

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
16 February 2006 (16.02.2006)

PCT

(10) International Publication Number  
**WO 2006/017117 A2**

(51) International Patent Classification<sup>7</sup>: **A61B 5/00**

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(21) International Application Number:  
PCT/US2005/024088

(22) International Filing Date: 7 July 2005 (07.07.2005)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
60/586,281 9 July 2004 (09.07.2004) US

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SM, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

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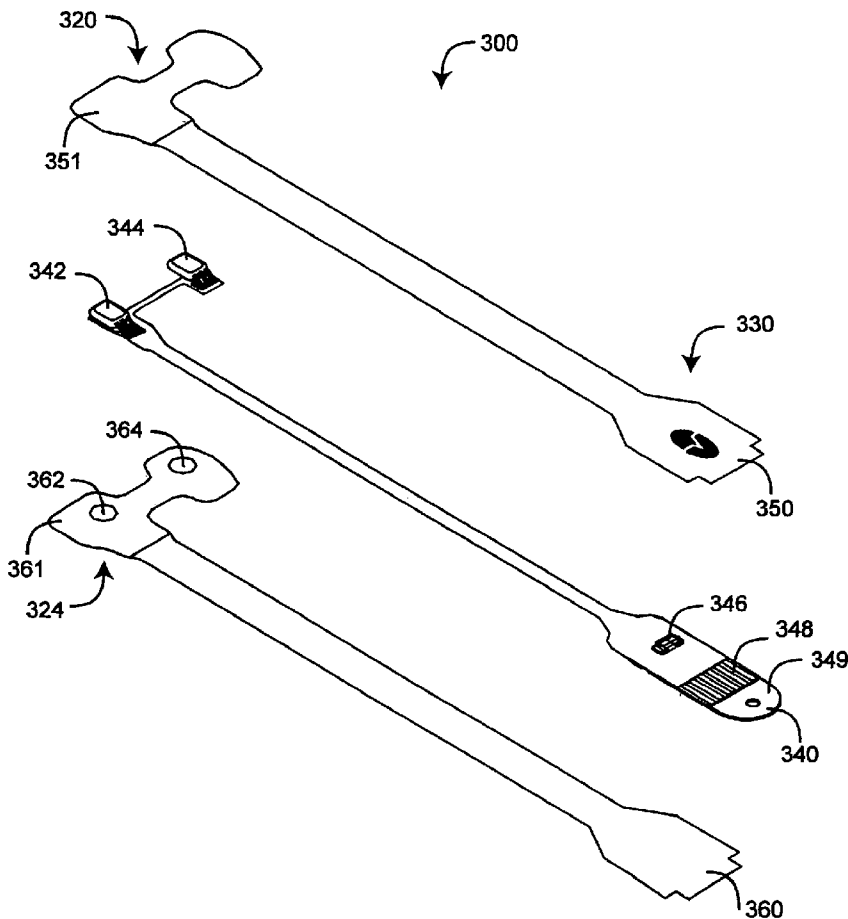
(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, NL, PL, PT,

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[Continued on next page]

(54) Title: CYANOTIC INFANT SENSOR



(57) Abstract: A pulse oximetry sensor comprises emitters configured to transmit light having a plurality of wavelengths into a fleshy medium. A detector is responsive to the emitted light after absorption by constituents of pulsatile blood flowing within the medium so as to generate intensity signals. A sensor head has a light absorbing surface adapted to be disposed proximate the medium. The emitters and the detector are disposed proximate the sensor head. A detector window is defined by the sensor head and configured so as to limit the field-of-view of the detector.

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RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

*For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.*

**Published:**

— *without international search report and to be republished upon receipt of that report*

## CYANOTIC INFANT SENSOR

### BACKGROUND OF THE INVENTION

[0001] Cyanosis is a congenital condition in which blood pumped to the body contains less than normal amounts of oxygen, resulting in a blue discoloration of the skin. The most common cyanotic condition is tetralogy of Fallot, which is characterized by an abnormal opening, or ventricular septal defect, that allows blood to pass from the right ventricle to the left ventricle without going through the lungs; a narrowing, or stenosis, proximate the pulmonary valve, which partially blocks the flow of blood from the right side of the heart to the lungs; a right ventricle that is abnormally muscular; and an aorta that lies directly over the ventricular septal defect. Another cyanotic condition is tricuspid atresia, characterized by a lack of a tricuspid valve and resulting in a lack of blood flow from the right atrium to the right ventricle. Yet another cyanotic condition is transposition of the great arteries, i.e. the aorta originates from the right ventricle, and the pulmonary artery originates from the left ventricle. Hence, most of the blood returning to the heart from the body is pumped back out without first going to the lungs, and most of the blood returning from the lungs goes back to the lungs.

[0002] Pulse oximetry is a useful tool for diagnosing and evaluating cyanotic conditions. A pulse oximeter performs a spectral analysis of the pulsatile component of arterial blood so as to measure oxygen saturation, the relative concentration of oxygenated hemoglobin, along with pulse rate. FIG. 1 illustrates a pulse oximetry system 100 having a sensor 110 and a monitor 140. The sensor 110 has emitters 120 and a detector 130 and is attached to a patient at a selected fleshy tissue site, such as a thumb or toe. The emitters 120 project light through the blood vessels and capillaries of the tissue site. The detector 130 is positioned so as to detect the emitted light as it emerges from the tissue site. A pulse oximetry sensor is described in U.S. Patent 6,088,607 entitled "Low Noise Optical Probe," which is assigned to Masimo Corporation, Irvine, CA and incorporated by reference herein.

