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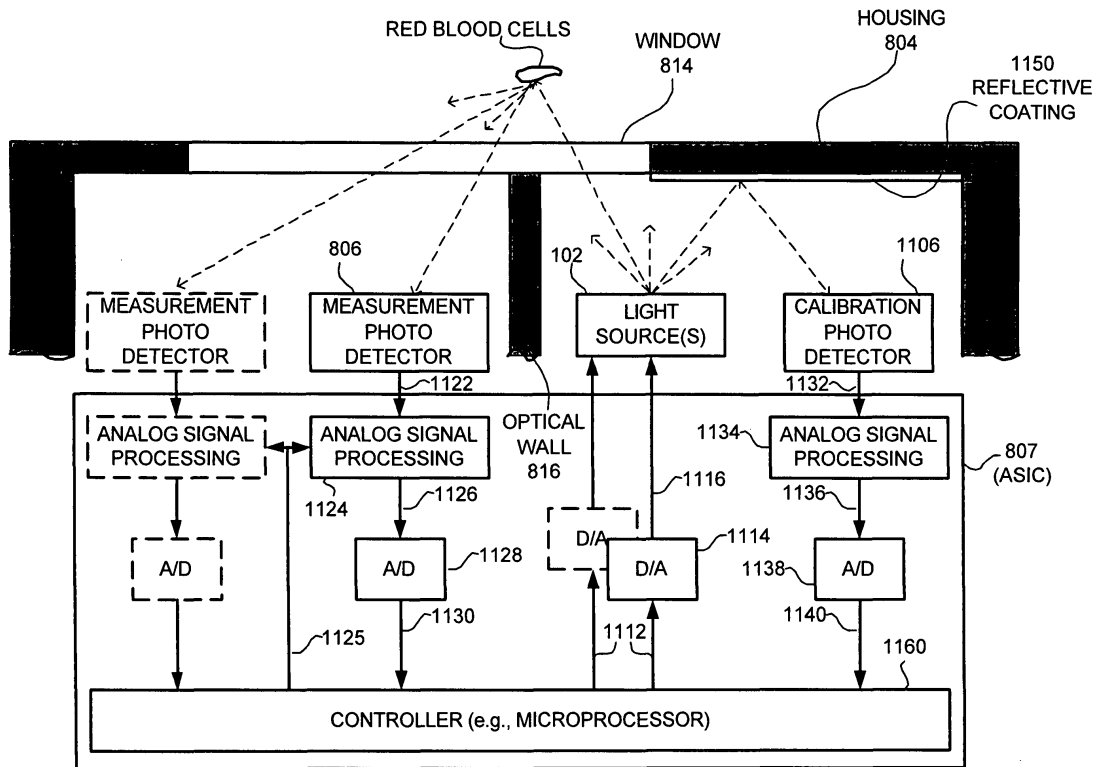
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(54) **Implantable self-calibrating optical sensors**

(57) A measurement light detector detects light transmitted by a light source (104,106,108) of an implantable system that is scattered back into an implantable housing (804), and produces a measurement signal indicative of the intensity of the light detected by the measurement light detector (806). A calibration light detector (1106) detects a portion of the transmitted light that has

not exited the housing (804), and produces a calibration signal (1132) that is indicative of the intensity of the light detected by the calibration light detector (1106), which is indicative of the intensity of the light transmitted by the light source. Changes in the intensity of the transmitted light are compensated for based on the calibration signal (1132) produced by the calibration light detector (106).



**FIG. 11A**

## Description

**[0001]** Embodiments of the present invention relate to implantable self-calibrating optical sensors that are used, e.g., for obtaining measures of blood oxygen saturation and/or hematocrit.

**[0002]** Blood oxygen saturation is the relative amount of oxygenated hemoglobin in all of the hemoglobin present in the blood stream. This hemoglobin is packaged in biconcave discs of approximately 10 micrometers diameter which commonly occur with a density of approximately five million red blood cells per cubic millimeter. When radiant energy (e.g., light) is incident upon red blood cells, the red blood cells both scatter and transmit the incident radiant energy. The differential absorption by oxygenated and non-oxygenated hemoglobin of the radiant energy reflected by and transmitted through the red blood cells furnishes the basis for the oxygen saturation measurements.

**[0003]** More specifically, pulse oximeters use light of two or more different centered wavelengths (e.g., produced by two or more light sources) to obtain measures of blood oxygen saturation by measuring the absorption and/or scattering of oxyhemoglobin and reduced hemoglobin. The measured scattering data allows for the calculation of the relative concentrations of reduced hemoglobin and oxyhemoglobin, and therefore blood oxygen saturation levels, since the scattering relationships are known.

**[0004]** Most multi-wavelength pulse oximeters are non-implantable devices that are clipped onto a patient's finger or ear lobe. However, it is believed that it would be beneficial to chronically implant pulse oximeters so that measures of oxygen saturation and hematocrit (the density of red blood cells) can be used as feedback for pacing optimization, disease monitoring, and the like.

**[0005]** Some multi-wavelength implantable oximeter catheters are known, as can be appreciated from U.S. Patent Nos. 3,847,483 and 4,114,604. For multi-wavelength oximeters to work properly, light from two or more light sources (e.g., from 670, 700 and 805 nm wavelength LEDs) should be combined into a single beam, to assure that the computed oxygen saturation is accurate with varying blood flow rate, pH, hematocrit and hemoglobin. In the devices of the '483 and '604 patents, fiber optic guides are used to combine the light of multiple wavelengths into the single beam. This, however, requires significant physical space. Thus, in the devices of the '482 and '604 patents, the light sources and fiber optic guides are located in a housing that is a distance from the measurement site, and optical fibers that are within a catheter are used to deliver the combined light beam to the measurement site at the distal end of the catheter.

**[0006]** It would be beneficial if an implantable optical combiner requiring less physical space can be provided, thereby enabling the optical combiner to be located at the measurement site.

**[0007]** The light sources that are used to produce the

light useful for obtaining measures of blood oxygen saturation, etc., may produce light of less intensity, as such light sources age. If not compensated for, this will affect the intensity of the scattered light detected by a photo detector, which will in turn adversely effect determinations of blood oxygen saturation, etc. Accordingly, there is also a need to compensate for changes in the intensity of the light produced by such light sources.

**[0008]** Embodiments of the present invention are directed to implantable systems, and methods for use therewith, that compensate for changes in the intensity of light transmitted by one or more light sources of the implantable systems. Such changes in intensity can be due, e.g., to aging of the light sources. The light sources can be, e.g., light emitting diodes (LEDs), but are not limited thereto.

**[0009]** In accordance with specific embodiments of the present invention, the implantable system includes an implantable housing including a window through which light can pass. The term window, as used herein, is intended to collectively encompass all portions of the housing through which light of interest can enter and exit the housing, even if such portions are separated from one another (e.g., by opaque portions). Included within the housing is at least one light source, a measurement light detector and a calibration light detector. Each light source transmits light of a corresponding wavelength. The intensity of the light transmitted by each light source is controlled by a corresponding drive signal that drives the light source. A portion of the light of each wavelength exits the housing through the window. The measurement light detector detects light of each wavelength scattered back into the housing through the window, and produces a measurement signal that is indicative of the intensity of the light of each wavelength detected by the measurement light detector. The calibration light detector detects a portion of the light of each wavelength that has not exited the housing, to produce a calibration signal that is indicative of the intensity of the light of the wavelength detected by the calibration light detector, which is indicative of the intensity of the light transmitted by each light source.

**[0010]** In accordance with specific embodiments, a controller adjusts each drive signal, based on the calibration signal, to keep the intensity of the light transmitted by each light source substantially constant. In accordance with other embodiments of the present invention, a controller adjusts the measurement signal, based on the calibration signal, to compensate for changes in the intensity of the light transmitted by each light source. In still other embodiments, rather than adjusting signals, a processor (that uses the measurement signal for a diagnostic and/or therapeutic purpose) detects changes in the intensity of the light transmitted by each light source based on the calibration signal, and takes into account the changes in intensity when using the measurement signal for a diagnostic and/or therapeutic purpose. For example, the processor can take such changes in intensity into

account by making appropriate adjustments to algorithms that are used to determine levels of blood oxygen saturation and/or levels hematocrit based on the measurement signal.

**[0011]** This invention may be carried into practice in various ways and some embodiments will now be described by way of example with reference to the accompanying drawings, in which:

**[0012]** FIG. 1 illustrates an apparatus for combining light of three different wavelengths from three physically separate light sources, according to an embodiment of the present invention;

**[0013]** FIG. 2 illustrates an apparatus for combining light of two different wavelengths from two physically separate light sources, according to an embodiment of the present invention;

**[0014]** FIG. 3 illustrates an apparatus for combining light of two different wavelengths from two physically separate light sources, according to another embodiment of the present invention;

**[0015]** FIG. 4 illustrates an apparatus for combining light of three different wavelengths from three physically separate light sources, according to still another embodiment of the present invention;

**[0016]** FIG. 5 illustrates an apparatus similar to the one shown in FIG. 1, but with the addition of combiner lenses between the light sources and prisms;

**[0017]** FIG. 6 illustrates an apparatus for combining light of three different wavelengths from three physically separate light sources, according to a further embodiment of the present invention;

**[0018]** FIG. 7 illustrates how panels can be used in place of prisms;

**[0019]** FIG. 8A illustrates an implantable oximetry sensor, according to an embodiment of the present invention;

**[0020]** FIG. 8B illustrates an implantable oximetry sensor, according to another embodiment of the present invention;

**[0021]** FIG. 9 illustrates an implantable lead that includes the sensor of FIG. 8A, in accordance with an embodiment of the present invention;

**[0022]** FIG. 10 illustrates a rough cross-section of the lead shown in FIG. 9;

**[0023]** FIGS. 11A and 11B illustrate implantable self-calibrating sensors, according to embodiments of the present invention;

**[0024]** FIG. 12A illustrates an exemplary implantable stimulation device in electrical communication with a patient's heart by way of three leads, which are suitable for delivering multi-chamber stimulation and shock therapy; and

**[0025]** FIG. 12B is a simplified block diagram of the multi-chamber implantable stimulation device of FIG. 12A.

**[0026]** In the description of the invention that follows, the left-most digit(s) of a reference number identifies the drawing in which the reference number first appears.

**[0027]** FIG. 1 shows a first embodiment of the present

invention that combines light of three different wavelengths from three physically separate miniature light sources using dichroic surfaces. Such dichroic surfaces are likely dichroic mirrors, but can be dichroic filters, or combinations thereof. Dichroic surfaces have the property of reflecting light of specific wavelengths and passing light of other wavelengths.

**[0028]** Referring to FIG. 1, a beam combiner structure 102, in accordance with an embodiment of the present invention, includes three physically separate light sources 104, 106 and 108, each of which produces radiation of a different wavelength (e.g., 670, 700 and 805 nm). The light sources are preferably light emitting diodes (LEDs), but can be other less preferable sources such as, but not limited to, laser diodes and incandescent lamps. The light sources are shown as being mounted to a structure (a cube in this example) which is made up of four triangular prisms 110a, 110b, 110c and 110d that are bonded together, e.g., using an optical cement or some other clear epoxy resin. Appropriate sides of the prisms are coated to thereby form a pair of dichroic surfaces, labeled dichroic surface #1 and dichroic surface #2. There are multiple ways this can be accomplished. However, it is believed that the most cost effective way is to have only one side of each prism 110a, 110b, 110c and 110d have a dichroic coating. For example, side 112a of prism 110a and side 112c of prism 110c can be coated to form dichroic surface #1, and side 112b of prism 110b and side 112d of prism 110d can be coated to form dichroic surface #2. While the prisms are likely made of glass, other suitable materials may be used, such as, but not limited to, plastics.

**[0029]** In accordance with an embodiment of the present invention, the dichroic surface #1 will reflect the wavelength ( $\lambda_1$ ) generated by the light source 104, and pass the wavelengths ( $\lambda_2$  and  $\lambda_3$ ) generated by light sources 106 and 108. Similarly, the dichroic surface #2 will reflect the wavelength ( $\lambda_3$ ) generated by the light source 108, and pass the wavelengths ( $\lambda_1$  and  $\lambda_2$ ) generated by light sources 104 and 106. This can be explained in more detail using an example where the wavelength generated by light source 104 is 670nm, the wavelength generated by light source 106 is 700nm, and the wavelength generated by light source 108 is 805nm (e.g.,  $\lambda_1$ ,  $\lambda_2$  and  $\lambda_3$  are, respectively, 670nm, 700nm and 805nm). Continuing with this example, the present invention can be implemented if dichroic surface #1 reflects light below 685nm and passes light above 685nm, and dichroic surface #2 reflects light above 750nm and passes light below 750 nm.

**[0030]** Still referring to FIG. 1, the dichroic surface #1 and the dichroic surface #2 and the light sources 104 and 108 are positioned (including angled) relative to one another such that light transmitted by the light source 104 is reflected by the dichroic surface #1 to travel in generally a same direction as light transmitted by the light source 108 that is reflected by the dichroic surface #2, as can be appreciated from the dashed lines shown. Ad-

ditionally, the light source 106 is positioned such that its light, which passes through the dichroic surfaces #1 and #2, travels in generally the same direction as the just mentioned reflected light, as can also be appreciated from the dashed lines shown.

**[0031]** In practice, the light sources 104, 106 and 108 are serially energized, in a non-overlapping temporal relationship. In the manner just described, the light of wavelengths  $\lambda_1$ ,  $\lambda_2$  and  $\lambda_3$  are combined into a single combined beam 130 that is transmitted toward patient tissue that includes red blood cells. The light of different wavelengths ( $\lambda_1$ ,  $\lambda_2$ , and  $\lambda_3$ ) are combined into the single beam so that the light of each wavelength shines equally on nearby red blood cells, to thereby increase the likelihood that the computed oxygen saturation is accurate with varying blood flow rate, pH, hematocrit and hemoglobin. A mask 120 may be used to reduce internal reflections.

**[0032]** When transmitted toward patient tissue, some of the light energy is scattered by blood. The different wavelengths are differently scattered, depending on the oxygen saturation level of the blood. After being scattered by blood, the interleaved light stream is received by a light detector (discussed below in more detail with reference to FIG. 8), which preferably produces a separate signal for each of the wavelengths. At a high level, time multiplexing is used to produce a signal path for each of the different wavelengths ( $\lambda_1$ ,  $\lambda_2$  and  $\lambda_3$ ) of received light. Each signal path will typically include one or more filters and an A/D converter to sample the received light signals. Using electronic circuitry, firmware and/or software, the received light signals can be analyzed so that oxygen saturation levels can be determined in any well known manner, or in any manner devised in the future.

