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(72) Inventors:

- **KIM, Kwang Tae**
157-220 Seoul (KR)
- **HYEON, Seog San**
157-220 Seoul (KR)

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(74) Representative: **Cabinet Chaillot**
16/20, avenue de l'Agent Sarre
B.P. 74
92703 Colombes Cedex (FR)

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(71) Applicant: **Irumedi Co.,ltd.**
Gyeonggi-do 410-380 (KR)

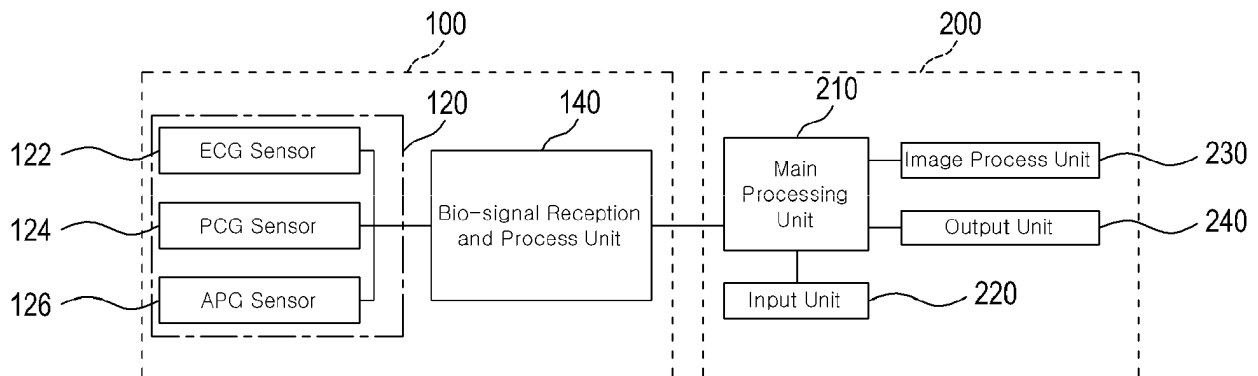
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(54) **CARDIOVASCULAR ANALYZER**

(57) The present invention relates to a cardiovascular analysis system, and more specifically to a cardiovascular analyzer which enables to detect cardiovascular diseases early and to define their causes. Unlike the conventional electrocardiographs, in each branch of the blood vessels of left and right coronary arteries, the car-

diovascular analyzer can further measure elastic coefficient of blood vessel (i.e., arterial stiffness) showing organic change, compliance of blood vessel showing organic and functional changes simultaneously, and volume, resistance and velocity of blood flow showing resistance characteristics of blood flow.

【Figure 1】



Description

[Technical Field]

5 **[0001]** The present invention relates to a cardiovascular analysis system, and more specifically to a cardiovascular analyzer which enables to detect cardiovascular diseases early and to define their causes. Unlike the conventional electrocardiographs, in each branch of the blood vessels of left and right coronary arteries, the cardiovascular analyzer can further measure elastic coefficient of blood vessel (i.e., arterial stiffness) showing organic change, compliance of blood vessel showing organic and functional changes simultaneously, and volume, resistance and velocity of blood flow
10 showing resistance characteristics of blood flow.

[Background Art]

15 **[0002]** In the present day, the incidence of vascular and cardiovascular diseases such as arteriosclerosis and myocardial infarction is rapidly increasing due to the meat-oriented dietary lifestyle. But the technology and the instrument for recognizing and preventing the diseases previously are poor.

[0003] In today's clinics, the electrocardiograph can't be used to early find out the ischemic diseases and to analyze the function of cardiac blood vessel. Also, the image processing technology and the angiography can be used to diagnose the apparent patient with the diseases because they only show the images of the cardiac blood vessel.

20 **[0004]** In order to early recognize the symptom of cardiovascular disease such as myocardial infarction, the determination of the coronary artery property, the blood flow characteristics and the blood state is more useful than that of the images of cardiac blood vessel and the electrocardiogram. The state of blood is easily determined by the blood test. However, the determination of the property of coronary artery and the characteristics of blood flow needs a new analyzing instrument.

25 **[0005]** The most important issue is an exact determination of characteristics of coronary artery. Unlike the other blood vessels, the coronary artery causes vasospasm and vasodilation by the external factors and the epidemiology relationship is complicated with the action of inside pressure of the coronary artery. Consequently, it is very difficult to obtain the properties and characteristics such as arterial stiffness, vascular compliance, blood flow volume, blood flow velocity and blood flow resistance in the coronary artery.

30 **[0006]** The automatic analyzing electrocardiograph system is widely used in clinics, but it is unable to early find out the risk of incidence of the coronary artery diseases and to determine the patient to surgery by a noninvasive testing method. The electrocardiogram records the electrical changes in the heart but not record the biodynamical properties of cardiac blood vessel such as elastic coefficient of blood vessel, compliance of blood vessel, and volume, resistance and velocity of blood flow.

35 **[0007]** The coronary artery disease analyzers developed until now are a single photon emission computerized tomography (SPECT), a contrast echocardiography (CE), a multidetector CT (MDCT) and a magnetic resonance imaging (MRI).

[0008] On purpose to apply into the surgery of coronary artery, the invasive testing method as catheterization has an advantage to directly observe the pathological changes of blood vessel itself but has a need of an essential and complex
40 invasive manipulation of blood vessel. About 40% of examinees have been revealed to persons without a need of that surgery.

[0009] The electrocardiograph is principally unable to exactly diagnose the ischemic diseases of coronary artery.

[0010] Additionally, the mentioned devices have a clinical significance but, owing to the high manufacturing and diagnostic cost, are able to be used in the particular hospital only. Commonly, the mentioned devices are unable to detect
45 the properties of blood vessel in spite of little difference. The property of blood flow in a left coronary artery differs from that of blood flow in a right coronary artery. The blood vessel of left coronary artery is pressed with an additive internal pressure because of the systolic tissue-pressure by the contraction of ventricular myocardium.

[0011] Consequently, because the blood flow of the left coronary artery has a very complex structure, the pressure waveform causing the blood flow in the left coronary artery is covered until now.

50 **[0012]** The right coronary artery perfuses the right ventricle.

[0013] The systolic pressure of the right ventricle is about 30 % of that of the left ventricle. The pressure of systolic coronary artery is comparably smaller in the right ventricular myocardium.

[0014] The invasive testing methods have been widely studied to measure an additive internal pressure transferred from a systolic tissue-internal pressure produced by an intrinsic myocardium contraction in coronary artery. However,
55 until now the noninvasive testing method is insignificantly used to develop the instrument for measuring blood flow volume, blood flow velocity, vascular compliance, elastic coefficient of blood vessel, and blood flow resistance in the coronary artery.

[0015] During the last 10 years, the blood flow property of coronary artery has been widely studied and it was found

out the blood flow of left coronary artery runs only during the diastole.

[0016] At the same time, Japanese researchers discovered that the blood flow also runs during the diastole in the capillary vessel of coronary artery by the radioisotope insertion method.

[0017] On the other hand, the property of blood vessel has also been studied. In 2006, Korean and American scientists suggested a method to calculate an elastic coefficient of artery. This method is to calculate an elastic coefficient of blood vessel by measuring atheroma but it is difficult to apply to the coronary artery. In addition, in 1997, Ridker and his colleagues of Harvard University have shown that high-sensitivity C-reactive protein has a relationship to cardiovascular diseases. Based on the above study, in 2006, j-CHROMA™ method has been developed to observe the disease process but has not provided information on the state of blood vessel.

[0018] However, the present invention provides the measuring methods of blood flow, compliance of blood vessel, blood flow velocity, blood flow resistance, and stiffness of artery (i.e., the degree of arteriosclerosis) in left and right coronary arteries by the synchronous analysis of the electrical property of heart and the biodynamic property of coronary artery.

[0019] In order to measure blood flow volume, compliance of blood vessel, blood flow velocity, and blood flow resistance in each branch of left and right coronary arteries, the first issue is to obtain an aortic arch internal pressure curve using the noninvasive testing method.

[0020] One related method to obtain the aortic arch internal pressure curve using the noninvasive testing method had been suggested in the international patent publication No. WO1995/016391 (METHOD AND APPARATUS FOR TREATING CARDIOVASCULAR PATHOLOGIES). However, because the curves obtained by the above method are very different from those of the invasive testing method in the same patient, it is virtually impossible to coincide with those curves.

[0021] Consequently, it is really impossible that the aortic arch internal pressure curve obtained by the method of WO1995/01639 is extrapolated into clinical trial as like as that curve obtained by using the invasive testing method.

[Disclosure]

[Technical Problem]

[0022] The present invention is contrived for solving the above-mentioned problems of conventional technology. The objective of the present invention is to provide a cardiovascular analyzer which comprises, unlike the known electrocardiography, to further measure elastic coefficient of blood vessel (i.e., arterial stiffness) showing organic change, compliance of blood vessel showing organic and functional changes simultaneously, and volume, resistance and velocity of blood flow showing resistance characteristics of blood flow in each branch of left and right coronary arteries and enables to detect cardiovascular diseases early and to define their causes.

[Technical Solution]

[0023] To achieve the above-mentioned objective, the present invention has the first feature that a cardiovascular analyzer comprises: a bio-signal measurement system including a bio-signal measuring sensor unit which comprises an electrocardiogram (ECG) sensor, a phonocardiogram (PCG) sensor and an accelerated plethysmogram (APG) sensor, and a bio-signal reception and process unit which is connected to each of the sensors of the bio-signal measuring sensor unit for receiving and processing bio-signals measured by the sensors; and an analysis indicator calculation system including a main processing unit which is connected to the bio-signal reception and process unit for communicating and calculating biodynamic indicators of a coronary artery from the bio-signals, an input unit which is connected to the main processing unit for receiving control commands of a user, and an output unit which is connected to the main processing unit for displaying the calculated results, wherein the main processing unit is configured to synthesize an aortic arch internal pressure curve P from the bio-signals measured by the bio-signal measurement system and to calculate the biodynamic indicators from an area of the aortic arch internal pressure curve P; and wherein the aortic arch internal pressure curve P is synthesized with a first and second cuff APG waveforms and a left or right carotid artery APG waveform among the bio-signals.

[0024] The present invention has the second feature that the bio-signal reception and process unit comprises: a microcontroller which controls to process the bio-signals received from the bio-signal measuring unit and to transmit processed bio-signals to the main processing unit; a multi-signal selector which selects one of the bio-signals received from the ECG sensor, the PCG sensor and the APG sensor by a control signal of the microcontroller; a noise eliminator and signal amplifier which eliminates noises and/or controls amplification degree of the bio-signal selected by the multi-signal selector by a control signal of the microcontroller; a signal switcher which receives the bio-signals from the noise eliminator and signal amplifier and selects one of the bio-signals to meet the control commands of the input unit or of embedded program in the main processing unit by a control signal of the microcontroller; a sample holder which samples

and holds the bio-signal selected by the signal switcher by a control signal of the microcontroller; and an A/D converter which converts a holding bio-signal of the sample holder to a digital bio-signal and sends to the microcontroller by a control signal of the microcontroller.

5 [0025] The present invention has the third feature that the APG sensor is assembled with a cuff sphygmomanometer and a pressure sensor electrically connected to the bio-signal reception and process unit; wherein the APG sensor is used as a cuff pulse wave sensor in an assembly state to measure the first and second cuff APG waveforms; and wherein the APG sensor is used as a carotid artery pulse wave sensor by the pressure sensor in a disassembly state to measure the left or right carotid artery APG waveform.

10 [0026] The present invention has the fourth feature that the first cuff APG waveform is measured by the cuff pulse wave sensor pressurized above the systolic blood pressure; wherein the second cuff APG waveform is measured by the cuff pulse wave sensor depressurized below the diastolic blood pressure; and wherein the left or right carotid artery APG waveform is measured by the carotid artery pulse wave sensor which is the pressure sensor electrically connected to the bio-signal reception and process unit.

15 [0027] The present invention has the fifth feature that the APG sensor comprises a rubber hose which is connected to an air pouch of the cuff sphygmomanometer, a branch hose which is connected to the rubber hose, and an adaptor which is connected to an exit of the branch hose, and the adaptor is removably assembled to an opening part of a housing body of the pressure sensor, the pressure sensor being used as the carotid artery pulse wave sensor.

20 [0028] The present invention has the sixth feature that the main processing unit is programmed to carry out the steps of: (1) ordering the bio-signal measurement system to measure the bio-signals and receiving the bio-signals from the bio-signal measurement system; (2) analyzing waveforms from the received bio-signals and synthesizing the aortic arch internal pressure curve P from the analyzed waveforms; and (3) calculating the biodynamic indicators from the area of the synthesized aortic arch internal pressure curve P and displaying the results of cardiovascular analysis.

25 [0029] The present invention has the seventh feature that step 3 comprises: calculating blood flow volumes S_l and S_r of the left and right coronary arteries from basic data including the area of the aortic arch internal pressure curve P; calculating compliances C_l and C_r and blood flow resistances R_l and R_r of the left and right coronary arteries from the aortic arch internal pressure curve P and the blood flow volumes S_l and S_r of the left and right coronary arteries; and transmitting the results of cardiovascular analysis to the output unit for showing the calculated compliances C_l and C_r and the calculated blood flow resistances R_l and R_r of the left and right coronary arteries on one C-R chart.

30 [0030] The present invention has the eighth feature that step 3 further comprises: calculating arterial stiffness As_l and As_r of the left and right coronary arteries from the blood flow volumes S_l and S_r , the compliances C_l and C_r and the blood flow resistances R_l and R_r of the left and right coronary arteries and transmitting to the output unit.

35 [0031] The present invention has the ninth feature that step 3 further comprises: calculating blood flow velocities V_l and V_r of the left and right coronary arteries from the aortic arch internal pressure curve P and the compliances C_l and C_r of the left and right coronary arteries and transmitting to the output unit.

[0032] The present invention has the tenth feature that the blood flow volumes S_l and S_r , the compliances C_l and C_r and the blood flow resistances R_l and R_r of the left and right coronary arteries are calculated by the predetermined equations.

40 [0033] The present invention has the eleventh feature that, in the predetermined equations, the coefficient K is calculated by another equation; the coefficient K_1 is related to a blood flow volume flowing from an entrance of the coronary artery to the right coronary artery and is 0.12~0.15; and the coefficient K_2 is a tissue internal pressure coefficient and is 0.7~0.75.

[0034] The present invention has the twelfth feature that the arterial stiffness As_l and As_r of the left and right coronary arteries are calculated by another equations.

45 [0035] The present invention has the thirteenth feature that the blood flow velocities V_l and V_r of the left and right coronary arteries are calculated by another equations.

[0036] The present invention has the fourteenth feature that analyzing waveforms from the received bio-signals in step 2 comprises: finding feature points, including systolic upstroke point, systolic peak point, incisura point, diastolic peak point and diastolic end point, of the aortic arch internal pressure curve P by analyzing ECG signals and PCG signals measured by the ECG sensor and the PCG sensor of the bio-signals measurement system, respectively; analyzing first cuff APG waveforms measured by a cuff pulse wave sensor, as the APG sensor of the bio-signals measurement system, which is pressurized above the systolic blood pressure; analyzing second cuff APG waveforms measured by the cuff pulse wave sensor which is depressurized below the diastolic blood pressure; and analyzing left and right carotid artery APG waveforms measured by a carotid artery pulse wave sensor as the APG sensor of the bio-signals measurement system, and wherein the synthesis of the aortic arch internal pressure curve P is based on basic information including the analyzed data of the first and second cuff APG waveforms and the analyzed data of the left and right carotid artery APG waveforms.

55 [0037] The present invention has the fifteenth feature that the main processing unit is further programmed to carry out the steps of: displaying an initial screen including a search menu window, a patient information window, a test and

diagnosis window and a test result window in the output unit before step 1; receiving and saving the information of patient if a registration command for new patient is received in the initial screen, otherwise, receiving an opening command to open a registered patient file; displaying a patient list in the registered patient file on the test result window if the opening command is received and receiving a signal for selecting a patient and new information of the selected patient, otherwise, displaying the initial screen continuously; and displaying the information of new patient or the selected patient on the patient information window and receiving a test and diagnosis command, and wherein the information of new patient or the selected patient comprises a personally identified information and body information including one or more of height, weight, blood pressure and race.