[0003] Also shown in FIG. 1, the monitor 140 has drivers 150, a controller 160, a front-end 170, a signal processor 180, a display 190. The drivers 150 alternately activate the emitters 120 as determined by the controller 160. The front-end 170 conditions and digitizes the resulting current generated by the detector 130, which is proportional to the intensity of the detected light. The signal processor 180 inputs the conditioned detector signal and determines oxygen saturation,

as described below, along with pulse rate. The display 190 provides a numerical readout of a patient's oxygen saturation and pulse rate. A pulse oximetry monitor is described in U.S. Patent 5,482,036 entitled "Signal Processing Apparatus and Method," which is assigned to Masimo Corporation, Irvine, CA and incorporated by reference herein.

### SUMMARY OF THE INVENTION

**[0004]** The Beer-Lambert law provides a simple model that describes a tissue site response to pulse oximetry measurements. The Beer-Lambert law states that the concentration  $c_i$  of an absorbent in solution can be determined by the intensity of light transmitted through the solution, knowing the mean pathlength,  $mpl_\lambda$ , the intensity of the incident light,  $I_{o,\lambda}$ , and the extinction coefficient,  $\varepsilon_{i,\lambda}$ , at a particular wavelength  $\lambda$ . In generalized form, the Beer-Lambert law is expressed as:

$$I_\lambda = I_{o,\lambda} e^{-mpl_\lambda \cdot \mu_{a,\lambda}} \quad (1)$$

$$\mu_{a,\lambda} = \sum_{i=1}^n \varepsilon_{i,\lambda} \cdot c_i \quad (2)$$

where  $\mu_{a,\lambda}$  is the bulk absorption coefficient and represents the probability of absorption per unit length. For conventional pulse oximetry, it is assumed that there are only two significant absorbers, oxygenated hemoglobin (HbO<sub>2</sub>) and reduced hemoglobin (Hb). Thus, two discrete wavelengths are required to solve EQS. 1-2, e.g. red (RD) and infrared (IR).

**[0005]** FIG. 2 shows a graph 200 depicting the relationship between RD/IR 202 and oxygen saturation (SpO<sub>2</sub>) 201, where RD/IR denotes the ratio of the DC normalized, AC detector responses to red and infrared wavelengths, as is well-known in the art and sometimes referred to as the "ratio-of-ratios." This relationship can be approximated from Beer-Lambert's Law, described above. However, it is most accurately determined by statistical regression of experimental measurements obtained from human volunteers and calibrated measurements of oxygen saturation. The result can be depicted as a curve 210, with measured values of RD/IR shown on an x-axis 202 and corresponding saturation values shown on a y-axis 201. In a pulse oximeter device, this empirical relationship can be stored in a read-only memory (ROM) for use as a look-up table so that SpO<sub>2</sub> can be directly read-out from an input RD/IR measurement. For example, an RD/IR value of

1.0 corresponding to a point **212** on the calibration curve **210** indicates a resulting SpO<sub>2</sub> value of approximately 85%.

[0006] Accurate and consistent pulse oximetry measurements on cyanotic infants have been difficult to obtain. An assumption inherent in the calibration curve **210** (FIG. **2**) is that the mean pathlength ratio for RD and IR is constant across the patient population. That is:

$$\frac{mpl_{RD}}{mpl_{IR}} = C \quad (3)$$

However, EQ. 3 may not be valid when cyanotic infants are included in that population. The reason may lie in what has been observed as abnormal tissue tone or lack of firmness associated with cyanotic defects, perhaps due to reduced tissue fiber. Such differences in tissue structure may alter the mean pathlength ratio as compared with normal infants. A cyanotic infant sensor addresses these problems by limiting variations in the RD over IR mean pathlength ratio and/or by providing a mean pathlength ratio measure so as to compensate for such variations. Alone or combined, these sensor apparatus and algorithms increase the accuracy and consistency of pulse oximetry measurements for cyanotic infants.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0007] FIG. **1** is a block diagram of a prior art pulse oximetry system;

[0008] FIG. **2** is an exemplar graph of a conventional calibration curve;

[0009] FIGS. **3A-B** are a perspective and an exploded perspective views, respectively, of a cyanotic infant sensor embodiment;

[0010] FIGS. **4-5** depict cross-sectional views of a tissue site and an attached pulse oximeter sensor, respectively;

[0011] FIG. **6** depicts a cross-sectional view of a tissue site and an attached cyanotic infant sensor;

[0012] FIGS. **7A-B** are plan and cross-sectional sensor head views of a conventional pulse oximeter sensor;

[0013] FIGS. **8-9** are plan and cross-sectional sensor head views of cyanotic infant sensor embodiments; and

[0014] FIG. **10** is an exemplar graph of a calibration surface incorporating a mean pathlength ratio measure.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0015] FIGS. 3A-B illustrate one embodiment of a cyanotic infant sensor. The sensor has a light absorbing surface, as described with respect to FIGS. 4-6, below. The sensor also has a detector window configured to limit the detector field-of-view (FOV), as described with respect to FIGS. 7-9, below. Advantageously, these features limit mean pathlength ratio variations that are particularly manifest in cyanotic patients.

[0016] The sensor emitters and detector are also matched so as to limit variations in the detector red over IR DC response, i.e.  $RD_{DC}/IR_{DC}$ , that are not attributed to variations in the mean pathlength ratio (EQ. 3). Such matching advantageously allows for measurement and calibration of the mean pathlength ratio, as described with respect to FIG. 10, below. In one embodiment, cyanotic infant sensors 300 are constructed so that:

$$\lambda_{RD} \approx c_1; \lambda_{IR} \approx c_2 \quad (4)$$

$$I_{0,RD}/I_{0,IR} \approx c_3; \text{ for } i_{DC}(RD), i_{DC}(IR) \quad (5)$$

$$RD_{DC}/IR_{DC} \approx c_4 \quad (6)$$

That is, sensors 300 are constructed from red LEDs and IR LEDs that are each matched as to wavelength (EQ. 4). The LEDs are further matched as to red over IR intensity for given DC drive currents (EQ. 5). In addition, the sensors 300 are constructed from detectors that are matched as to red over IR DC response (EQ. 6).