**[0033]** While three-wavelength pulse oximetry provides more accuracy than two-wavelength pulse oximetry, the accuracy obtained using two-wavelength pulse oximetry is satisfactory for many applications. Accordingly, in accordance with embodiments of the present invention, one of the light sources 104, 106 and 108 can be eliminated. If light source 106 is eliminated, then two dichroic surfaces are still needed, as can be appreciated from FIG. 3. However, if light source 104 (or light source 108) is eliminated, then only a single dichroic surface is necessary, as shown in FIG. 2.

**[0034]** Referring to FIG. 2, the single dichroic surface reflects the wavelength generated by the light source 104 and passes the wavelength generated by the light source 106. Since only one dichroic surface is used, the assembly of prisms can be simplified. More specifically, the structure (also a cube in this example) can be made up of only two triangular prisms 210a and 210b.

**[0035]** In FIGS. 1, 2 and 3, the overall structures, formed from multiple prisms, were shown as being cubic. While embodiments of the present invention encompass such cubic structures, they should not be limited thereto. For example, other shapes, such as the ones shown in FIGS. 4 and 6, can be used. As can be seen from FIG. 4, the prisms 410a, 410b, 410c and 410d that make up

the structure form a shape that resembles a trapezoid. Also shown in FIG. 4 is that not all outer sides of the structure need be flat. More specifically, in this example, the outer side 414 of prism 410d, through which the combined light beam travels, is shown as being concave, to increase the exit angle. Also shown in FIG. 4 is that not all of the prisms need be of the same size and shape.

**[0036]** Referring now to FIG. 5, in accordance with an embodiment of the present invention, combiner lenses 522 can be added for reducing the emitted light angle before the light is combined by the dichroic surfaces. Such lenses 522 can be added in any of the embodiments described herein.

**[0037]** FIG. 6 illustrates a variant of the present invention that has a simpler but likely somewhat larger overall size than the structure shown in FIG. 1. In this embodiment, only three prisms 610a, 610b and 610c are used to form a three-dimensional rectangular structure. Another difference is that the pair of dichroic surfaces do not intersect each other, as was the case in the previously discussed embodiments where there were three light sources. The beam combining structure 602 functions in a similar manner as the other structures discussed above. That is, dichroic surface #1 reflects the wavelength of light generated by the light source 104, and passes the wavelengths of light generated by the light sources 106 and 108. The dichroic surface #2 reflects the wavelength of light generated by the light source 108 and passes the wavelength of light generated by the light source 106. Because the light generated by the light source 104 is not incident upon the dichroic surface #2, it is not required that the dichroic surface #2 pass the wavelength generated by the light source 104, but it is allowed.

**[0038]** In the above discussed FIGS. 1 through 6, the dichroic surfaces were described as being formed on sides of prisms. The use of such structures is beneficial because the prisms can be bonded together to form a sturdy structure to which the light sources can be securely attached, as shown in the FIGS. However, in alternative embodiments, explained below with reference 7, this need not be the case.

**[0039]** Referring to FIG. 7, rather than using prisms, panels 714 are attached on at least one edge to a substrate 724, and dichroic surface(s) are formed on sides of the panels 714. While the panels 714 are likely made of glass, other suitable materials such as plastics may be used. (For FIG. 7, picture the substrate 724 being in the same plane as the page, and panels 714 extending perpendicularly out of the page.) In this embodiment, rather than securing the light sources 104, 106 and 108 to prisms, as could be done in the previously discussed embodiments, the light sources 104, 106 and 108 are secured to the same substrate 724 to which the panels 714 are secured. As was discussed above with reference to FIGS. 2 and 3, one of the light sources can be eliminated if two-wavelength pulse oximetry is to be used. Further, as was explained with reference to FIG. 2, if the

light source to be eliminated is light source 104 or 108, then only one dichroic surface is required, which can be implemented using a single panel 714. In a similar manner as was described above with reference to FIGS. 4 and 6, the light sources and dichroic surfaces can be repositioned, so long as the arrangement results in the light of various wavelengths generally being combined into a single beam. Further, as was described with reference to FIG. 5, combiner lenses 522 can be added to the configuration shown in FIG. 7.

**[0040]** While the above described embodiments included either two or three separate light sources, one of ordinary skill in the art would understand, based on the above description, that light from more than three light sources can be combined in a similar manner. Accordingly, it is within the spirit and scope of the present invention that more than three light sources and more than two dichroic surfaces can be used. Such embodiments can be used for multi-wavelength oximetry that uses more than three wavelengths.

**[0041]** In accordance with other embodiments of the present invention, critical angle reflectors could be used instead of dichroic surfaces to accomplish combining of light from the two or more separate light sources. The critical angle is the largest angle off a surface at which light will be totally reflected from the surface. Sides of prisms or panels can be positioned relative to light sources such that light of two or more wavelengths, from two or more separate light sources, can be combined into a single beam in much the same way as was described above with the use of dichroic surfaces.

**[0042]** In accordance with embodiments of the present invention, the beam combiner assemblies discussed above can be built into a sensor assembly 802, such as those shown in FIGS. 8A and 8B. The sensor 802, in turn, can be built into an implantable lead 902, such as that shown in FIG. 9.

**[0043]** Referring to FIG. 8A, in accordance with an embodiment of the present invention the sensor assembly 802 includes a sensor enclosure or housing 804 within which are one of the beam combiner structures discussed above, a photo detector 806 and an optional application specific integrated circuit (ASIC) 807. In FIG. 8A, the beam combiner 102 is shown. However, any of the other beam combiners 202, 302, 402, 502, 602 and 702 may alternatively be used. In accordance with an embodiment of the present invention, the housing 804 includes a tube 808 and a pair of end caps 810 and 812 that can be used to hermetically seal the components within the housing 802. The tube 808 can be made of an opaque material, such as metal (e.g., titanium or stainless steel) or ceramic, so long as it includes a window 814 that passes light of all the wavelengths of interest in the combined light beam (e.g., 130). In an alternative embodiment, the entire tube 808 can be made of a material that passes light of all the wavelengths of interest in the combined beam, and thus, in this embodiment the entire tube can be considered a window. The window

814 can for example be made of synthetic sapphire or some other appropriate material that passes light of all the wavelengths of interest. Alternatively, the entire tube 808 can be made from synthetic sapphire or some other appropriate material that passes light of all the wavelengths of interest. Exemplary synthetic sapphires are marketed by Imetra, Inc. (Elmsford, New York) and Swiss Jewel (Philadelphia, Pennsylvania).

**[0044]** The beam combiner structure (e.g., 102), the window 814 and the photo detector 806 should be positioned such that the combined light beam produced by the beam combiner exits the housing 804 through the window 814 and such that the light backscattered from blood (outside the window) will be scattered back toward the photo detector 806. The optional ASIC 807, which can include filters, analog-to-digital circuitry, multiplexing circuitry, and the like, controls the light sources and processes the photo detector signals produced by the photo detector 806 in any manner well known in the art. The ASIC 807 preferably provides digital signals indicative of the photo detector signals to an implantable device, such as an implantable monitor, pacemaker, or ICD. If the ASIC 807 or equivalent circuitry is not included within the sensor, analog signals can be delivered between the sensor 802 and the implantable device. However, it is preferred that digital signals are sent to and from the sensor 802 because digital signals are less susceptible to noise and other degradation.

**[0045]** An opaque optical wall 816 is positioned between the beam combiner structure 102 and the photo detector 806, so that light is not internally reflected from the beam combiner 102 to the photo detector 806. The beam combiner 102, optical wall 816, photo detector 806 and ASIC 807 can be attached to a substrate 820, e.g., by an epoxy 818. The substrate can be, e.g., a printed circuit board (PCB). Bond wires 822 can be used to attach the various components to the substrate 820, as well as to attach the substrate 820 to terminals 824 which extend through an insulated feedthrough 826 in the end cap 810. The housing 804, the feedthrough 826 and the endcaps 810 and 812 preferably provide hermeticity. In an alternative embodiment, shown in FIG. 8B, the endcaps 810' and 812' are made of a conductive material, and the tube 808 is made of a nonconductive material (so that the endcaps are electrically isolated from one another). In such an embodiment, there is no need for the feedthrough 826 shown in FIG. 8A because the terminals 824 can be connected directly to the conductive endcaps 810' and 812'. Nevertheless, a feedthrough may be used in the embodiment of FIG. 8B if desired.

**[0046]** Referring now to FIG. 9, in accordance with specific embodiments of the present invention, the sensor module 802 is built into an implantable lead 902. Accordingly, in this embodiment, the housing 804 of the sensor module 802 is sized to fit within the implantable lead 902. More specifically, the size of the beam combiner is preferably about 2 millimeters (mm) or less, and the size (shown as "d" in FIG. 10) of the sensor module 802 is

about 4 mm or less, and preferably about 3 mm. The length of the sensor module 802, which extends axially in the lead 902 can be somewhat larger, because the length of the lead 902 is relatively large as compared to the diameter of the lead.

**[0047]** Further, the portion of the lead 902 that is adjacent to the window of the 814 of the sensor module, where light is to exit and enter, should allow the light to pass in and out of the sensor 802. Thus, the lead 902 may be transparent, or include its own window, opening, or the like. The lead 902 is shown as including tines 912 for attaching the lead in its desired position, but may include any other type of fixation means, or none at all. Additionally, the lead 902 may also include a lumen 916 for a stylet, which can be used for guiding the lead to its desired position. Also shown in FIG. 9 are wires 914 that provide power and possibly control signals to the sensor 802 from an implantable device, and provide pulse oxymetry signals from the sensor 802 to the implantable device. As discussed below, preferably there are only two wires 914, but there may be more. If the sensor 802 of FIG. 8B is used, then one wire 914 is attached to the terminal 824 that extends from the endcap 810', while another wire 914 is attached to the terminal 824 that extends from the other endcap 812'.

**[0048]** The lead 902 can be, e.g., an implantable right atrial lead for implant in a patient's right atrial appendage, a right ventricular lead for transvenous insertion into the heart, a coronary sinus lead for placement in the coronary sinus region, or some other lead. The lead 902 can be implanted in or near a patient's heart, but this is not necessary. The exemplary lead 902 shown in FIG. 9 is a right ventricular lead that includes a ring electrode 908 and a tip electrode 910 that are connected to an implantable device by way of wires 904 and 906. Instead of being placed in a lead that includes cardiac electrodes, the sensor can be within a catheter intended for placement in a blood vessel or other blood confining space.

**[0049]** Referring now to FIG. 10, which is a rough cross-sectional view along the dashed line shown in FIG. 9, in accordance with an embodiment of the present invention the tube portion 808 of the sensor housing 804 is generally "D" shaped, so that it can be readily included with the implantable lead 902, while still allowing the lumen 916 (for a stylet) and wires 904 and 906 to fit within the same inner-space of the lead 902. Alternative shapes are also within the scope of the present invention. If the sensor 802 of FIG. 8B is used, then one of the wires 914 would also be seen in the cross-section of FIG. 10.

**[0050]** After the ASIC 807 controls the light sources the processes signals produced by the photo detector 806 in a manner well known in the art, it delivers signals indicative of the intensity of the detected light to an implantable device, an example of which is discussed below with reference to FIGS. 12A and 12B. The implantable device further processes the signal, e.g., for diagnostic and/or therapeutic use. Preferably, the ASIC 807 has all electronics to provide a two-wire 914 digital interface to

the implantable device, as shown in FIG. 9. Further, one of the two sensor wires 914 may be combined with one of the pacing electrode wires 904 or 906 so that only three total wires are needed. Even further, a more complex 2-wire approach could use sub-pacing threshold signals between the implantable device and the sensor 802 using the same two wires 904 and 906 that connect to the pacing electrodes 908 and 910 resulting in a total of two wires in the lead 902 to the implantable device.

**[0051]** The lead 902 within which the sensor 802 is contained is attached to an implantable device. It is also possible that the sensor 802 is within a self contained hermetically sealed housing that communicates wirelessly with the implantable device. As mentioned above, the implantable device can be, e.g., a monitor, pacemaker, or ICD. For completeness, an exemplary implantable device 1210, that can be used to perform pacing, detect an arrhythmia, perform anti-arrhythmia therapy, detect specific cardiac events, etc., is described with reference to FIGS. 12A and 12B.

**[0052]** In accordance with embodiments of the present invention, the components are hermitically sealed within the sensor 802. Preferably the only elements running to and from the sensor 802 are wires 914 for providing power and possibly control signals to the sensor 802, and receiving pulse oxymetry signals from the sensor 802.

**[0053]** In accordance with other embodiments of the present invention, the oxymetry sensor module 802 is located within the housing of an implantable device that includes a window through which light can be transmitted and received. In still another embodiment, the oxymetry sensor module 802 is in its own hermetically sealed housing that is attached directly to an implantable cardiac device. Additional details of how this can be accomplished are provided in commonly assigned U.S. Patent Application No. 10/913,942, entitled "Autonomous Sensor Modules for Patient Monitoring".

**[0054]** As mentioned above, the ASIC 807 (and/or other circuitry) controls the light sources and processes signals produced by the photo detector 806, as well as delivers signals indicative of the intensity of the detected light to an implantable device, an example of which is discussed below with reference to FIGS. 12A and 12B. The implantable device further processes the signal, e.g., for diagnostic and/or therapeutic use. For example, the implantable device can include a microcontroller that determines levels of blood oxygen saturation and/or hematocrit based on the signals it receives from the photo detector 806. Such measures of oxygen saturation can be used, e.g., for pacing optimization, disease monitoring, and the like. Additionally or alternatively, the measures of oxygen saturation can be stored in memory for later transmission to an external device.

**[0055]** As also mentioned above, the ASIC 807 (and/or other circuitry) can include filters, analog-to-digital circuitry, multiplexing circuitry, and the like, to control the light sources and process the photo detector signals produced by the photo detector 806. The ASIC 807 prefer-

ably provides digital signals indicative of the photo detector signals to an implantable device, such as an implantable monitor, pacemaker, or ICD. If the ASIC 807 or equivalent circuitry is not included within the sensor, analog signals can be delivered between the sensor 802 and the implantable device. However, it is preferred that digital signals are sent to and from the sensor 802 because digital signals are less susceptible to noise and other degradation. It is also possible, as mentioned above, that the sensor module 802 is located within the housing of an implantable device that includes a window through which light can be transmitted and received, or that the sensor module 802 is in its own hermetically sealed housing that is attached directly to an implantable cardiac device.