[0038] The present invention has the sixteenth feature that performance of step 1 by the main processing unit further includes the steps of: (1-1) displaying a command selection window for the bio-signal measurement if a test command is received from the test and diagnosis window, otherwise, keeping the previous state; (1-2-1) receiving ECG, PCG and first cuff APG waveforms measured by the ECG sensor, the PCG sensor and a pressurized cuff pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of a systolic pulse wave is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command; (1-2-2) receiving ECG, PCG and second cuff APG waveforms measured by the ECG sensor, the PCG sensor and a depressurized cuff pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of a diastolic pulse wave is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command; (1-2-3) receiving ECG, PCG and left carotid artery APG waveforms measured by the ECG sensor, the PCG sensor and a carotid artery pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of the left carotid artery is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command; (1-2-4) receiving ECG, PCG and right carotid artery APG waveforms measured by the ECG sensor, the PCG sensor and a carotid artery pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of the right carotid artery is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command; (1-2-5) receiving ECG, PCG and femoral artery APG waveforms measured by the ECG sensor, the PCG sensor and a femoral artery pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of the femoral artery is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command; and (1-3) capturing a screen showing a selected ideal waveform among the waveforms displayed on the test result window and saving if a waveform selection command is received after each of steps 1-2-1 to 1-2-5, otherwise, keeping the measurement and displaying the measured waveforms continuously.

[0039] The present invention has the seventeenth feature that analyzing waveforms from the received bio-signals and synthesizing the aortic arch internal pressure curve P from the analyzed waveforms in step 2 comprise: (2-1) displaying an analysis menu window if an analysis command is received from the test and diagnosis window, otherwise, keeping the previous step; (2-2) analyzing automatically feature points of the saved ECG, PCG and first cuff APG waveforms and displaying on the test result window if a systolic bio-signal analysis command is received from the analysis menu window, otherwise, keeping the previous step; (2-3) analyzing automatically feature points of the saved ECG, PCG and second cuff APG waveforms and displaying on the test result window if a diastolic bio-signals analysis command is received from the analysis menu window, otherwise, keeping the previous step; (2-4) displaying the saved left and right carotid artery waveforms on the test result window if a synthesized signal analysis command is received from the analysis menu window, otherwise, keeping the previous step; (2-5) displaying enlarged waveforms analyzed in a selected interval on a lower left corner of the test result window if a detail analysis interval is selected in the left and right carotid artery waveforms showing on the test result window, otherwise, keeping the previous step; and (2-6) displaying an aortic arch internal pressure curve, which is synthesized with the information including the saved ECG, PCG and APG waveforms, in a place clicked on the test results window if a vacant space of a lower right corner of the test results window is clicked after the sequential displays of the enlarged left and right carotid artery waveforms on the lower left corner of the test results window, otherwise, keeping the previous step.

[0040] The present invention has the eighteenth feature that step 3 comprises: (3-1) displaying a result menu window and a output device icon if a result display command is received from the test and diagnosis window, otherwise, displaying a patient list in the registered patient file on the test result window and receiving a signal for selecting a patient and new information of the selected patient till receiving a command; (3-2) displaying a selected menu result if one is selected on the result menu window, otherwise, keeping step 3-1; and (3-3) outputting the selected menu result if an output command is received from the output device icon after displaying the selected menu result, otherwise, keeping step 3-2.

[0041] The present invention has the nineteenth feature that each of steps 2-2, 2-3, and 2-4 causes the main processing unit to return to step 1-1 if a test command is received from the result and diagnosis window after displaying each waveform on the test result window, and if the test command is not received, each of steps 2-2, 2-3, and 2-4 is followed

by the subsequent step.

[0042] The present invention has the twentieth feature that the result menu window comprises a Compliance-Resistance (C-R) chart; and the C-R chart is divided into sectors to show the coronary artery states according to the clinical results and is dotted to show the states of the left and right coronary arteries of an examinee.

[Advantageous Effects]

[0043] A cardiovascular analyzer of the present invention comprises, unlike the known electrocardiography, to further measure elastic coefficient of blood vessel (i.e., arterial stiffness) showing organic change, compliance of blood vessel showing organic and functional changes simultaneously, and volume, resistance and velocity of blood flow showing resistance characteristics of blood flow in each branch of left and right coronary arteries and enables to early diagnose several refractory diseases such as a myocardial infarction of a coronary artery and to define a patient needed to do surgery of the coronary artery by a non-invasive testing method.

[Description of Drawings]

[0044]

Fig. 1 is a block diagram of a cardiovascular analyzer according to an exemplary embodiment of the present invention.

Fig. 2 is a block diagram conceptually showing the constitution and the signal flow of the bio-signal reception and process unit in Fig. 1.

Fig. 3 is a front and disassembled perspective views of an exemplary embodiment of the APG sensor showed in Fig. 1.

Fig. 4 is a representative diagram of cardiac blood flow showing an aortic arch and left and right coronary arteries connected to the aortic arch.

Fig. 5 is a model diagram of elasticity of the left and right coronary arteries according to the present invention.

Fig. 6 is a blood pressure property diagram showing feature points and pressures of an aortic arch internal pressure curve obtained by a catheter.

Fig. 7 is a comparative diagram of the aortic arch internal pressure curves obtained by a catheter and by the present invention respectively.

Fig. 8 is an exemplary flowchart of the main processing unit showed in Fig. 1.

Figs. 9 to 12 are exemplary flowcharts showing more detail than Fig. 8.

Fig. 13 is an exemplary diagram of the test and result window showing ECG, PCG and first APG waveforms analyzed by the main processing unit in Fig. 1.

Fig. 14 is an exemplary diagram of the test and result window showing ECG, PCG and second APG waveforms analyzed by the main processing unit in Fig. 1.

Fig. 15 is an exemplary diagram of the test and result window showing left and right carotid artery APG waveforms analyzed by the main processing unit in Fig. 1.

Fig. 16 is an exemplary diagram of the test and result window showing C-R chart analyzed by the main processing unit in Fig. 1.

[0045] The following reference numbers are used throughout the drawings: reference number 10 indicates a cuff sphygmomanometer, 11 indicates a cuff band, 12 indicates an adhesive means (Velcro), 13 indicates an air pouch, 14, 17 and 18 indicate a rubber hose, 15 indicates an air valve, 16 indicates an air supply means, 19 indicates a pressure gauge, 20 indicates an adapter, 21 indicates a branch hose, 22 indicates a branch hose connecting part, 24 indicates a cover, 26 indicates a projecting part for connecting to a pressure sensor, 30 indicates the pressure sensor, 31 indicates a vent hole, 32 indicates an opening part, 34 indicates a housing body, 36 indicates a sensing read line for electrically connecting the pressure sensor to the bio-signal reception and process unit, 40 indicates an aortic arch, 42 indicates a left coronary artery, 44 indicates a right coronary artery, 50 indicates an aortic arch internal pressure curve obtained by a catheter, 60 indicates an aortic arch internal pressure curve obtained by the present invention, 70 indicates a test result window of output unit, 71 and 72 indicate ECG waveforms, 73 and 74 indicate PCG waveforms, 75 indicates a first cuff APG waveform, 76 indicates a second cuff APG waveform, 77 indicates a left carotid artery APG waveform, 78 indicates a right carotid artery APG waveform, 81 indicates an amplified left carotid artery APG waveform, 82 indicates an amplified right carotid artery APG waveform, and 83 indicates a synthesized aortic arch internal pressure curve.

[Mode for Invention]

[0046] A detailed description of preferred embodiments of the present invention is provided below with respect to accompanying drawings. Because the present invention can be embodied in various forms, the technical idea of the

present invention has to be not limited to the drawings and the embodiments described herein.

[0047] Fig. 1 is a block diagram of a cardiovascular analyzer according to an exemplary embodiment of the present invention. Fig. 2 is a block diagram conceptually showing the constitution and the signal flow of the bio-signal reception and process unit in Fig. 1. Fig. 3 is a front and disassembled perspective views of an exemplary embodiment of the APG sensor showed in Fig. 1. Fig. 4 is a representative diagram of cardiac blood flow showing an aortic arch and left and right coronary arteries connected to the aortic arch. Fig. 5 is a model diagram of elasticity of the left and right coronary arteries according to the present invention. Fig. 6 is a blood pressure property diagram showing feature points and pressures of an aortic arch internal pressure curve obtained by a catheter. And Fig. 7 is a comparative diagram of the aortic arch internal pressure curves obtained by a catheter and by the present invention respectively.

[0048] As shown in Fig. 1, a cardiovascular analyzer according to one embodiment of the present invention is characterized by basically comprising: a bio-signal measurement system 100 including a bio-signal measuring sensor unit 120 which comprises an electrocardiogram (ECG) sensor 122, a phonocardiogram (PCG) sensor 124 and an accelerated plethysmogram (APG) sensor 126, and a bio-signal reception and process unit 140 which is connected to the bio-signal measuring sensor unit 120 for receiving and processing bio-signals measured by each sensor of the bio-signals measuring sensor unit 120; and an analysis indicator calculation system 200 including a main processing unit 210 which is connected to the bio-signal reception and process unit 140 for communicating and calculating biodynamic indicators of a coronary artery from the bio-signals, an input unit 220 which is connected to the main processing unit 210 for receiving control commands of a user, and an output unit 240 which is connected to the main processing unit 210 for displaying the calculated results, wherein the main processing unit 210 is configured to synthesize an aortic arch internal pressure curve P from the bio-signals measured by the bio-signal measurement system 100 and to calculate the biodynamic indicators from an area of the aortic arch internal pressure curve P.

[0049] Here, the ECG sensor 122 comprises at least three electrodes and is used to obtain an ECG waveform and to define the feature points (i.e., systolic upstroke point, systolic peak point, incisura point, diastolic peak point and diastolic end point) of the aortic arch internal pressure curve P with the PCG sensor.

[0050] The PCG sensor 124 comprises a microphone to perceive the sound of open-and-shut of heart valves and is used to obtain a PCG waveform for defining the feature points of the aortic arch internal pressure curve P.

[0051] The APG sensor 126 is used to obtain an APG waveform by sensing a pulse wave of the pulsatory motion. The APG waveform is a waveform originally measured by the APG sensor 126 and can be secondarily analyzed to get the second derivative by the bio-signal reception and process unit 140 and/or the main processing unit 210. The APG sensor 126 comprises a pressure sensor having a piezoelectric element, but not limited to, or other device (e.g., a hall sensor) which senses the pulse wave.

[0052] In this embodiment, the APG sensor 126 is called, according to the sensing positions, as follows: a cuff pulse wave sensor to get a first cuff APG waveform on being pressurized above the systolic blood pressure and a second cuff APG waveform on being depressurized below the diastolic blood pressure in the upper arm (i.e., cuff), a carotid artery pulse wave sensor to get a left and right carotid artery APG waveforms for a basic waveform of the aortic arch by directly measuring pulse waves of the left and right carotid arteries, and a femoral artery pulse sensor to get a femoral artery APG waveform for a pulse wave velocity (PWV) etc by directly measuring a pulse wave of the femoral artery.

[0053] Here, it is possible that the carotid artery pulse wave sensor and the femoral artery pulse wave sensor are the same pressure sensor electrically connected to the bio-signal reception and process unit 140. The cuff pulse wave sensor is a cuff sphygmomanometer equipped with a pressure sensor. Thus, the APG sensor 126 can be assembled with a cuff sphygmomanometer and a pressure sensor electrically connected to the bio-signal reception and process unit 140 for being used as the cuff pulse wave sensor in an assembly state and as the carotid artery pulse wave sensor or the femoral artery pulse sensor in a disassembly state. As an embodiment, the detailed structure of the APG sensor 126 is shown in Fig. 3. A branch hose 21 is connected to a rubber hose 14 or 17 which is connected to an air pouch 13 in the cuff sphygmomanometer 10. An adaptor 20 is connected to an exit of the branch hose 21 and is removably assembled to an opening part 32 of a housing body 34 of the pressure sensor 30 electrically connected to the bio-signal reception and process unit 140 by a sensing read line 36. Thus, the APG sensor 126 can be used as the cuff pulse wave sensor in an assembly state as shown in the front view of Fig. 3 and also used as the carotid artery pulse wave sensor or the femoral artery pulse sensor by the pressure sensor 30 removed from the adaptor 20 in the disassembled perspective view of Fig. 3.

[0054] In other words, the cuff pulse wave sensor can be configured with a cuff sphygmomanometer 10, a pressure sensor 30 electrically connected to the bio-signal reception and process unit 140 by a sensing read line 36, and connecting means including a branch hose 21 connected to a rubber hose 14 or 17 that is connected to an air pouch 13 of the cuff sphygmomanometer 10 and an adaptor 20 connected to an exit of the branch hose 21 and assembled to an opening part 32 of a housing body 34 of the pressure sensor 30. Here, the adaptor 20 can be comprised of a hat-shaped cover 24, a branch hose connecting part 22 formed on the top side of the cover 24 and a projecting part 26 formed on the bottom side of the cover 24 having a screwed outer surface for removably connecting to the opening part 32 of the pressure sensor 30, the cover 24, the branch hose connecting part 22 and the projecting part 26 having a through hole

to transfer the pressure generated in the air pouch 13 of the cuff sphygmomanometer 10 as shown in the disassembled perspective view of Fig. 3.

[0055] The carotid artery pulse wave sensor and the femoral artery pulse sensor can be configured with the pressure sensor 30 electrically connected to the bio-signal reception and process unit 140 by a sensing read line 36. Here, the pressure sensor 30 can be comprised of a cup-shaped housing body 34, an opening part 32 having a screwed inner surface corresponding to the screwed outer surface of the projecting part 26 of the adaptor 20, a partition having vent holes 31, and one or more pressure-sensor cells located below the partition and electrically connected to the bio-signal reception and process unit 140 by a sensing read line 36 as shown in the disassembled perspective view of Fig. 3. As above mentioned, the bio-signal measuring sensor unit 120 essentially comprises the ECG sensor 122, the PCG sensor 124 and the APG sensor 126 for sensing the different bio-signals. The device embedded with the bio-signal reception and process unit 140 has at least three connectors for connecting to each of the sensors of the bio-signal measuring sensor unit 120.

[0056] Also, as shown in Fig. 2, the bio-signals reception and process unit 140 comprises: a microcontroller 146 which controls to process the bio-signals received from the bio-signal measuring unit 120 and to transmit processed bio-signals to the main processing unit 210; a multi-signal selector 141 which selects one of the bio-signals received from the ECG sensor 122, the PCG sensor 124 and the APG sensor 126 by a control signal of the microcontroller 146; a noise eliminator and signal amplifier 142 which eliminates noises and/or controls amplification degree of the bio-signal selected by the multi-signal selector 141 by a control signal of the microcontroller 146; a signal switcher 143 which receives the bio-signals from the noise eliminator and signal amplifier 142 and selects one of the bio-signals to meet the control commands of the input unit 220 or of embedded program in the main processing unit 210 by a control signal of the microcontroller 146; a sample holder 144 which samples and holds the bio-signal selected by the signal switcher 143 by a control signal of the microcontroller 146; and an A/D converter 145 which converts a holding bio-signal of the sample holder 144 to a digital bio-signal and sends to the microcontroller 146 by a control signal of the microcontroller 146.

[0057] Here, the multi-signal selector 141 is used to sequentially process the signals which are simultaneously measured and inputted by the ECG sensor 122, the PCG sensor 124 and the APG sensor 126. The noise eliminator and signal amplifier 142 is used to make a standard waveform by filtering the noises of the obtained bio-signals and to control an amplification degree according to a patient (examinee).

[0058] As above mentioned, the bio-signal reception and process unit 140 is preferable to involve in the bio-signal measurement system 100 but, according to a circuit design, can be embedded in the main processing unit 210.

[0059] Next, the bio-signals obtained and processed by the bio-signal measurement system 100 are transferred to the analysis indicator calculator system 200 for synthesizing the aortic arch internal pressure curve P. The area of the aortic arch internal pressure curve P is used to calculate the biodynamic indicators.

[0060] As shown in Fig. 1, when the bio-signal reception and process unit 140 is separated from the main processing unit 210, a predetermined communicating means (e.g., RS-232C) is used to exchange the data between them.

[0061] The main processing unit 210 is a core unit, as like as a central processing unit (CPU) of computer, to process the measured data from the bio-signal reception and process unit 140 by the program saved in an internal memory part or an external memory part for calculating the biodynamic indicators which is used to analyze the coronary artery.

[0062] Here, the biodynamic indicators for analysis of the coronary artery are blood flow volumes S_1 and S_r , compliances C_1 and C_r , blood flow resistances R_1 and R_r , arterial stiffness As_1 and As_r , and blood flow velocities V_1 and V_r of the left and right coronary arteries.

[0063] First, the definition and the relationship of the biodynamic indicators used in this embodiment are simply described.