[0017] As shown in FIG. 3A, the sensor 300 has a body 310 physically connecting and providing electrical communication between a sensor head 320 and a connector 330. The sensor head 320 houses the emitters and detector and attaches to a patient tissue site. The connector mates with a patient cable so as to electrically communicate with a monitor. In one embodiment, a sensor head surface 324 is constructed of light absorbing material.

[0018] As shown in FIG. 3B, the sensor 300 has a face tape 330, a flex circuit 340 and a base tape 360, with the flex circuit 340 disposed between the face tape 330 and the base tape 360. The flex circuit 340 has a detector 342, an emitter 344 with at least two light emitting diodes (LEDs), an information element 346, and contacts 348 disposed on a connector tab 349. Neonatal sensors having a detector, LEDs, an information element, contacts and connector tab are described in U.S. Patent 6,256,523 entitled "Low-Noise Optical Probes," which is assigned to Masimo Corporation, Irvine, CA and incorporated by reference herein. In one embodiment, the face tape

350 and base tape 360 are constructed of Betham tape having attached polyethylene head tapes 351, 361. In a particular embodiment, the base head tape 361 is made of black polyethylene, and the face head tape 351 is made of white polyethylene. In one embodiment, a clear tape layer is disposed on the base head tape 361 tissue side over the detector window 362. The base head tape 361 has a detector window 362 and an emitter window 364 each allowing light to pass through the base head tape 361. In one embodiment, the base head tape 361 has a 4 mil thickness and the flex circuit has a 10 mil thickness. The combined 14 mil material thickness functions to limit the detector FOV, as described with respect to FIGS. 6 and 8, below.

[0019] FIGS. 4-6 illustrate some of the pathlength control aspects of a cyanotic infant sensor 300. FIG. 4 depicts a fleshy tissue site 10 for sensor attachment, such as a finger or thumb 400. The tissue 10 has an epidermis 12, a dermis 14, subcutaneous and other soft tissue 16 and bone 18.

[0020] FIG. 5 depicts a conventional pulse oximetry sensor 20 having a detector 22, an emitter 24 and a tape 26 attached to the fleshy tissue 10. Transmitted light 30 propagating from the emitter 24 to the detector 22 that results in a significant contribution to pulse oximetry measurements passes through and is absorbed by the pulsatile blood in the dermis 14. A portion of the transmitted light 30 is scattered out of the epidermis 12 and reflected by the tape 26 back into the fleshy tissue 10. The detector field-of-view (FOV) 40 is relatively wide and, as a result, the detector responds to transmitted light 30 that has propagated, at least in part, outside of the fleshy tissue 10.

[0021] FIG. 6 depicts a cyanotic infant sensor 300 that is configured to limit variations in the mean pathlength ratio. In particular, the sensor 300 has a light absorbing tape inner surface 324 that reduces transmitted light reflection back into the tissue site 10, as described with respect to FIGS. 3A-B, above. Further, the detector 342 has a limited FOV 50 so as to reduce the detection of transmitted light that has propagated outside of the tissue site 10, as described in detail with respect to FIGS. 7-9, below.

[0022] FIGS. 8-9 illustrate cyanotic infant sensor embodiments having a limited detector field-of-view (FOV). FIGS. 7A-B illustrate a conventional sensor 700 having a tape portion 760, a detector window 762 and a detector 742 having a relatively wide FOV 701. In particular, the window thickness does little to restrict the FOV. FIGS. 8A-B illustrate one embodiment of a cyanotic infant sensor 300 having a material portion 360, a detector window 362

and a detector 342 having a restricted FOV 801. In particular, the material thickness 360 functions to define the FOV 801. In one embodiment, the material thickness 360 comprises a flex circuit thickness and a base head tape thickness, as described with respect to FIG. 3B, above. FIGS. 9A-B illustrate another embodiment of a cyanotic infant sensor 900 having a material portion 960, a detector window 962 and a detector 942 having a restricted FOV 901. In particular, an O-ring 980 deposited around the window 962 defines the FOV 901.

[0023] FIG. 10 depicts an exemplar calibration surface 1000 for a cyanotic infant sensor 300 (FIGS. 3A-B) calculated along a DC response ratio axis 1001, a ratio-of-ratios axis 1003 and a resulting oxygen saturation axis 1005. Matching the emitters and detectors, as described with respect to FIG 3A, above, allows for pathlength calibration. In particular, variations in the detector DC response ratio ( $RD_{dc}/IR_{dc}$ ) are attributed to variations in the mean pathlength ratio (EQ. 3). As such, a calibration surface is determined by statistical regression of experimental measurements obtained from human volunteers and calibrated measurements of oxygen saturation, as is done for a conventional calibration curve (FIG. 2). A calculated DC response ratio 1001 in combination with a conventionally calculated ratio-of-ratios 1003 is then used to derive an oxygen saturation 1005 for the calibration surface 1000.

[0024] A cyanotic infant sensor has been disclosed in detail in connection with various embodiments. These embodiments are disclosed by way of examples only and are not to limit the scope of the claims that follow. One of ordinary skill in art will appreciate many variations and modifications.

