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(54) **IMAGING CATHETER WITH INTEGRATED REFERENCE REFLECTOR**

BILDGEBUNGSKATHETER MIT INTEGRIERTEM REFERENZREFLEKTOR

CATHÉTER D'IMAGERIE AVEC RÉFLECTEUR DE RÉFÉRENCE INTÉGRÉ

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Description

Field of Invention

[0001] This invention relates to optical imaging, and more specifically to the design of fiber optic probes for optical coherence tomography (OCT) and related imaging techniques.

Background

[0002] Optical interference is a phenomena used widely throughout the sciences. In particular, the use of short-coherence (or 'low-coherence') interferometric imaging has become an important imaging modality in several fields and notably in medical applications. In interferometric imaging, light from a known and controlled optical path (the 'reference path') is caused to interfere with light returned from an unknown path such that information about this unknown path (the 'sample path') may be determined by an analysis of the resulting interferogram.

[0003] In short-coherence imaging, the interferogram contains the depth location information of structures within the sample being analyzed. Scanning short-coherence light over a sample volume to produce tomographic images is known as Optical Coherence Tomography, or OCT. In recent years, practical laser-based light sources with coherence lengths of 20 μm or less have become available, promoting the use of OCT in several fields including ophthalmology, general microscopy, cardiology and oncology.

[0004] A particular advantage of OCT is its inherent compatibility with fiber optics making it a nearly ideal imaging modality for non-invasive or minimally invasive medical procedures.

[0005] Central to all OCT implementations is the requirement that the lengths of the sample and reference paths be matched to ensure the interference effect being recorded corresponds to a desired scan region within the sample. In the case of relatively long optical catheters required in many procedures (approximately 1.5 to 2 meters is common) this requirement for matching the path lengths may become difficult to achieve, especially when many practical implementations of OCT require matching on the millimeter scale. Furthermore, the very thin fibers used in these catheters can easily stretch or contract several millimeters during use.

[0006] When using OCT in any application, the optical 'zero-point' is critical. This defines where, in the image space, the so-called reference plane exists. By convention, surface planes are in the x-y plane, and the depth occurs along the z-axis. In a microscope application for example, it may be beneficial to set the zero point at the surface of the microscope slide, so specimens can be measured against this known surface. In a catheter inserted into a bodily lumen, the most useful reference plane is the outer surface of the catheter tip itself, and all distances are measured outward from this location.

[0007] For a rotating catheter, the x-y-z space is best represented in polar coordinates (angle and radial distance). Hence the z-axis becomes the radial distance from the center. Practically, setting a match point means that the optical length from the chosen reference plane in the sample is equal to the primary optical length in the reference arm. The high speed changing of the reference arm length in scanning represents only a small variation on the primary length. Because OCT penetrates tissue only a few millimeters at most, the scan is practically limited to typically 1-5 mm, whereas the actual lengths of the sample and reference arms may be several meters.

[0008] For example, in the case of optical catheters used in cardiology, the instrument itself will be located outside the nominal 'sterile field' surrounding the patient, the catheter itself will be inside this field, and an umbilical will be used to join the two. The total optical length of the sample arm (catheter plus umbilical) can easily approach 5 meters, which will also be the primary length of the reference arm. Since scanning will be perhaps 5 mm, this represents 0.1% of the total length. Measurement accuracy is required to be 0.1 mm or better in this application. Since it is not cost-effective to control the lengths of each optical fiber within the catheter and umbilical to sub-millimeter dimensions, most design approaches use an adjustable reference path within the optical imaging equipment to adjust to each catheter as it is used.

[0009] However, a medical application may use many disposable catheters per day; all interfaced to the same imaging equipment. Thus, while the primary path length adjustment can work quite effectively, it usually requires an initial adjustment by a skilled operator who understands the optical reflection pattern or 'signature' of the catheters that will be recorded by OCT to determine how to adjust the reference path to coincide with the outer surface of the catheter tip. Again, the adjustment of the image zero-point, or reference plane location is performed by adjusting the primary path-length of the reference arm. This adjustment is often termed 'z-offset' of the reference arm and is controlled via a motor, called simply the z-offset motor. By convention, the instrument z-offset is zero when the sample arm length (catheter) is manufactured exactly as designed; is negative when the catheter is too short; and positive when the catheter is too long.

[0010] These optical catheters typically have a lens and reflector structure placed at their distal tip to focus and direct the light for scanning purposes. The light typically propagates through one or more transparent sheaths that comprise the catheter outer structure. Each of the interfaces can and will cause a reflection that will be detected by OCT. Hence, it may be challenging to determine which of those reflections corresponds to the desired optical reference point ('zero-point') of the system. Since measurements are made based on this zero-point setting, setting it correctly can have significant importance in medical applications. Furthermore, because there may be several closely spaced and similar intensity

reflections, the use of software to detect the proper zero-offset ('z-offset') is extremely problematic and unreliable.

[0011] As noted, the optical fiber can stretch significantly on these scales when the catheter is advanced or retracted. For example, using the known yield strength of standard optical fibers used in OCT, and the catheter length, it is easy to show that 10 mm of stretch can occur before the fiber breaks. Typical forces encountered in real situations will only cause a 1 mm stretch or less, but many medical measurements require accuracy of ¼ millimeter or better.

[0012] Therefore, a simple, cost effective method for reliably determining the optical match point ('zero-point') of the catheter is needed. Furthermore, this method should be compatible with real-time video rate imaging so that the zero-point can be tracked as the catheter is maneuvered, retracted or advanced. The present invention addresses these issues.

[0013] US 2006/264743 discloses a method for tomographically displaying a cavity by optical coherence tomography. An OCT device is disclosed comprising a scanning head provided at the distal end of a catheter. The outer edge of the catheter is reproduced by a concentric ring in the OCT image. The diameter of the ring is determined to calibrate the tomographic image.

Summary of the Invention

[0014] The invention provides an imaging probe as set out in claim 1.

[0015] In embodiments, the cover of the probe tip may be a membrane having a first surface and a second surface. The membrane includes a polymer and a plurality of back-scattering particles for controlled optical back-scattering disposed therein. Further, the membrane allows transmission of substantially undistorted imaging light.

[0016] In one embodiment, the membrane is shaped to form a curved surface suitable for engulfing, surrounding, enveloping or otherwise covering an optical fiber endface or micro-lens.

[0017] The particle dimension, in some preferred embodiments, is less than about 1.5 µm. Further, the particles can include titanium, zinc, aluminum, and/or other materials suitable for scattering light. The plurality of scattering elements can have a concentration of about 0.1% doping concentration by volume. The imaging probe further includes an elongate section, wherein the membrane is shaped to form a sheath within which the elongate section is disposed to form a portion of a probe tip.

[0018] Embodiments also relate to an imaging probe. The probe includes an elongate section having a first end and a second end; the second end forming a probe tip capable of intra-lumen imaging, the probe tip comprising a scattering material, the elongate section adapted to transmit light reflected by the scattering material to the first end of the elongate section.

[0019] In one embodiment, the elongate section is an

optical fiber. The elongate section can be a sheath. Also, the probe can further include an optical fiber disposed within the sheath. The scattering material can include a plurality of light scattering particles dispersed in a matrix.

5 The scattering particles can include titanium and/or other materials known to scatter light. Also, the matrix can include polyethylene terephthalate and/or other polymers.

[0020] In embodiments, the imaging probe may further comprise

10 a lens assembly. The lens assembly includes a micro-lens; a beam director in optical communication with the micro-lens; and the cover may be a substantially transparent film. The substantially transparent film is capable of bi-directionally transmitting light, and generating a controlled amount of backscatter. In addition, the film surrounds a portion of the beam director.

[0021] In one embodiment, the controlled amount of backscatter is in an amount of light at least sufficient to generate a reference point in an imaging system for calibration of at least one imaging system parameter. The substantially transparent film includes a plurality of scattering particles. The micro-lens can be in optical communication with an optical fiber. Further, the substantially transparent film can be shaped to form an imaging probe tip. Also, the probe tip can be used for optical coherence tomography imaging.

[0022] Embodiments also relate to a method of calibrating an optical coherence tomography system comprising an imaging probe as set out in claim 1. system. The method includes generating scan data in response to light reflected from a sample, the reflected light passing through the cover; generating reference data in response to scattered light reflected from the back-scattering particles disposed within the cover; and calibrating the optical coherence tomography system to determine the relative position of subsequent scans in response to the reference data.

[0023] In one embodiment, scan data includes a set of angles and a set of radial distances. Further, the reference data can include a set of angles and a set of radial distances. The step of calibrating can include searching for a ring pattern within the reference data.

[0024] The disclosure also relates to a method of fabricating an optical element. The method includes selecting a membrane material suitable for intra-lumen use in an animal; selecting a dopant suitable for dispersion in the membrane material, the dopant adapted to scatter light in response to an optical source; determining a dopant volume concentration such that a radial scan of a doped membrane generates a defined pattern; doping the membrane with the selected dopant to substantially obtain the determined dopant volume concentration; and shaping the membrane for intra-lumen use in an animal.

55 **[0025]** The membrane may include polyethylene terephthalate. The dopant volume concentration can include about 0.1% doping concentration by volume. The selected dopants can include an oxide. Further, the de-

fined pattern can be selected from the group consisting of a ring and a spiral.

Brief Description of the Drawings

[0026]

Fig. 1 is a block diagram of an OCT system suitable for use with the optical probe of the invention;

Fig. 2 is a schematic diagram of an optical catheter system, suitable for use with OCT imaging in coronary arteries;

Fig. 3 is a schematic diagram of the optical fiber tip, with micro lens and protective cover;

Fig. 3a is a photomicrograph of an embodiment of the probe shown schematically in Fig. 3.

Figs. 4a and 4b depict an image taken with a doped plastic lens cover and an undoped plastic (such as PET) cover, respectively;

Fig. 4c depicts an OCT image in which an over-concentration of the dopant TiO_2 is used and the resulting clumping leads to optical shadowing;

Figure 5a depicts a frequency domain OCT image with proper scan line orientation and detected PET reflection indicated by a hashed line.