[0064] The blood flow volume is the volume of blood flowing in the left or right coronary artery. The unit of blood flow volume is $m\ell$, Q or $Q(t)$ is used to express it as a function of time, and S is used to express a blood volume having flowed for a time period (i.e., integral of Q for time). The blood flow volume is generally in direct proportion to the difference $P-P_v$ of blood pressures and in inverse proportion to the blood flow resistance R between two sites longitudinally separated in the coronary artery. The small value of the blood flow volume causes the ischemic symptoms.

[0065] The compliance is a change of volume occurred at the unit volume of blood vessel forced by the unit force. The unit of compliance is $m\ell/mmHg$ and the compliance is simply written as C . The small value of C means the more stiffness or contraction of the blood vessel wall. On the contrary, the large value of C means the more flex or extending spasm occurs in the blood vessel wall.

[0066] The blood flow resistance means the resistance against the flow of blood in the left or right coronary artery. The unit of blood flow resistance is $mmHg/\ell$ and is simply written as R . R is approximately determined by the rate of the difference $P-P_v$ of the blood pressures and the blood flow volume Q between two sites longitudinally separated in the coronary artery.

[0067] The arterial stiffness Asc is an indicator showing how much power is needed to change the unit length of blood vessel and, in other words, showing the stiffness of blood vessel. The Asc reflects the organic change of blood vessel. The unit of Asc is Kg/cm^2 and Asc is generally proportional to the square of the propagation velocity of elastic wave.

[0068] Lastly, the blood flow velocity V is the speed of blood flowing in the left or right coronary artery and the unit of V is cm/s. The pulse wave velocity (PWV) reflects the elastic status of an aorta and is measured by method recording pulse wave in the carotid artery and the femoral artery. The more stiffness of blood vessel wall is the more rapid of the velocity. Especially, the harder change of arteriosclerosis is the more rapid of the velocity of blood flow or the pulse wave velocity.

[0069] Also, in the words of the described biodynamic indicators, a subscript 'l' means a 'left' and a subscript 'r' means a 'right'.

[0070] On the other hand, the main processing unit 210 is connected to the input unit 220 for receiving the control commands of a user and to the output unit 240 for displaying the results calculated in the main processing unit 210.

[0071] Here, the output unit 240 comprises a screen output part through a monitor as well as a printer. Therefore, the image process unit 230 of Fig. 1 can be embedded in the screen output part.

[0072] Also, the input unit 220 comprises not only a keyboard and a mouse, but also a touch input means on the monitor of the screen output part.

[0073] In the above mentioned configuration, the core part is the calculation of the biodynamic indicators by some equations using the measurement and analysis of the bio-signals under the control of the main processing unit 210. Therefore, it is described in detail.

[0074] As shown in Fig. 8, the control of the main processing unit 210 comprises the steps of: step S100, synthesizing the aortic arch internal pressure curve P from the bio-signals measured by the bio-signal measurement system 100; step S200, calculating the blood flow volumes of the left and right coronary arteries using the synthesized aortic arch internal pressure curve P ; step S300, calculating the C and R of the left and right coronary arteries based on the aortic arch internal pressure curve P and the blood flow volumes of the left and right coronary arteries; step S400, calculating the stiffness of the left and right coronary arteries based on the calculated biodynamic indicators; and step S500, displaying a status diagram (e.g., C - R chart) in the output unit 240 by transmitting the calculated biodynamic indicators.

[0075] By the way, the control of the main processing unit 210 can be carried out by a program embedded in the main processing unit 210. The control program of the main processing unit 210 basically comprises the steps of: (1) ordering the bio-signal measurement system 100 to measure the bio-signals and receiving the bio-signals from the bio-signal measurement system 100; (2) analyzing waveforms from the received bio-signals and synthesizing the aortic arch internal pressure curve P from the analyzed waveforms; and (3) calculating the biodynamic indicators from the area of the synthesized aortic arch internal pressure curve P and displaying the results of cardiovascular analysis. The control of the main processing unit 210 can be variously carried out by the program as follows.

[0076] Above all, in step 1 to measure the bio-signals by the bio-signal measurement system 100, it is preferable to control as the following protocols: ECG, PCG and first cuff APG waveforms are simultaneously measured by the ECG sensor 122, the PCG sensor 124 and the APG sensor 126, the APG sensor being used as a cuff pulse wave sensor pressurized to 10~15 mmHg more than the systolic blood pressure to get a first cuff APG waveform 75 showing the feature points as shown in Fig. 13; ECG, PCG and second cuff APG waveforms are simultaneously measured by the ECG sensor 122, the PCG sensor 124 and the APG sensor 126, the APG sensor being used as a cuff pulse wave sensor depressurized to 20~30 mmHg less than the diastolic blood pressure to get a second cuff APG waveform 76 showing the feature points as shown in Fig. 14; ECG, PCG and left carotid artery APG waveforms are simultaneously measured by the ECG sensor 122, the PCG sensor 124 and the APG sensor 126, the APG sensor being used as a carotid artery pulse wave sensor to get a left carotid artery APG waveform 77 showing the feature points as shown in Fig. 15; ECG, PCG and right carotid artery APG waveforms are simultaneously measured by the ECG sensor 122, the PCG sensor 124 and the APG sensor 126, the APG sensor being used as a carotid artery pulse wave sensor to get a right carotid artery APG waveform 78 showing the feature points as shown in Fig. 15; and ECG and femoral artery APG waveforms are simultaneously measured by the ECG sensor 122 and the APG sensor 126, the APG sensor being used as a femoral artery pulse wave sensor.

[0077] Also, in step 2 the waveform analysis of the received bio-signals comprises, first of all, analyzing the ECG and PCG waveforms measured by the ECG sensor 122 and the PCG sensor 124 of the bio-signals measurement system 100, respectively, for finding the feature points of the aortic arch internal pressure curve P .

[0078] Here, the feature points of the aortic arch internal pressure curve P , as shown in Fig. 6, are systolic upstroke point t_1 , systolic peak point t_2 , incisura point t_3 , diastolic peak point t_4 and diastolic end point t_5 . The systolic period of the aortic arch internal pressure curve P is from the systolic upstroke point t_1 to the incisura point t_3 and the diastolic period is from the incisura point t_3 to the diastolic end point t_5 .

[0079] And, in step 2, the synthesis of the aortic arch internal pressure curve P is based on the information including the first and second cuff APG waveforms 75 and 76 showing its feature points, respectively, and the left and right carotid artery APG waveforms 77 and 78 showing its feature points, respectively

[0080] Also, in step 3, calculating the biodynamic indicators from the area of the aortic arch internal pressure curve P for showing the cardiovascular analysis results is based on the facts that, as like as mentioned below, the synthesized aortic arch internal pressure curve P 60 has a different waveform, but has the same area as the aortic arch internal

pressure curve P 50 which is measured by the invasive testing method using a catheter as shown in Fig. 7.

[0081] Step 3 for calculating the biodynamic indicators comprises specifically: calculating blood flow volumes S_1 and S_r of the left and right coronary arteries from the basic data including the area of the synthesized aortic arch internal pressure curve P; calculating compliances C_1 and C_r and blood flow resistances R_1 and R_r of the left and right coronary arteries from the aortic arch internal pressure curve P and the blood flow volumes S_1 and S_r of the left and right coronary arteries; and transmitting the results of cardiovascular analysis to the output unit for showing the calculated compliances C_1 and C_r and the calculated blood flow resistances R_1 and R_r of the left and right coronary arteries on one status diagram (e.g., C-R chart).

[0082] At this time, the blood flow volumes S_1 and S_r , the compliances C_1 and C_r and the blood flow resistances R_1 and R_r of the left and right coronary arteries are calculated by the following equations.

[0083] The blood flow volume S_1 of the left coronary artery is

$$S_1 = KA_d \left(\frac{t_* + \Delta t_d}{\Delta t_d} \right)$$

Equation 1

[0084] The blood flow volume S_r of the right coronary artery is

$$S_r = K_1 p R^2 (1 - v^2)^{1/2} P_m (1 + A_d / K_2 A_s) / (\rho a)$$

Equation 2

[0085] The compliance C_1 of the left coronary artery is

$$C_1 = \frac{(S_1 - A_d / R_1)}{(P_* - P_d)}$$

Equation 3

[0086] The compliance C_r of the right coronary artery is

$$C_r = \frac{k_2 A_s - A_d}{P_s^* - P_d} \cdot \frac{S_r}{k_2 A_s + A_d}$$

Equation 4

[0087] The blood flow resistances R_{11} and R_{12} of the left coronary artery are

$$R_{11} = \frac{P_d - P_v}{S_1}$$

Equation 5

$$R_{12} = \frac{\bar{P}}{S_v}$$

Equation 6

[0088] And the blood flow resistance R_r of right coronary artery is

$$Rr = \frac{k_2 A_s + A_d}{Sr}$$

Equation 7

5
 [0089] In Equations 1 to 7, A_d is an area of the aortic arch internal pressure curve P at diastole (i.e., for diastolic period), A_s is an area of the aortic arch internal pressure curve P at systole (i.e., for systolic period), t_* is a time (i.e., an incisura point) at which the first-order derivative function of the aortic arch internal pressure curve P is zero between at systole and at diastole, ν is Poisson constant of blood vessel, R is an equivalent radius of blood vessel, P_m is an average blood pressure, ρ is a blood density, a is a propagation velocity of pulse wave, P_d is a blood pressure of the aortic arch internal pressure curve P at diastole, P_s is a blood pressure of the aortic arch internal pressure curve P at systole, P^* and P_{s^*} are blood pressure of the aortic arch internal pressure curve P at an incisura point, P_v is a blood pressure at random point of the left coronary artery, S_v is a cardiac output, and K , K_1 and K_2 are coefficients.

10
 [0090] Here, the coefficient K is calculated by Equation 8. The coefficient K_1 is related to a blood flow volume flowing from an entrance of the coronary artery to the right coronary artery and is 0.12~0.15. The coefficient K_2 is a tissue internal pressure coefficient and is 0.7~0.75.

$$20 \quad K = kA \cdot \sqrt{C_s} = kA \left[(2mP_d + 1) \cdot \frac{A_d/R - n(P_s^2 - P_d^2)}{(P_s - P_d) + m(P_s^2 - P_d^2)} + 2nP_d \right]$$

Equation 8

25 [0091] In Equation 8, k is a coefficient related to a blood flow volume flowing from an entrance of the coronary artery to the left coronary artery and is 0.85~0.88, $A = \pi R^2$ is an equivalent area of the left coronary artery, C_s is a compliance at systole, and m and n are Cope constants.

30 [0092] Also, it is preferable that step 3 further comprises calculating arterial stiffness As_l and As_r of the left and right coronary arteries from the blood flow volumes S_l and S_r , the compliances C_l and C_r and the blood flow resistances R_l and R_r of the left and right coronary arteries and transmitting to the output unit 240.

[0093] At this time, the arterial stiffness As_l and As_r of the left and right coronary arteries are calculated by the following Equations 9 and 10.

[0094] The arterial stiffness As_l of the left coronary artery is

$$35 \quad As_l = K_3 \frac{R_l^{0.25}}{C_l R_{l1}} (1 - S_l)$$

Equation 9

40 [0095] And the arterial stiffness As_r of the right coronary artery is

$$45 \quad As_r = K_3 \frac{R_r^{0.25}}{C_r R_r} (1 - S_r)$$

Equation 10

[0096] In Equations 9 and 10, K_3 is a coefficient derived from the clinics and is 0.7~0.89.

50 [0097] In addition, it is preferable that step 3 further comprises calculating blood flow velocities V_l and V_r of the left and right coronary arteries from the aortic arch internal pressure curve P and the compliances C_l and C_r of the left and right coronary arteries and transmitting to the output unit 240.

[0098] At this time, the blood flow velocities V_l and V_r of the left and right coronary arteries are calculated by the following Equations 11 and 12.

55 [0099] The blood flow velocity V_l of the left coronary artery is

$$V_l = \frac{C_l}{A_0} \left(\frac{dp}{dt} \right)_{DW}$$

Equation 11

[0100] And the blood flow velocity V_r of the right coronary artery is

$$V_r = \frac{C_r}{A_0} \left(\frac{dp}{dt} \right)_{DW}$$

Equation 12

[0101] In Equations 11 and 12,

$$\left(\frac{dp}{dt} \right)_{DW} = \frac{P(x_1, t_2) - P(x_1, t_1)}{t_2 - t_1}$$

[0102] Next, referring to Figs. 9 to 16, the more specific control embodiments of the main processing unit 210 are described.

[0103] Figs. 9 to 12 are exemplary flowcharts showing more detail than Fig. 8. Fig. 13 is an exemplary diagram of the test and result window 70 showing ECG, PCG and first cuff APG waveforms 71, 73 and 75 analyzed by the main processing unit 210 in Fig. 1. Fig. 14 is an exemplary diagram of the test and result window 70 showing ECG, PCG and second cuff APG waveforms 72, 74 and 76 analyzed by the main processing unit 210 in Fig. 1. Fig. 15 is an exemplary diagram of the test and result window 70 showing left and right carotid artery APG waveforms 77 and 78 analyzed by the main processing unit 210 in Fig. 1. Fig. 16 is an exemplary diagram of the test and result window 70 showing C-R chart analyzed by the main processing unit 210 in Fig. 1.

[0104] As shown in Fig. 9, the main processing unit 210 is further programmed to display an initial screen including a search menu window, a patient information window, a test and diagnosis window and a test result window in the output unit 240 before step 1 (S10).

[0105] And the main processing unit 210 makes to receive and save the information of patient if a registration command for new patient is received in the initial screen (S13), otherwise, to receive an opening command to open a registered patient file (S12).

[0106] Next, the main processing unit 210 makes to display a patient list in the registered patient file on the test result window if the opening command is received and to receive a signal for selecting a patient and new information of the selected patient (S14), otherwise, to display the initial screen continuously.

[0107] Next, the main processing unit 210 makes to display the information of new patient or the selected patient on the patient information window and to receive a test and diagnosis command (S18).

[0108] Here, the information of new patient or the selected patient preferably comprises a personally identified information and body information including one or more of height, weight, blood pressure and race. Especially, the height, blood pressure, race and etc can be used to calculate the biodynamic indicators as the basic data of the patient (examinee).

[0109] Afterward, the measurement and reception of the bio-signals in step 1, as shown in Figs. 9 and 10, may be comprised of the following steps.

[0110] First of all, as step 1-1, the main processing unit 210 makes to display a command selection window for the bio-signal measurement (S20) if a test command is received from the test and diagnosis window (S18), otherwise, to keep the previous state.

Next, as step 1-2-1, the main processing unit 210 makes to receive ECG, PCG and first cuff APG waveforms measured by the ECG sensor 122, the PCG sensor 124 and a pressurized cuff pulse wave sensor as the APG sensor 126 of the bio-signal measuring sensor unit and to display on the test result window (S26) if the measurement command of a systolic pulse wave is received from the command selection window (S21), otherwise, to keep the previous state as a standby step for receiving a bio-signal measurement command.

As step 1-2-2, the main processing unit 210 makes to receive ECG, PCG and second cuff APG waveforms measured by the ECG sensor 122, the PCG sensor 124 and a depressurized cuff pulse wave sensor as the APG sensor 126 of the bio-signal measuring sensor unit and to display on the test result window (S26) if the measurement command

of a diastolic pulse wave is received from the command selection window (S22), otherwise, to keep the previous state as a standby step for receiving a bio-signal measurement command.

As step 1-2-3, the main processing unit 210 makes to receive ECG, PCG and left carotid artery APG waveforms measured by the ECG sensor 122, the PCG sensor 124 and a carotid artery pulse wave sensor as the APG sensor 126 of the bio-signal measuring sensor unit and to display on the test result window (S26) if the measurement command of the left carotid artery is received from the command selection window (S23), otherwise, to keep the previous state as a standby step for receiving a bio-signal measurement command.

As step 1-2-4, the main processing unit 210 makes to receive ECG, PCG and right carotid artery APG waveforms measured by the ECG sensor 122, the PCG sensor 124 and a carotid artery pulse wave sensor as the APG sensor 126 of the bio-signal measuring sensor unit and to display on the test result window (S26) if the measurement command of the right carotid artery is received from the command selection window (S24), otherwise, to keep the previous state as a standby step for receiving a bio-signal measurement command.

As step 1-2-5, the main processing unit 210 makes to receive ECG, PCG and femoral artery APG waveforms measured by the ECG sensor 122, the PCG sensor 124 and a femoral artery pulse wave sensor as the APG sensor 126 of the bio-signal measuring sensor unit and to display on the test result window (S27) if the measurement command of the femoral artery is received from the command selection window (S25), otherwise, to keep the previous state as a standby step for receiving a bio-signal measurement command.