WHAT IS CLAIMED IS:

1. A pulse oximetry sensor comprising:
  - a plurality of emitters configured to transmit light having a plurality of wavelengths into a fleshy medium;
  - at least one detector responsive to said light after absorption by constituents of pulsatile blood flowing within said medium so as to generate a plurality of intensity signals;
  - a sensor head having a light absorbing surface adapted to be disposed proximate said medium,
  - said emitters and said at least one detector disposed proximate said sensor head; and
  - a detector window defined by said sensor head, said window configured so as to limit the field-of-view of said at least one detector.
  
2. The pulse oximetry sensor according to claim 1 wherein said sensor head is configured to attach to a human digit with said light absorbing surface disposed around the periphery of the digit so as to at least partially absorb emitter transmitted light that is scattered out of said digit.
  
3. The pulse oximetry sensor according to claim 2 wherein a material thickness of said sensor head proximate said detector window limits the field-of-view of said at least one detector.
  
4. The pulse oximetry sensor according to claim 2 further comprising an O-ring disposed around the periphery of said detector window so as to limit the field-of-view of said at least one detector.
  
5. The pulse oximetry sensor according to claim 1 wherein said emitters are selected from a plurality of matched emitters having a first wavelength intensity over a second wavelength intensity ratio for at least one predetermined DC drive current that varies less than a predetermined amount.
  
6. The pulse oximetry sensor according to claim 1 wherein said at least one detector is selected from a plurality of matched detectors each having a first wavelength response over a

second wavelength response ratio for at least one predetermined DC incident intensity that varies less than a predetermined amount.

7. A pulse oximetry sensor comprising:

a plurality of emitters configured to transmit light having a plurality of wavelengths into a fleshy medium; and

a detector responsive to said light after absorption by constituents of pulsatile blood flowing within said medium so as to generate a plurality of intensity signals,

wherein said emitters and said detector selected from a plurality of matched emitters and matched detectors so that variations in a DC detector response ratio at said wavelengths can be generally attributed to variations in a mean pathlength ratio at said wavelengths.

8. The pulse oximetry sensor according to claim 7 wherein each of said emitters are matched according to a predetermined tolerance for a corresponding one of said wavelengths.

9. The pulse oximetry sensor according to claim 8 wherein said emitters are matched according to a DC intensity ratio tolerance at said wavelengths.

10. The pulse oximetry sensor according to claim 7 wherein said detector is matched according to a DC response ratio at said wavelengths.

11. The pulse oximetry sensor according to claim 7 further comprising:

a sensor head for mounting said emitters and said at least one detector, said sensor head adapted to be disposed around the periphery of a human digit so that a light absorbing surface of said sensor head at least partially prevents emitter transmitted light from being reflected from said surface back into said digit.

12. The pulse oximetry sensor according to claim 7 further comprising a detector window configured so as to limit the field-of-view of said detector.

13. A pulse oximetry method comprising the steps of:

transmitting light having a plurality wavelengths into a fleshy medium;  
detecting said transmitted light after absorption by constituents of pulsatile blood flowing within said medium so as to generate a corresponding plurality of intensity signals;  
and  
calculating a DC response ratio from said intensity signals as an indicator of a ratio of mean pathlengths of said transmitted light through said fleshy medium.

14. The pulse oximetry method according to claim 13 comprising the further step of deriving a calibration surface for calculating oxygen saturation as a function of said DC response ratio.

15. The pulse oximetry method according to claim 14 comprising the further step of matching emitters for said transmitted light according to a DC intensity ratio tolerance at said wavelengths.

16. The pulse oximetry method according to claim 15 comprising the further step of matching detectors for said detecting step according to a DC intensity ratio tolerance at said wavelengths.

17. The pulse oximetry method according to claim 13 comprising the further step of absorbing at least portions of said transmitted light that are scattered out of said fleshy medium.

18. The pulse oximetry method according to claim 13 comprising the further step of limiting a detector field-of-view so as to substantially limit said detected light to portions of said transmitted light that propagate entirely through said fleshy medium.