**[0056]** Each light source (e.g., LED) transmits light in response to being driven by a drive signal, which is typically a current signal, but can be a voltage signal. As the light sources age they become less efficient in that for a same drive signal they will transmit light of less intensity. If not compensated for, this will affect the intensity of the light detected by the photo detector 806, which will in turn adversely effect determinations of blood oxygen saturation, etc. In accordance with specific embodiments of the present invention, to overcome this problem, a calibration photo detector 1106 is added, the output of which is used to compensate for aging or other changes to the light source(s), as will now be described with reference to FIG. 11A.

**[0057]** FIG. 11A shows additional details of the ASIC 807, in accordance with specific embodiments of the present invention. However, it should be noted that the circuitry shown in FIG. 11A need not be implemented within the ASIC 807. For clarity, the photo detector 806 that detects light scattered back into the housing 804 through the window 814 will often be referred to hereafter as the measurement photo detector 806, and the added photo detector 1106 that is used to compensate for changes in the light sources (e.g., due to aging) will be referred to as the calibration photo detector 1106. Additionally, when discussing FIG. 11A, the beam combiner structure 102 will often be referred to simply as light source(s) 102, because the embodiments that relate to compensation can be used with a single light source, or with a device that does not necessarily use the specific beam combiners described above. Nevertheless, the embodiments described with reference to FIG. 11A would be very useful with the beam combiners described above.

**[0058]** Referring to FIG. 11A, each light source transmits light having an intensity that is controlled by a corresponding drive signal 1112/1116. Such drive signal is controlled by a controller 1160, which likely outputs a digital drive control signal 1112 which is converted to an analog drive signal 1116 by a digital-to-analog converter (D/A) 1114. The controller 1160 in this embodiment, and other embodiments, can be a microcontroller, a processor, a state machine, random logic, or the like. The light

output by the light source(s) is projected over a wide range of angles (e.g., from 120 degrees to 180 degrees). Accordingly, a portion of this light exits the housing 804 through the window 814, while other portions of the light are internally reflected.

**[0059]** As explained above, the opaque optical wall 816 is positioned between the light source(s) 102 and the measurement photo detector 806, to prevent the measurement photo detector 806 from detecting internally reflected light. (It is noted, that due to imperfections, the measurement photo detector 806 may detect a small amount of internally reflected light, which is allowed). In contrast, the calibration photo detector 1106 is placed on the same side of the wall 816 as the light sources 102, and positioned relative to the window 814 such that the calibration photo detector 1106 detects internally reflected light from the light source(s) 102 without detecting light that is scattered back into the housing 804 through the window 814. (It is noted, that due to imperfections, the calibration photo detector 806 may detect a small amount of scattered light, which is allowed). Alternatively, the region of the window above the calibration photo detector 1106 can have a blocking or a reflecting coating such that the calibration photo detector 1106 generally only detects internally reflected light from the light source (s) 102. It is also possible that the calibration photo detector 1106 is arranged such that it detects light transmitted directly from the light source(s) 102, i.e., the light need not be internally reflected. For simplicity, the window 814 in FIG. 11A and the previously described FIGS. has been generally shown as a single portion through which light of interest can enter and exit the housing 804. However, it is noted that such window 814 can be made up of more than one distinct portion through which light of interest can enter and exit the housing 804. For example, light may exit the housing 804 through a first portion of the window 814, while scattered light enters the housing 804 through a second portion of the window 814, where the first and second portions of the window are not contiguous. In other words, the term window 814, as used herein, is intended to collectively encompass all portions of the housing through which light can enter and exit the housing, even if such portions are separated from one another (e.g., by opaque portions).

**[0060]** In the above arrangement of FIG. 11A, the measurement photo detector 1106 detects light scattered back into the housing 804 through the window 814, and produces a measurement signal 1122 that is indicative of the intensity of the light detected by the measurement light detector 1106. The measurement signal 1112 is preferably filtered and amplified by an analog signal processing block 1124 (e.g., which includes a filter and amplifier), and digitized by an analog-to-digital (A/D) converter 1128, so that a digitized version 1130 of the signal is provided to the controller 1160.

**[0061]** The calibration light detector 1106, on the other hand, detects a portion of the light transmitted by the light source(s) that has not exited the housing 804 (e.g., the

light is internally reflected and/or received directly from the light source(s)), and produces a calibration signal 1132 that is indicative of the intensity of such detected light. The calibration signal 1132 is preferably filtered and amplified by an analog signal processing block 1134 (e.g., which includes a filter and/or amplifier) and digitized by an analog-to-digital (A/D) converter 1140, so that a digitized version 1140 of the signal is provided to the controller 1160.

**[0062]** In FIG. 11A, a separate D/A converter 1114 and drive signal 1112 are shown for each light source. In an alternative embodiment, the controller can output a time multiplexed drive signal 1112 that is provided to a single D/A converter 1114, and a demultiplexer can be provided at the output of the D/A converter 1114. Such a demultiplexer will provide the analog version of the drive signal to the appropriate light source. Similarly, in FIG. 11A the measurement photo detector 806 is shown as having its own analog signal processing block 1124 and A/D converter 1128, and the calibration photo detector 1106 has its own analog signal processing block 1134 and A/D converter 1138. In an alternative embodiment, a multiplexer is provided at the outputs of the detectors 806 and 1106 so that a single analog signal processing block and A/D converter can be used. In other words, such a multiplexer can be provided between a single analog signal processing block and the detectors 806 and 1106. Such embodiments would reduce the circuitry, e.g., of the ASIC 807.

**[0063]** The calibration signal 1132, or the filtered, amplified and digitized version thereof (i.e., 1140), is used to compensate for changes to the lights source(s) 102, e.g., due to aging, as will be described below. For example, in specific embodiments, the controller 1160, adjusts the drive signal 1112, based on the intensity of the light detected by the calibration photo detector 1106, in order to keep the intensity of light transmitted by a light source substantially constant. More specifically, the controller 1160 adjusts the drive signal 1112, based on the calibration output signal 1132, or the filtered, amplified and digitized version thereof (i.e., 1140), to keep the intensity of the light transmitted by each light source substantially constant. Where there are two or more light sources, this does not necessarily mean that all the light sources will be kept at a same substantially constant intensity. Rather, this means that the intensity of each individual light source is kept substantially constant, but that the intensity of one light source can be different than the intensity of another light source. In a specific embodiment, the intensity of light transmitted by a light source is kept substantially constant by adjusting the drive signal 1112 in an effort to keep the portion of the calibration signal 1132 corresponding to that light source at a specified level.

**[0064]** In alternative embodiments, rather than adjusting the drive signals 1112 to compensate for changes to the lights source(s) 102, adjustments are made to the measurement signal 1122 to compensate for changes in the intensity of the light source(s) 102. This can be ac-

complished as follows. The controller 1160 detects changes (likely reductions) in the intensity of the light source(s) 102 by detecting changes in the calibration signal 1132, or the filtered, amplified and digitized version thereof (i.e., 1140), in a similar manner as was discussed above. Then, based on the changes in the calibration output signal 1132, or the filtered, amplified and digitized version thereof (i.e., 1140), the controller 1160 adjusts the measurement signal 1122. This can be accomplished, e.g., by using a gain adjustment signal 1125 to adjust the gain of an amplifier within the analog signal processing block 1124. For example, if the controller detects a 5% reduction in the intensity of light of a specific wavelength (i.e., light from a specific light source) based on the calibration signal 1132, the controller can increase the gain in an amplifier of the analog signal processing block 1124 by 5%.

**[0065]** In still other embodiments, rather than adjusting actual signals (e.g., a drive signal or measurement signal), a processor algorithmically compensates for changes to the intensity of the lights source(s) 102. More generally, a processor that uses the measurement signal 1122 (for a diagnostic and/or therapeutic purpose), detects changes in the intensity of the light transmitted by each light source based on the calibration signal, and the processor takes into account such changes in intensity when using the measurement signal for its diagnostic and/or therapeutic purpose. For example, if the controller detects a 5% reduction in the intensity of light of a specific wavelength (i.e., light from a specific light source) based on the calibration signal 1132, the processor can take such reduction into account when determining levels of blood oxygen saturation and/or levels of hematocrit. For example, if the processor uses a multi-dimensional lookup table to determine levels of blood oxygen saturation, based on the intensity of detected scattered light, the processor can adjust where to look in the look-up table based on changes in the calibration signal. For another example, if the processor uses an algorithm to determine levels of blood oxygen saturation, based on the intensity of detected scattered light, the processor can make adjustments to the algorithm based on changes in the calibration signal. These are just a few examples of how a processor can take into account changes in the intensity of the calibration signal when using the measurement signal for a diagnostic and/or therapeutic purpose. In specific embodiments, the processor that uses the measurement signal for its diagnostic and/or therapeutic purpose is in a separate implantable housing that is connected to the housing 804 by one or more lead. For example, the processor can be within a housing of a stimulation device (e.g., device 1210 of FIG. 12A).

**[0066]** As mentioned above, in addition to using the above described sensors to measure levels of blood oxygen saturation, such sensors can also be used to measure levels of hematocrit, which refers to the percentage of packed red blood cells in a volume of whole blood. Various techniques are known for determining hemat-

ocrit based on scattered light. For example, light of about 500 nm and light of about 800 nm can be directed at a blood sample, and an algorithm can be used to calculate hematocrit based on the intensities of detected scattered light. In another technique, a pair of spatially separated photo detectors can be used to detect reflected infra red (IR) light, e.g., of 805 nm. The intensity of the IR light detected by the photo detector that is nearer to the IR light source is referred to as IR<sub>near</sub>, and the intensity of the IR light detected by the photo detector farther from the IR light source is referred to as IR<sub>far</sub>. As described in article by Bornzin et al., entitled "Measuring Oxygen Saturation and Hematocrit Using a Fiberoptic Catheter", IEEE 19th Annual Conf. of the Eng. & Biol. Soc. (1997), the ratio:  $R = IR_{near} / IR_{far}$  is directly related to the level of hematocrit, but independent of oxygen saturation because 805 nm is an isobestic wavelength. To implement this technique using the sensor configuration shown in FIG. 11A, a second measurement photo detector 806 (shown in dashed line) can be added, with the second measurement photo detector being further from (or closer to) the light source(s) 102 than the other measurement photo detector 806. This second measurement photo detector can have its own corresponding analog signal processing block and A/D converter, or such circuitry can be shared (e.g., multiplexed) with the other measurement photo detector. The above described embodiments of the present invention can be used to compensate for changes in the intensity of the IR light source, e.g., due to aging. In specific embodiments of the present invention, the second measurement photo detector is placed within the housing 804 as shown in FIGS. 8A, 8B, 9 and 10, thereby enabling levels of hematocrit to be measured without the need for relatively large fiber optic guides, use of which was taught in the above mentioned Bornzin et al. article. For example, referring back to FIGS. 8A, 8B, 9 and 10, such second measurement photo detector can be located farther from the optical wall 816 than the photo detector 806 shown, as can be appreciated from FIG. 11A.

**[0067]** In an alternative embodiment, rather than having two spatially separated measurement photo detectors, two light sources (e.g., two 805 nm LEDs) can be spatially separated and time multiplexed, with one light source being closer to the measurement photo detector 806 than the other. In this alternative embodiment, the same ratio  $R = IR_{near} / IR_{far}$  can be determined, with the IR<sub>near</sub> corresponding to scattered light originating from the LED that is closer to the measurement photo detector 806, and the IR<sub>far</sub> corresponding to scattered light originated from the LED farther from the measurement photo detector 806. An example of this is shown in FIG. 11 B, which shows an exemplary layout of elements that can be inserted into a sealed tube 808 (not shown in FIG. 11 B), as described above in the discussion of FIG. 8A. Using a pair of spatially separated 805nm light sources is advantageous, as compared to using a pair of spatially separated measurement light detectors, be-

cause light sources (such as LEDs) are typically significantly smaller than photo detectors, thus resulting in space savings. As with the previously described embodiments, the calibration photo detector 806 will detect internally reflected light from the near and far light sources 202, and the measurement photo detector 806 will detect scattered light from the near and far light sources 202.

**[0068]** Combinations of the above described embodiments that compensated for changes in light intensity are also within the scope of the present invention. For example, it may be that the drive signal 1112 is only increased when the intensity of a light source has decreased by a specific level, and that up to that point a processor performs any necessary compensation algorithmically. This is just one example of how the above described embodiments can be combined, which is not meant to be limiting. It is also noted that the above described embodiments that compensate for changes in the intensity of light produced by one or more implanted light source can also be used with implantable photo plethysmography (PPG) devices, such as, but not limited to those described in the following commonly assigned patents and application: U.S. Patent No. 6,491,639 (Turcott); U.S. Patent No. 6,561,984 (Turcott); U.S. Patent No. 6,731,967 (Turcott); U.S. No. 6,942,622 (Turcott); and U.S. Patent Application No. 10/764,419 (Turcott), filed January 23, 2004.

#### Exemplary Stimulation Device

**[0069]** Referring to FIG. 12A, the exemplary implantable stimulation device 1210 is shown as being in electrical communication with a patient's heart 1212 by way of three leads, 1220, 1224 and 1230, suitable for delivering multi-chamber stimulation and shock therapy. The sensor module 802 of the present invention can be placed within any of these leads, as was described above. Alternatively, a further dedicated lead or catheter can be provided for the purpose of containing the sensor 802 and placing the sensor 802 at a desired measurement site.

**[0070]** To sense atrial cardiac signals and to provide right atrial chamber stimulation therapy, the stimulation device 1210 is coupled to an implantable right atrial lead 1220 having at least an atrial tip electrode 1222, which typically is implanted in the patient's right atrial appendage.

**[0071]** To sense left atrial and ventricular cardiac signals and to provide left-chamber pacing therapy, the stimulation device 1210 is coupled to a "coronary sinus" lead 1224 designed for placement in the "coronary sinus region" via the coronary sinus for positioning a distal electrode adjacent to the left ventricle and/or additional electrode(s) adjacent to the left atrium. As used herein, the phrase "coronary sinus region" refers to the vasculature of the left ventricle, including any portion of the coronary sinus, great cardiac vein, left marginal vein, left posterior ventricular vein, middle cardiac vein, and/or small cardiac

vein or any other cardiac vein accessible by the coronary sinus.