[0111] And, as a step 1-3, the main processing unit 210 makes to capture a screen showing a selected ideal waveform among the waveforms displayed on the test result window and to save (S30) if a waveform selection command is received after each of the steps 1-2-1 to 1-2-5 (S28, S29), otherwise, to keep the measurement and to display the measured waveforms continuously.

[0112] Here, when the ideal waveforms are not displayed on the test result window, the received signals are controlled by the noise eliminator and signal amplifier 142 through the input unit 220 and the microcontroller 146.

[0113] Also, the waveform analysis of the received bio-signals and the synthesis of the aortic arch internal pressure curve P in step 2, as shown in Figs.10 to 12, may be comprised of the following steps.

As step 2-1, the main processing unit 210 makes to display an analysis menu window (S34) if an analysis command is received from the test and diagnosis window (S32), otherwise, to keep the previous step.

As step 2-2, the main processing unit 210 makes to analyze automatically feature points of the saved ECG waveform 71, PCG waveform 73 and first cuff APG waveform 75 and to display on the test result window 70 as shown in Fig. 13 (S38) if a systolic bio-signal analysis command is received from the analysis menu window (S36), otherwise, to keep the previous step.

As step 2-3, the main processing unit 210 makes to analyze automatically feature points of the saved ECG waveform 72, PCG waveform 74 and second cuff APG waveform 76 and to display on the test result window 70 as shown in Fig. 14 (S42) if a diastolic bio-signals analysis command is received from the analysis menu window (S40), otherwise, to keep the previous step.

As step 2-4, the main processing unit 210 makes to display the saved left and right carotid artery APG waveforms 77 and 78 on the test result window 70 as shown in Fig. 15 (S46) if a synthesized signal analysis command is received from the analysis menu window (S44), otherwise, to keep the previous step.

As step 2-5, the main processing unit 210 makes to display enlarged waveforms 81 and 82 analyzed in a selected interval on a lower left corner of the test result window 70 as shown in Fig. 15 (S50) if a detail analysis interval is selected in the left and right carotid artery APG waveforms 77 and 78 showing on the test result window 70 (e.g., by the mouse dragging in Fig. 15) (S48), otherwise, to keep the previous step.

As step 2-6, the main processing unit 210 makes to display an aortic arch internal pressure curve 83, which is synthesized with the information including the saved ECG, PCG and APG waveforms, in a place clicked on the test results window 70 (S54) if a vacant space of a lower right corner of the test results window 70 is clicked after the sequential displays of the enlarged left and right carotid artery APG waveforms 81 and 82 on the lower left corner of the test results window 70 (S52), otherwise, to keep the previous step.

[0114] At this time, it is preferable that the main processing unit 210 makes to return to the step 1-1 after displaying each waveform on the test result window in the steps 2-2 to 2-4 (S38, S42, S46) if a test command is received from the result and diagnosis window (S18), otherwise, to go to each next step.

[0115] Finally, step 3 showing the results of cardiovascular analysis through the calculation of the biodynamic indicators from the area of the synthesized aortic arch internal pressure curve P, as shown in Fig. 12, may be comprised of the following steps.

As step 3-1, the main processing unit 210 makes to display a result menu window and a output device (S58) if a

result display command is received from the test and diagnosis window (S56), otherwise, to keep the previous step. As step 3-2, the main processing unit 210 makes to display a selected menu result (S62) if one is selected on the result menu window (S60), otherwise, to keep the previous step.

As a step 3-2, the main processing unit 210 makes to output the selected menu result (S66) if an output command is received from the output device after displaying the selected menu result (S64), otherwise, to keep the previous step.

[0116] At this time, the result menu window, as shown in Fig. 16, preferably comprises a Compliance-Resistance (C-R) chart assessment. The C-R chart is divided into sectors to show the coronary artery states according to the clinical results and is dotted to show the states of the left and right coronary arteries of an examinee as the result of the C-R chart assessment.

[0117] It is reasonable that the sectors of C-R chart shown in Fig. 16 can be further divided to increase the precision according to the various results of clinics. By the exemplary embodiment of clinical result, the sectors can be defined as the followings.

Sector ① is the cardiovascular stenosis area. Although a symptom does not show, a coronary artery stenosis should be suspected. If examinees have the symptom, 90% or more of them have a coronary artery obstructed with 50% or more.

Sector ② is the very suspicious area of cardiovascular stenosis. If examinees have the symptom, 80 % or more of them can be diagnosed as stenosis.

Sector ③ is the suspicious area of cardiovascular stenosis. If examinees have the symptom, they can be examined and treated pursuant to the obstruction.

Sector ④ is the area with about 50% frequency of the cardiovascular stenosis. If examinees have the symptom, the cardiovascular state can be determined as bad even though it comes with a normal cardiovascular angiography.

Sector ⑤ is the area of cardiovascular extending spasm. Although a symptom does not show, the state can be diagnosed as an abnormal and the observation is needed. This can be suspected the drug over-dose for abnormal extension of coronary artery.

Sector ⑥ is the suspected area of the instability of cardiovascular blood flow because of the micro-regurgitation in blood vessel by internal pressure of myocardial tissue or others. Frequently, it is normal in the cardiovascular angiography. The observation is needed according to the symptom.

Sector ⑦ is the area generally diagnosed as a normal. The states of bloodstream and blood vessel are not normal, but are shown with no obstruction in the cardiovascular angiography.

Sector ⑧ is the normal area.

[0118] In the followings, the supplementary theories and clinical data are described to support the above mentioned embodiments.

[0119] The blood flows in the left coronary artery only at diastole. The research result is proved by the observation of the movement of the light marked niobium element in the coronary artery using the CCD type in vivo microscopy.

[0120] In the present invention, it is assumed that the blood flow in the left coronary artery is present only at diastole because of the tissue internal pressure and the self control property of myocardium occurring at systole of heart.

[0121] From the fact, it is suggested that the systole and diastole of aortic arch 40 is as like as that of a heart and supplies blood to the left and right coronary arteries 42 and 44 in the view of the blood circulation of coronary artery (ref. Fig. 4).

[0122] On the other hand, the systolic pressure of right ventricle is 25-30% of that of left ventricle and the systole of myocardium in the right ventricle wall presses the coronary artery weakly.

[0123] So, in the right coronary artery the maximum bloodstream is occurring at systole of heart and the waveform of the bloodstream has a pressure property in proportion to the aortic arch internal pressure curve.

[0124] On the other hand, according to other experimental data, blood flow volume changes linearly with blood pressure at the systole and diastole of blood vessel under 170 of blood pressure. So, the compliance of systolic blood vessel is the same as that of diastolic blood vessel.

[0125] Therefore, the problem of finding an area of the aortic arch internal pressure curve by the noninvasive testing method is the same as the problem of solving the pump function of heart tank for assessing the blood circulation of coronary artery, in other words, the working of pump to supply the blood to coronary artery.

[0126] Thus, first at the problem of configuration of the aortic arch internal pressure curve, the most accurate waveform and systolic and diastolic blood pressures in the aortic arch can be measured by the invasive testing method plugging the catheter in the blood vessel and then drawing the aortic arch internal pressure curve.

[0127] However, because it is not really usable in such a way, the aortic arch internal pressure curve has to be obtained by the noninvasive testing method.

[0128] If blood pressure is measured at the state pressurized above the systolic blood pressure or depressurized below the diastolic blood pressure after wearing on the cuff (i.e., upper arm) of examinee with a cuff pulse wave sensor as shown in the front view of Fig. 3, the waves formed by the vibration of blood flow is transmitted from the air pouch 13 to the pressure sensor 30 of the cuff pulse wave sensor as the APG sensor 126. And the vibration waveforms measured at the states pressurized above the systolic blood pressure and depressurized below the diastolic blood pressure can be obtained as first and second cuff APG waveforms 75 and 76, respectively, by a computer such as the main processing unit 210 connected to the bio-signal reception and process unit 140 electrically connecting the pressure sensor 30. The waveform displayed on the computer is formed by the air in the air pouch of cuff pulse wave sensor, but not the pulse wave itself. However, the waves measured by the cuff pulse wave sensor in the upper arm (i.e., cuff) accurately transmit the whole process of blood flow to the computer. Thus, the first and second cuff APG waveforms 75 and 76 are not the second derivatives but vibration waveforms originally measured by the cuff pulse wave sensor as the APG sensor 126.

[0129] When P_{sis} is the systolic pressure measured by sphygmomanometer, P_{dia} is the diastolic pressure measured by sphygmomanometer, P_{sis}^* is the systolic pressure to cause the first cuff APG waveforms 75, and P_{dia}^* is the diastolic pressure to cause the second cuff APG waveforms 76, the related equations are as followings.

$$P_{sis}^* = P_{sis} + \Delta 1 \quad \text{Equation 13}$$

$$P_{dia}^* = P_{dia} - \Delta 2 \quad \text{Equation 14}$$

[0130] On the other hand, Tables 1 and 2 are showing the conduit test data measured from 24 examinees by the catheter and the cuff pulse wave sensor.

[Table 1] Comparison of Systolic Blood Pressures measured by Catheter and Cuff pulse wave sensor

Blood Pressure Type	Frequency	Cuff Sensor	Conduit System	Blood Pressure Difference	Δ_1 Percent (%)	Remarks
Low blood pressure	3	100	110	10	10	
Normal blood pressure	4	120	130	10	9.2	
	3	140	151	11	7.8	
High blood pressure	4	160	172	12	7.5	
	5	180	192	12	6.7	
	5	200	212	12	6	
Total	24			11.16	7.8	

[Table 2] Comparison of Diastolic Blood Pressures measured by Catheter and Cuff pulse wave sensor

Blood Pressure Type	Frequency	Cuff Sensor	Conduit System	Blood Pressure Difference	Δ_2 Percent (%)	Remarks
Low blood pressure	3	70	50	20	28	
Normal blood pressure	4	80	57	23	28.7	
	3	90	62	27	30	
High blood pressure	4	100	70	30	30	
	5	110	76	34	31	
	5	120	84	38	31.6	

(continued)

Blood Pressure Type	Frequency	Cuff Sensor	Conduit System	Blood Pressure Difference	Δ_2 Percent (%)	Remarks
Total	24			20~38	29.5	

[0131] As obtained from Table 1, if the pulse wave is measured considering about 11 and 20~38 for the systolic and diastolic blood pressures, respectively, it can be found that the first and second cuff APG waveforms 75 and 76 respectively have the systolic and diastolic blood pressures similar to those of the aortic arch internal pressure curve.

[0132] On the other hand, because a carotid artery pulse wave is a wave which is not formed by the vibration in the air pouch of the cuff pulse wave sensor but measured on a surface of blood vessel by contacting a neck skin over the left or right carotid artery with the opening part 32 of the pressure sensor 30 as a carotid artery pulse wave sensor removed from the adaptor 20 in the disassembled perspective view of Fig. 3. And it has not a reflecting point. So, as shown in Fig. 15, a left or right carotid artery APG waveform 77 or 78 originally measured (i.e., not the second derivative) by the carotid artery pulse wave sensor is similar to the aortic arch internal pressure curve.

[0133] Therefore, in the present invention, the aortic arch internal pressure curve can be synthesized with a carotid artery APG waveform and the first and second cuff APG waveforms. Here, the carotid artery APG waveform is one of both the left and right carotid artery APG waveforms 77 and 78. The aortic arch internal pressure curve can be made simply by the superposition (i.e., addition in time domain) of the carotid artery APG waveform and the first and second cuff APG waveforms shifted to the same feature point (e.g., a systolic peak point). For obtaining the more useful aortic arch internal pressure curve, it can be synthesized by the superposition having some coefficients (e.g., α , β and γ below) in the carotid artery APG waveform and the first and second cuff APG waveforms shifted to the same feature point according to the program embedded in the main processing unit 210.

[0134] As an embodiment, a systolic aortic arch internal pressure curve P_{cs} synthesized in a systolic period can be

$$P_{cs} = \frac{\alpha P_{ss}}{\alpha + \beta + \gamma} + \frac{\beta P_{ds}}{\alpha + \beta + \gamma} + \frac{\gamma P_c}{\alpha + \beta + \gamma}$$

Equation 15

[0135] And a diastolic aortic arch internal pressure curve P_{cd} synthesized in a diastolic period can be

$$P_{cd} = P_{dia} + \frac{\beta}{\gamma + \beta} [P_{dia} - P_{ds}(t)] + \frac{\gamma}{\gamma + \beta} [P_{dia} - P_c(t)]$$

Equation 16

[0136] At the incisura point t_s , it must be satisfied with the following condition.

$$\left[\frac{\alpha P_{ss}(t_s)}{\alpha + \beta + \gamma} + \frac{\beta P_{ds}(t_s)}{\alpha + \beta + \gamma} + \frac{\gamma P_c(t_s)}{\alpha + \beta + \gamma} \right] = P_{dia} + \frac{\beta}{\gamma + \beta} [P_{dia} - P_{ds}(t_s)] + \frac{\gamma}{\gamma + \beta} [P_{dia} - P_c(t_s)]$$

Equation 17

where P_{ss} is a first cuff APG waveform measured in the upper arm by the cuff pulse wave sensor pressurized above the systolic blood pressure, P_{ds} is a second cuff APG waveform measured in the upper arm by the cuff pulse wave sensor depressurized below the diastolic blood pressure, and P_c is a carotid artery APG waveform measured in the left or right carotid artery by the carotid artery pulse wave sensor.

[0137] In Equations 15 to 17, the coefficients α , β , and γ may be calculated by the least square method of functionals $J_s[u(a, \beta, \gamma)]$ and $J_d[u(a, \beta, \gamma)]$ which are the difference between pulse waveforms gained by the intravascular ultrasound Doppler and the above synthesized curves P_{cs} and P_{cd} in the systolic and diastolic periods, respectively.

[0138] Though the noninvasive synthesized aortic arch internal pressure curve is different from the invasive aortic arch internal pressure curve, the area of the invasive aortic arch internal pressure curve is not different from that of the noninvasive aortic arch internal pressure curve between persons.

[0139] Therefore, in the present invention, the methods are suggested to obtain the clinical indicators using the area

data of a noninvasive synthesized aortic arch internal pressure curve.

[0140] By the least square method of the functionals $J_s(u)$ and $J_d(u)$ using the conduit test data measured from 24 examinees, the coefficients α , β , and γ are obtained as followings.

[Table 3] Conduit Test Data of 24 Examinees

No	α	β	γ	No	α	β	γ	No	α	β	γ
1	0.22	0.13	0.65	9	0.23	0.14	0.63	17	0.22	0.13	0.62
2	0.21	0.14	0.66	10	0.23	0.13	0.64	18	0.23	0.12	0.63
3	0.20	0.13	0.64	11	0.24	0.14	0.62	19	0.24	0.12	0.64
4	0.20	0.13	0.63	12	0.20	0.15	0.65	20	0.23	0.14	0.63
5	0.24	0.12	0.64	13	0.22	0.14	0.64	21	0.24	0.14	0.62
6	0.24	0.14	0.65	14	0.23	0.14	0.63	22	0.25	0.13	0.61
7	0.21	0.13	0.66	15	0.23	0.15	0.62	23	0.23	0.12	0.64
8	0.22	0.14	0.64	16	0.26	0.13	0.61	24	0.21	0.12	0.63

[0141] From the data of Table 3, the systolic and diastolic areas of the synthesized aortic arch internal pressure curve can be calculated from Equations 15 and 16, respectively, where $\alpha=0.22$, $\beta=0.13$, and $\gamma=0.65$.

[0142] Next, it is described to obtain the clinical indicators for assessing the state of blood vessel of coronary artery.

[0143] As above mentioned, in the left coronary artery, the blood starts to flow at diastole, but not at systole.

[0144] Because the change of coronary artery is very small and almost isotropic deformation, the compliance of systole is approximately same to that of diastole. So the compliance of the left coronary artery can be considered as that of the coronary artery even though it is calculated by the diastolic blood pressure causing blood flow in the left coronary artery and the deformation of the left coronary artery.

[0145] By this idea and from the model diagram of Fig. 5, when $T_s \leq t < T$, the pulse waveform $P(t)$ is obtained as Equation 21.

$$C_1 \frac{dP}{dt} + \frac{P - P_v}{R_1} = Q_1$$

Equation 21

[0146] In Equation 21, R_1 is the peripheral resistance of the left coronary artery, C_1 is the compliance of the left coronary artery, and Q_1 is the blood flow volume in the left coronary artery.

[0147] According to the experimental data, the relationship between pressure and volume in blood vessel shows that the deformation of blood vessel is linearly proportional to the pressure till around 170 mmHg of blood pressure.