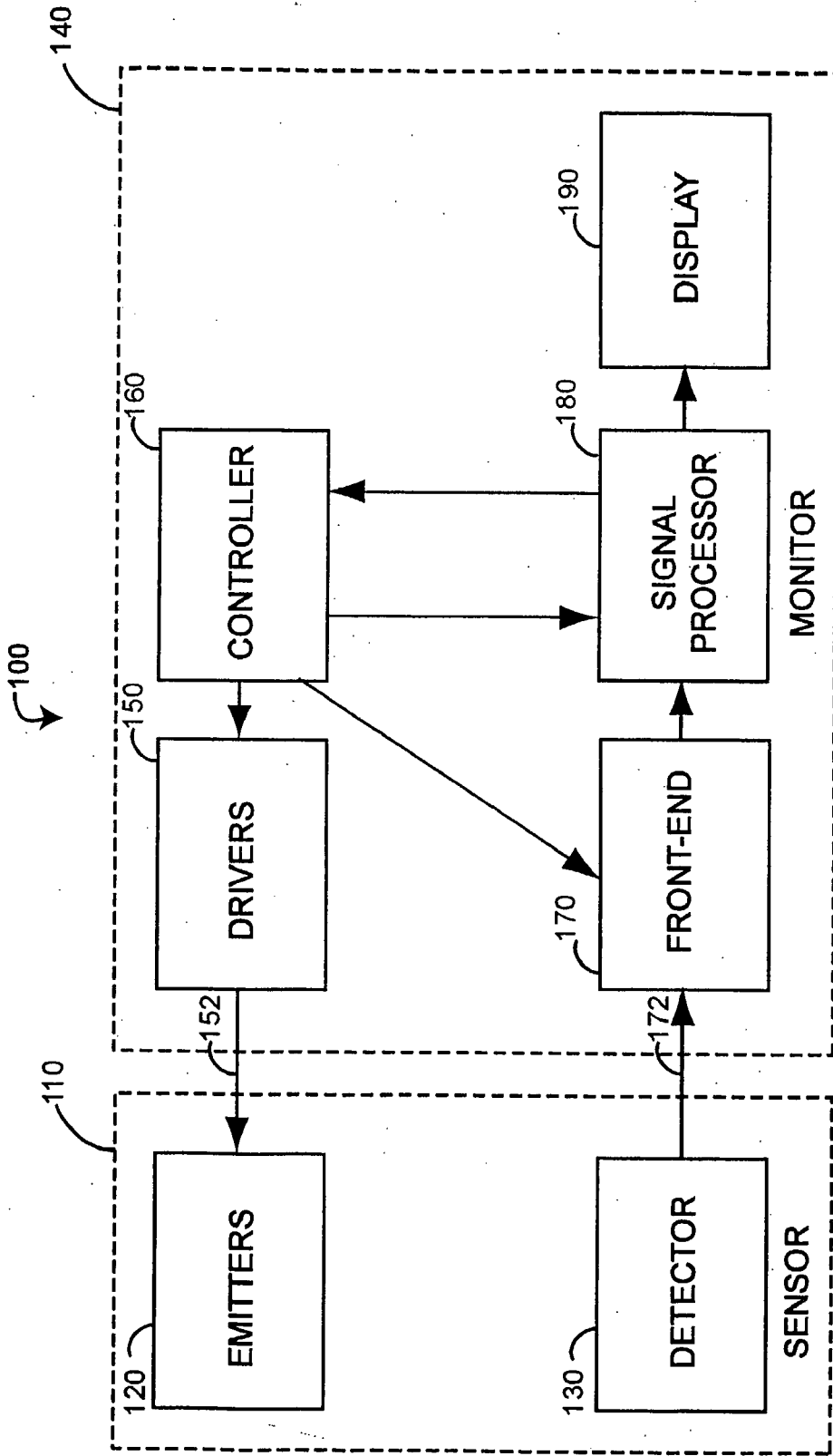


FIG. 1 (Prior Art)

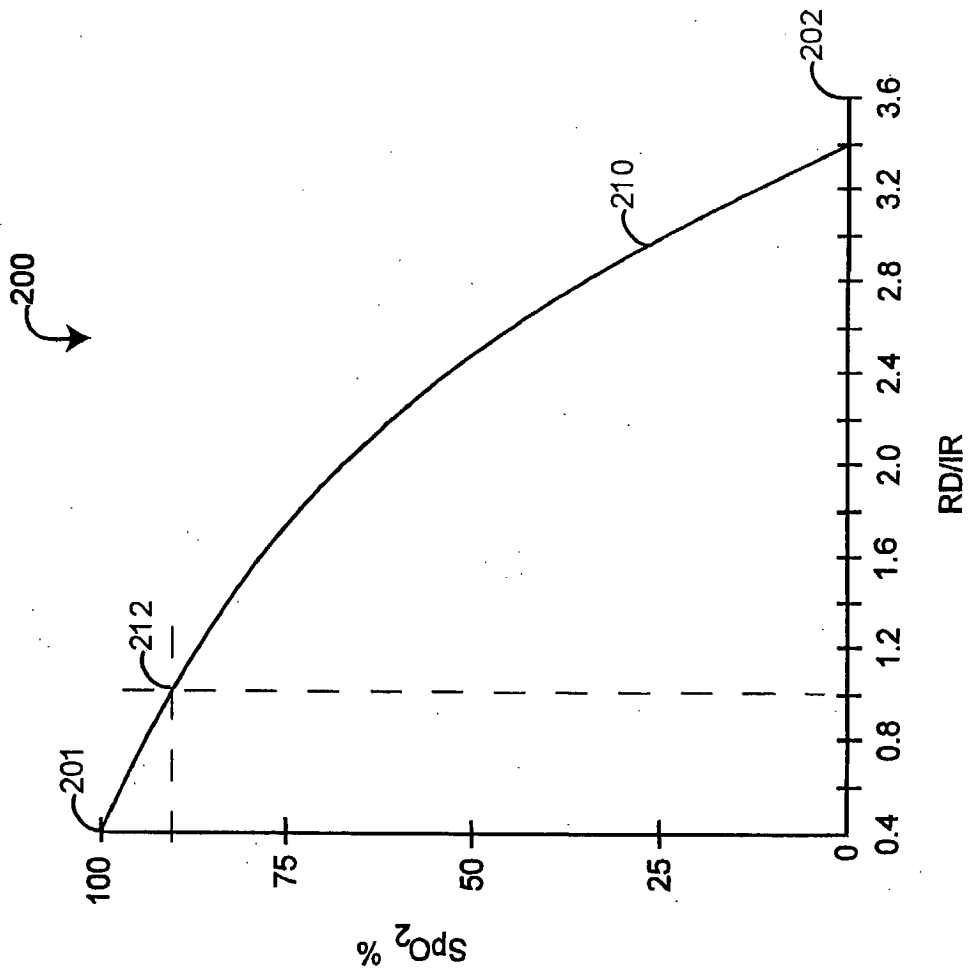


FIG. 2 (Prior Art)