**[0072]** The exemplary coronary sinus lead 1224 is designed to receive atrial and ventricular cardiac signals and to deliver left ventricular pacing therapy using at least a left ventricular tip electrode 1226, left atrial pacing therapy using at least a left atrial ring electrode 1227, and shocking therapy using at least a left atrial coil electrode 1228.

**[0073]** The stimulation device 1210 is also shown in electrical communication with the patient's heart 1212 by way of an implantable right ventricular lead 1230 having, in this embodiment, a right ventricular tip electrode 1232, a right ventricular ring electrode 1234, a right ventricular (RV) coil electrode 1236, and an SVC coil electrode 1238. Typically, the right ventricular lead 1230 is transvenously inserted into the heart 1212 so as to place the right ventricular tip electrode 1232 in the right ventricular apex so that the RV coil electrode 1236 will be positioned in the right ventricle and the SVC coil electrode 1238 will be positioned in the superior vena cava. Accordingly, the right ventricular lead 1230 is capable of receiving cardiac signals and delivering stimulation in the form of pacing and shock therapy to the right ventricle.

**[0074]** As illustrated in FIG. 12B, a simplified block diagram is shown of the multi-chamber implantable stimulation device 1210, which is capable of treating both fast and slow arrhythmias with stimulation therapy, including cardioversion, defibrillation, and pacing stimulation. While a particular multi-chamber device is shown, this is for illustration purposes only, and one of skill in the art could readily duplicate, eliminate or disable the appropriate circuitry in any desired combination to provide a device capable of treating the appropriate chamber(s) with cardioversion, defibrillation and pacing stimulation.

**[0075]** The housing 1240 for the stimulation device 1210, shown schematically in FIG. 12B, is often referred to as the "can", "case" or "case electrode" and may be programmably selected to act as the return electrode for all "unipolar" modes. The housing 1240 may further be used as a return electrode alone or in combination with one or more of the coil electrodes, 1228, 1236 and 1238, for shocking purposes. The housing 1240 further includes a connector (not shown) having a plurality of terminals, 1242, 1244, 1246, 1248, 1252, 1254, 1256, and 1258 (shown schematically and, for convenience, the names of the electrodes to which they are connected are shown next to the terminals).

**[0076]** As such, to achieve right atrial sensing and pacing, the connector includes at least a right atrial tip terminal (AR TIP) 1242 adapted for connection to the atrial tip electrode 1222.

**[0077]** To achieve left chamber sensing, pacing and shocking, the connector includes at least a left ventricular tip terminal (VL TIP) 1244, a left atrial ring terminal (AL RING) 1246, and a left atrial shocking terminal (AL COIL) 1248, which are adapted for connection to the left ventricular tip electrode 1226, the left atrial ring electrode

1227, and the left atrial coil electrode 1228, respectively.

**[0078]** To support right chamber sensing, pacing and shocking, the connector further includes a right ventricular tip terminal (VR TIP) 1252, a right ventricular ring terminal (VR RING) 1254, a right ventricular shocking terminal (RV COIL) 1256, and an SVC shocking terminal (SVC COIL) 1258, which are adapted for connection to the right ventricular tip electrode 1232, right ventricular ring electrode 1234, the RV coil electrode 1236, and the SVC coil electrode 1238, respectively.

**[0079]** The connector is also shown as including terminals 1259 and 1261 (OXYMETRY TERMINALS), which are configured for connection to the wires 914 that are connected to the sensor module 802, to support the delivery of control signals to the sensor module 802, and to collect oxymetry data from the sensor module 802.

**[0080]** At the core of the stimulation device 1210 is a programmable microcontroller 1260 which controls the various modes of stimulation therapy, including pacing optimization and anti-arrhythmia therapy. The microcontroller 1260 can also determine measures of blood oxygen saturation and/or hematocrit based on the signals it receives from an oximetry sensor of the present invention. Such measures of oxygen saturation and/or hematocrit can be used, e.g., for pacing optimization, disease monitoring, and the like. Additionally or alternatively, the measures of oxygen saturation and/or hematocrit can be stored in memory 1294 for later transmission to an external device 1202 using the telemetry circuit 1201.

**[0081]** If the oxymetry sensor module 802 provides analog signals to the implantable device, then the terminals 1259 and 1261, through switch 1274, can provide such signals to an analog-to-digital (A/D) converter 1290 that converts the signals to a digital format understood by the microcontroller 1260. It is also possible that a dedicated A/D converter be provided within the implantable device 1210 for the purpose of digitizing signals received from the oximetry sensor. If the oximetry sensor 802 provides digital signals to the implantable device 1210, then such signals may be provided directly to the microcontroller 1210, assuming it is the microcontroller 1260 that performs the processing that determines measures of blood oxygen saturation and/or hematocrit based on the signals. It is also possible that the implantable device 1210 include circuitry, external to the microcontroller 1260, which is dedicated to determining measures of blood oxygen saturation and/or hematocrit.

**[0082]** As is well known in the art, the microcontroller 1260 typically includes a microprocessor, or equivalent control circuitry, designed specifically for controlling the delivery of stimulation therapy and can further include RAM or ROM memory, logic and timing circuitry, state machine circuitry, and I/O circuitry. Typically, the microcontroller 1260 includes the ability to analyze signals (data) as controlled by a program code stored in a designated block of memory. The details of the design of the microcontroller 1260 are not critical to the present invention. Rather, any suitable microcontroller 1260 can be used

to carry out the functions described herein. The use of microprocessor-based control circuits for performing timing, control and data analysis functions are well known in the art.

**[0083]** Representative types of control circuitry that may be used with the invention include the microprocessor-based control system of U.S. Pat. No. 4,940,052 (Mann et. al.) and the state-machines of U.S. Pat. No. 4,712,555 (Thornander et al.) and U.S. Pat. No. 4,944,298 (Sholder). For a more detailed description of the various timing intervals used within the stimulation device and their inter-relationship, see U.S. Pat. No. 4,788,980 (Mann et. al.).

**[0084]** As shown in FIG. 12B, an atrial pulse generator 1270 and a ventricular pulse generator 1272 generate pacing stimulation pulses for delivery by the right atrial lead 1220, the right ventricular lead 1230, and/or the coronary sinus lead 1224 via an electrode configuration switch 1274. It is understood that in order to provide stimulation therapy in each of the four chambers of the heart, the atrial and ventricular pulse generators, 1270 and 1272, may include dedicated, independent pulse generators, multiplexed pulse generators, or shared pulse generators. The pulse generators, 1270 and 1272, are controlled by the microcontroller 1260 via appropriate control signals, 1276 and 1278, respectively, to trigger or inhibit the stimulation pulses.

**[0085]** The microcontroller 1260 further includes timing control circuitry 1279 which is used to control pacing parameters (e.g., the timing of stimulation pulses) as well as to keep track of the timing of refractory periods, PVARP intervals, noise detection windows, evoked response windows, alert intervals, marker channel timing, etc., which is well known in the art. Examples of pacing parameters include, but are not limited to, atrio-ventricular delay, interventricular delay and interatrial delay.

**[0086]** The switch bank 1274 includes a plurality of switches for connecting the desired electrodes to the appropriate I/O circuits, thereby providing complete electrode programmability. Accordingly, the switch 1274, in response to a control signal 1280 from the microcontroller 1260, determines the polarity of the stimulation pulses (e.g., unipolar, bipolar, combipolar, etc.) by selectively closing the appropriate combination of switches (not shown) as is known in the art. The switch 1274 can also be used to connect wires from an oximetry sensor 802 to appropriate I/O circuits.

**[0087]** Atrial sensing circuits 1282 and ventricular sensing circuits 1284 may also be selectively coupled to the right atrial lead 1220, coronary sinus lead 1224, and the right ventricular lead 1230, through the switch 1274 for detecting the presence of cardiac activity in each of the four chambers of the heart. Accordingly, the atrial (ATR. SENSE) and ventricular (VTR. SENSE) sensing circuits, 1282 and 1284, may include dedicated sense amplifiers, multiplexed amplifiers, or shared amplifiers. The switch 1274 determines the "sensing polarity" of the cardiac signal by selectively closing the appropriate

switches, as is also known in the art. In this way, the clinician may program the sensing polarity independent of the stimulation polarity.

**[0088]** Each sensing circuit, 1282 and 1284, preferably employs one or more low power, precision amplifiers with programmable gain and/or automatic gain control, band-pass filtering, and a threshold detection circuit, as known in the art, to selectively sense the cardiac signal of interest. The automatic gain control enables the device 1210 to deal effectively with the difficult problem of sensing the low amplitude signal characteristics of atrial or ventricular signals.

**[0089]** The outputs of the atrial and ventricular sensing circuits, 1282 and 1284, are connected to the microcontroller 1260 which, in turn, are able to trigger or inhibit the atrial and ventricular pulse generators, 1270 and 1272, respectively, in a demand fashion in response to the absence or presence of cardiac activity, in the appropriate chambers of the heart. The sensing circuits, 1282 and 1284, in turn, receive control signals over signal lines, 1286 and 1288, from the microcontroller 1260 for purposes of measuring cardiac performance at appropriate times, and for controlling the gain, threshold, polarization charge removal circuitry (not shown), and timing of any blocking circuitry (not shown) coupled to the inputs of the sensing circuits, 1282 and 1286.

**[0090]** For arrhythmia detection, the device 1210 utilizes the atrial and ventricular sensing circuits, 1282 and 1284, to sense cardiac signals to determine whether a rhythm is physiologic or pathologic. The timing intervals between sensed events (e.g., P-waves, R-waves, and depolarization signals associated with fibrillation which are sometimes referred to as "F-waves" or "Fib-waves") are then classified by the microcontroller 1260 by comparing them to a predefined rate zone limit (i.e., bradycardia, normal, low rate VT, high rate VT, and fibrillation rate zones) and various other characteristics (e.g., sudden onset, stability, physiologic sensors, and morphology, etc.) in order to assist with determining the type of remedial therapy that is needed (e.g., bradycardia pacing, anti-tachycardia pacing, cardioversion shocks or defibrillation shocks, collectively referred to as "tiered therapy").

**[0091]** Cardiac signals are also applied to the inputs of an analog-to-digital (A/D) data acquisition system 1290. The data acquisition system 1290 is configured to acquire intracardiac electrogram signals, convert the raw analog data into a digital signal, and store the digital signals for later processing and/or telemetric transmission to an external device 1202. The data acquisition system 1290 is coupled to the right atrial lead 1220, the coronary sinus lead 1224, and the right ventricular lead 1230 through the switch 1274 to sample cardiac signals across any pair of desired electrodes.

**[0092]** Advantageously, the data acquisition system 1290 can be coupled to the microcontroller 1260, or other detection circuitry, for detecting an evoked response from the heart 1212 in response to an applied stimulus, there-

by aiding in the detection of "capture". Capture occurs when an electrical stimulus applied to the heart is of sufficient energy to depolarize the cardiac tissue, thereby causing the heart muscle to contract. The microcontroller 1260 detects a depolarization signal during a window following a stimulation pulse, the presence of which indicates that capture has occurred. The microcontroller 1260 enables capture detection by triggering the ventricular pulse generator 1272 to generate a stimulation pulse, starting a capture detection window using the timing control circuitry 1279 within the microcontroller 1260, and enabling the data acquisition system 1290 via control signal 1292 to sample the cardiac signal that falls in the capture detection window and, based on the amplitude, determines if capture has occurred.

**[0093]** The implementation of capture detection circuitry and algorithms are well known. See for example, U.S. Pat. No. 4,729,376 (Decote, Jr.); U.S. Pat. No. 4,708,142 (Decote, Jr.); U.S. Pat. No. 4,686,988 (Sholder); U.S. Pat. No. 4,969,467 (Callaghan et. al.); and U.S. Pat. No. 5,350,410 (Kleks et. al.). The type of capture detection system used is not critical to the present invention.

**[0094]** The microcontroller 1260 is further coupled to a memory 1294 by a suitable data/address bus 1296, wherein the programmable operating parameters used by the microcontroller 1260 are stored and modified, as required, in order to customize the operation of the stimulation device 1210 to suit the needs of a particular patient. Such operating parameters define, for example, pacing pulse amplitude, pulse duration, electrode polarity, rate, sensitivity, automatic features, arrhythmia detection criteria, and the amplitude, waveshape and vector of each shocking pulse to be delivered to the patient's heart 1212 within each respective tier of therapy.

**[0095]** Data acquired by the data acquisition system 1290 (and optionally stored) can be used for subsequent analysis to guide the programming of the device and/or to monitor oxygen saturation and/or hematocrit, appropriately adjust pacing interval parameters, select optimum pacing intervals, and/or select appropriate anti-arrhythmia therapy.

**[0096]** Advantageously, the operating parameters of the implantable device 1210 may be non-invasively programmed into the memory 1294 through a telemetry circuit 1201 in telemetric communication with the external device 1202, such as a programmer, transtelephonic transceiver, or a diagnostic system analyzer. The telemetry circuit 1201 is activated by the microcontroller by a control signal 1206. The telemetry circuit 1201 advantageously allows intracardiac electrograms, oxygen saturation information, hematocrit information and status information relating to the operation of the device 1210 (as contained in the microcontroller 1260 or memory 1294) to be sent to an external device 1202 through an established communication link 1204.

**[0097]** For examples of such devices, see U.S. Pat. No. 4,809,697, entitled "Interactive Programming and Diagnostic System for use with Implantable Pacemaker"

(Causey, III et al.); U.S. Pat. No. 4,944,299, entitled "High Speed Digital Telemetry System for Implantable Device" (Silvian); and U.S. Pat. No. 6,275,734 entitled "Efficient Generation of Sensing Signals in an Implantable Medical Device such as a Pacemaker or ICD" (note: this relates to transfer of EGM data) (McClure et al.).

**[0098]** The stimulation device 1210 can further include one or more physiologic sensors 1208, which can be located within the stimulation device housing 1240 as shown, or can be located external to the housing.