Figure 5b depicts a frequency domain OCT image with inverted scan line orientation (or inversion state) and detected PET reflection indicated by a hashed line.

Fig. 6 is a flow chart of an embodiment of an algorithm used to detect the PET ring;

Fig. 7 is a flow chart of an embodiment of an algorithm used to set the location of the PET ring;

Fig. 8 depicts an image of a coronary artery made using the components in Figs 1 and 2 in which the zero-point offset is set correctly;

Fig. 9 depicts an image of a coronary artery made using the components in Figs 1 and 2 in which the zero-point offset is set incorrectly (the zero-point is too short and has been moved within the optical fiber causing the image to expand away from the center);

Fig. 10 depicts an image of a coronary artery made using the components in Figs 1 and 2 in which the zero-point offset is set incorrectly (the zero-point is too long and has moved to a point outside the fiber, causing the image to contract towards the center); and

Fig. 11 depicts a magnified OCT image of a catheter center showing characteristic ring reflections according to an embodiment of the invention

Detailed Description of the Preferred Embodiment

[0027] In brief overview and referring to Fig. 1, a generalized OCT interferometer 10 is shown which is suitable for use with the catheter imaging system of the invention. A light source 14, such as a diode laser, produces short-coherence length light that passes by way of an optical

fiber 18 into an optical fiber coupler 22. Light entering the coupler 22 is the split along two optical fiber paths 26 and 30. One path 26 terminates at a movable reflector 34, while the other enters a probe 38 and is emitted toward an object of interest 42.

[0028] Light reflected by the movable reflector 34 passes back along optical fiber 26 to the coupler 22. Similarly light reflected by the object of interest 42 passes back along optical fiber 30 to the coupler 22 and combines with the light reflected by the movable reflector 34 to form an interference pattern. This combined light passes through optical fiber 46 and is detected by a detector 50. The output signal from the detector 50 is processed by electronics 54 and an image formed on display 58.

[0029] An example of an imaging catheter suitable for use as the probe in Fig. 1 is shown in Fig. 2. In this embodiment, the imaging probe 38 is the tip of a coronary vessel imaging catheter. A connector 62 attaches to the optical coupler 22 of the system of Fig. 1. The optical fiber 30 enters a y-body connector 66 attached to a balloon catheter 70. This catheter 70 includes a flushing port 74 and a balloon inflation port 78 as well as a flush exit 82.

[0030] Fig. 3 depicts an embodiment of the image wire tip of the probe 38. The optical fiber 30 terminates in a micro-lens assembly 86 which focuses the light at a distance from the micro-lens assembly 86. Light emitted from the micro-lens assembly 86 is reflected by a beam deflector 90 so as to pass at substantially right angles to the optical axis of the fiber 30. The entire fiber assembly is covered by a protective transparent sheath 94 sealed at one end 98 as discussed below.

[0031] As explained in US patent 6,891,894, a particularly advantageous fiber lens design uses total internal reflection from a silica-air interface to provide the needed radial scan inside a lumen, such as an artery, by simply rotating the fiber. Since the total internal reflection depends on the refractive index mismatch between the silica and air, direct immersion in a fluid will eliminate this reflection and the light will propagate forward instead, destroying the ability to take useful radial scan. As shown in the '894 patent and in Figs. 3 and 3a, the air-silica interface can be preserved by using a clear protective cover 94 adhered directly to the fiber lens assembly. Such a cover can be made preferably from a heat-shrinkable material such as polyester (Polyethylene Terephthalate, or PET). PET is widely used in industry and medical devices and has good biomedical compatibility properties.

[0032] Such a PET cover has inherent low back-reflection, so in its usual format it is unsuitable for the purpose of providing a fixed reference reflection. However, with care, dopants can be added to the raw PET material (before the tube shape is formed) increasing the native back-reflection.

[0033] Several materials exist as a suitable dopant. In particular titanium dioxide (TiO_2) is advantageous. TiO_2 is used in many paint formulations due to its excellent light scattering properties. Further it is inert and can be made in bulk. The particle size can be made much smaller

than the optical wavelengths of interest (nominally 1.3 μm), making the scattering 'Rayleigh' in nature. Thus the outgoing and returning light wavefronts are not appreciably disturbed, thereby minimizing any potential image degradation at sufficiently low concentrations of dopant.

[0034] A key step in the creation of the material is uniformly mixing TiO_2 particles in the raw PET such that, when drawing the PET into tubing, the correct concentration is realized with high uniformity. In addition, because OCT imaging has tremendous sensitivity and large dynamic range (typically 100 dB of sensitivity and >60 dB of dynamic range can be achieved in practical instruments) care must be used to calculate then achieve the optimal doping level of TiO_2 in the material.

[0035] Basic scattering theory can be used to arrive at a doping concentration in the material. In a typical OCT image in the coronary arteries, the minimum noise in the instrument is about -100 dB. That is, about 1 ten-billionth of the optical output power applied to the object of interest and a typical image has approximately 40 dB of useful dynamic range. The image processing electronics and software are optimized for this range, so the probe reflector element should be optimized to be near the maximum detectable peak of the image intensity, which is about -60dB (-100 + 40). This means that the probe reflector should be the brightest object in the image.

[0036] As described herein the probe reflector element can include, but is not limited to, a membrane, a film, a cap, a cover, or other material. In some embodiments, the reflector element is flexible or inflexible. The reflector element can be shaped in various geometries, such that portions of the reflector are curved, planar, or substantially planar.

[0037] Basic scattering theory for particles and classic radar cross-section theory estimates that the fraction of light reflected from a single TiO_2 particle is given by the expression:

$$L_R = \frac{\sigma_b}{V_i} l_c \Delta\Omega$$

where L_R is the return light fraction, σ_b is the scattering cross-section (calculated from standard MIE theory), V_i is the volume of the particle, l_c is the interaction length (from Radar theory), in this case the coherence length of the OCT light, and $\Delta\Omega$ is acceptance angle (solid angle) of the micro-lens. Thus, for a particle size of roughly 45 nm with a scattering cross section of approximately $4.26 \times 10^{-7} \mu\text{m}^2$, and light having a coherence length of about 15 μm irradiating the particle through a micro-lens having a solid angle of ~ 0.004 , the reflected light fraction, L_R , is about 0.006, or -32 dB.

[0038] Therefore the total light returned from the probe reference reflector element material should be equal to the single particle light fraction times the volume fraction (doping concentration). Because this should be equal to about -60 dB (from above), a reduction of -30 dB (or

0.001) is required. Therefore, the volume fraction should be about 0.001, or about 0.1% doping concentration by volume. This should result in a strong, but not overpowering reference reflection by the TiO_2 particles.

[0039] When the zero point offset position is stable, the doped PET material produces a consistent, bright ring in the image as shown in Fig. 4a, as compared to an undoped cover Fig. 4b. When the zero point offset position is unstable, either by purposely modifying the reference path length or through stretching or compressing of the fibers during normal use, the ring is more of a spiral shape. If the concentration of TiO_2 particles is too high, the particles cast shadows due to clumping as shown in Fig. 4c. In one embodiment, the probe reflector element is a membrane that is capable of transmitting substantially undistorted imaging light. The term "substantially undistorted imaging light" means light that is suitable for generating an image of a sample or a sample element.

[0040] The captured data in 'raw' format is a series of radial scans, each occurring at evenly spaced angles, very much like the spokes in bicycle wheel. The raw data is stored simply in a conventional array memory format, where columns represent angles, and each row is a particular radial distance. Hence, the image of a perfect circle stored in memory would occur along the same row for each column, i.e. a straight line with zero (flat) slope. A spiral pattern is stored as a straight line with a slope, positive if the spiral is expanding, negative if the spiral is contracting.

[0041] Hence the signal from the PET material produces a line in the image that may have a flat, positive or negative slope depending on whether the optical path length is constant, increasing or decreasing. The magnitude of the slope is then proportional to the rate of change of the fiber path length in either direction due to stretching or shrinking. Because the zero point offset position is now detectable, a software algorithm can be used to isolate the PET ring by taking advantage of its bright reflection, known thickness and expected straight line representation in memory.

[0042] In frequency domain OCT systems, the sign of the slope must also be considered. Due to frequency aliasing effects, the OCT image can appear inverted over certain ranges of the z-offset motor track. A properly oriented image is shown in Figure 5a (with detected PET shown as a hashed line), while an inverted image is shown in Figure 5b. In the inverted image, the scan lines are inverted, so targets close to the origin appear in the periphery and targets in the periphery appear near the origin. When the image is inverted, the slope of the PET signal has the opposite sign (an inversion state) as when the orientation is normal. This fact can be used to determine the orientation of the image.

[0043] The basic steps of the algorithm are shown in Fig. 6. The OCT image is obtained (Step 1) and first analyzed on a statistical basis. This analysis calculates the number of pixels for each given intensity value. The histogram is then used to generate a "Global Threshold"

value to separate the foreground tissue from background noise (Step 2). Because the image intensity will eventually fall to the background noise level, the intensity at large radial distances can be used to estimate the overall 'noise-floor' of the system. This value is then be used to produce a binary image (Step 3). Intensity values above the threshold are set to one; those below the threshold are set to zero. By analyzing the binary image and not the input OCT image, the dependence on the absolute level of the doped PET reflection is minimized.

[0044] Once the binary image is available, it is filtered with a one dimensional spatial filter (Step 4) that is designed to have peak response for a signal with thickness similar to the known PET layer thickness and adjacent black space. As shown in the figure, the influence of the tissue is greatly minimized by the spatial filter, while the PET ring is preserved.

[0045] With respect to time domain OCT systems, the image is assumed to be of normal orientation and step 5 is omitted. In contrast, with respect to frequency domain OCT systems, the next step in the process (step 5) is to determine the orientation of the image by computing a representative scan line for the entire filtered image by averaging all of the scan lines of the filtered image together. This averaging process takes the expected slope S into account and adjusts the scan line positions relative to their neighbors linearly so that the sloped PET signal adds constructively across all of the lines. This "slope corrected" average line can also be computed with the opposite slope $-S$ to see which result yields the strongest peak signal. If the correction using S produces the best result then the frame is properly oriented (Figure 5a) and the frame should be used. If the correction using $-S$ (or negative S) produces the best result then the frame is inverted (Figure 5b) and should be discarded. Thus, in certain calibration or orientation method embodiments, a negative slope value, an inversion state, or certain patterns relating to or indicative of the same can be detected in certain underlying data originating from an OCT scan and used to calibrate an OCT system (or component thereof).