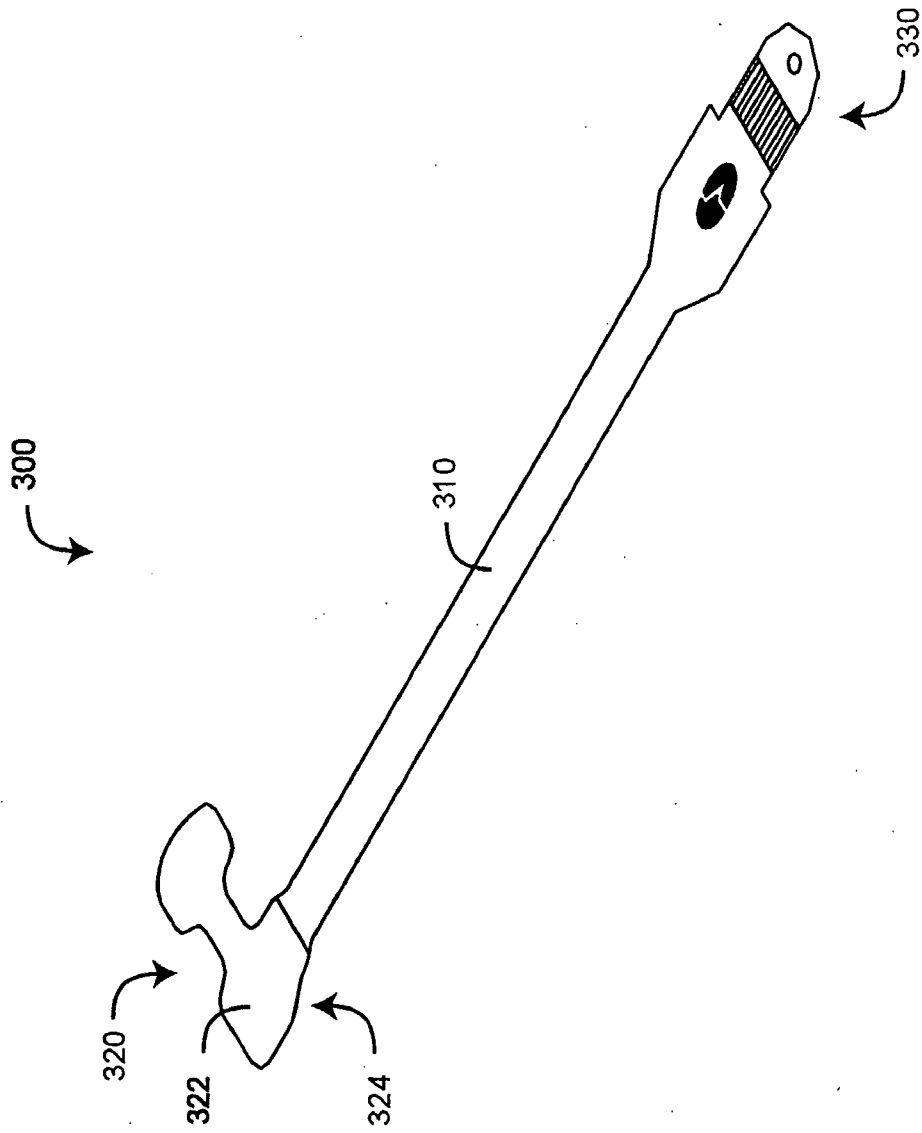


FIG. 3A

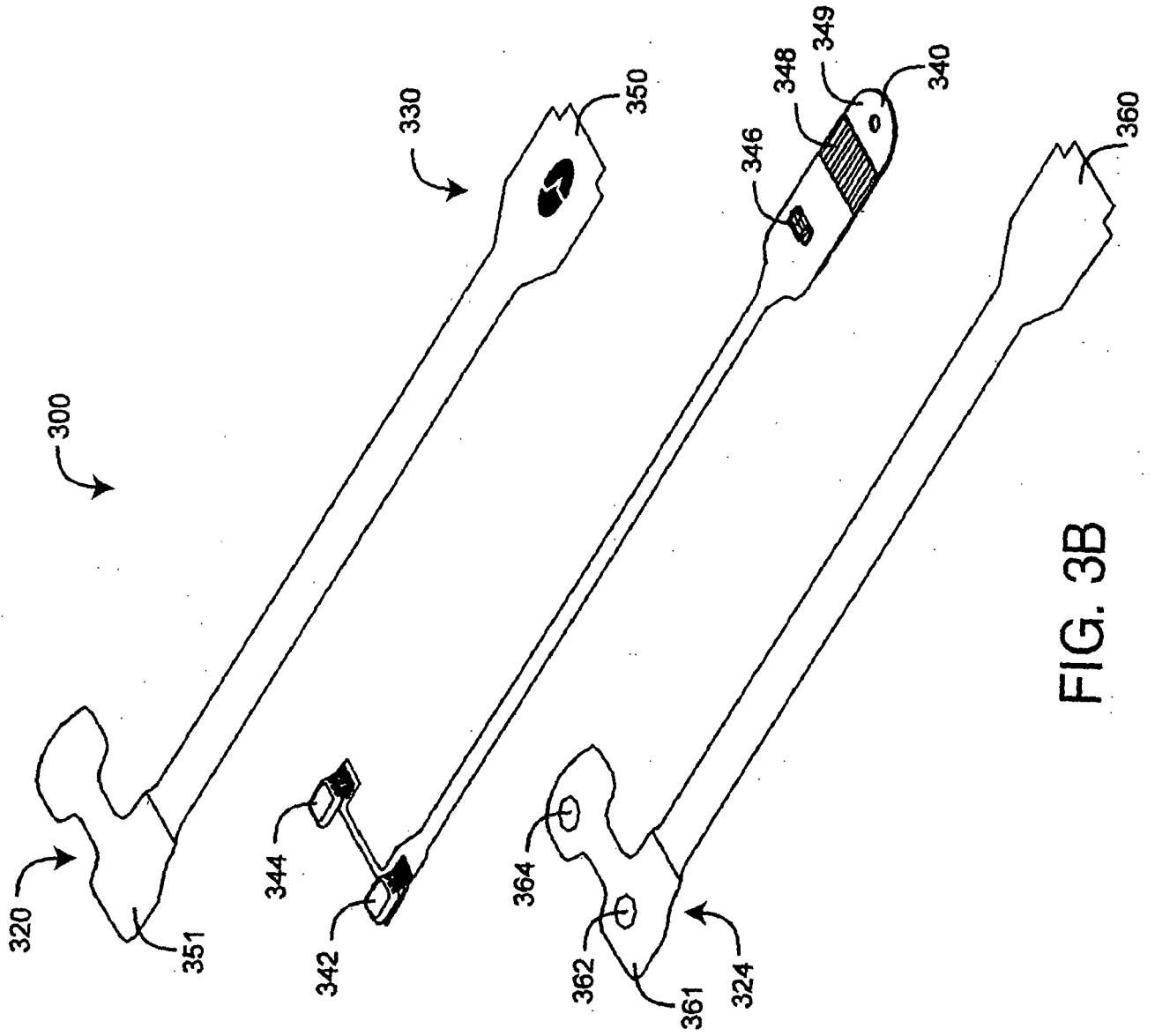


FIG. 3B

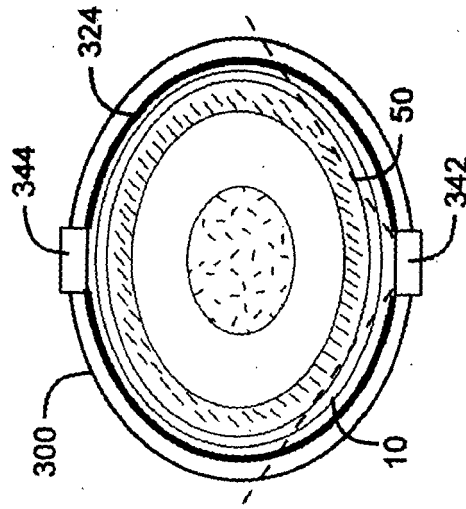


FIG. 6