[0148] Thus, C_1 is a constant as follows:

$$C_1 = \frac{(S_1 - A_v / R_1)}{(P_s - P_d)}$$

Equation 3

$$R_{11} = \frac{P_d - P_v}{S_1}$$

Equation 5

$$R_{12} = \frac{\bar{P}}{S_v}$$

Equation 6

[0149] Because the blood flows in right coronary artery at systole too, P , Q_r , R_r , and C_r have the relationship as

Equations 22 and 23.

$$C_r \frac{dP}{dt} + \frac{P - P_v}{R_r} = Q_r \quad 0 < t \leq T_s \quad \text{Equation 22}$$

$$C_r \frac{dP}{dt} + \frac{P - P_v}{R_r} = Q_r \quad T_s < t \leq T (Q = Q_s + Q_d) \quad \text{Equation 23}$$

[0150] R_r and C_r can be calculated by the function relationship between the area of aortic arch internal pressure curve P and the area of blood flow curve instead of adjusting R and C for coinciding those curves.

[0151] The reproducible R and C can be calculated by the function relationship between the areas.

$$\frac{k_2 A_s + A_d}{k_2 A_s - A_d} (P_s^* - P_d) = \frac{S_r}{C_r} \quad \text{Equation 24}$$

[0152] The left side of Equation 24 is that the systolic aortic arch internal pressure curve area is added to the diastolic aortic arch internal pressure curve area, divided by the systolic aortic arch internal pressure curve area subtracted by the diastolic aortic arch internal pressure curve area, and multiplied by the blood pressure of the incisura point subtracted by that of the diastole. The left side of Equation 24 is same to the blood flow volume divided by the compliance.

[0153] In other words, when input signal is the area of the aortic arch internal pressure curve and output signal is the blood flow volume, the function relationship is

$$k_2 A_s + A_d = f(k_2 A_s, A_d, P_s^*, P_d, C_r) S_r \quad \text{Equation 25}$$

[0154] From Equation 25, the compliance C_r is

$$C_r = \frac{k_2 A_s - A_d}{P_s^* - P_d} \cdot \frac{S_r}{k_2 A_s + A_d} \quad \text{Equation 4}$$

[0155] And the resistance R_r is

$$R_r = \frac{k_2 A_s + A_d}{S_r} \quad \text{Equation 7}$$

[0156] Therefore, the changes of blood pressure, blood flow volume, and area of aortic arch internal pressure curve are sensitive to the arteriosclerosis of blood vessel, the seizure and spasm of blood vessel, the drug reaction, and the blood pressure changes.

[0157] Next, when the coronary artery is an elastic tube as a simple pipe with blood flow, the organic and the functional changes of the coronary artery are distinguished as the solution of fluid elastic function in the elastic tube with blood flow.

[0158] From Fig. 4, when the left coronary artery 42 and the right coronary artery 44 are a single pipe, the continuity equation and the motion equation are described as

$$\frac{A}{\rho p w v^2} \cdot \frac{\partial P}{\partial t} + \frac{\partial Q}{\partial X} = 0$$

Equation 26

$$\frac{\rho}{A} \frac{\partial Q}{\partial t} = - \frac{\partial P}{\partial X} - \frac{8\mu\pi Q}{A^2}$$

Equation 27

[0159] In Equation 26, $p w v$ is the pulse wave velocity ($p w v = \sqrt{\frac{A \cdot dP}{\rho \cdot dA}}$), P is a curve of blood pressure, Q is a curve of blood flow volume, μ is a viscosity, A is a cross-section area of blood vessel, and ρ is a density of blood.

[0160] Now, when $\frac{\rho}{A} \frac{\partial Q}{\partial t}$ is ignored, the integral on X is

$$\frac{A}{\rho a^2} \frac{dP}{dt} + \frac{A^2 (P - P_v)}{8\pi\mu_p} = Q_d$$

Equation 28

[0161] From Equation 28, Equations 29 and 30 are derived in the single elastic tube.

$$\frac{A}{\rho w v^2} = C$$

Equation 29

$$R = \frac{8\pi\mu}{A^2}$$

Equation 30

[0162] On the other hand, according to Moensu Korteweg, because

$$P W V = \sqrt{(E/\rho)(h/d)} = a(h/d)$$

the elastic coefficient is $E = \rho(d/h)PWV^2$.

[0163] Consequently, because the elastic coefficient (i.e., the arterial stiffness) E is expressed as the elastic wave velocity a , E represents the organic change in coronary artery, but not related to the blood pressure change, the seizure, the spasm and the drug reaction in the coronary blood vessel.

[0164] Therefore, the arterial stiffness A_{sc} (elastic coefficient) of coronary artery is obtained by eliminating A from C and R and then transformed as:

$$A_{sc} = K_3 \frac{R^{0.25}}{C R} (1 - S)$$

Equation 31

[0165] In Equation 31, S is $S = f(PWV)$ and K_3 is a coefficient from clinics.

[0166] Next, in order to use the above mentioned indicators reflecting the property of coronary blood vessel and the

characters of the bloodstream in clinics, the blood flow volume which flows to the coronary artery must be calculated.

[0167] Now, in order to clarify this issue, it is needed to consider as the left and right coronary arteries are distinguished each other.

5 [0168] First, when L is the length of right coronary and A is a cross-section area, as already known from hydraulics, in lineal pipe, the waveform of blood pressure is similar to the waveform of blood flow volume in one-dimensional flow of slurry fluid.

[0169] Based on the above facts, the equation of blood flow volume which flows in the right coronary artery can be made as below.

10 [0170] From the experimental result, the blood pressure curve of the right coronary artery is as the following.

[0171] The curves of systolic and diastolic blood pressures are integrated as:

$$15 \quad k_2 A_s = \int_0^{T_s} k_2 P(t) dt \quad \text{Equation 32}$$

$$20 \quad A_d = \int_{T_s}^T P(t) dt \quad \text{Equation 33}$$

[0172] In Equations 32 and 33, T_s is a systolic time, T is a period of heart beat, and k_2 is 0.7~0.75.

25 [0173] From Frank's law, among the pulse pressure, blood flow velocity, elastic wave velocity and blood density in right coronary artery, Equation 34 is established as:

$$30 \quad \Delta P = \rho V a \quad \text{Equation 34}$$

where V is a blood flow velocity, a is a pulse wave propagation speed, ρ is a blood density, and ΔP is a pulse pressure.

[0174] When the right coronary artery is a single elastic tube, Frank equation is converted to McDonald equation and the blood flow can be calculated as:

$$35 \quad S_r = K_1 \rho R^2 (1 - \nu^2)^{1/2} P_m (1 + A_d / K_2 A_s) / (\rho a) \quad \text{Equation 2}$$

40 where ν is Poisson constant of blood vessel, R is a diameter of blood vessel, P_m is an average of blood pressure, K_1 is a coefficient related to the blood flow volume flowed in the right coronary artery from the entrance of coronary artery and is 0.12~0.15, and K_2 is a tissue internal coefficient and is 0.7~0.75.

$$P_m = (K_2 A_s + A_d) / R \quad \text{Equation 35}$$

45 [0175] Next, it is discussed that the blood flow volume flows in the left coronary artery.

[0176] In the left coronary artery, the blood flow is occurred by the stored potential energy in aorta during the diastole. For this reason, in a systolic aorta, the compliance of blood vessel is as a supplementary factor for inducing the blood flow in the coronary artery.

50 [0177] According to the mentioned Frank equation, $S_{vc} = \Delta P \pi R^2 T / (2 \rho a)$. In the present invention, when the systole of aortic arch is considered as a heart to supply blood to the coronary artery, the vascular blood flow volume is calculated with McDonald equation $S_v = K P_m (1 + A_d / A_s)$ and can be constructed as:

$$55 \quad S_i = K A_d \left(\frac{t_s + \Delta t_d}{\Delta t_d} \right) \quad \text{Equation 1}$$

[0178] In Equation 1, A_d is area of the diastolic aortic arch internal pressure curve P , t_* is time to 0 of first-order derived function.

[0179] On the other hand, the coefficient K is

$$K = kA \cdot \sqrt{C_s} = kA \left[(2mP_d + 1) \cdot \frac{A_d/R - n(P_*^2 - P_d^2)}{(P_* - P_d) + m(P_*^2 - P_d^2)} + 2nP_d \right] \quad \text{Equation 8}$$

[0180] In Equation 8, k is a coefficient related to a blood flow volume flowing from an entrance of the coronary artery to the left coronary artery and is 0.85-0.88, $A = \pi R^2$ is an equivalent area of the left coronary artery, C_s is a compliance at systole, and m and n are Cope constants.

[0181] Tables 4 and 5 show the Cope constant on race and the systolic compliance on age.

[Table 4] Cope Constant on Race

Race	m		n	
	$1/P_a$	$1/mmHg$	m/P_a	m/P_a
European	-2.03×10^{-5}	-2.703×10^{-3}	3.36×10^{-8}	0.6445×10^{-4}
Asian	-2.5×10^{-5}	-3.0×10^{-5}	5.07×10^{-8}	0.9×10^{-4}

[Table 5] Systolic Compliance on Age

Age	Normal	Morbid	***
40 years	1.007 ± 0.05	0.917 ± 0.08	0.771 ± 0.07
50 years	0.918 ± 0.05	0.817 ± 0.09	0.667 ± 0.08
60 years	0.854 ± 0.04	0.772 ± 0.09	0.548 ± 0.09

[0182] Equation 1 is similar to McDonald equation and is exactly reflecting the diastolic blood flow volume of the left coronary artery. In the present invention, Equation 1 is confirmed by the experiment with six dogs.

[0183] In the experiment, using the Doppler catheter, the blood flow volume is measured in the proximal circumflex of left coronary artery at the blood vessel extension. The cuff pulse wave and the carotid artery pulse wave are used to make the aortic arch internal pressure curve. The blood flow volume is calculated by Equation 1 suggested in the present invention.

[0184] According to the experimental result, it is suggested that the blood flow volume measured by Doppler catheter shows to have high relationship with the blood flow volume calculated from the aortic arch internal pressure curve.

[0185] In the examined dog, the pulse is 35-207 beats/min, the diastolic average artery pressure is 16-60mmHg, the blood flow volume 0.12-0.14ml, and the cardiac cycles is 481.

[0186] The blood flow velocity calculated by Doppler method is obtained if the distribution of blood flow velocity measured by Doppler catheter forms the Poiseuille velocity distribution and the space maximum velocity equals to the half of the spectrum maximum velocity.

[0187] Next, the blood flow volume measured by an ultrasound Doppler is calculated from $S_c = AV$. A is the cross-section area of the proximal circumflex of left coronary artery measured from the angiograph and V is the blood flow velocity.

[0188] The Doppler used to draw the blood flow curve is the Doppler Blood Vessel Forming Guide-wire Type Blood Flow Volume System with a Blood Flow Velocimetry for spectrum analysis.

[0189] The length of Guide-wire is 175 cm, the diameter is 18 inch, and the ultrasound Doppler type catheter has one end with a 12MHz piezoelectric ultrasound sensor.

[0190] The equation for the blood flow volume of left coronary artery has $\pm 6\%$ error of experimentally measured values.

[0191] Using the same method, after experimenting in the right coronary artery, the result is follows: $S_c = 1.21S^*c - 0.21$, $\gamma^2 = 0.86$, and $Se = 3.98ff$.

[0192] Now, the above equations are integrated from T_s to T .

[0193] At this time, because P_v is much smaller than P , if P_v is ignored,

$$S_{cv} = \int_{T_s}^T Q_{in} dt, \int_{T_s}^T P dt = A_d, CP \Big|_{T_s}^T = C(P_s - P_d)$$

Equation 36

[0194] If the related equations are substituted, the result is

$$C(P_s - P_d) + \frac{A_d}{R} = S_{cv}$$

Equation 37

[0195] In Equation 37, P^* is the blood pressure of the incinura point and is

$$P^* = P_d + P \frac{h_1}{h_2} (P_s - P_d)$$

Equation 38

[0196] On the other hand, $R=(A_s+A_d)/Scl$, Scl is the blood flow volume of left coronary artery.

[0197] Next, the blood flow velocity in the aorta is calculated.

[0198] The slope of the aortic arch internal pressure curve by invasive testing method is much different from that of the aortic arch internal pressure curve by noninvasive testing method at systole in one man.

[0199] However, the slope of the curves from the average blood pressure point to the diastolic end point shows a high relationship.

[0200] The relationship obtained from the 24 examinees is as follows:

$$\text{Grad Hc} = 0.918 \text{Grad Hn} + 0.024, \gamma^2 = 0.92, \text{Se} = 1.68f$$

Equation 39

[0201] In Equation 39, Grad Hc is the slope of the aortic arch internal pressure curve by invasive testing method and Grad Hn is the slope of the aortic arch internal pressure curve by noninvasive testing method.

[0202] On the other hand, if the blood flow in blood vessel is assumed as a Newtonian fluid with one-dimensional motion, the blood flow is considered as a fluid motion in terms of Euler because the blood flow is uniform by the mean of average S .

[0203] In other words, $V_1 = (dx/dt)x_1$ at a point x of artery.

[0204] On the other hand, in the aortic arch internal pressure curve, the pulse wave is nearly linear on the change of pressure from the average point of artery pulse pressure to the diastolic end point and the follow equation is possible.

$$\left(\frac{dp}{dt}\right)_{DW} = \frac{P(x_1, t_2) - P(x_1, t_1)}{t_2 - t_1} = A_0 V_0 / C$$

Equation 40

[0205] In Equation 40, V_0 is the average velocity of blood flow during the diastole and t_1 and t_2 are two time points in the diastole period.

[0206] From above mentioned, in the left coronary artery, Blood flow velocity V_1 is

55

$$V_l = \frac{C_l}{A_0} \left(\frac{dp}{dt} \right)_{DW}$$

Equation 11

The compliance of blood vessel C_l is

$$C_l = \frac{(S_l - A_d / R_l)}{(P_* - P_d)}$$

Equation 3

The resistance of blood flow R_{l1} is

$$R_{l1} = \frac{P_d - P_v}{S_l}$$

Equation 5

The resistance of blood flow R_{l2} is

$$R_{l2} = \frac{\bar{P}}{S_v}$$

Equation 6

The stiffness of artery A_{s1} is

$$A_{s1} = K_3 \frac{R_{l1}^{0.25}}{C_l R_{l1}} (1 - S_l)$$

Equation 9

The blood flow volume S_l is

$$S_l = K A_d \left(\frac{t_* + \Delta t_d}{\Delta t_d} \right)$$

Equation 1

[0207] On the other hand, in the right coronary artery, The compliance of blood vessel Q_l is

$$C_r = \frac{k_2 A_s - A_d}{P_s^* - P_d} \cdot \frac{S_r}{k_2 A_s + A_d}$$

Equation 4

The resistance of blood flow R_r is

$$Rr = \frac{k_2 A_s + A_d}{S_r}$$

Equation 7

The blood flow velocity V_r is

$$V_r = \frac{C_r}{A_0} \left(\frac{dp}{dt} \right)_{DW}$$

Equation 12

The artery stiffness A_{sr} is

$$A_{sr} = K_3 \frac{Rr^{0.25}}{C_r Rr} (1 - S_r)$$

Equation 10

The blood flow S_r is

$$S_r = K_1 p R^2 (1 - v^2)^{1/2} P_m (1 + A_d / K_2 A_s) / (\rho a)$$

Equation 2

[0208] Finally, the cardiovascular analyzer of the present invention is clinically tested to the patients in University Hospital in Korea and the results are described.

[0209] The following clinical examinations are tested to the 34 patients with the coronary artery disease-like who are measured with angiography and the results are showed in Tables 6 and 7.

[Table 6] Population Statistics of Patients (n = 34)

Parameter	Result
Age (year)	60.8±11.0
No. of Male (%)	18(52.9)
No. of Clinical Diagnosis (%)	
No. of Stable Angina (%)	34(100)
Left Ventricular Ejection Rate (%)	67.7±7.6
No. of Previous Myocardial Infection (%)	1(2.9)
No. of Severe Coronary Artery Disease (Stenosis>50%) (%)	18(52.9)

[Table 7] Device Sensitivity and Characteristics for Detecting Severe Coronary Artery Disease

	Mild Coronary Artery Disease	Severe Coronary Artery Disease	Total
Negative	6	4	10
Low Possibility	7	1	8
High Possibility	0	4	4
Positive	3	7	10
Total	16	16	32

[0210] In Tables 6 and 7, severe coronary artery disease (CAD) shows above 50% of stenosis, at least, in one of the major coronary arteries by angiography.

[0211] When severe coronary artery disease is positive result, it is certainly the category of high possibility, but the categories of low possibility and negative are divided into several uncertain results of severe coronary artery disease.