[0046] The next step in the process (Step 6) is to average all of the scan lines in each quadrant of the filtered binary image together to produce one representative scan line per quadrant. This means, in stored memory, the columns are divided into four equal groups, and for each group, all columns are averaged together across rows to produce one representative column for each of the four 90 degree quadrants of the original image. This process serves to emphasize image content that is concentric or nearly concentric. The average is performed on a quadrant basis, as opposed to the full 360 degrees, so that the PET signal from a moving reference path (which would be spiral shaped) is not lost in the summation process. The resulting four average lines are each smoothed with a simple boxcar filter, and the brightest three peaks on each are located.

[0047] Finally, in the next step (Step 7) the peak from

each quadrant's average line is selected that together produces the best ring. A recursive algorithm is used to analyze each potential group by first computing the sum of the four points and then the mean square error (MSE) of a line fitted to the points using a least squares fit algorithm. The resulting MSE is combined with the sum of the four points to form a score. This score serves to emphasize potential rings that are bright (larger sum) and flat (smaller MSE). The group with the largest score is chosen as the winner and its sum is compared to a cutoff to determine if the result is valid.

[0048] In operation, when a new image catheter is connected to the system, an initial coarse calibration is performed by rotating the fiber and adjusting the reference path control motor as shown in Fig. 7. The z-offset motor in the reference arm is initially swept at high speed (Step 10) between its limits while searching for the PET ring. Once the ring is found, the motor speed is slowed (Step 12) and the PET image is moved close to its desired location (zero-point, here termed the "Loose Range").

[0049] Further, once within the loose range, the motor is stepped (Step 14) until the PET image is in its final allowed range (the "Tight Range"). During live scanning the Z-Offset may drift slightly, resulting in the PET moving outside of the tight range. When this occurs, the motor is reactivated to step the PET back into the tight range. The tight range allowance is a balance set by the desired measurement accuracy and the minimization of constant z-offset motor movements

[0050] During real-time imaging, the PET ring, as defined by the least squares fitted line of the winning group, is displayed at a fixed location (radius) on the screen based on the known physical location of the PET in the micro-lens assembly. The z-offset of each image frame is adjusted in or out so that the PET ring ends up at the desired location.

[0051] The final result is that the Z-Offset corrected image is displayed on the screen and stored in the saved image files, allowing correct clinical measurements to be performed in a straightforward manner. Fig 8 is an OCT image of a coronary artery in which the z-offset is set correctly. The vessel diameter is thus correctly measured as 2.55 mm. Fig. 9 is an OCT image of a coronary artery in which the z-offset is set incorrectly such that the z-offset is positioned within the lens assembly. The vessel diameter is thus incorrectly measured as 2.97 mm.

[0052] Fig. 10 is an OCT image of a coronary artery in which the z-offset is set incorrectly such that the z-offset is positioned outside the protective PET cover. The vessel diameter is thus incorrectly measured as 2.00 mm. Thus, the present invention provides a method for determining the equalization of the reference and sample paths in an OCT interferometer, to thereby provide an accurate measure of the objects of interest.

[0053] Fig. 11 is another OCT image generated in accordance with aspects of the invention. Specifically, it is a magnified OCT image of a catheter center showing characteristic ring reflections arising from the micro-lens

PET layer (innermost) 100 and the image wire plastic sheath (middle) 102. The outer ring 104 corresponds to the inside wall edge of the plastic tubing into which the image wire was inserted to generate the image depicted in Fig. 11. However, due to thickness of the tubing, the outer wall edge is not seen in the image.

[0054] In Fig. 11, the PET ring is generated using standard, un-doped PET. As shown, the image wire is pressed against the side of the tubing thereby causing the third outer ring 104 to be non-concentric.

[0055] It should be understood that the above-described embodiments and the following examples are given by way of illustration, not limitation. Various changes and modifications within the scope of the present invention will become apparent to those skilled in the art from the present description.

Claims

1. An imaging probe (38), the probe comprising:

an elongate section having a first end and a second end, the second end forming a probe tip capable of intra-lumen imaging,
the probe tip comprising a cover (94) having a first surface and a second surface, the cover comprising a polymer and a plurality of back-scattering particles for controlled optical back-scattering disposed therein for providing a reference point for calibration of at least one imaging system parameter in an imaging system comprising the imaging probe,
the cover (94) allowing transmission of substantially undistorted imaging light,
the elongate section being adapted to transmit light reflected by the back-scattering particles to the first end of the elongate section.

2. The imaging probe of claim 1 wherein each of the plurality of back-scattering particles has a particle dimension, the plurality of back-scattering particles being disposed within the polymer.
3. The imaging probe of claim 2 wherein the particle dimension is less than about 1.5 μm .
4. The imaging probe of any preceding claim wherein the particles comprise titanium, zinc, or aluminum.
5. The imaging probe of any preceding claim wherein the plurality of back-scattering particles have a concentration of about 0.1% doping concentration by volume.
6. The imaging probe of any preceding claim wherein the cover (94) is shaped to form a sheath within which the elongate section is disposed to form a portion of

a probe tip.

7. The imaging probe of any preceding claim wherein at least portions of the cover are curved.
8. The imaging probe of any preceding claim wherein the elongate section is an optical fiber (30).
9. The imaging probe of any of claims 1 to 7 wherein the elongate section is a sheath and wherein the probe further comprises an optical fiber disposed within the sheath.
10. The imaging probe of any preceding claim wherein the back-scattering particles are dispersed in a matrix of the polymer.
11. The imaging probe of claim 10 wherein the back-scattering particles comprise titanium and wherein the matrix comprises polyethylene terephthalate.
12. An optical coherence tomography imaging system comprising the imaging probe of any of claims 1 to 11.
13. A method of calibrating an optical coherence tomography imaging system (10) comprising the imaging probe (38) of any of claims 1 to 11, the method comprising:
- generating scan data in response to light reflected from a sample, the reflected light passing through the cover (94);
generating reference data in response to scattered light reflected from the back-scattering particles disposed within the cover (94); and
calibrating the optical coherence tomography imaging system to determine the relative position of subsequent scans in response to the reference data.
14. The method of claim 13 wherein the scan data comprises a set of angles and a set of radial distances, and/or the reference data comprises a set of angles and a set of radial distances.
15. The method of claim 13 or 14 wherein the step of calibrating includes searching the reference data for a pattern selected from the group consisting of a ring pattern, a spiral pattern, negative slope value, and an inversion state.

Patentansprüche

1. Bildgebungssonde (38), wobei die Sonde umfasst:
- einen langgestreckten Abschnitt mit einem ers-

- ten Ende und einem zweiten Ende, wobei das zweite Ende eine Sondenspitze bildet, die zur Intra-Lumen-Bildgebung geeignet ist, wobei die Sondenspitze eine Abdeckung (94) mit einer ersten Oberfläche und einer zweiten Oberfläche umfasst, wobei die Abdeckung ein Polymer und eine Vielzahl von darin angeordneten Rückstreupartikeln für die kontrollierte optische Rückstreuung umfasst, um einen Referenzpunkt für die Kalibrierung mindestens eines Bildsystemparameters in einem die Bildsonde umfassenden Bildgebungssystem bereitzustellen, wobei die Abdeckung (94) die Übertragung von im Wesentlichen unverzerrtem Bildgebungslicht ermöglicht, wobei der langgestreckte Abschnitt eingerichtet ist, um von den Rückstreupartikeln reflektiertes Licht an das erste Ende des langgestreckten Abschnitts zu übertragen.
2. Bildgebungssonde nach Anspruch 1, bei der jeder der Vielzahl von Rückstreupartikeln eine Partikelgröße aufweist, wobei die Vielzahl von Rückstreupartikeln innerhalb des Polymers angeordnet ist.
 3. Bildgebungssonde nach Anspruch 2, bei der die Partikelgröße kleiner als etwa $1,5 \mu\text{m}$ ist.
 4. Bildgebungssonde nach einem der vorhergehenden Ansprüche, bei der die Partikel Titan, Zink oder Aluminium umfassen.
 5. Bildgebungssonde nach einem der vorhergehenden Ansprüche, bei der die Vielzahl der rückstreuenden Partikel eine Konzentration von etwa 0,1 Vol.-% Dotierungskonzentration aufweist.
 6. Bildgebungssonde nach einem der vorhergehenden Ansprüche, bei der die Abdeckung (94) geformt ist, um eine Hülle zu bilden, in der der langgestreckte Abschnitt angeordnet ist, um einen Abschnitt einer Sondenspitze zu bilden.
 7. Bildgebungssonde nach einem der vorhergehenden Ansprüche, bei der mindestens Teile der Abdeckung gekrümmt sind.
 8. Bildgebungssonde nach einem der vorhergehenden Ansprüche, bei der der langgestreckte Abschnitt eine optische Faser (30) ist.
 9. Bildgebungssonde nach einem der Ansprüche 1 bis 7, bei der der langgestreckte Abschnitt eine Hülle ist und bei der die Sonde ferner eine innerhalb der Hülle angeordnete optische Faser umfasst.
 10. Bildgebungssonde nach einem der vorhergehenden Ansprüche, bei der die rückstreuenden Partikel in einer Matrix des Polymers dispergiert sind.
 11. Bildgebungssonde nach Anspruch 10, bei der die rückstreuenden Partikel Titan umfassen und bei der die Matrix Polyethylenterephthalat umfasst.
 12. Optisches Kohärenztomographie-Bildgebungssystem, umfassend die Bildgebungssonde nach einem der Ansprüche 1 bis 11.
 13. Verfahren zum Kalibrieren eines die Bildgebungssonde (38) nach einem der Ansprüche 1 bis 11 umfassenden optischen Kohärenztomographie-Bildgebungssystems (10), wobei das Verfahren umfasst:
 - Erzeugen von Scandaten als Reaktion auf das von einer Probe reflektierte Licht, wobei das reflektierte Licht durch die Abdeckung (94) hindurchtritt;
 - Erzeugen von Referenzdaten als Reaktion auf Streulicht, das von den innerhalb der Abdeckung (94) angeordneten rückstreuenden Partikeln reflektiert wird; und
 - Kalibrieren des optischen Kohärenztomographie-Bildgebungssystems, um als Reaktion auf die Referenzdaten die relative Position nachfolgender Scans zu bestimmen.
 14. Verfahren nach Anspruch 13, bei dem die Abtastdaten einen Satz von Winkeln und einen Satz von Radialabständen umfassen, und/oder die Referenzdaten einen Satz von Winkeln und einen Satz von Radialabständen umfassen.
 15. Verfahren nach Anspruch 13 oder 14, bei dem der Schritt des Kalibrierens das Absuchen der Referenzdaten nach einem Muster umfasst, das aus der Gruppe ausgewählt ist, die aus einem Ringmuster, einem Spiralmuster, einem negativen Steigungswert und einem Inversionszustand besteht.