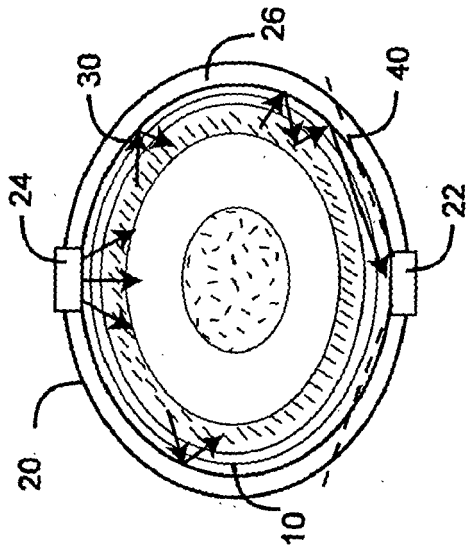


FIG. 5 (Prior Art)

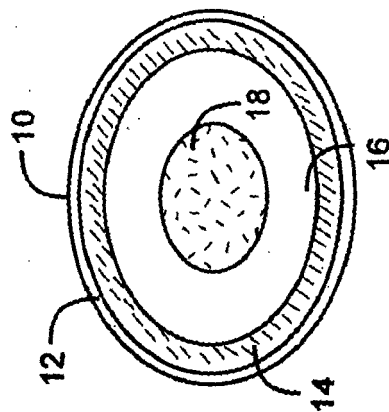


FIG. 4

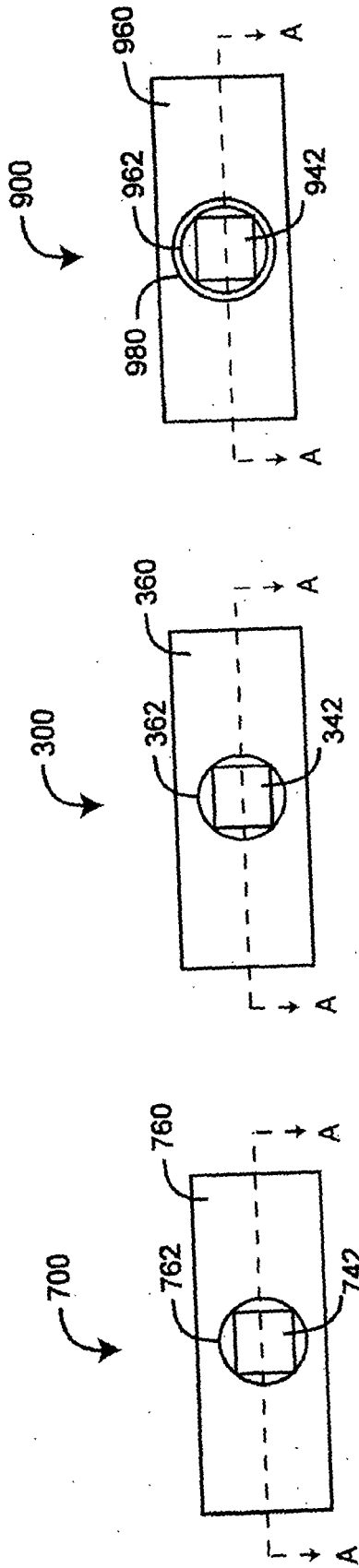


FIG. 9A

FIG. 8A

FIG. 7A (Prior Art)