**[0099]** The stimulation device 1210 additionally includes a battery 1212 which provides operating power to all of the circuits shown in FIG. 12B. For the stimulation device 1210, which employs shocking therapy, the battery 1212 must be capable of operating at low current drains for long periods of time, and then be capable of providing high-current pulses (for capacitor charging) when the patient requires a shock pulse. The battery 1212 should also have a predictable discharge characteristic so that elective replacement time can be detected. Accordingly, the device 1210 preferably employs lithium/silver vanadium oxide batteries, but is not limited thereto.

**[0100]** The stimulation device 1210 can further include a magnet detection circuitry (not shown), coupled to the microcontroller 1260. It is the purpose of the magnet detection circuitry to detect when a magnet is placed over the stimulation device 1210, which magnet may be used by a clinician to perform various test functions of the stimulation device 1210 and/or to signal the microcontroller 1260 that the external programmer 1202 is in place to receive or transmit data to the microcontroller 1260 through the telemetry circuits 1201.

**[0101]** As further shown in Fig. 12B, the device 1210 is shown as having an impedance measuring circuit 1213 which is enabled by the microcontroller 1260 via a control signal 1214. The known uses for an impedance measuring circuit 1213 include, but are not limited to, lead impedance surveillance during the acute and chronic phases for proper lead positioning or dislodgement; detecting operable electrodes and automatically switching to an operable pair if dislodgement occurs; measuring respiration or minute ventilation; measuring thoracic impedance for determining shock thresholds; measuring thoracic impedance for detecting and assessing the severity of pulmonary edema; detecting when the device has been implanted; measuring stroke volume; and detecting the opening of heart valves, etc. The impedance measuring circuit 1213 is advantageously coupled to the switch 1274 so that any desired electrode may be used. In addition, to facilitate the measurement of peripheral tissue edema, extra electrodes can be added to the device housing, thereby limiting the test electric field to the peripheral tissue.

**[0102]** In the case where the stimulation device 1210 is also intended to operate as an implantable cardioverter/defibrillator (ICD) device, it must detect the occurrence of an arrhythmia, and automatically apply an appropriate electrical shock therapy to the heart aimed at terminating

the detected arrhythmia. To this end, the microcontroller 1260 further controls a shocking circuit 1216 by way of a control signal 1218. The shocking circuit 1216 generates shocking pulses of low (up to 0.5 Joules), moderate (0.5-10 Joules), or high energy (12 to 40 Joules), as controlled by the microcontroller 1260. Such shocking pulses are applied to the patient's heart 1212 through at least two shocking electrodes, and as shown in this embodiment, selected from the left atrial coil electrode 1228, the RV coil electrode 1236, and/or the SVC coil electrode 1238. As noted above, the housing 1240 may act as an active electrode in combination with the RV electrode 1236, or as part of a split electrical vector using the SVC coil electrode 1238 or the left atrial coil electrode 1228 (i.e., using the RV electrode as a common electrode).

**[0103]** Cardioversion shocks are generally considered to be of low to moderate energy level (so as to minimize pain felt by the patient), and/or synchronized with an R-wave and/or pertaining to the treatment of tachycardia. Defibrillation shocks are generally of moderate to high energy level (i.e., corresponding to thresholds in the range of 5-40 Joules), delivered asynchronously (since R-waves may be too disorganized to be recognize), and pertaining exclusively to the treatment of ventricular fibrillation. Accordingly, the microcontroller 1260 is capable of controlling the synchronous or asynchronous delivery of the shocking pulses. Another approach to electrical anti-arrhythmia therapy is anti-tachycardia pacing, in which low-voltage pacing pulses are applied to pace-terminate the arrhythmia. This approach is particularly effective in low rate ventricular tachycardias.

### Claims

1. An implantable system, comprising: an implantable housing (804) comprising a window (814) through which light can pass; at least one light source (104,106,108), within the housing (804), each of which transmits light of a corresponding wavelength, wherein a portion of the light of each wavelength exits the housing (804) through the window (814); a measurement light detector (806), within the housing (804), arranged to detect light of each wavelength scattered back into the housing (804) through the window (814), and to produce a measurement signal (1122) that is indicative of the intensity of the light of each wavelength detected by the measurement light detector (806); a calibration light detector (1106), within the housing (804), arranged to detect a portion of the light of each wavelength that has not exited the housing (804), and to produce a calibration signal (1132) that is indicative of the intensity of the light of each wavelength detected by the calibration light detector (1106), which is indicative of the intensity of the light transmitted by each light source (104,106,108).
2. A system as claimed in Claim 1, **characterised in that** the intensity of the light transmitted by each light source (104,106,108) is controlled by a corresponding drive signal (112) that drives the light source (104,106,108) circuitry (1160) operative to detect changes in the intensity of the light transmitted by each light source (104,106,108) based on the calibration signal (1132).
3. A system as claimed in Claim 1 or Claim 2, **characterised in that** the at least one light source comprises a single light source (104).
4. A system as claimed in Claim 1 or Claim 2, **characterised in that** the at least one light source comprises a first light source (104) that transmits light of a first wavelength and a second light source (106) that transmits light of a second wavelength.
5. A system as claimed in Claim 1 or Claim 2, **characterised in that** the at least one light source comprises a first, a second and a third light source (104,106,108), that transmit, respectively, light of a first wavelength, light of a second wavelength, and light of a third wavelength.
6. A system as claimed in Claim 1 or Claim 2, **characterised in that** the at least one light source comprises first and second spatially separated light sources that transmit light of about 805nm, wherein the first light source is located closer to the measurement light detector than the second light source.
7. A system as claimed in any preceding Claim, **characterised in that** the circuitry (1160) comprises a processor, state machine or random logic.
8. A system as claimed in any preceding Claim, **characterised in that** the measurement signal (1122) is used to determine levels of blood oxygen saturation and/or levels of hematocrit.
9. A system as claimed in any preceding Claim, **characterised by**: an opaque wall (8161) that separates the light source (104,106,108) from the measurement light detector (806) to prevent the measurement light detector (806) from detecting internally reflected light or light transmitted directly from the light source, and in which the opaque wall (806) does not prevent the calibration light detector (1106) from detecting internally reflected light or light transmitted directly from the light source (104,106,108).
10. A system, as claimed in any preceding Claim, **characterised by** comprising: a controller (1160) to adjust the measurement signal (1122), based on the calibration signal (1132), to compensate for changes in the intensity of the light transmitted by each light

source (104,106,108).

11. A system as claimed in Claim 10, **characterised in that** the controller (1160) adjusts amplification of the measurement signal (1122) to compensate for changes in the intensity of each light source due to aging of the light source. 5
12. A system as claimed in Claim 10 or Claim 11, **characterised in that** the controller adjusts amplification by adjusting the gain of an amplifier that amplifies the measurement signal. 10
13. A method for compensating for changes in the intensity of light transmitted by a light source (104,106,108) in an implantable system, comprising the steps: driving a light source (104,106,108) with a drive signal (1116) to transmit light having an intensity that is controlled by the drive signal (1116); detecting light scattered by blood, and producing a measurement signal (1122) indicative of the intensity of the light detected by the measurement light detector (806); detecting a portion of the transmitted light that has not exited a housing (804) within which the light source (104,106,108) is contained, and producing a calibration signal (1132) that is indicative of the intensity of the light transmitted by the light source (104,106,108); and compensating for changes in the intensity of the transmitted light, based on the calibration signal (1132). 15  
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14. A method as claimed 13, **characterised in that** the compensating step includes adjusting the drive signal (1116), based on the calibration signal (1132), to keep the intensity of the light transmitted by the light source substantially constant. 35
15. A method as claimed in Claim 13 or Claim 14, **characterised in that** the compensating step includes detecting changes in the intensity of the light transmitted by the light source (104,106,108) based on the calibration signal (1132) and taking into account the detected changes in the intensity of the transmitted light when using the measurement signal for a diagnostic and/or therapeutic purpose. 40  
45
16. A method as claimed in any of Claims 13 to 15, **characterised by** the further step of using the measurement signal (1122) to determine levels of blood oxygen saturation and/or levels of hematocrit, wherein the detected changes in the intensity of the transmitted light are taken into account when using the measurement signal (1122) to determine levels of blood oxygen saturation and/or levels of hematocrit. 50  
55
17. A method as claimed in any of Claims 13 to 16, **characterised in that** the compensating step includes adjusting the measurement signal (1132), based on

the calibration signal, to compensate for changes in the intensity of the light transmitted by the light source (104,106,108).