Revendications

1. Sonde d'imagerie (38), la sonde comprenant :

une section allongée ayant une première extrémité et une seconde extrémité, la seconde extrémité formant une pointe de sonde capable d'une imagerie intra-lumière, la pointe de sonde comprenant un capuchon (94) ayant une première surface et une seconde surface, le capuchon comprenant un polymère et une pluralité de particules à rétrodiffusion pour une rétrodiffusion optique commandée disposées dans celui-ci afin de fournir un point de référence pour un étalonnage d'au moins un pa-

- ramètre de système d'imagerie dans un système d'imagerie comprenant la sonde d'imagerie, le capuchon (94) permettant la transmission d'une lumière d'imagerie sensiblement non distordue, la section allongée étant adaptée pour transmettre une lumière réfléchi par les particules à rétrodiffusion à la première extrémité de la section allongée.
2. Sonde d'imagerie selon la revendication 1, dans laquelle chacune de la pluralité de particules à rétrodiffusion a une dimension de particule, la pluralité de particules à rétrodiffusion étant disposée à l'intérieur du polymère.
 3. Sonde d'imagerie selon la revendication 2, dans laquelle la dimension de particule est inférieure à environ 1,5 μm .
 4. Sonde d'imagerie selon l'une quelconque des revendications précédentes, dans laquelle les particules comprennent du titane, du zinc ou de l'aluminium.
 5. Sonde d'imagerie selon l'une quelconque des revendications précédentes, dans laquelle la pluralité de particules à rétrodiffusion a une concentration d'environ 0,1 % de concentration de dopage en volume.
 6. Sonde d'imagerie selon l'une quelconque des revendications précédentes, dans laquelle le capuchon (94) est mis en forme pour former une gaine à l'intérieur de laquelle la section allongée est disposée pour former une partie d'une pointe de sonde.
 7. Sonde d'imagerie selon l'une quelconque des revendications précédentes, dans laquelle au moins des parties du capuchon sont incurvées.
 8. Sonde d'imagerie selon l'une quelconque des revendications précédentes, dans laquelle la section allongée est une fibre optique (30).
 9. Sonde d'imagerie selon l'une quelconque des revendications 1 à 7, dans laquelle la section allongée est une gaine et dans laquelle la sonde comprend en outre une fibre optique disposée à l'intérieur de la gaine.
 10. Sonde d'imagerie selon l'une quelconque des revendications précédentes, dans laquelle les particules à rétrodiffusion sont dispersées dans une matrice du polymère.
 11. Sonde d'imagerie selon la revendication 10, dans laquelle les particules à rétrodiffusion comprennent du titane et dans laquelle la matrice comprend du polyéthylène téréphtalate.
 12. Système d'imagerie par tomographie par cohérence optique comprenant la sonde d'imagerie selon l'une quelconque des revendications 1 à 11.
 13. Procédé d'étalonnage d'un système d'imagerie par tomographie par cohérence optique (10) comprenant la sonde d'imagerie (38) selon l'une quelconque des revendications 1 à 11, le procédé comprenant les étapes consistant à :
 - généraliser des données de balayage en réponse à de la lumière réfléchi par un échantillon, la lumière réfléchi passant à travers le capuchon (94) ;
 - généraliser des données de référence en réponse à de la lumière diffusée réfléchi par les particules à rétrodiffusion disposées dans le capuchon (94) ; et
 - étalonner le système d'imagerie par tomographie par cohérence optique pour déterminer la position relative de balayages ultérieurs en réponse aux données de référence.
 14. Procédé selon la revendication 13, dans lequel les données de balayage comprennent un ensemble d'angles et un ensemble de distances radiales, et/ou les données de référence comprennent un ensemble d'angles et un ensemble de distances radiales.
 15. Procédé selon la revendication 13 ou 14, dans lequel l'étape de calibrage comprend la recherche dans les données de référence d'un motif sélectionné dans le groupe comprenant un motif en anneau, un motif en spirale, une valeur de pente négative et un état d'inversion.