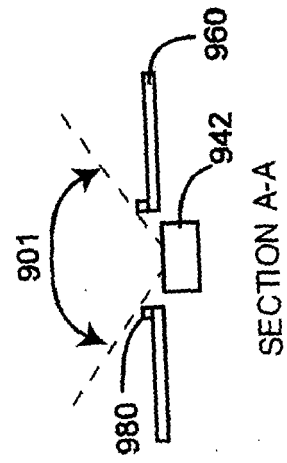


FIG. 9B

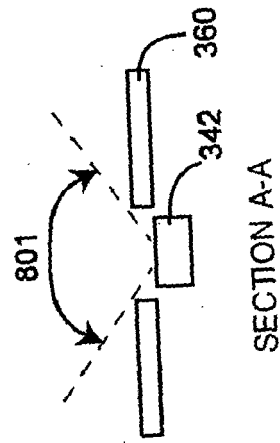


FIG. 8B

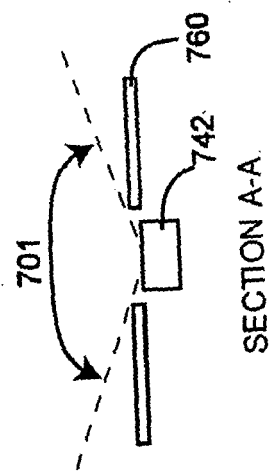


FIG. 7B (Prior Art)

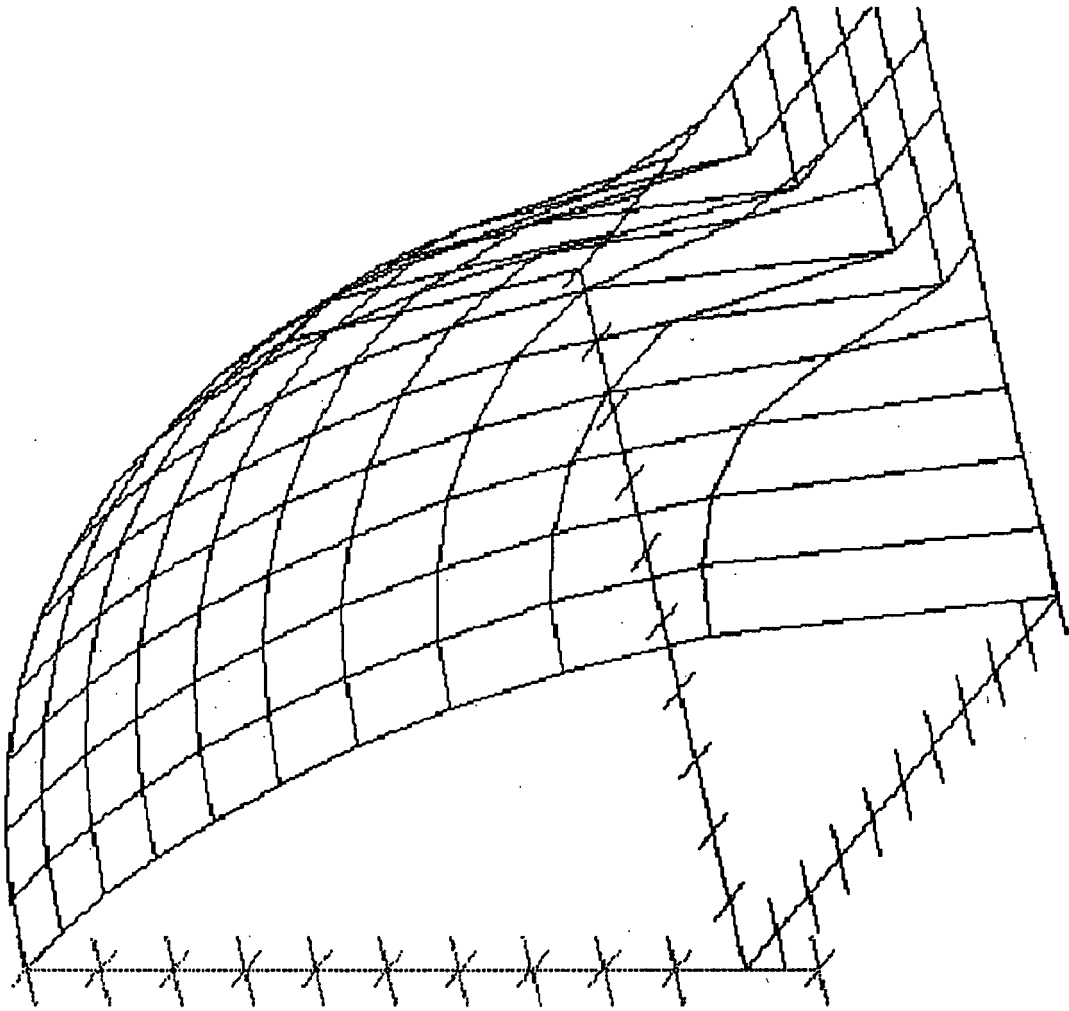


Figure 10

专利名称(译)	Cyanotic婴儿传感器		
公开(公告)号	<a href="#">EP1771109A2</a>	公开(公告)日	2007-04-11
申请号	EP2005772104	申请日	2005-07-07
[标]申请(专利权)人(译)	梅西莫股份有限公司		
申请(专利权)人(译)	Masimo公司		
当前申请(专利权)人(译)	Masimo公司		
[标]发明人	AL ALI AMMAR		
发明人	AL-ALI, AMMAR		
IPC分类号	A61B5/00 A61B5/1455		
CPC分类号	A61B5/14552 A61B5/1495 A61B5/6826 A61B5/6831 A61B2503/045		
代理机构(译)	法思博事务所		
其他公开文献	EP1771109B1		
外部链接	<a href="#">Espacenet</a>		

#### 摘要(译)

脉搏血氧饱和度传感器包括发射器，其配置成将具有多个波长的光传输到肉质介质中。检测器在被介质内流动的脉动血液的成分吸收后响应于发射的光，以产生强度信号。传感器头具有光吸收表面，适于靠近介质设置。发射器和检测器靠近传感器头设置。检测器窗口由传感器头限定并配置成限制检测器的视场。