[0212] Consequently, the cardiovascular analyzer of the present invention shows considerably excellent sensitivity and diagnostic characteristics for diagnosis of severe coronary artery diseases more than that of the other screen diagnosis instruments such as electrocardiography and ultrasound heart diagnosis device.

[0213] In addition, the cardiovascular analyzer of the present invention has some advantages such as the measuring time, the noninvasive property, and the adaptability to almost all patients with disability in walking and/or the side effect of dobutamine.

[Industrial Applicability]

[0214] The cardiovascular analyzer of the present invention shows considerably excellent sensitivity and diagnostic characteristics for diagnosis of severe coronary artery diseases more than that of the other screen diagnosis instruments such as electrocardiography and ultrasound heart diagnosis device, and also shows the diagnosis of the organic and functional states which are not detected by angiography. Consequently, the cardiovascular analyzer of the present invention has a very high industrial applicability because of the early diagnosis of the several cardiovascular incurable diseases and the selection of the cardiovascular surgery examinee by the noninvasive testing method.

Claims

1. A cardiovascular analyzer comprising:

a bio-signal measurement system including a bio-signal measuring sensor unit which comprises an electrocardiogram (ECG) sensor, a phonocardiogram (PCG) sensor and an accelerated plethysmogram (APG) sensor, and a bio-signal reception and process unit which is connected to each of the sensors of the bio-signal measuring sensor unit for receiving and processing bio-signals measured by the sensors; and

an analysis indicator calculation system including a main processing unit which is connected to the bio-signal reception and process unit for communicating and calculating biodynamic indicators of a coronary artery from the bio-signals, an input unit which is connected to the main processing unit for receiving control commands of a user, and an output unit which is connected to the main processing unit for displaying the calculated results, wherein the main processing unit is configured to synthesize an aortic arch internal pressure curve P from the bio-signals measured by the bio-signal measurement system and to calculate the biodynamic indicators from an area of the aortic arch internal pressure curve P; and

wherein the aortic arch internal pressure curve P is synthesized with a first and second cuff APG waveforms and a left or right carotid artery APG waveform among the bio-signals.

2. The cardiovascular analyzer of claim 1, wherein the bio-signal reception and process unit comprises:

a microcontroller which controls to process the bio-signals received from the bio-signal measuring unit and to transmit processed bio-signals to the main processing unit;

a multi-signal selector which selects one of the bio-signals received from the ECG sensor, the PCG sensor and the APG sensor by a control signal of the microcontroller;

a noise eliminator and signal amplifier which eliminates noises and/or controls amplification degree of the bio-signal selected by the multi-signal selector by a control signal of the microcontroller;

a signal switcher which receives the bio-signals from the noise eliminator and signal amplifier and selects one of the bio-signals to meet the control commands of the input unit or of embedded program in the main processing unit by a control signal of the microcontroller;

a sample holder which samples and holds the bio-signal selected by the signal switcher by a control signal of the microcontroller; and

an A/D converter which converts a holding bio-signal of the sample holder to a digital bio-signal and sends to the microcontroller by a control signal of the microcontroller.

3. The cardiovascular analyzer of claim 1 or 2, wherein the APG sensor is assembled with a cuff sphygmomanometer and a pressure sensor electrically connected

to the bio-signal reception and process unit;
 wherein the APG sensor is used as a cuff pulse wave sensor in an assembly state to measure the first and second
 cuff APG waveforms; and
 wherein the APG sensor is used as a carotid artery pulse wave sensor by the pressure sensor in a disassembly
 state to measure the left or right carotid artery APG waveform.

4. The cardiovascular analyzer of claim 3,
 wherein the first cuff APG waveform is measured by the cuff pulse wave sensor pressurized above the systolic
 blood pressure;
 wherein the second cuff APG waveform is measured by the cuff pulse wave sensor depressurized below the diastolic
 blood pressure; and
 wherein the left or right carotid artery APG waveform is measured by the carotid artery pulse wave sensor which is
 the pressure sensor electrically connected to the bio-signal reception and process unit.

5. The cardiovascular analyzer of claim 3,
 wherein the APG sensor comprises a rubber hose which is connected to an air pouch of the cuff sphygmomanometer,
 a branch hose which is connected to the rubber hose, and an adaptor which is connected to an exit of the branch
 hose; and
 wherein the adaptor having a through hole is removably assembled to an opening part of a housing body of the
 pressure sensor, the pressure sensor being used as the carotid artery pulse wave sensor.

6. The cardiovascular analyzer of claim 1,
 wherein the main processing unit is programmed to carry out the steps of:

- (1) ordering the bio-signal measurement system to measure the bio-signals and receiving the bio-signals from
 the bio-signal measurement system;
- (2) analyzing waveforms from the received bio-signals and synthesizing the aortic arch internal pressure curve
 P from the analyzed waveforms; and
- (3) calculating the biodynamic indicators from the area of the synthesized aortic arch internal pressure curve P
 and displaying the results of cardiovascular analysis.

7. The cardiovascular analyzer of claim 6,
 wherein step 3 comprises:

- calculating blood flow volumes S_l and S_r of the left and right coronary arteries from basic data including the
 area of the aortic arch internal pressure curve P;
- calculating compliances C_l and C_r and blood flow resistances R_l and R_r of the left and right coronary arteries
 from the aortic arch internal pressure curve P and the blood flow volumes S_l and S_r of the left and right coronary
 arteries; and
- transmitting the results of cardiovascular analysis to the output unit for showing the calculated compliances C_l
 and C_r and the calculated blood flow resistances R_l and R_r of the left and right coronary arteries on one C-R chart.

8. The cardiovascular analyzer of claim 7,
 wherein step 3 further comprises:

- calculating arterial stiffness A_{s_l} and A_{s_r} of the left and right coronary arteries from the blood flow volumes S_l
 and S_r , the compliances C_l and C_r and the blood flow resistances R_l and R_r of the left and right coronary arteries
 and transmitting to the output unit.

9. The cardiovascular analyzer of claim 7,
 wherein step 3 further comprises:

- calculating blood flow velocities V_l and V_r of the left and right coronary arteries from the aortic arch internal
 pressure curve P and the compliances C_l and C_r of the left and right coronary arteries and transmitting to the
 output unit.

10. The cardiovascular analyzer of claim 7, wherein the blood flow volumes S_l and S_r , the compliances C_l and C_r and
 the blood flow resistances R_l and R_r of the left and right coronary arteries are calculated by the equations of:

the blood flow volume S_l of the left coronary artery is

$$S_l = KA_d \left(\frac{t_* + \Delta t_d}{\Delta t_d} \right),$$

the blood flow volume S_r of the right coronary artery is

$$S_r = K_1 p R^2 (1 - \nu^2)^{1/2} P_m (1 + A_d / K_2 A_s) / (\rho a),$$

the compliance C_l of the left coronary artery is

$$C_l = \frac{(S_l - A_d / R_l)}{(P_* - P_d)},$$

the compliance C_r of the right coronary artery is

$$C_r = \frac{k_2 A_s - A_d}{P_s^* - P_d} \cdot \frac{S_r}{k_2 A_s + A_d},$$

the blood flow resistances R_{l1} and R_{l2} of the left coronary artery are

$$R_{l1} = \frac{P_d - P_v}{S_l}$$

and

$$R_{l2} = \frac{\bar{P}}{S_v}$$

and

the blood flow resistance R_r of right coronary artery is

$$R_r = \frac{k_2 A_s + A_d}{S_r}$$

where A_d is an area of the aortic arch internal pressure curve P at diastole (i.e., for diastolic period), A_s is an area of the aortic arch internal pressure curve P at systole (i.e., for systolic period), t_* is a time (i.e., an incisura point) at which the first-order derivative function of the aortic arch internal pressure curve P is zero between at systole and at diastole, ν is Poisson constant of blood vessel, R is an equivalent radius of blood vessel, P_m is an average blood pressure, ρ is a blood density, a is a propagation velocity of pulse wave, P_d is a blood pressure of the aortic arch

internal pressure curve P at diastole, Ps is a blood pressure of the aortic arch internal pressure curve P at systole, P* and Ps* are blood pressure of the aortic arch internal pressure curve P at an incisura point, Pv is a blood pressure at random point of the left coronary artery, Sv is a cardiac output, and K, K1 and K2 are coefficients.

- 5 11. The cardiovascular analyzer of claim 10,
 wherein the coefficient K1 is related to a blood flow volume flowing from an entrance of the coronary artery to the
 right coronary artery and is 0.12~0.15;
 wherein the coefficient K2 is a tissue internal pressure coefficient and is 0.7~0.75;
 and
 10 wherein the coefficient K is calculated by

$$15 \quad K = kA \cdot \sqrt{C_s} = kA \left[(2mP_d + 1) \cdot \frac{A_d/R - n(P_s^2 - P_d^2)}{(P_s - P_d) + m(P_s^2 - P_d^2)} + 2nP_d \right]$$

20 where k is a coefficient related to a blood flow volume flowing from an entrance of the coronary artery to the left
 coronary artery and is 0.85~0.88, A=πR² is an equivalent area of the left coronary artery, Cs is a compliance at
 systole, and m and n are Cope constants.

- 25 12. The cardiovascular analyzer of claim 8,
 wherein the arterial stiffness Asl and Asr of the left and right coronary arteries are calculated by the equations of:
 the arterial stiffness Asl of the left coronary artery is

$$30 \quad As_l = K_3 \frac{R_{l1}^{0.25}}{C_l R_{l1}} (1 - S_l)$$

35 and the arterial stiffness Asr of the right coronary artery is

$$40 \quad As_r = K_3 \frac{R_r^{0.25}}{C_r R_r} (1 - S_r)$$

where K3 is a coefficient derived from the clinics and is 0.7~0.89.

- 45 13. The cardiovascular analyzer of claim 9,
 wherein the blood flow velocities Vl and Vr of the left and right coronary arteries are calculated by the equations of:
 the blood flow velocity Vl of the left coronary artery is

$$50 \quad V_l = \frac{C_l}{A_0} \left(\frac{dp}{dt} \right)_{DW}$$

and the blood flow velocity Vr of the right coronary artery is

$$55 \quad V_r = \frac{C_r}{A_0} \left(\frac{dp}{dt} \right)_{DW}$$

where

$$\left(\frac{dp}{dt}\right)_{DW} = \frac{P(x_1, t_2) - P(x_1, t_1)}{t_2 - t_1}$$

14. The cardiovascular analyzer of one of claims 6 to 13,
wherein analyzing waveforms from the received bio-signals in step 2 comprises:

finding feature points, including systolic upstroke point, systolic peak point, incisura point, diastolic peak point and diastolic end point, of the aortic arch internal pressure curve P by analyzing ECG signals and PCG signals measured by the ECG sensor and the PCG sensor of the bio-signals measurement system, respectively;
analyzing first cuff APG waveforms measured by a cuff pulse wave sensor, as the APG sensor of the bio-signals measurement system, which is pressurized above the systolic blood pressure;
analyzing second cuff APG waveforms measured by the cuff pulse wave sensor which is depressurized below the diastolic blood pressure; and
analyzing left and right carotid artery APG waveforms measured by a carotid artery pulse wave sensor as the APG sensor of the bio-signals measurement system, and

wherein the synthesis of the aortic arch internal pressure curve P is based on basic information including the analyzed data of the first and second cuff APG waveforms and the analyzed data of the left and right carotid artery APG waveforms.

15. The cardiovascular analyzer of claim 14,
wherein the main processing unit is further programmed to carry out the steps of:

displaying an initial screen including a search menu window, a patient information window, a test and diagnosis window and a test result window in the output unit before step 1;
receiving and saving the information of patient if a registration command for new patient is received in the initial screen, otherwise, receiving an opening command to open a registered patient file;
displaying a patient list in the registered patient file on the test result window if the opening command is received and receiving a signal for selecting a patient and new information of the selected patient, otherwise, displaying the initial screen continuously; and
displaying the information of new patient or the selected patient on the patient information window and receiving a test and diagnosis command, and

wherein the information of new patient or the selected patient comprises a personally identified information and body information including one or more of height, weight, blood pressure and race.

16. The cardiovascular analyzer of claim 15,
wherein performance of step 1 by the main processing unit further includes the steps of:

(1-1) displaying a command selection window for the bio-signal measurement if a test command is received from the test and diagnosis window, otherwise, keeping the previous state;
(1-2-1) receiving ECG, PCG and first cuff APG waveforms measured by the ECG sensor, the PCG sensor and a pressurized cuff pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of a systolic pulse wave is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command;
(1-2-2) receiving ECG, PCG and second cuff APG waveforms measured by the ECG sensor, the PCG sensor and a depressurized cuff pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of a diastolic pulse wave is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command;
(1-2-3) receiving ECG, PCG and left carotid artery APG waveforms measured by the ECG sensor, the PCG sensor and a carotid artery pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of the left carotid artery is received from the

command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command;

(1-2-4) receiving ECG, PCG and right carotid artery APG waveforms measured by the ECG sensor, the PCG sensor and a carotid artery pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of the right carotid artery is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command;

(1-2-5) receiving ECG, PCG and femoral artery APG waveforms measured by the ECG sensor, the PCG sensor and a femoral artery pulse wave sensor as the APG sensor of the bio-signal measuring sensor unit and displaying on the test result window if the measurement command of the femoral artery is received from the command selection window, otherwise, keeping the previous state as a standby step for receiving a bio-signal measurement command; and

(1-3) capturing a screen showing a selected ideal waveform among the waveforms displayed on the test result window and saving if a waveform selection command is received after each of steps 1-2-1 to 1-2-5, otherwise, keeping the measurement and displaying the measured waveforms continuously.

17. The cardiovascular analyzer of claim 16, wherein analyzing waveforms from the received bio-signals and synthesizing the aortic arch internal pressure curve P from the analyzed waveforms in step 2 comprise:

(2-1) displaying an analysis menu window if an analysis command is received from the test and diagnosis window, otherwise, keeping the previous step;

(2-2) analyzing automatically feature points of the saved ECG, PCG and first cuff APG waveforms and displaying on the test result window if a systolic bio-signal analysis command is received from the analysis menu window, otherwise, keeping the previous step;

(2-3) analyzing automatically feature points of the saved ECG, PCG and second cuff APG waveforms and displaying on the test result window if a diastolic bio-signals analysis command is received from the analysis menu window, otherwise, keeping the previous step;

(2-4) displaying the saved left and right carotid artery waveforms on the test result window if a synthesized signal analysis command is received from the analysis menu window, otherwise, keeping the previous step;

(2-5) displaying enlarged waveforms analyzed in a selected interval on a lower left corner of the test result window if a detail analysis interval is selected in the left and right carotid artery waveforms showing on the test result window, otherwise, keeping the previous step; and

(2-6) displaying an aortic arch internal pressure curve, which is synthesized with the information including the saved ECG, PCG and APG waveforms, in a place clicked on the test results window if a vacant space of a lower right corner of the test results window is clicked after the sequential displays of the enlarged left and right carotid artery waveforms on the lower left corner of the test results window, otherwise, keeping the previous step.

18. The cardiovascular analyzer of claim 17, wherein step 3 comprises:

(3-1) displaying a result menu window and a output device icon if a result display command is received from the test and diagnosis window, otherwise, displaying a patient list in the registered patient file on the test result window and receiving a signal for selecting a patient and new information of the selected patient till receiving a command;

(3-2) displaying a selected menu result if one is selected on the result menu window, otherwise, keeping step 3-1; and

(3-3) outputting the selected menu result if an output command is received from the output device icon after displaying the selected menu result, otherwise, keeping step 3-2.

19. The cardiovascular analyzer of claim 17, wherein each of steps 2-2, 2-3, and 2-4 causes the main processing unit to return to step 1-1 if a test command is received from the result and diagnosis window after displaying each waveform on the test result window, and wherein if the test command is not received, each of steps 2-2, 2-3, and 2-4 is followed by the subsequent step.

20. The cardiovascular analyzer of claim 18, wherein the result menu window comprises a Compliance-Resistance (C-R) chart; and wherein the C-R chart is divided into sectors to show the coronary artery states according to the clinical results and

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is dotted to show the states of the left and right coronary arteries of an examinee.