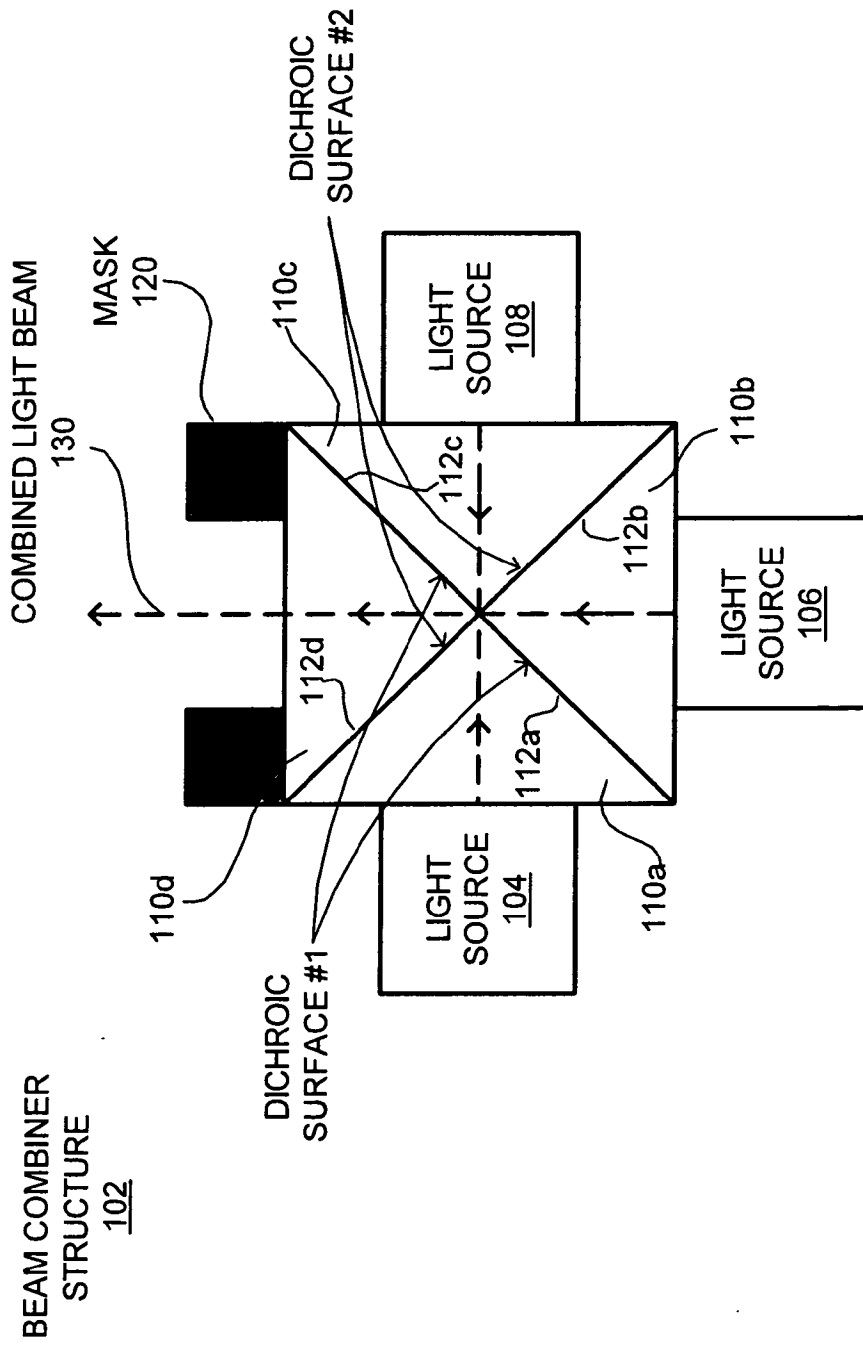


FIG. 1

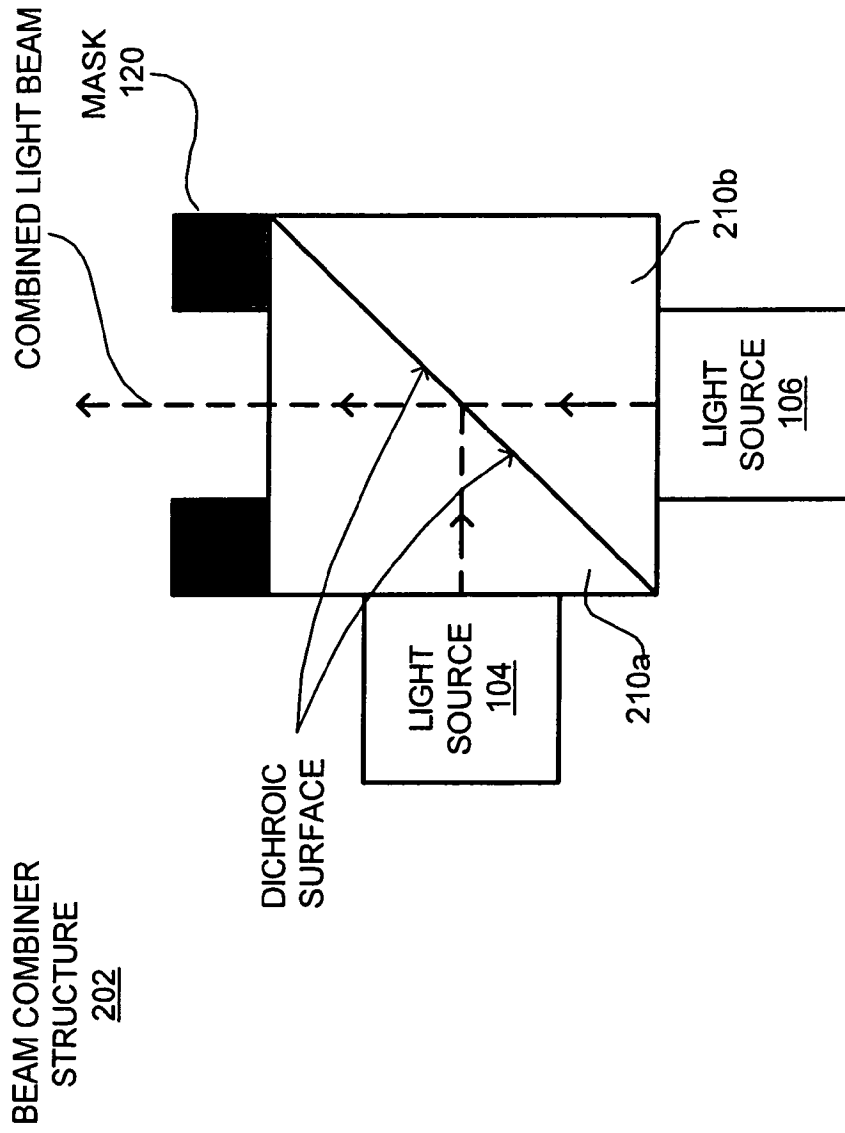


FIG. 2

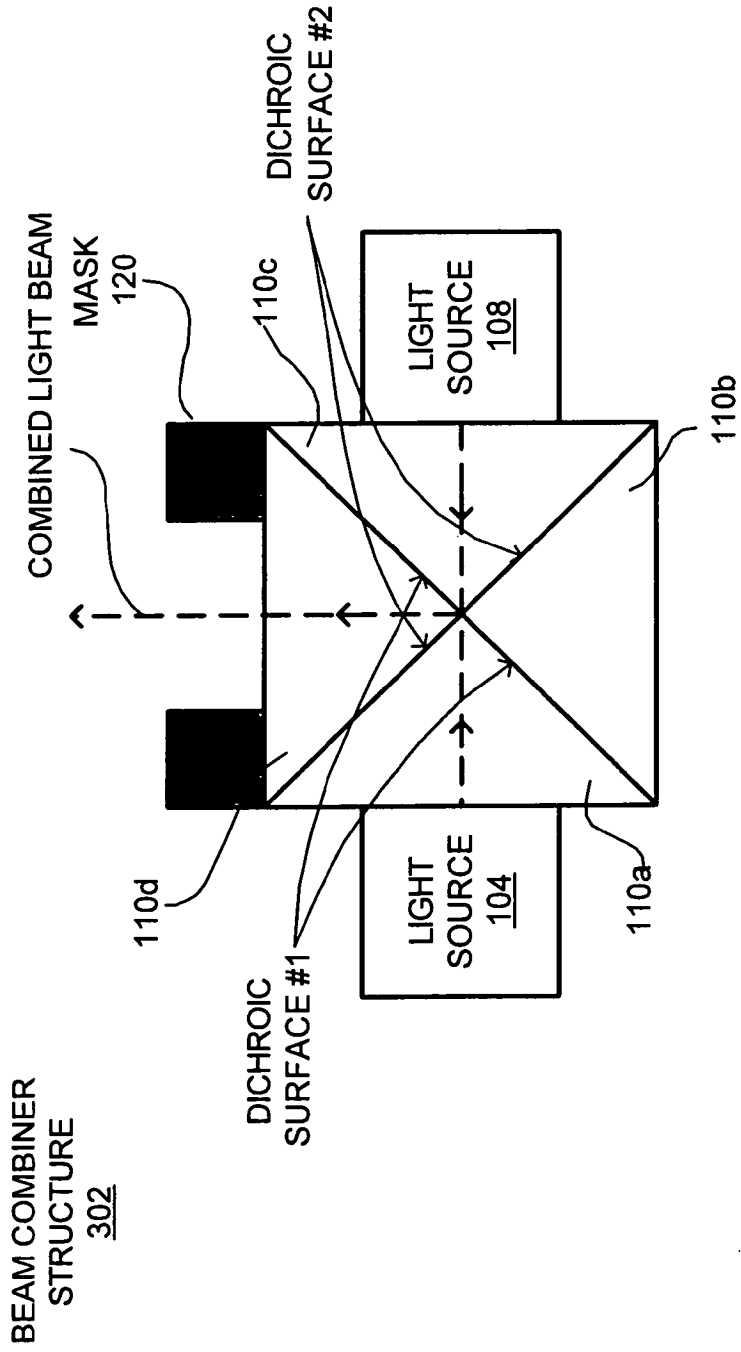


FIG. 3

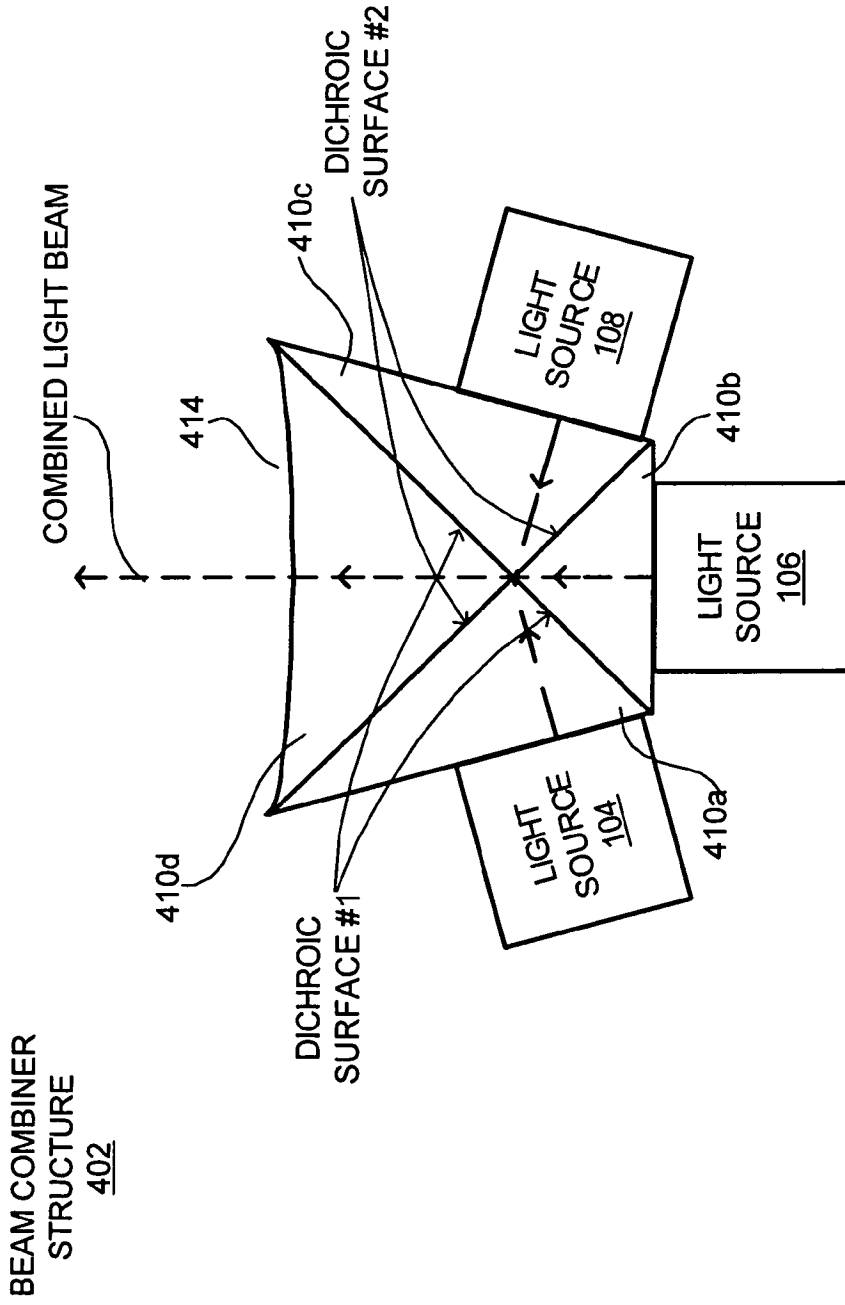


FIG. 4

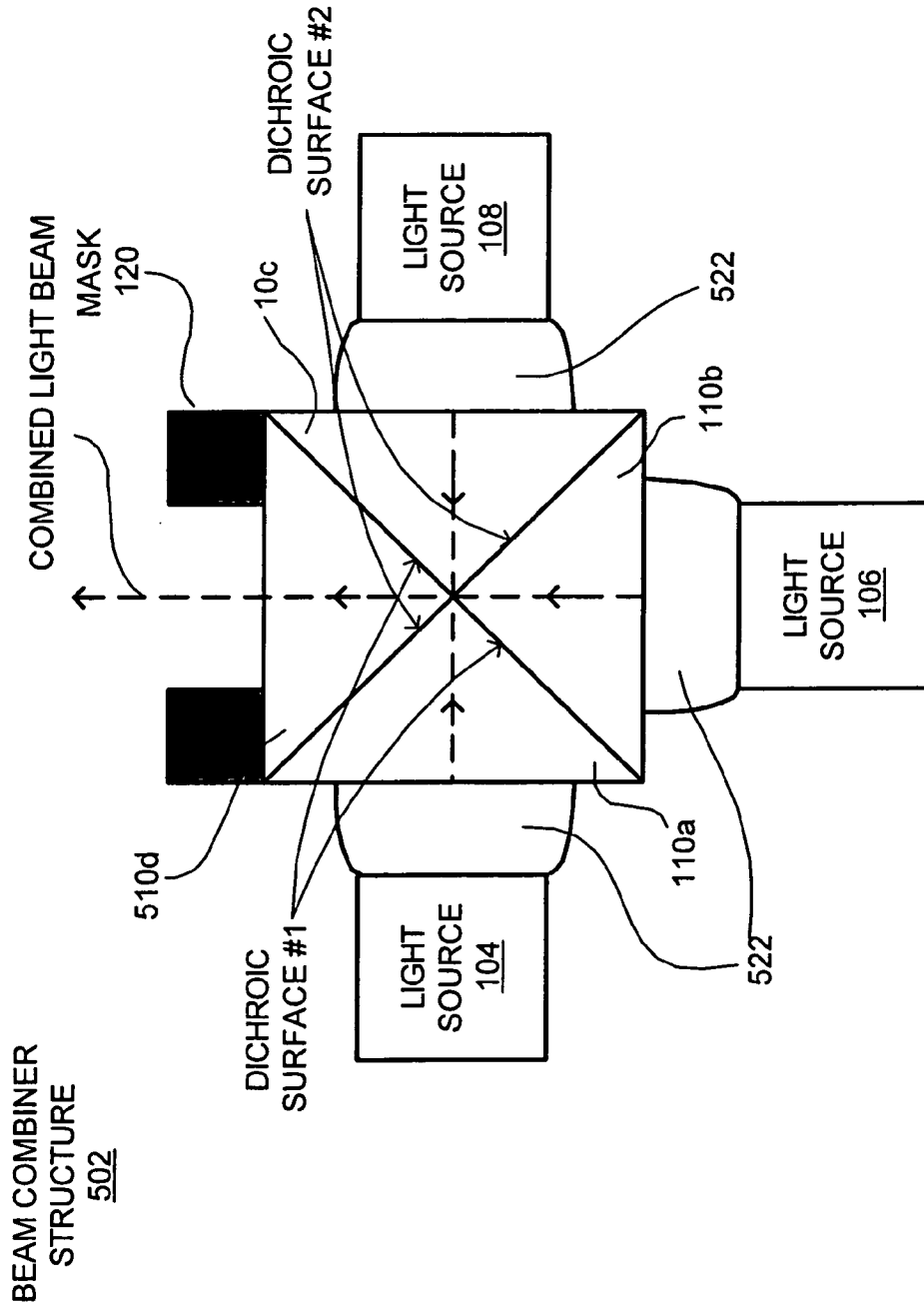


FIG. 5