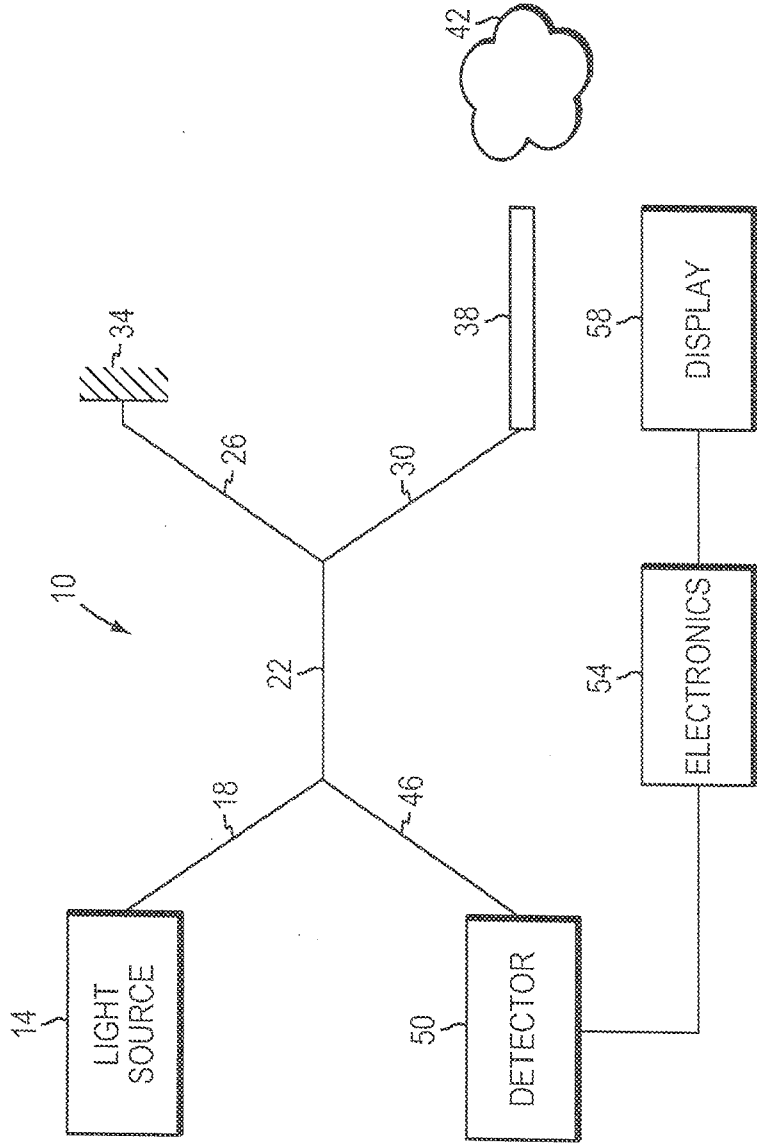


FIG. 1

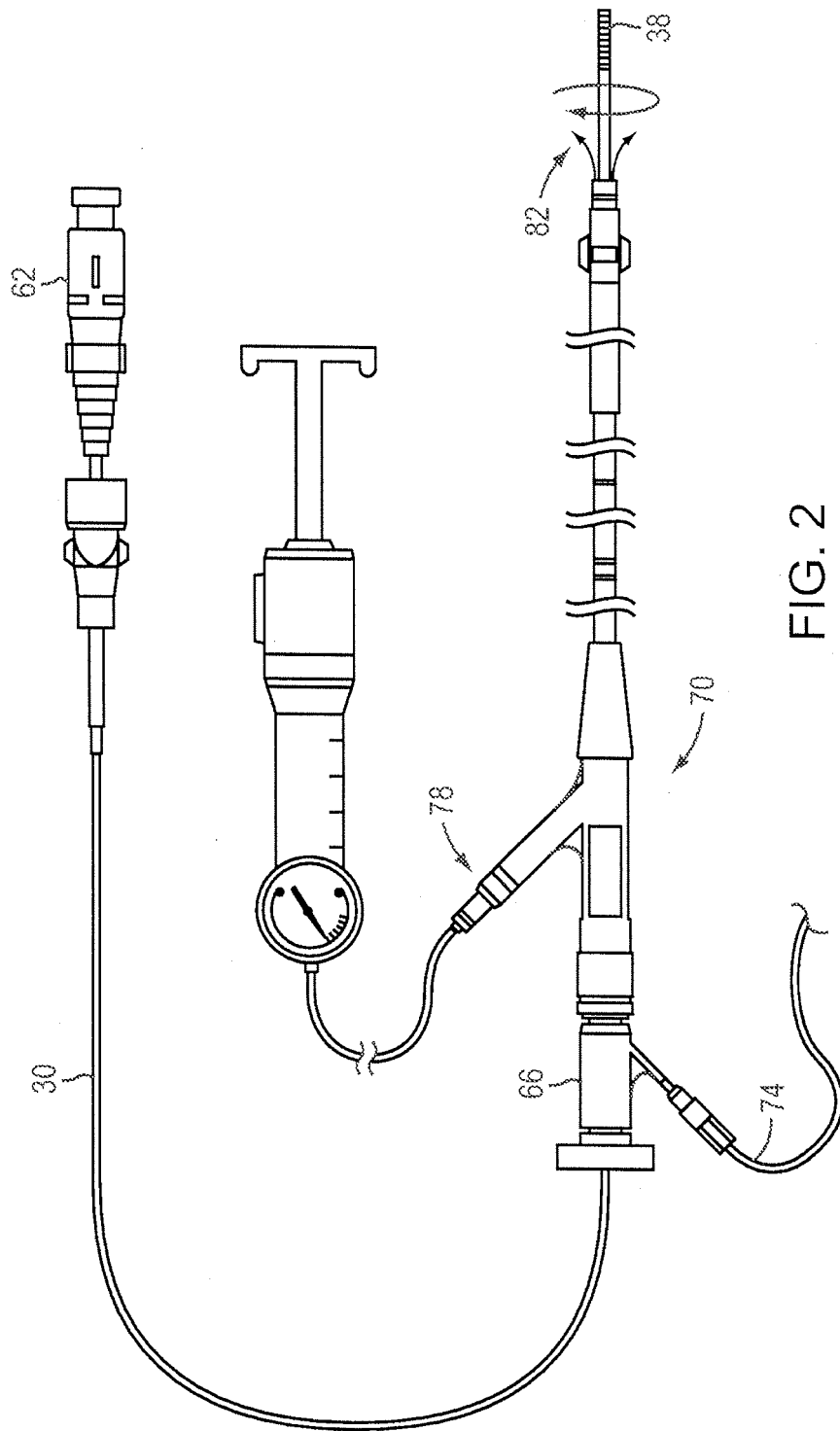


FIG. 2

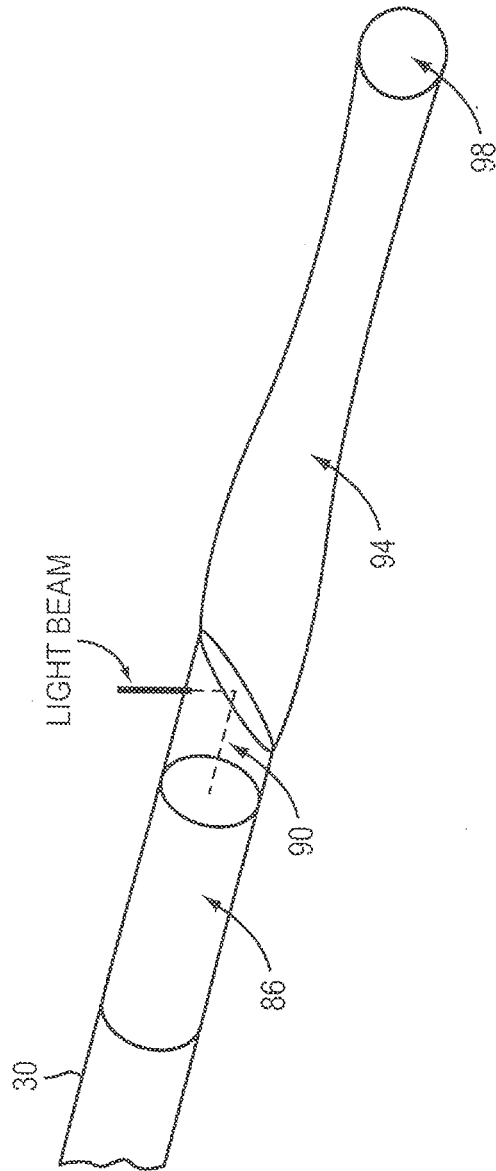


FIG. 3

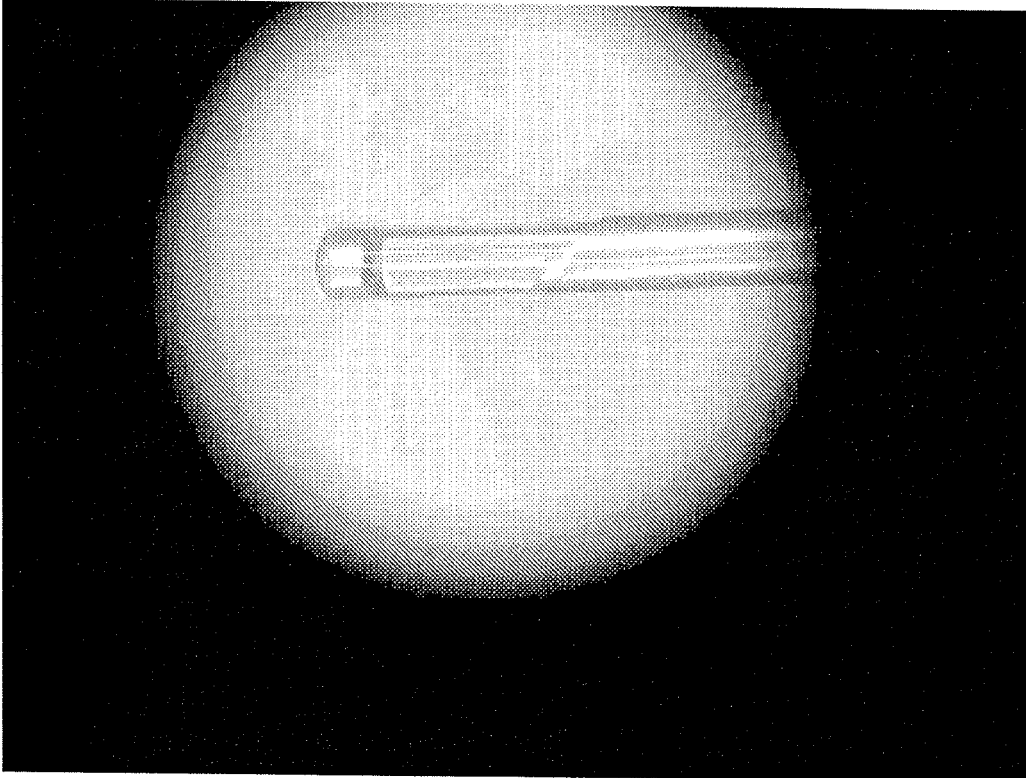


FIG. 3A

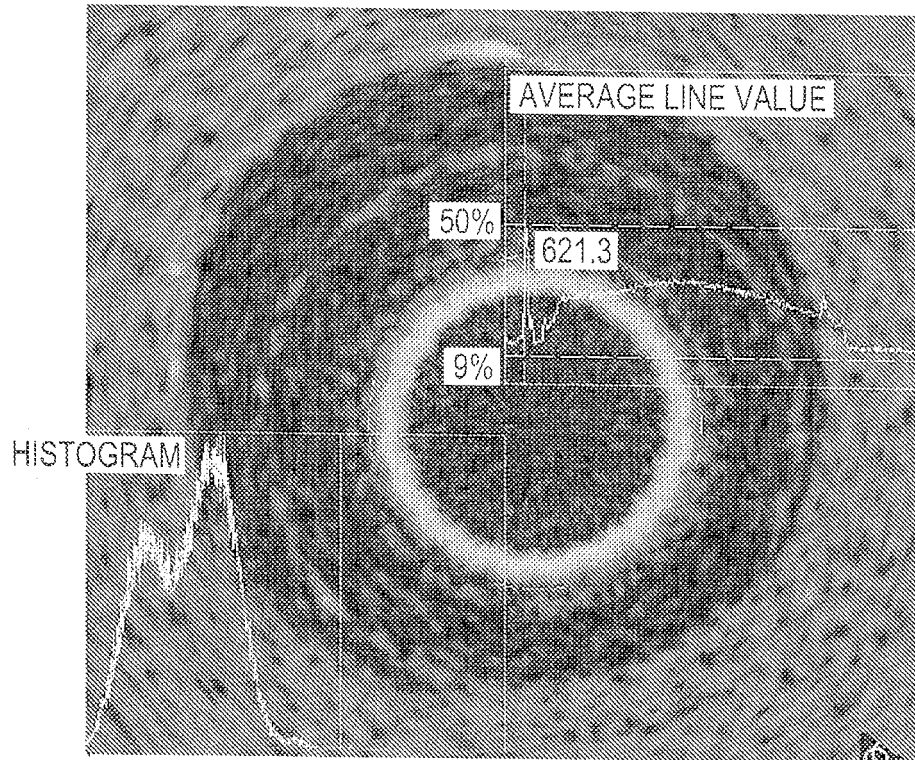


FIG. 4A

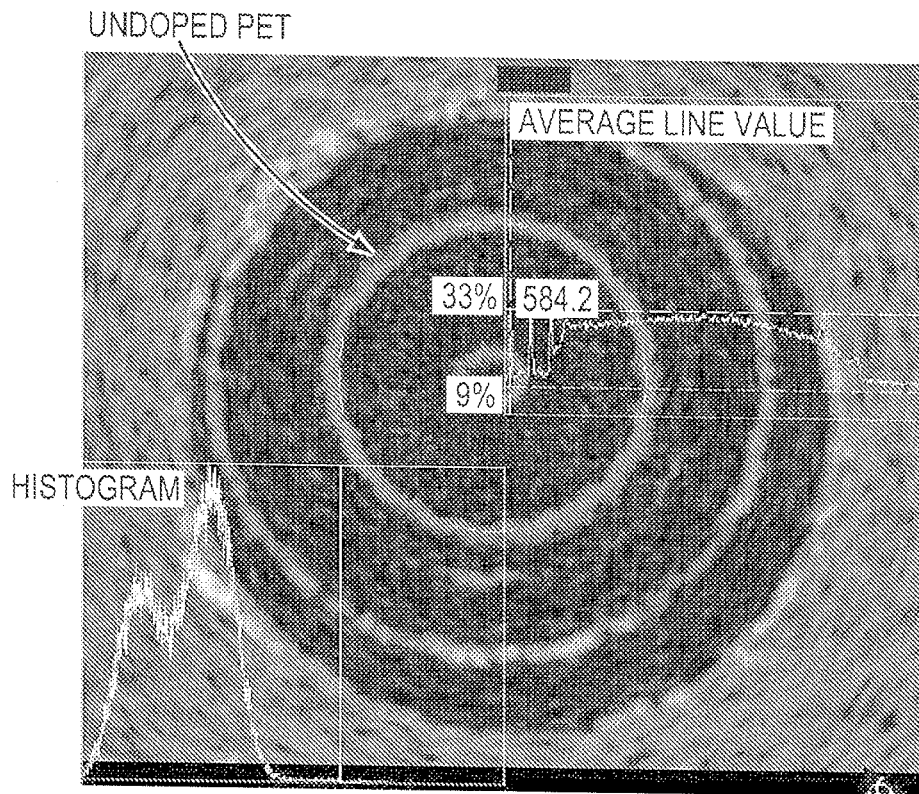


FIG. 4B

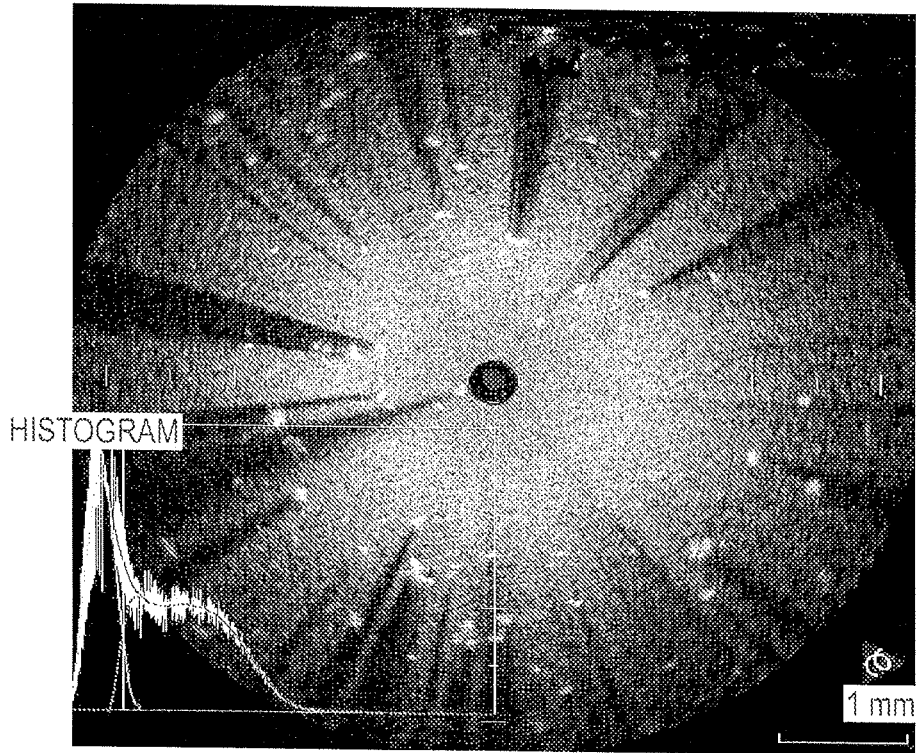