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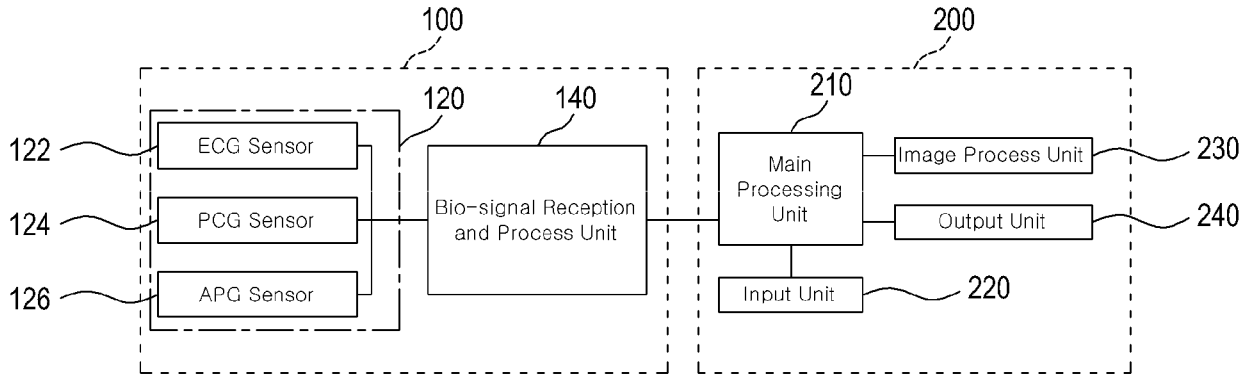
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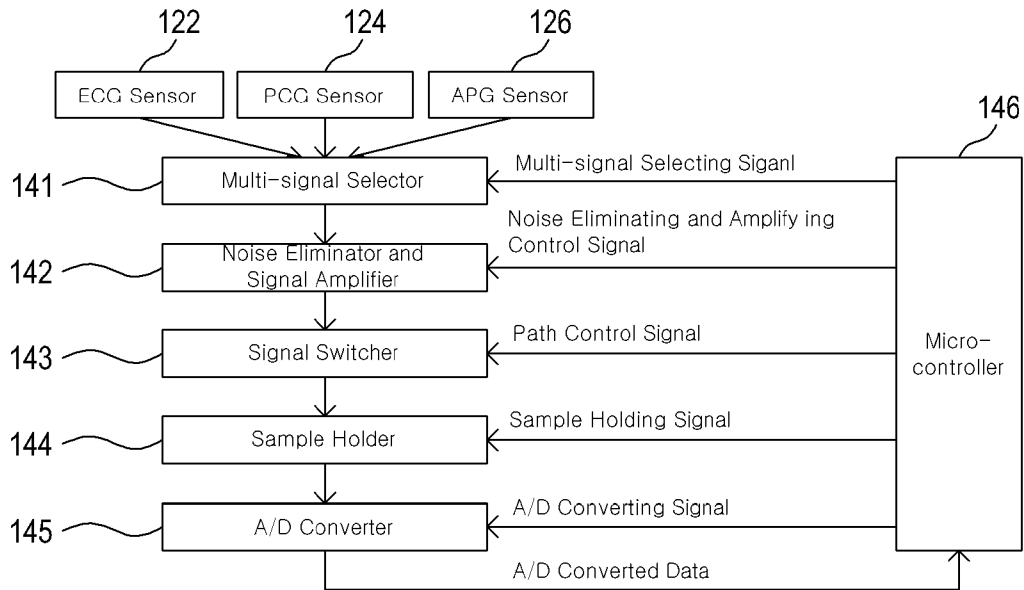
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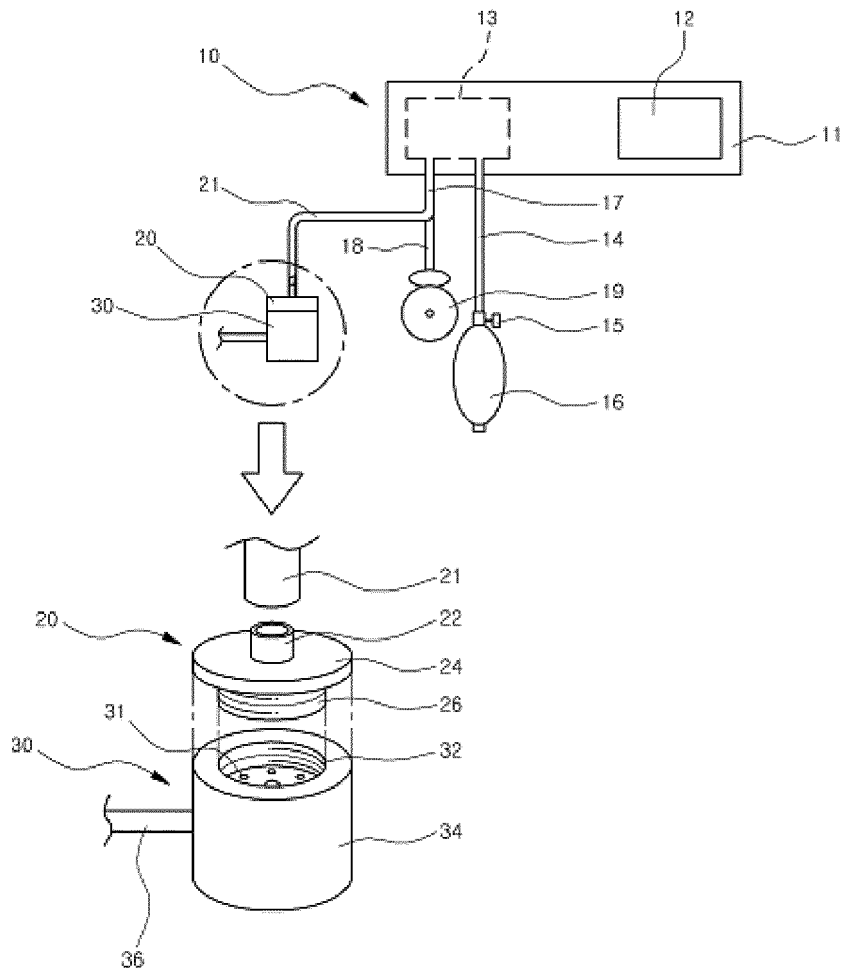
【Figure 1】



