$ and $X_3 = +0.10$ obtained by measurement at the same time according to the inventive method into the above equation yielded $C = 101$ mg/dL. Further, when the glucose concentration was 208 mg/dL according to the enzymatic electrode method in an example of measurement values for a diabetic patient, substituting the normalized parameters $X_1 = +1.35$, $X_2 = -1.22$ and $X_3 = -1.24$ obtained by measurement at the same time according to the inventive method into the above equation yielded $C = 181$ mg/dL. Although the calculation results indicate an error of about 13%, this level of accuracy is considered sufficient because normally errors between 15% and 20% are considered acceptable in blood sugar level measuring apparatuses in general. Thus, it has been confirmed that the method of the invention can allow glucose concentrations to be determined with high accuracy.

[0153] FIG. 15 shows a chart plotting on the vertical axis the values of glucose concentration calculated by the inventive method and on the horizontal axis the values of glucose concentration measured by the enzymatic electrode method, based on measurement values obtained from a plurality of patients. A good correlation is obtained by measuring according to the invention (correlation coefficient=0.8932).

What is claimed is:

1. A blood sugar level measuring apparatus comprising:

a heat amount measurement portion for measuring a plurality of temperatures derived from a body surface and obtaining information used for calculating the amount of heat transferred by convection and the amount of heat transferred by radiation, both related to the dissipation of heat from said body surface;

an oxygen amount measuring portion for obtaining information about blood oxygen amount;

a storage portion for storing a relationship between parameters individually corresponding to said plurality of temperatures and blood oxygen amount and blood sugar levels;

a calculating portion which converts a plurality of measurement values fed from said heat amount measuring portion and said oxygen amount measurement portion into said parameters, and which computes a blood sugar level by applying said parameters to said relationship stored in said storage portion;

a display portion for displaying the blood sugar level calculated by said calculating portion; and

an apparatus chassis, wherein

said oxygen-amount measuring portion comprises a blood flow volume measuring portion for obtaining information about the volume of blood flow, and an optical measuring portion for obtaining hemoglobin concentration and hemoglobin oxygen saturation in blood,

said blood flow volume measuring portion comprises a body-surface contact portion, an adjacent-temperature detector disposed adjacent to said body-surface contact portion, an indirect-temperature detector for detecting the temperature at a position spaced away from said body-surface contact portion, and a heat-conducting member connecting said body-surface contact portion and said indirect-temperature detector, and

said apparatus chassis comprises a plurality of legs on a bottom surface thereof for supporting itself.

2. The blood sugar level measuring apparatus according to claim 1, wherein said legs are made of a material with a smaller heat conductivity than that of said chassis.

3. The blood sugar level measuring apparatus according to claim 1, wherein the sum of the cross-sectional areas of said plurality of legs at said bottom surface of said chassis is not more than one tenth of the area of said bottom surface of said chassis.

4. The blood sugar level measuring apparatus according to claim 1, wherein said legs have a length of not less than 1 mm.

5. A blood sugar level measuring apparatus comprising:

an ambient temperature measuring device for measuring ambient temperature;

a body-surface contact portion to which a body surface is brought into contact;

an adjacent-temperature detector disposed adjacent to said body-surface contact portion;

a radiant heat detector for measuring radiant heat from said body surface;

a heat conducting member disposed in contact with said body-surface contact portion;

an indirect-temperature detector disposed at a position that is adjacent to said heat conducting member and that is spaced apart from said body-surface contact portion, said indirect-temperature detector measuring temperature at the position spaced apart from said body-surface contact portion;

a light source for irradiating said body-surface contact portion with light of at least two different wavelengths;

a photodetector for detecting reflected light produced as said light is reflected by said body surface;

a calculating portion including a converting portion for converting outputs from said adjacent-temperature detector, said indirect-temperature detector, said ambient temperature detector, said radiant temperature detector and said photodetector, into parameters, and a processing portion in which a relationship between said parameters and blood sugar levels is stored in advance

and which calculates a blood sugar level by applying said parameters to said relationship;

a display for displaying the blood sugar level outputted from said calculating portion; and

an apparatus chassis, wherein said chassis comprises a plurality of legs on a bottom surface thereof for supporting itself.

6. The blood sugar level measuring apparatus according to claim 5, wherein said legs are made of a material with a smaller heat conductivity than that of said chassis.

7. The blood sugar level measuring apparatus according to claim 5, wherein the sum of the cross-sectional areas of said plurality of legs at said bottom surface of said chassis is not more than one tenth of the area of said bottom surface of said chassis.

8. The blood sugar level measuring apparatus according to claim 5, wherein said legs have a length of not less than 1 mm.

9. A blood sugar level measuring apparatus comprising:

an ambient temperature measuring device for measuring ambient temperature;

a body-surface contact portion to which a body surface is brought into contact;

an adjacent-temperature detector disposed adjacent to said body-surface contact portion;

a radiant heat detector for measuring radiant heat from said body surface;

a heat conducting member disposed in contact with said body-surface contact portion;

an indirect-temperature detector disposed at a position that is adjacent to said heat conducting member and that is spaced apart from said body-surface contact

portion, said indirect-temperature detector measuring temperature at the position spaced apart from said body-surface contact portion;

a storage portion where information about blood hemoglobin concentration and blood hemoglobin oxygen saturation is stored;

a calculating portion including a converting portion for converting outputs from said adjacent-temperature detector, said indirect-temperature detector, said ambient temperature measuring device and said radiant heat detector, into a plurality of parameters, and a processing portion in which a relationship between said parameters and blood sugar levels is stored in advance and which calculates a blood sugar level by applying said parameters to said relationship;

a display for displaying the blood sugar level outputted from said calculating portion; and

an apparatus chassis, wherein said chassis comprises a plurality of legs on a bottom surface thereof for supporting itself.

10. The blood sugar level measuring apparatus according to claim 9, wherein said legs are made of a material with a smaller heat conductivity than that of said chassis.

11. The blood sugar level measuring apparatus according to claim 9, wherein the sum of the cross-sectional areas of said plurality of legs at said bottom surface of said chassis is not more than one tenth of the area of said bottom surface of said chassis.

12. The blood sugar level measuring apparatus according to claim 9, wherein said legs have a length of not less than 1 mm.

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专利名称(译)	血糖水平测量仪		
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摘要(译)

基于温度测量，非侵入地测量血糖水平。通过血氧饱和度和血流量校正通过温度测量方案获得的非侵入性测量的血糖水平值，从而稳定测量数据。