FIG. 4C

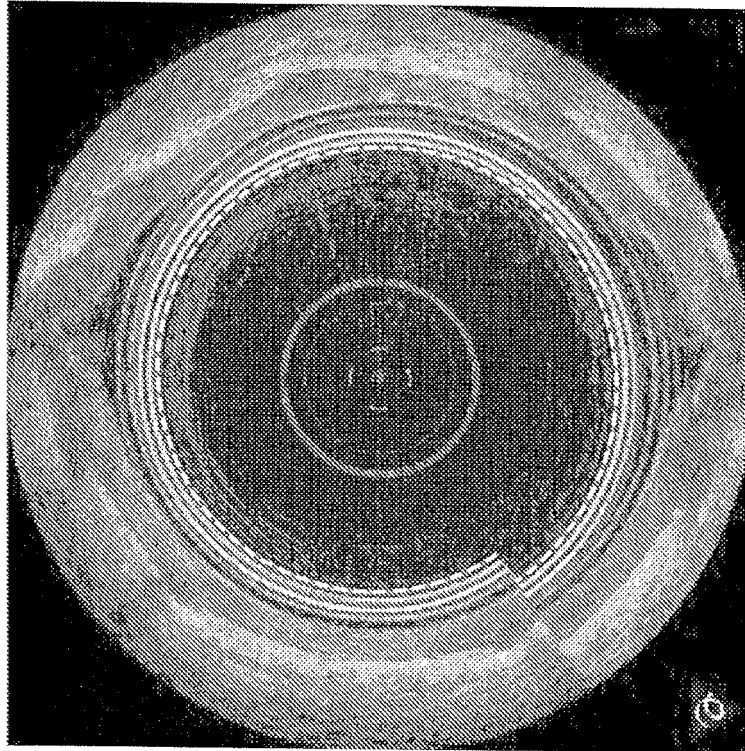


FIG. 5A

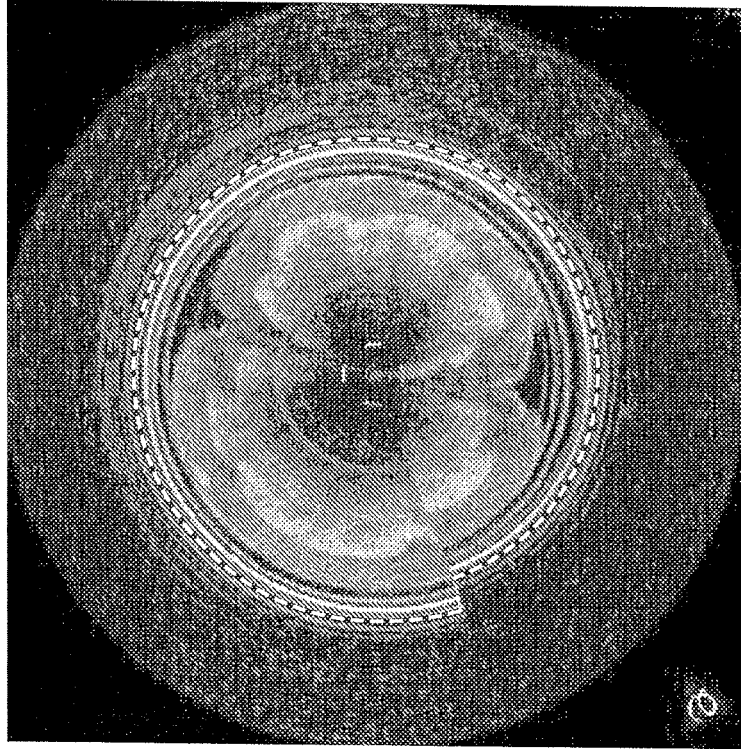
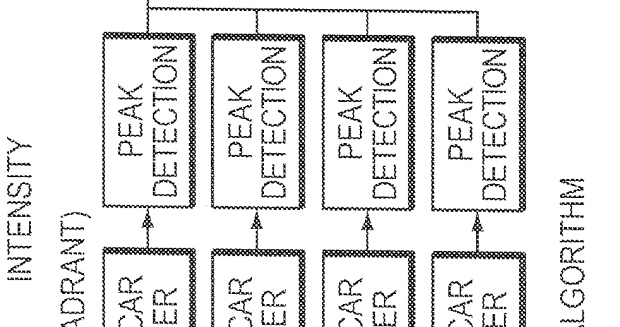
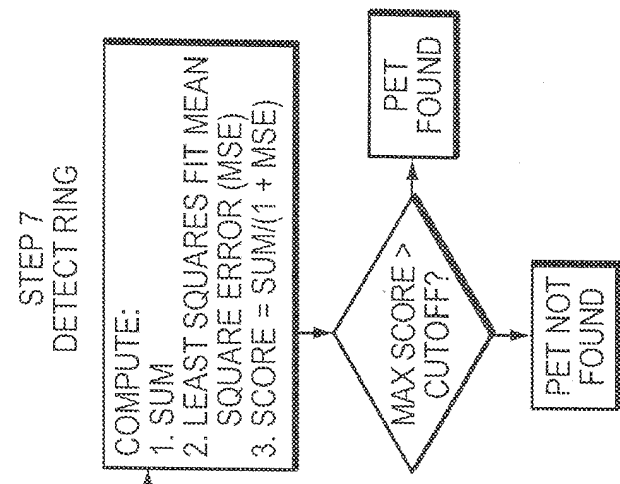
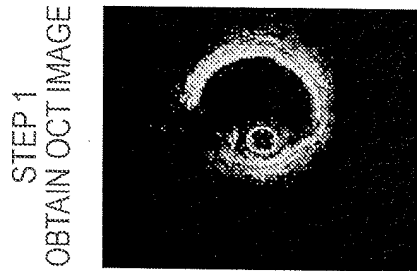
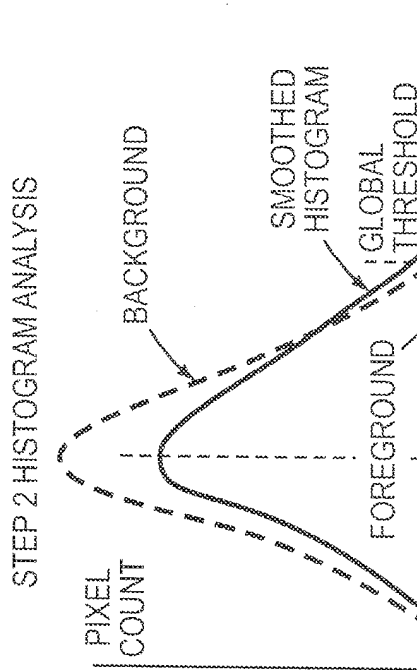
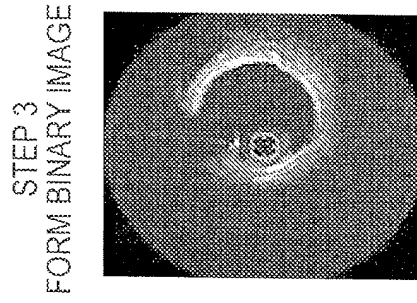
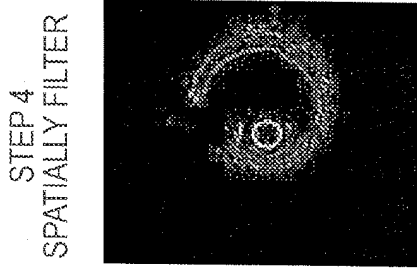