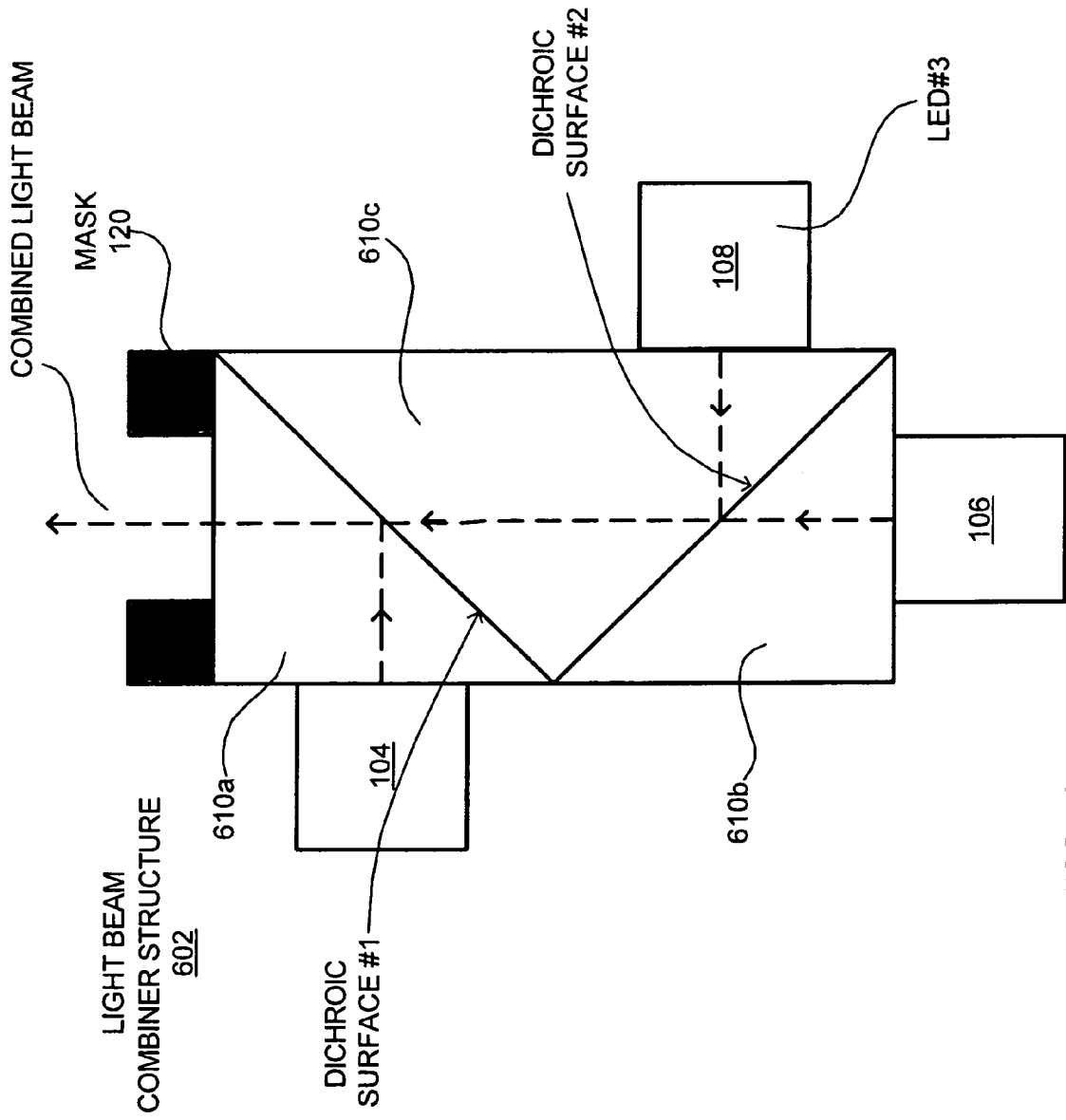


FIG. 6

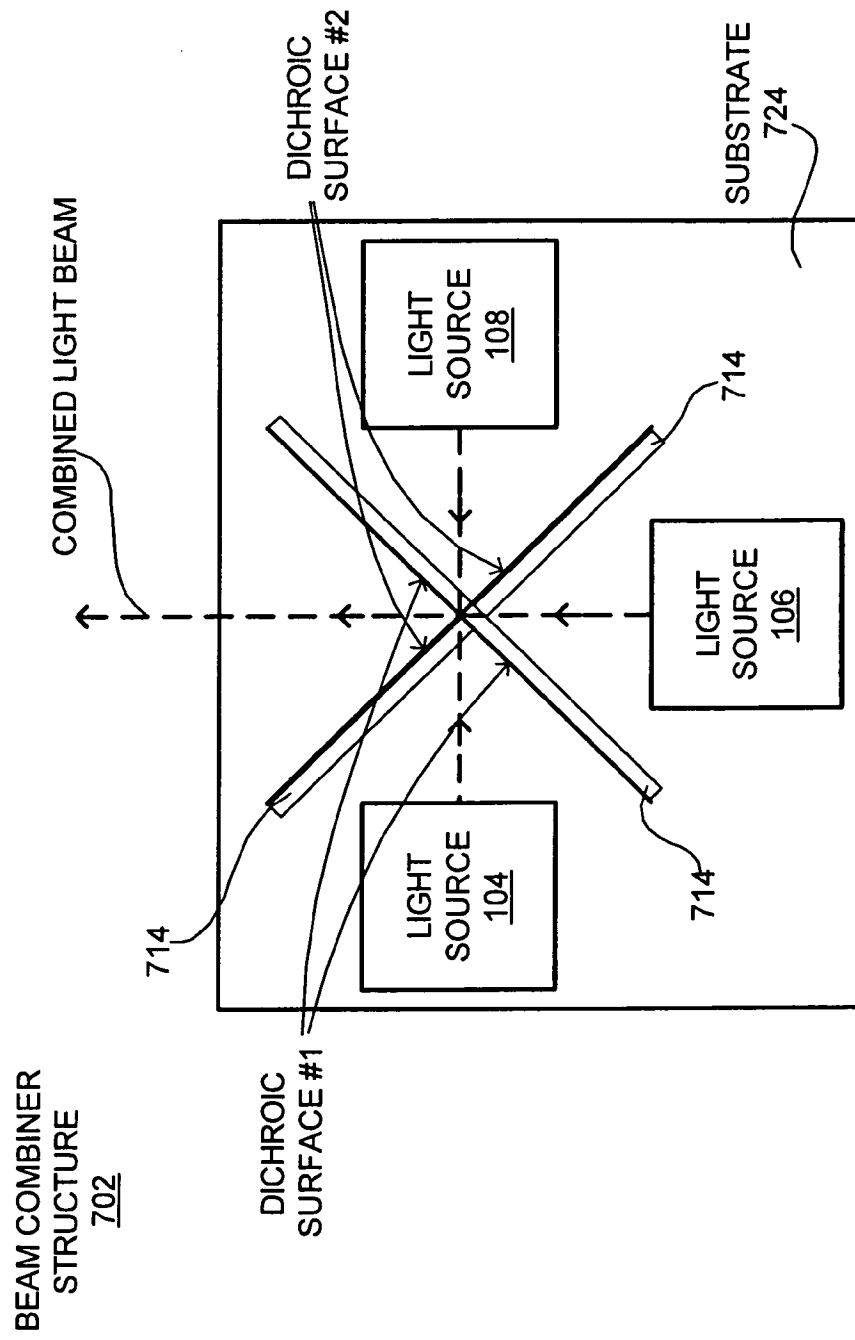


FIG. 7

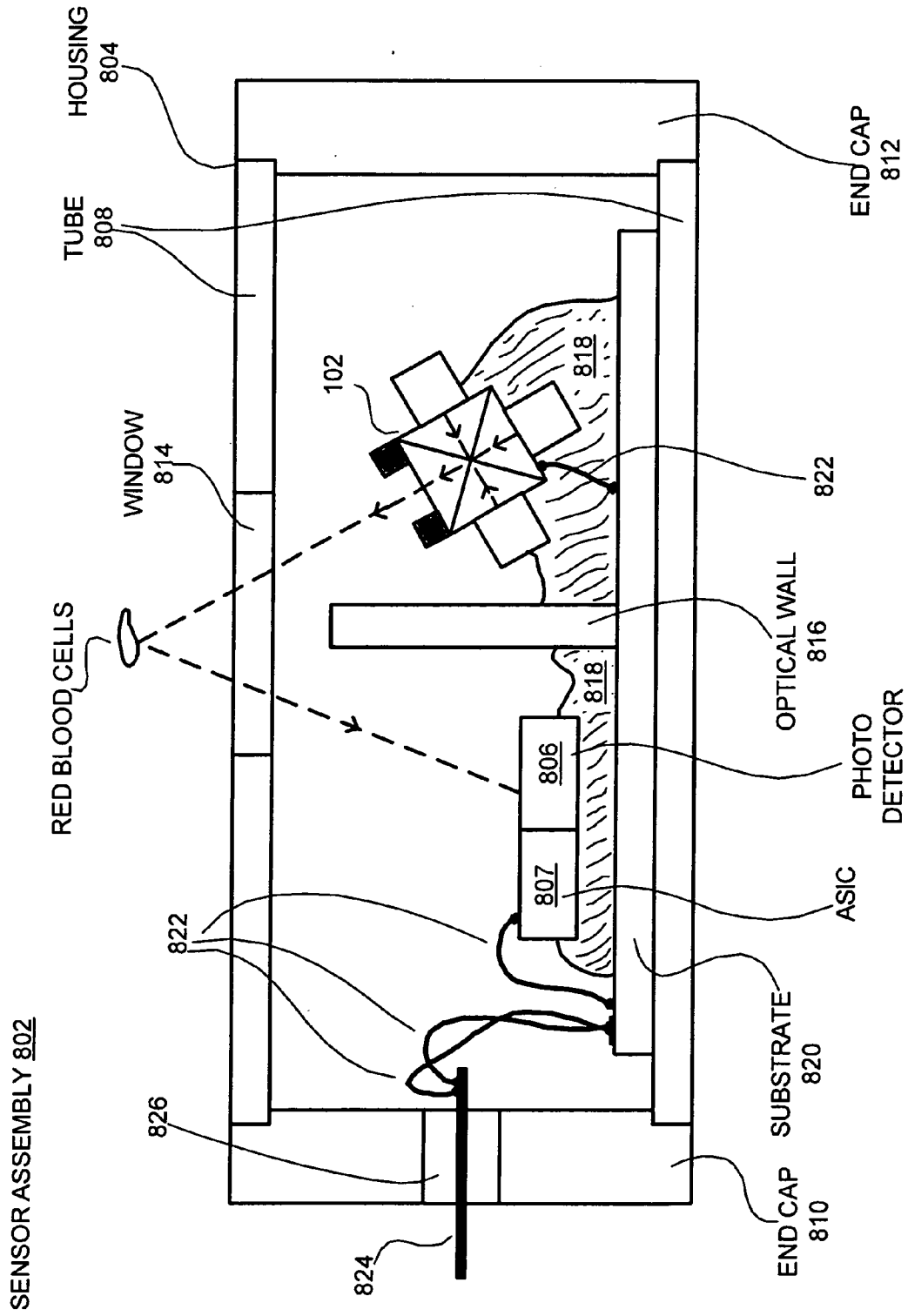


FIG. 8A

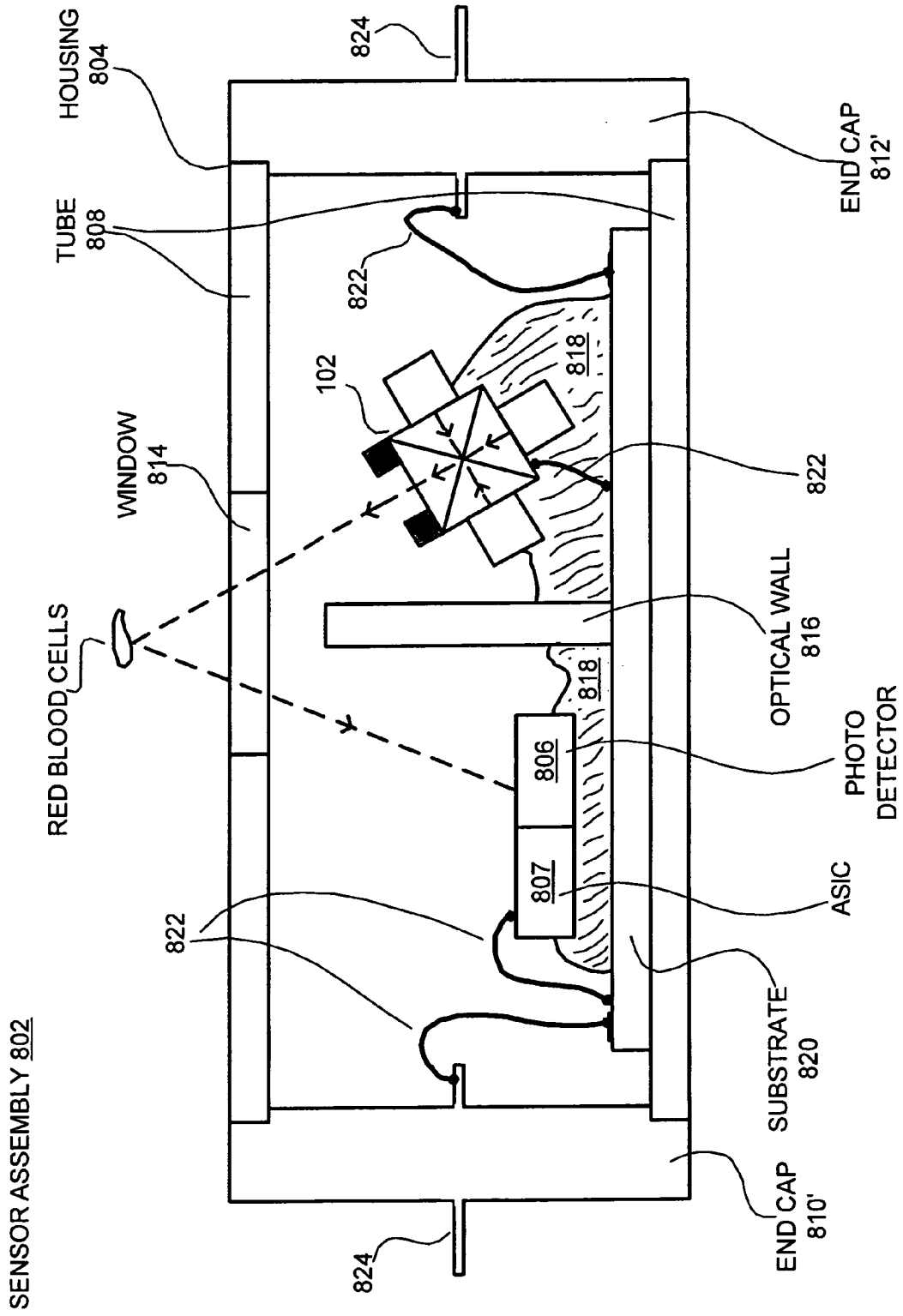
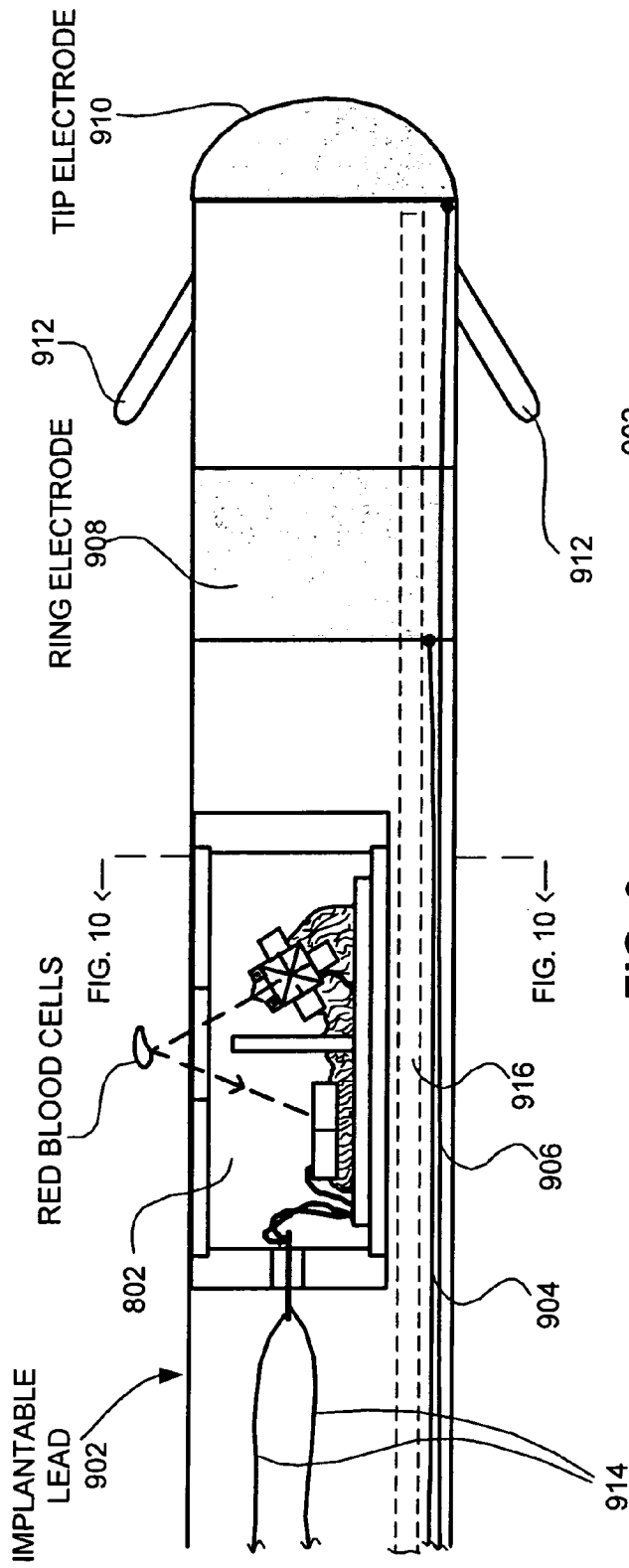
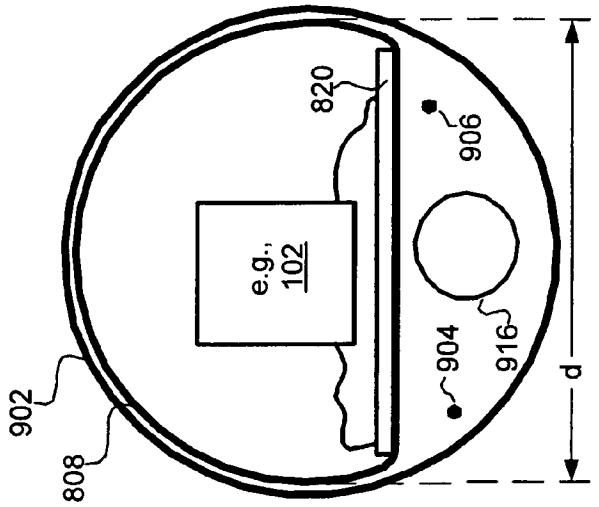