FIG. 5B



1. COMPUTE EXPECTED PET SLOPE S FROM Z-OFFSET MOTOR SPEED, FRAME RATE AND LINES PER FRAME

2. COMPUTE SLOPE CORRECTED AVERAGE LINE ON FILTERED DATA FOR NORMAL ORIENTATION AND FIND PEAK SAMPLE

3. COMPUTE SLOPE CORRECTED AVERAGE LINE FOR INVERTED ORIENTATION (SLOPE=-S) AND FIND PEAK SAMPLE

4. ORIENTATION DETERMINED BY WHICH HAS THE LARGER RESULT

PET DETECTION ALGORITHM

FIG. 6

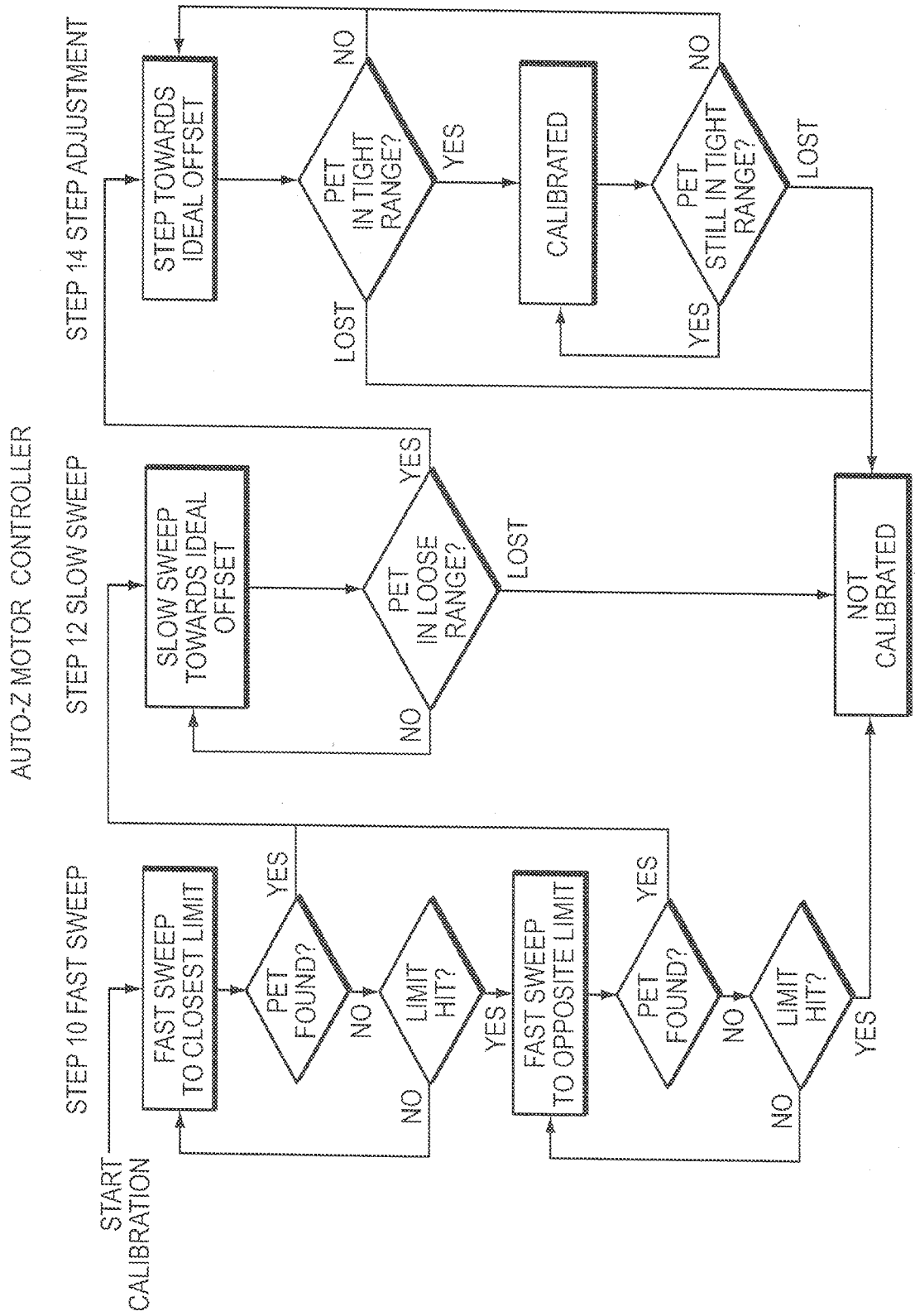


FIG. 7

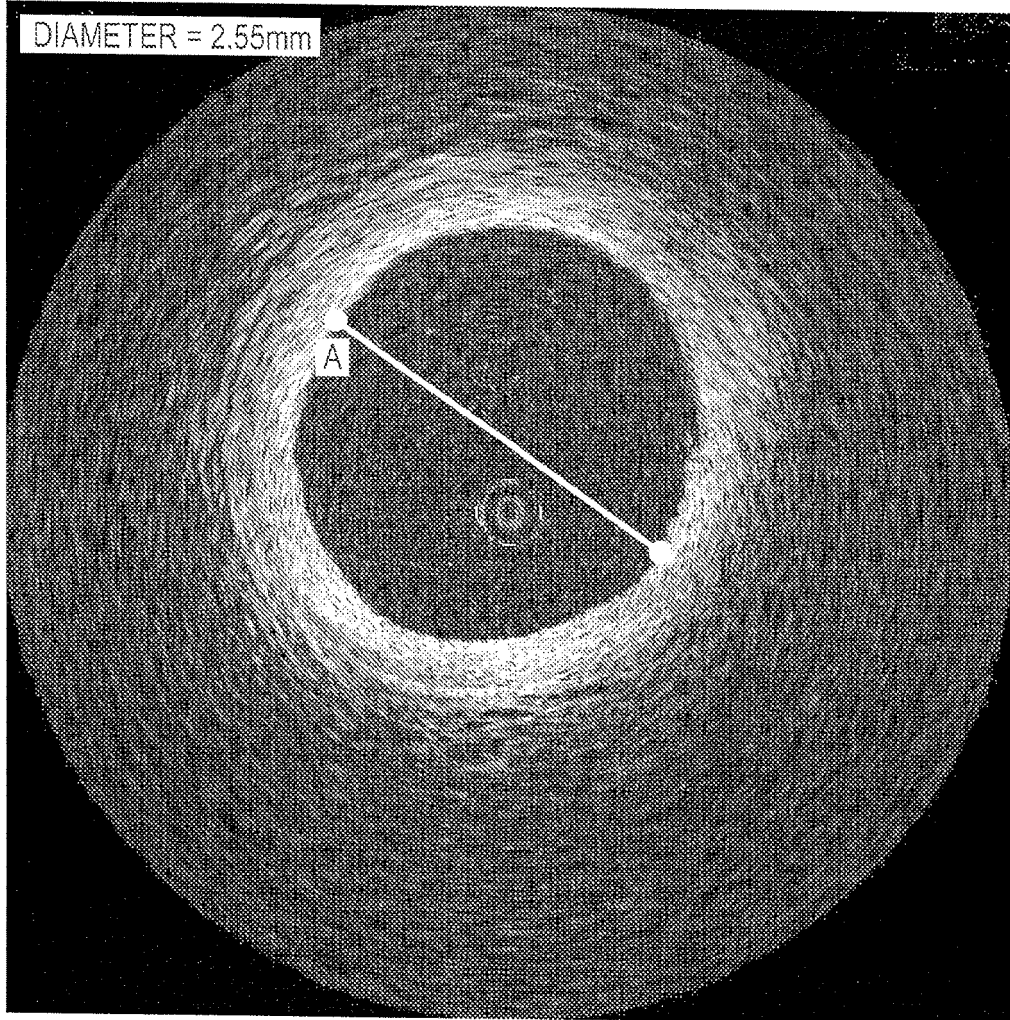


FIG. 8

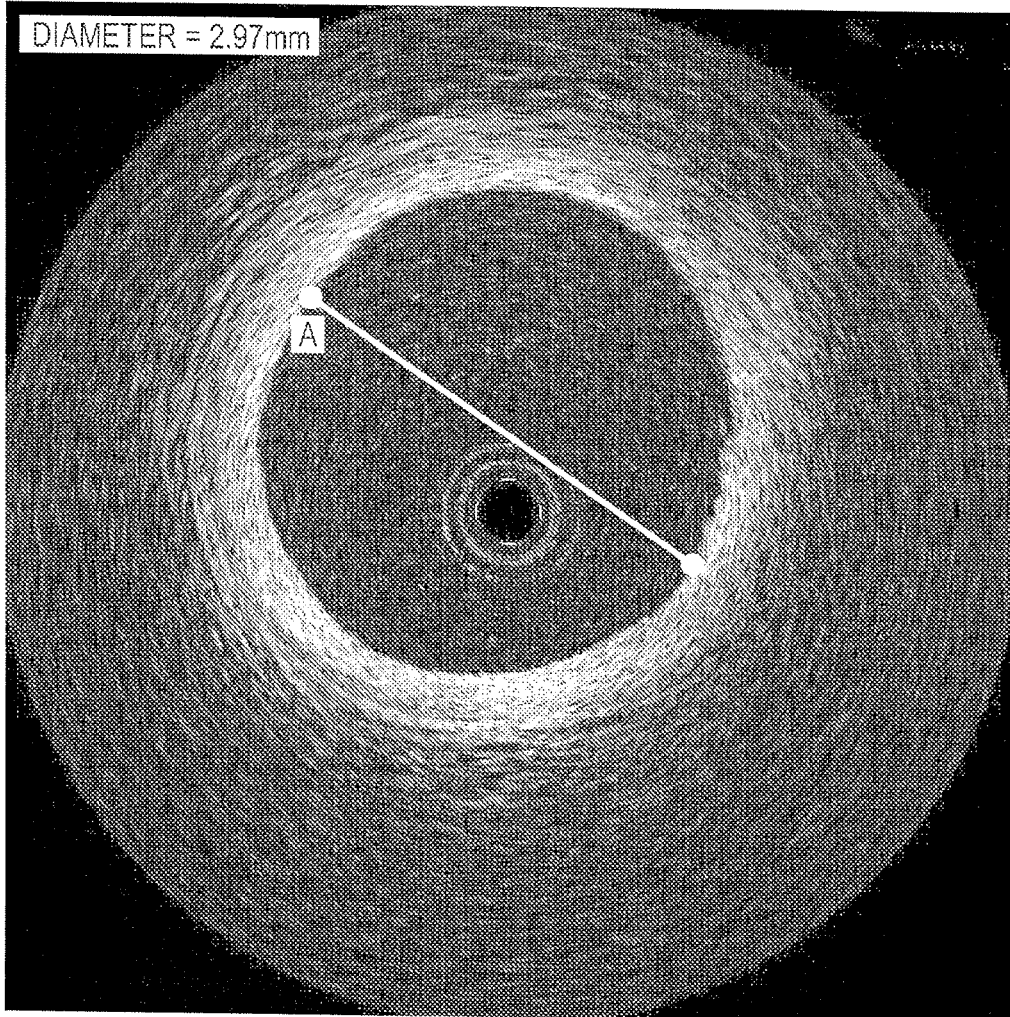


FIG. 9

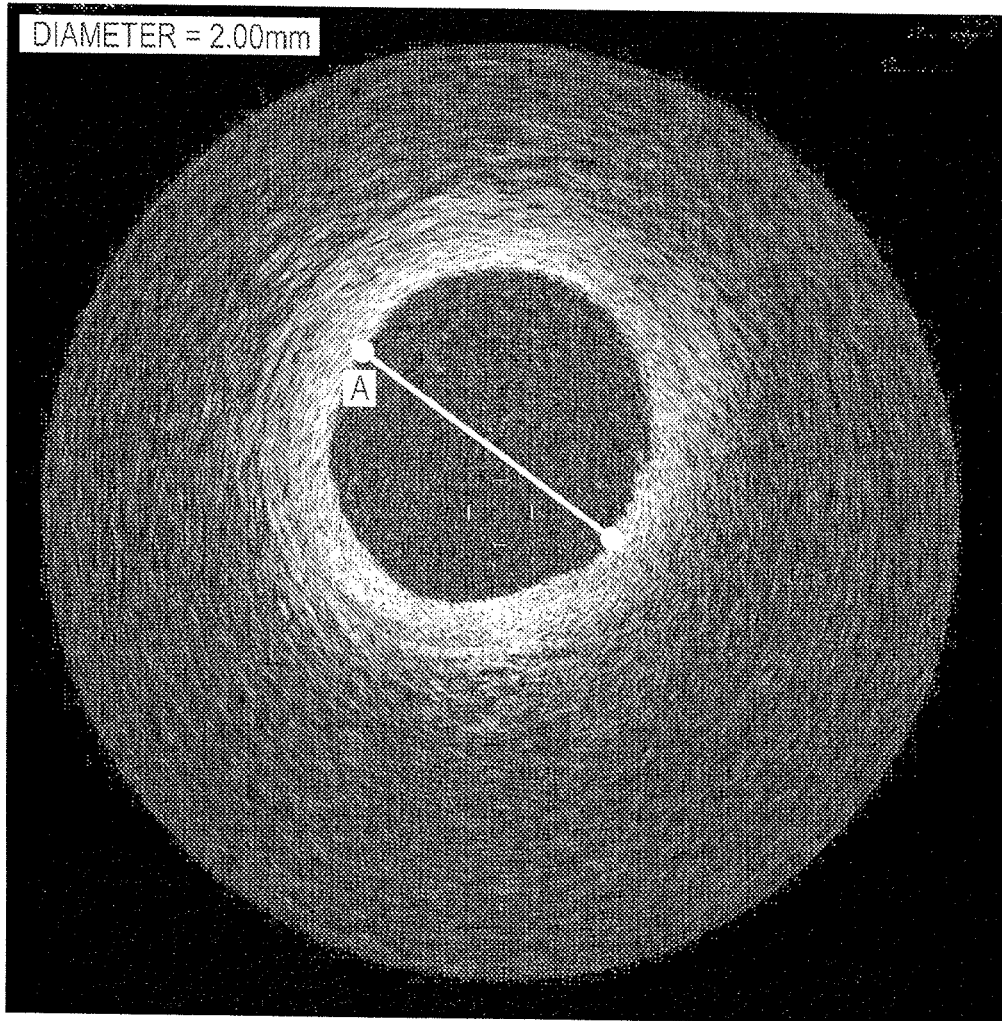


FIG. 10

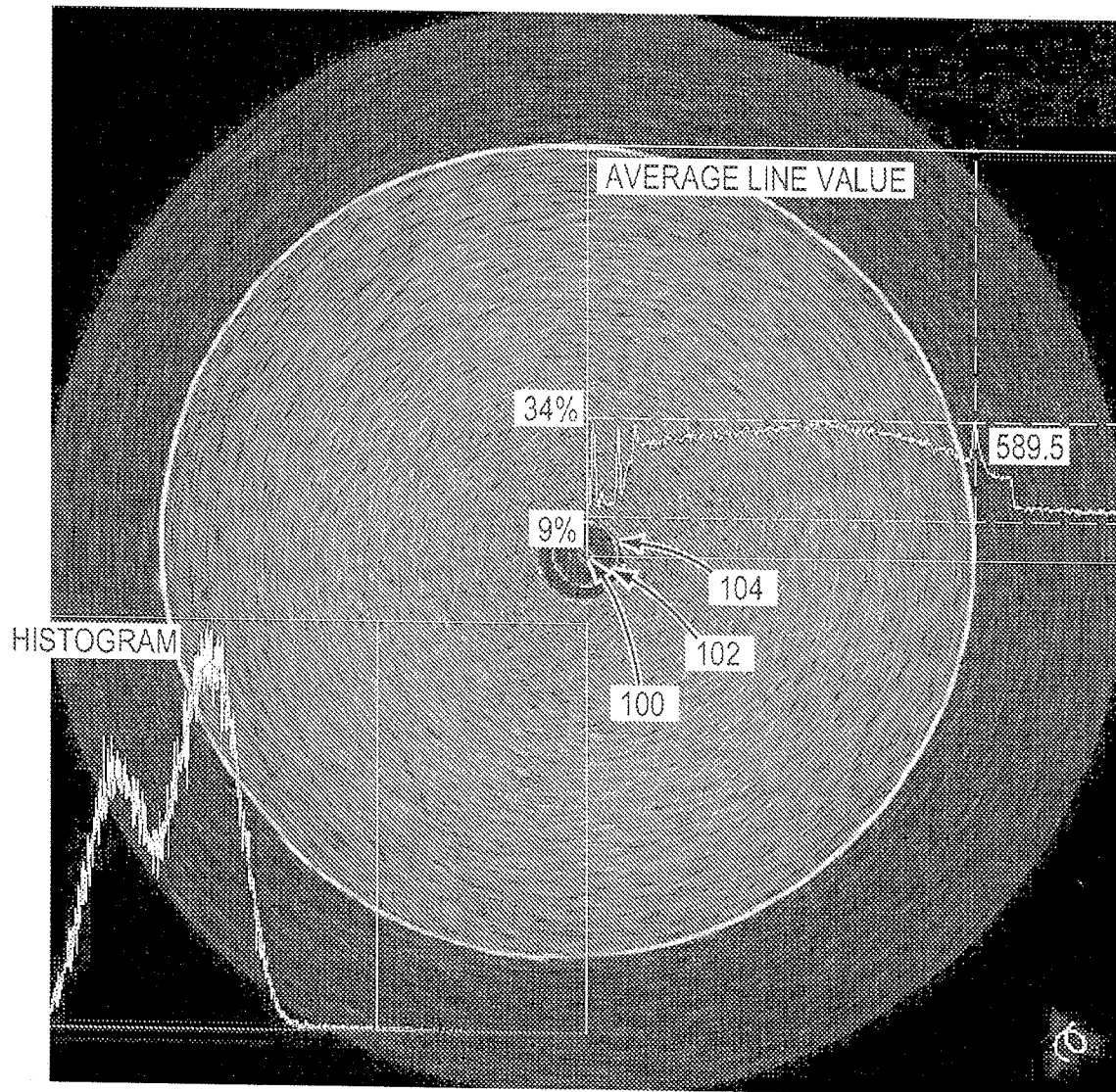


FIG. 11

REFERENCES CITED IN THE DESCRIPTION

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- US 6891894 B [0031]

专利名称(译)	带有集成参考反射器的成像导管		
公开(公告)号	EP3045108B1	公开(公告)日	2019-09-25
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[标]申请(专利权)人(译)	光学实验室成像公司		
申请(专利权)人(译)	LIGHTLAB IMAGING , INC.		
当前申请(专利权)人(译)	LIGHTLAB IMAGING , INC.		
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IPC分类号	A61B5/00 G02B5/00		
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优先权	11/983526 2007-11-12 US PCT/US2008/012701 2008-11-12 WO		
其他公开文献	EP3045108A1		
外部链接	Espacenet		

摘要(译)

本公开涉及一种成像探针，特别是光学相干断层扫描成像系统的成像探针，该探针包括能够进行腔内成像的探针尖端，该探针尖端包括覆盖物，该覆盖物包括聚合物和用于控制的多个反向散射粒子光学反向散射设置在其中，以提供用于校准至少一个成像系统参数的参考点。

$$L_R = \frac{\sigma_b}{V_i} l_c \Delta\Omega$$