FIG. 8B



**FIG. 9**



**FIG. 10**



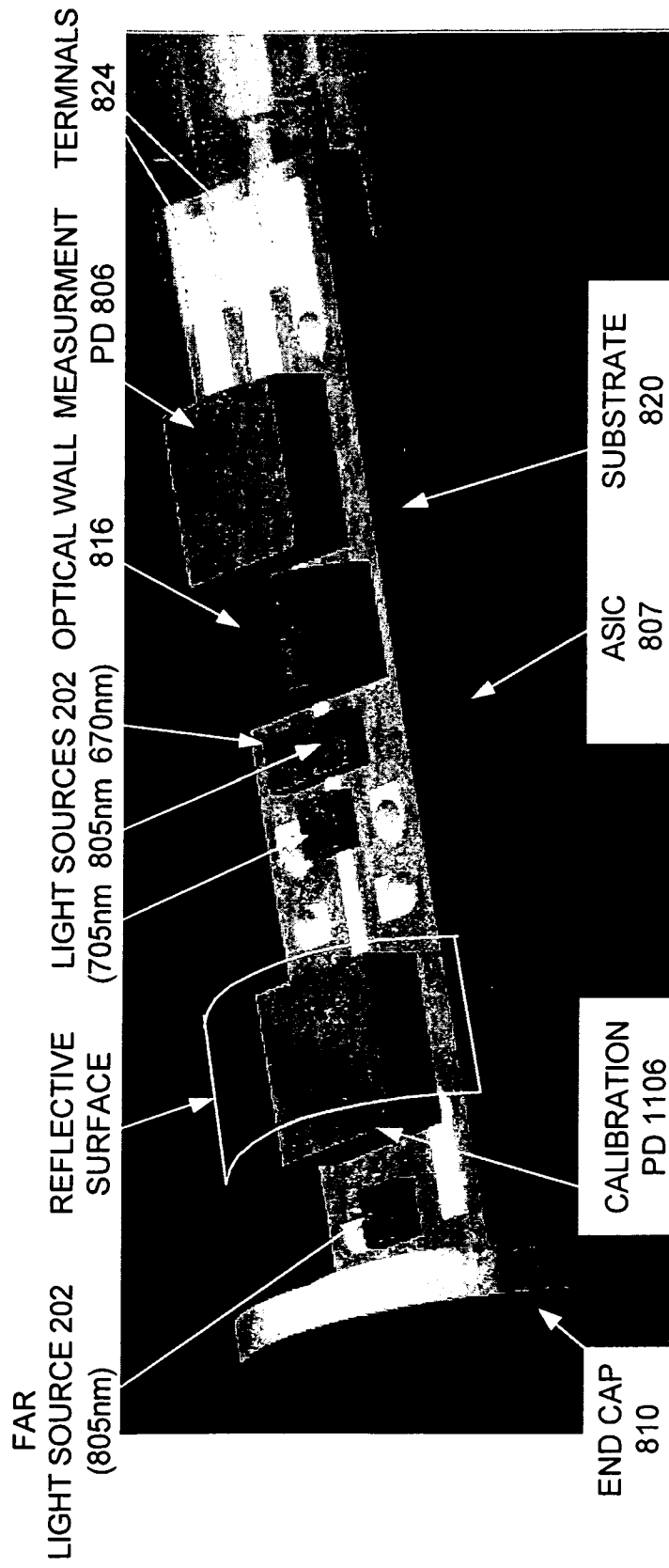


FIG. 11B

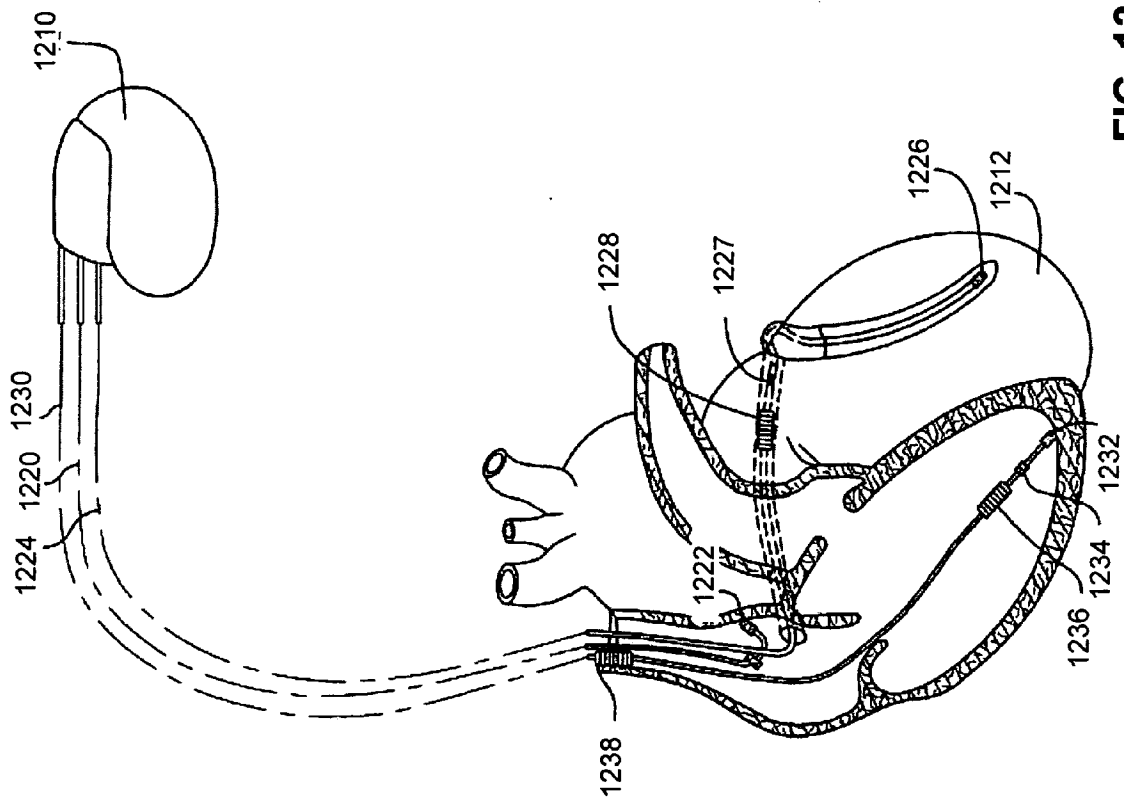


FIG. 12A

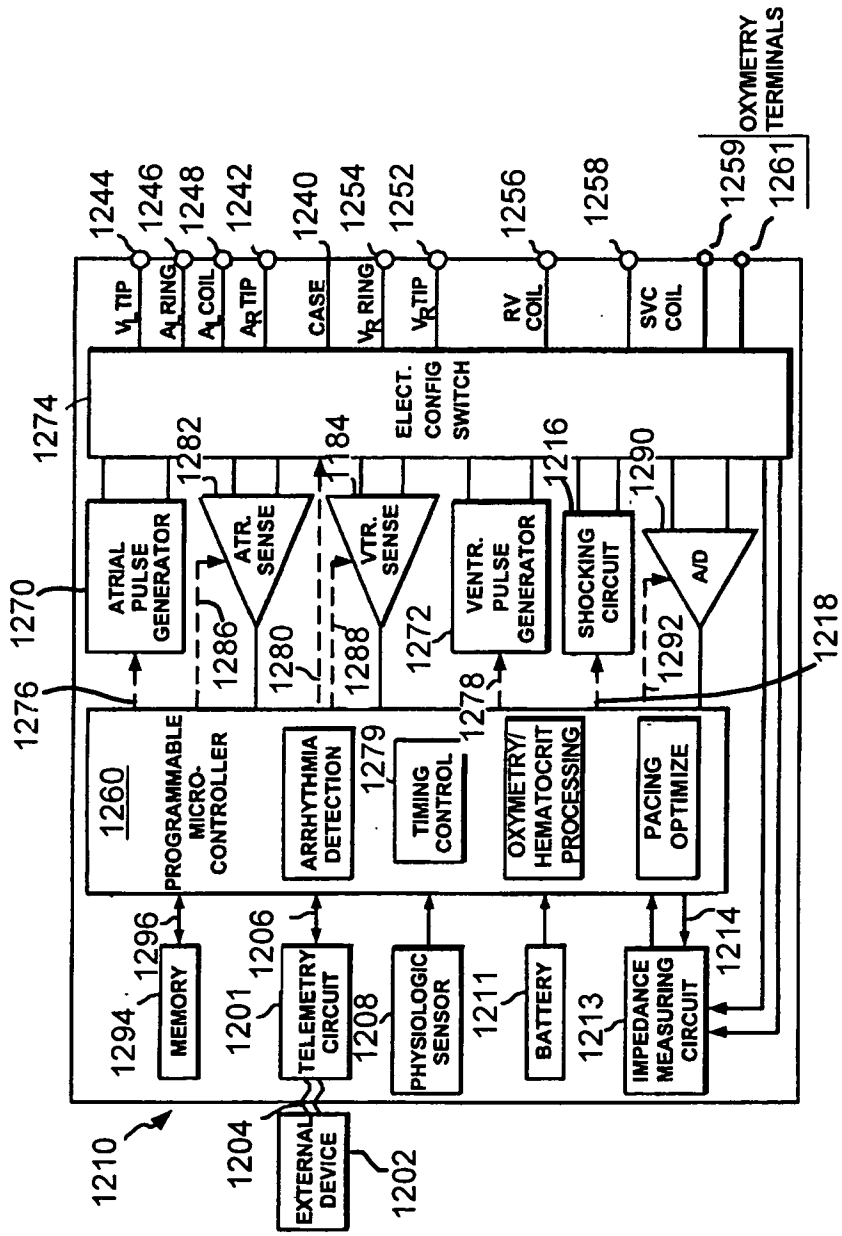


FIG. 12B

**REFERENCES CITED IN THE DESCRIPTION**

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专利名称(译)	可植入的自校准光学传感器		
公开(公告)号	<a href="#">EP1764034A2</a>	公开(公告)日	2007-03-21
申请号	EP2006254869	申请日	2006-09-20
[标]申请(专利权)人(译)	标兵		
申请(专利权)人(译)	PACESETTER, INC.		
当前申请(专利权)人(译)	PACESETTER, INC.		
[标]发明人	POORE JOHN W		
发明人	POORE, JOHN W.		
IPC分类号	A61B5/00 A61B5/1495 A61B5/1459		
CPC分类号	A61B5/14542 A61B5/14535 A61B5/1459 A61B5/1495		
代理机构(译)	里斯DAVID CHRISTOPHER		
优先权	11/231555 2005-09-20 US 11/282198 2005-11-17 US		
其他公开文献	EP1764034B1 EP1764034A3		
外部链接	<a href="#">Espacenet</a>		

摘要(译)

测量光检测器检测由可植入系统的光源 ( 104,106,108 ) 传输的光, 该光被散射回可植入壳体 ( 804 ), 并产生指示由测量光检测器检测到的光强度的测量信号 ( 806 )。 )。校准光检测器 ( 1106 ) 检测未离开壳体 ( 804 ) 的透射光的一部分, 并产生校准信号 ( 1132 ), 该校准信号指示校准光检测器 ( 1106 ) 检测到的光的强度。 , 这表示光源透射的光的强度。基于校准光检测器 ( 106 ) 产生的校准信号 ( 1132 ) 补偿透射光强度的变化。

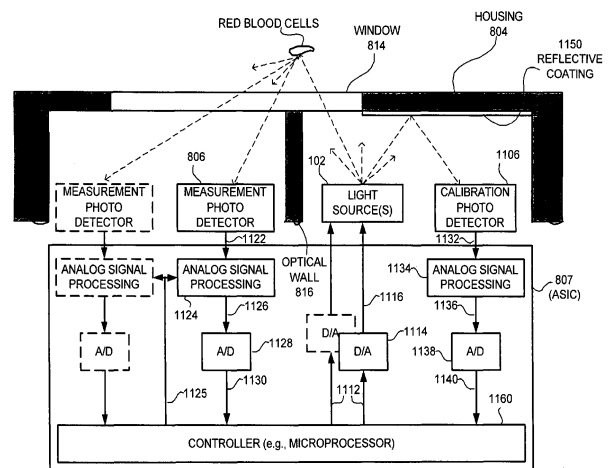


FIG. 11A