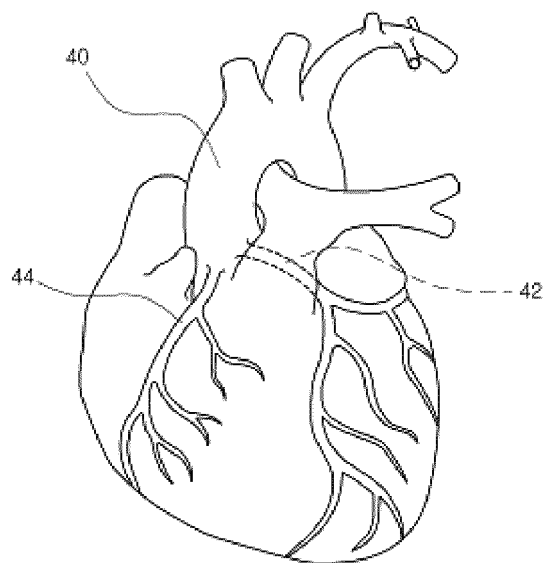
【Figure 2】



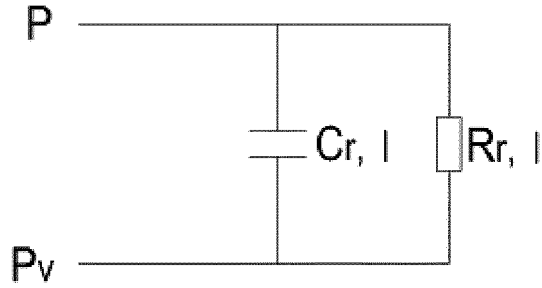
【Figure 3】



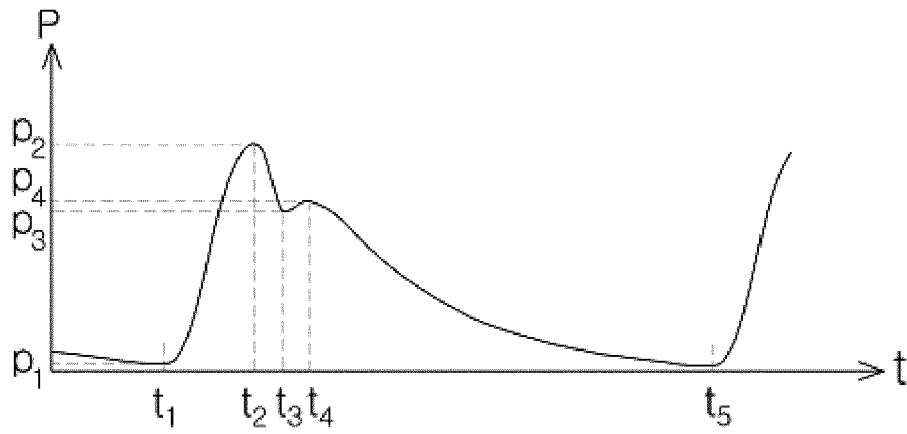
【Figure 4】



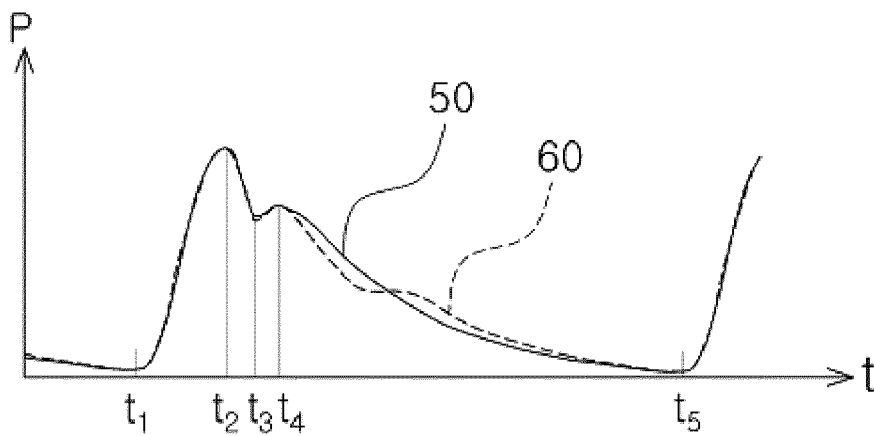
【Figure 5】



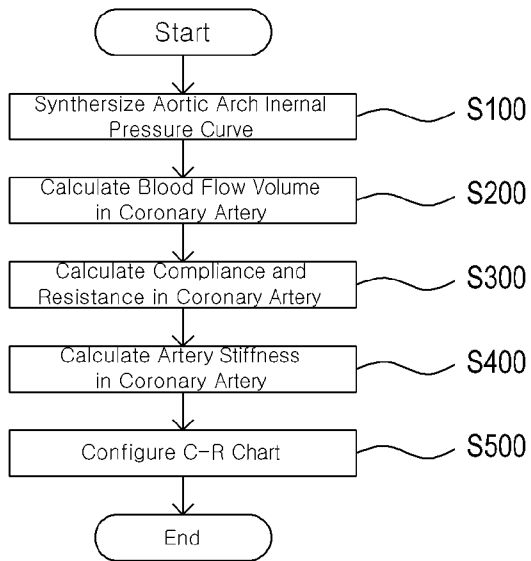
【Figure 6】



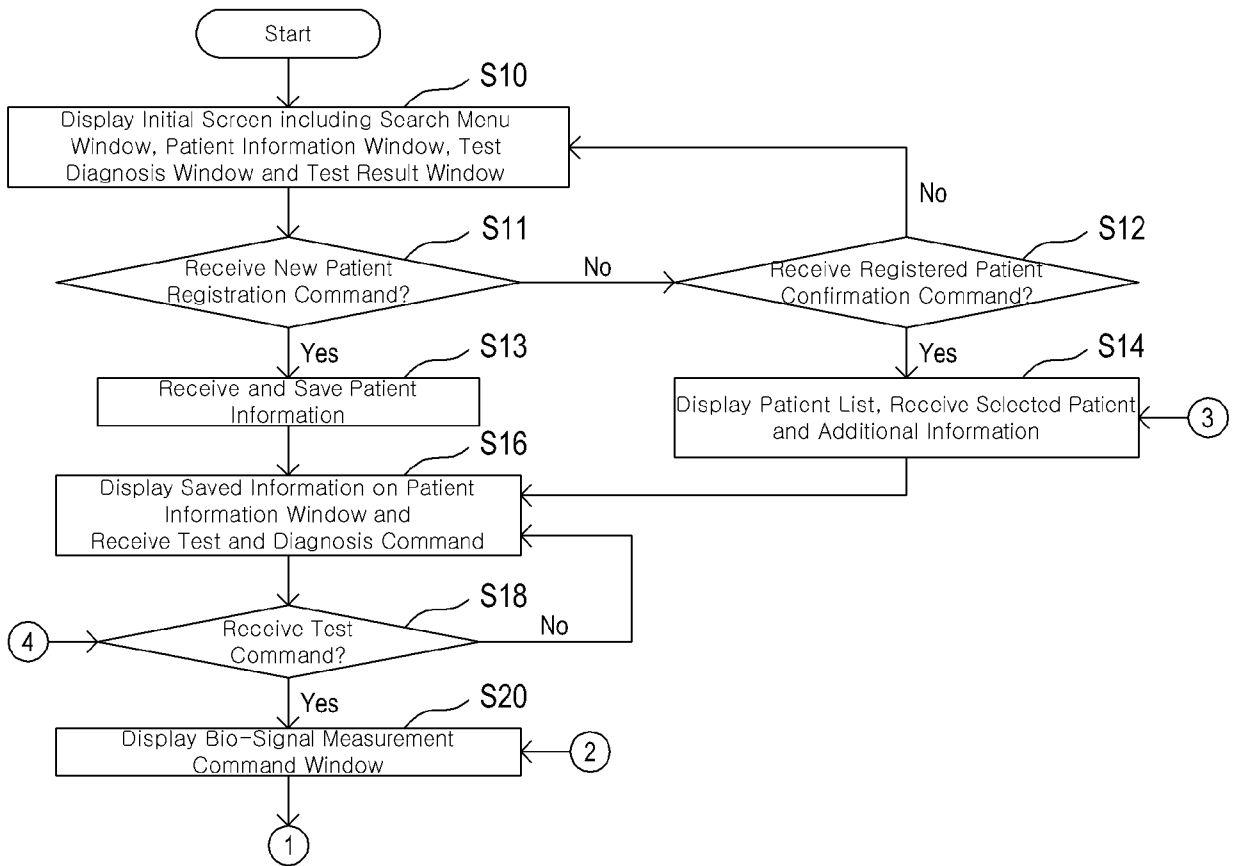
【Figure 7】



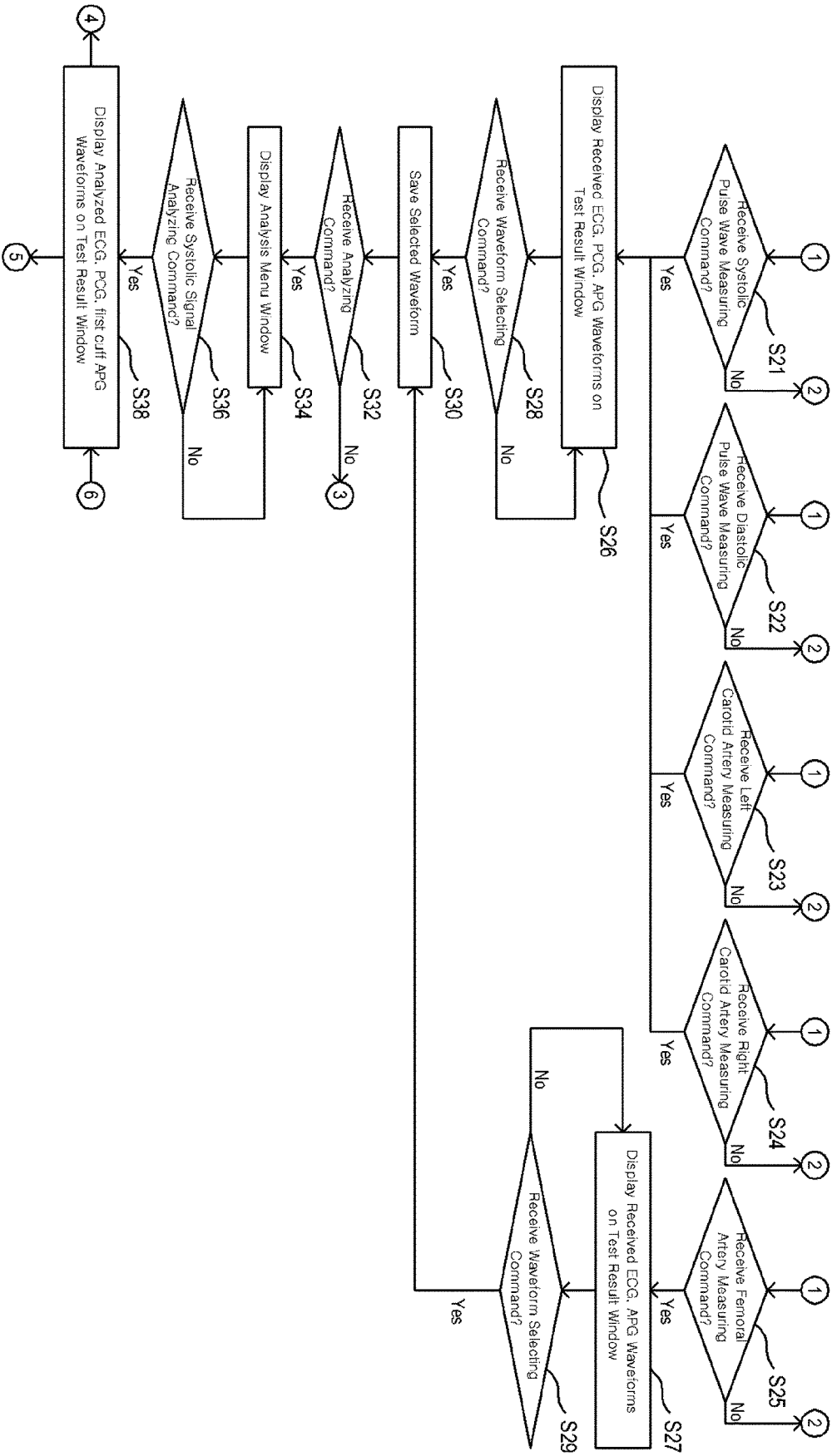
【Figure 8】



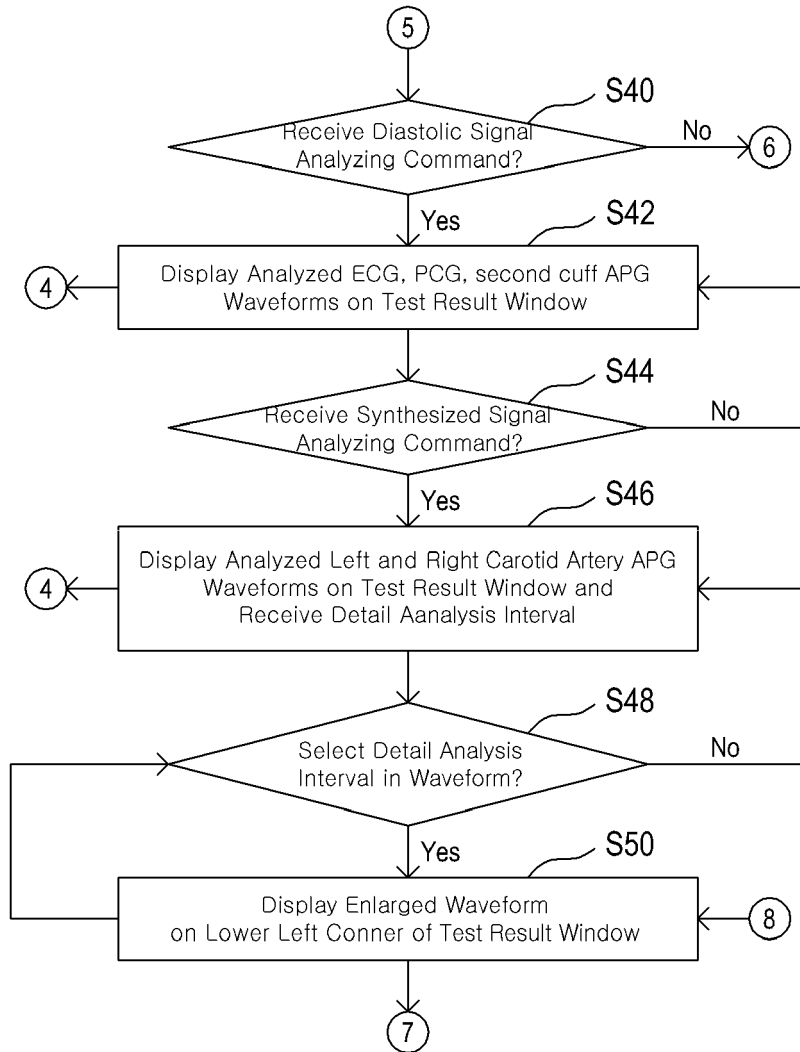
【Figure 9】



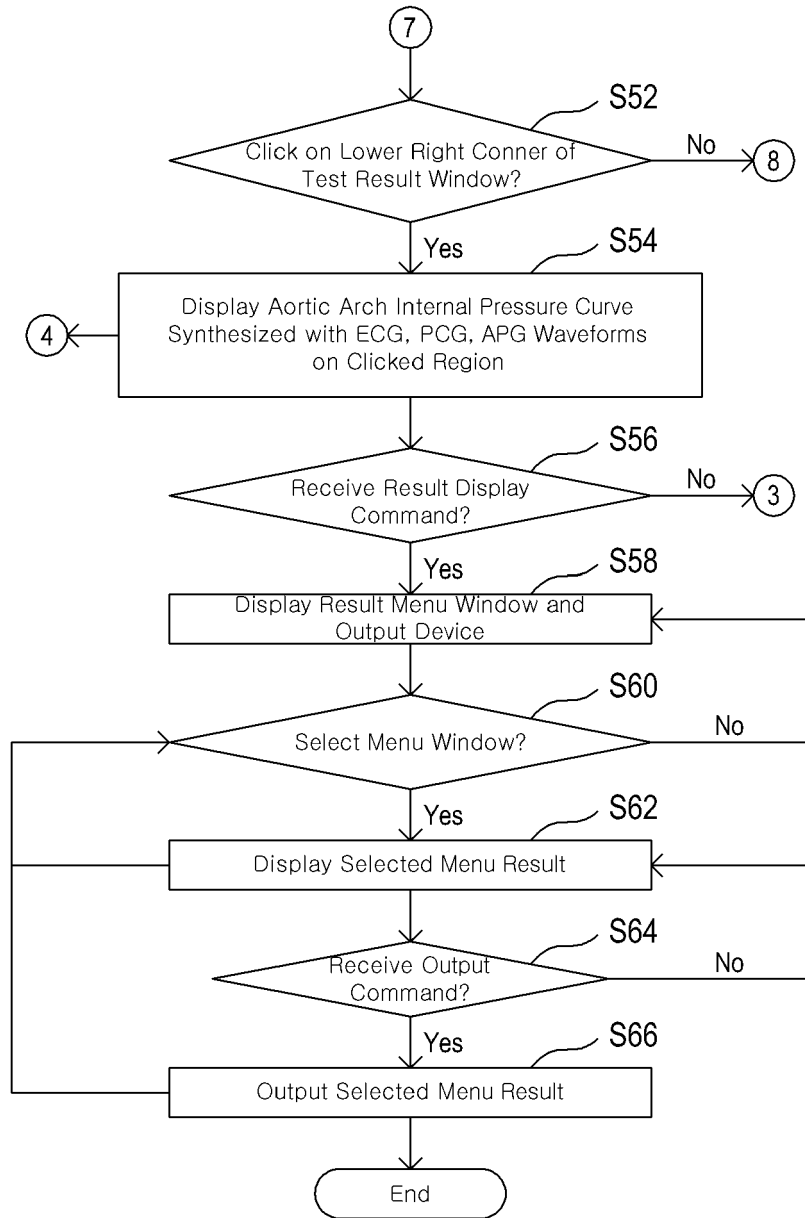
【Figure 10】



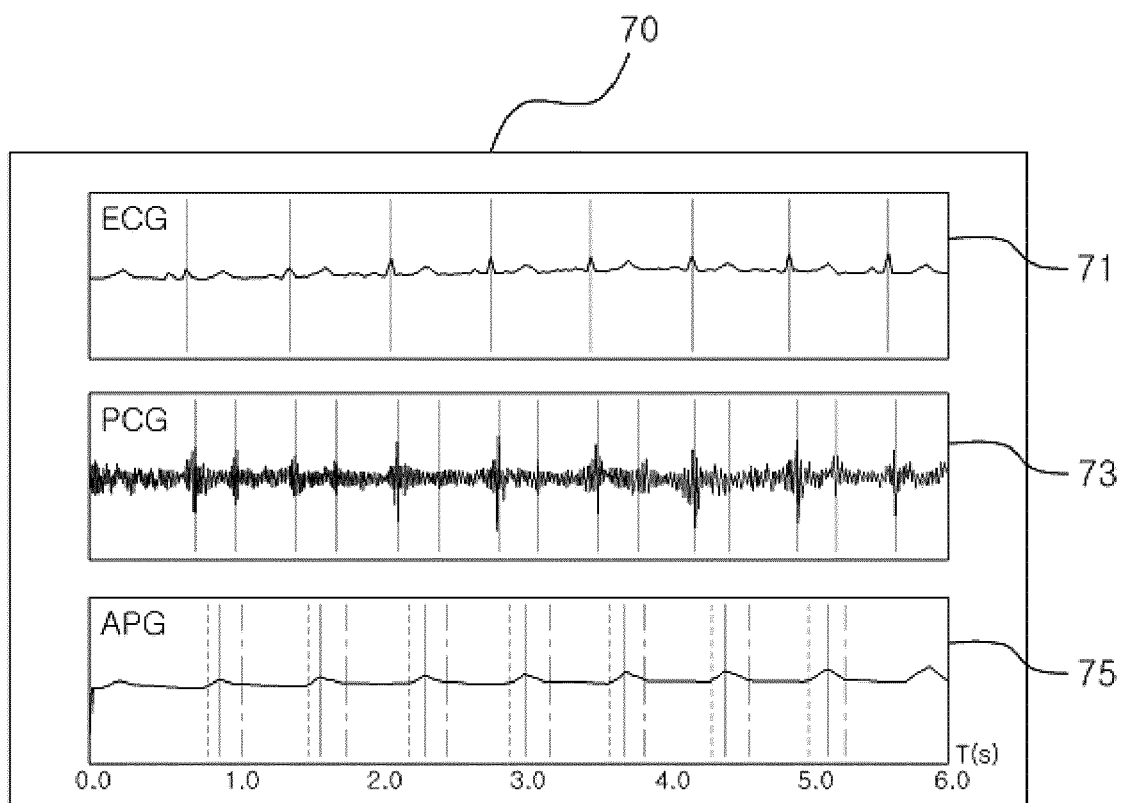
【Figure 11】



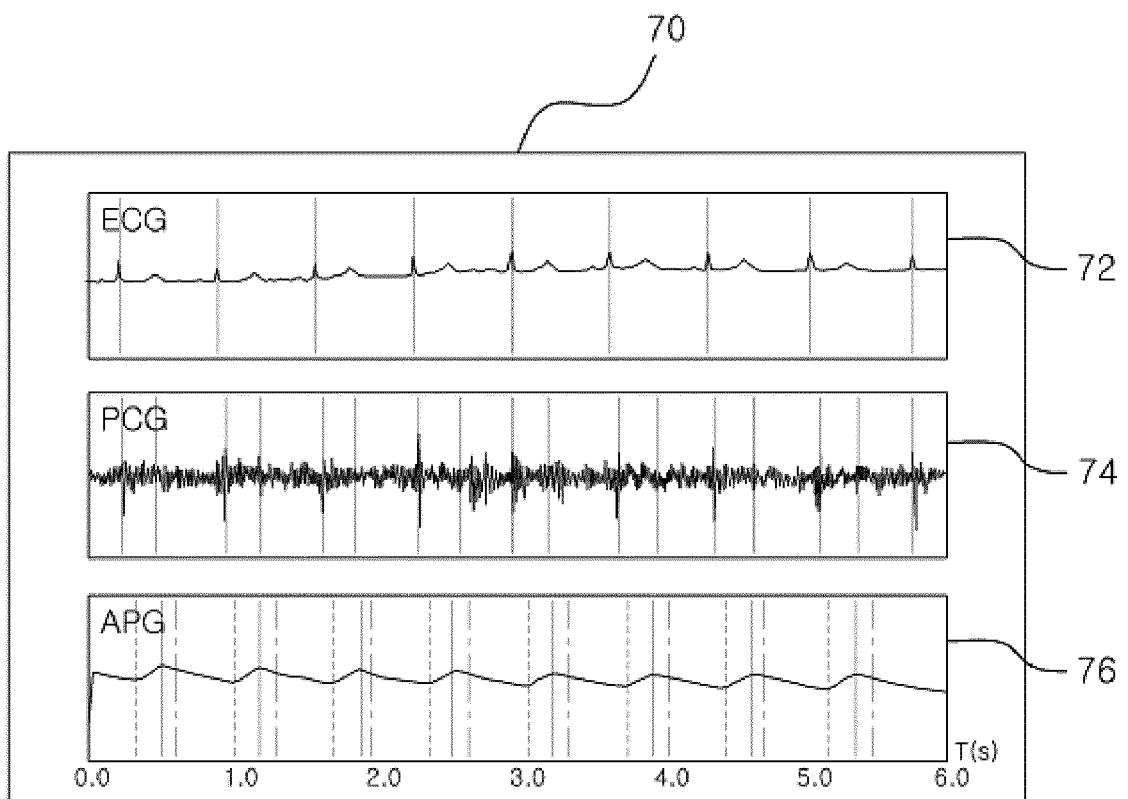
【Figure 12】



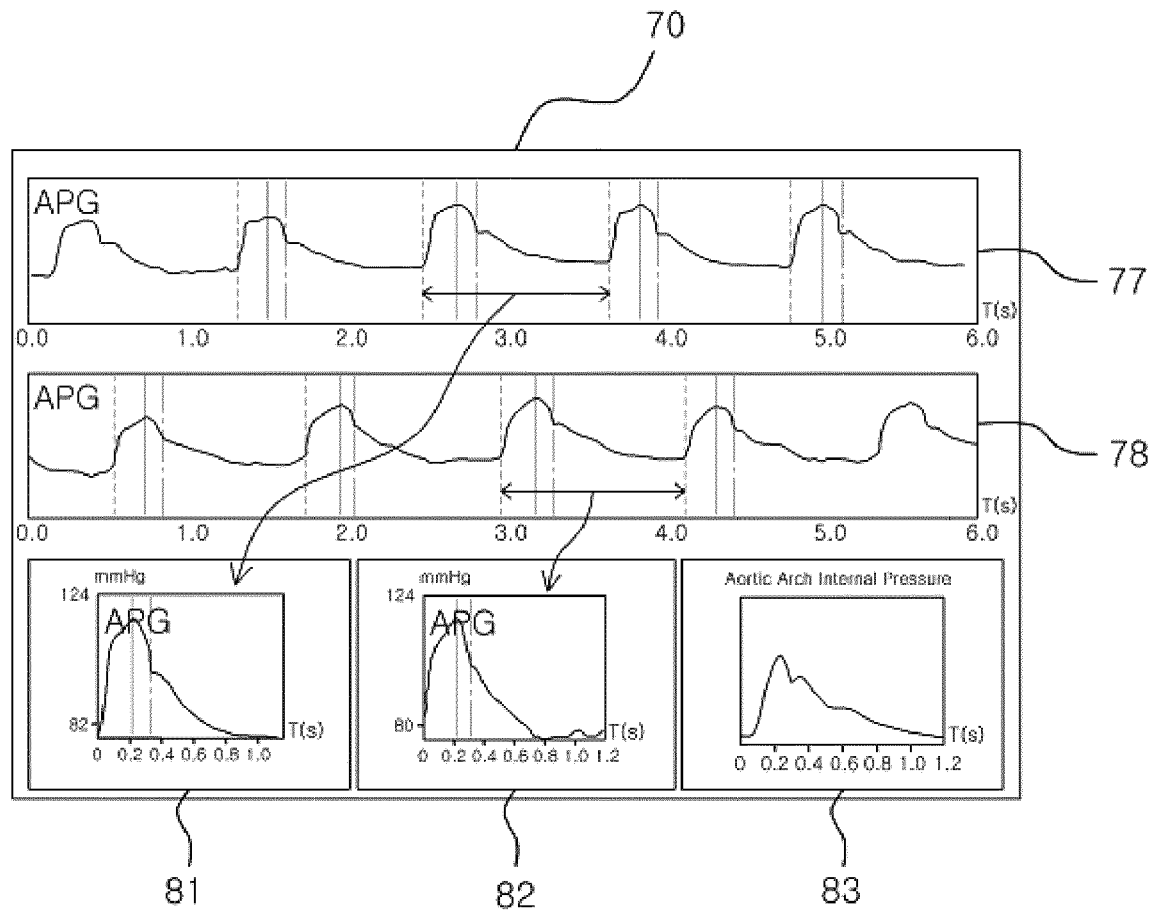
【Figure 13】



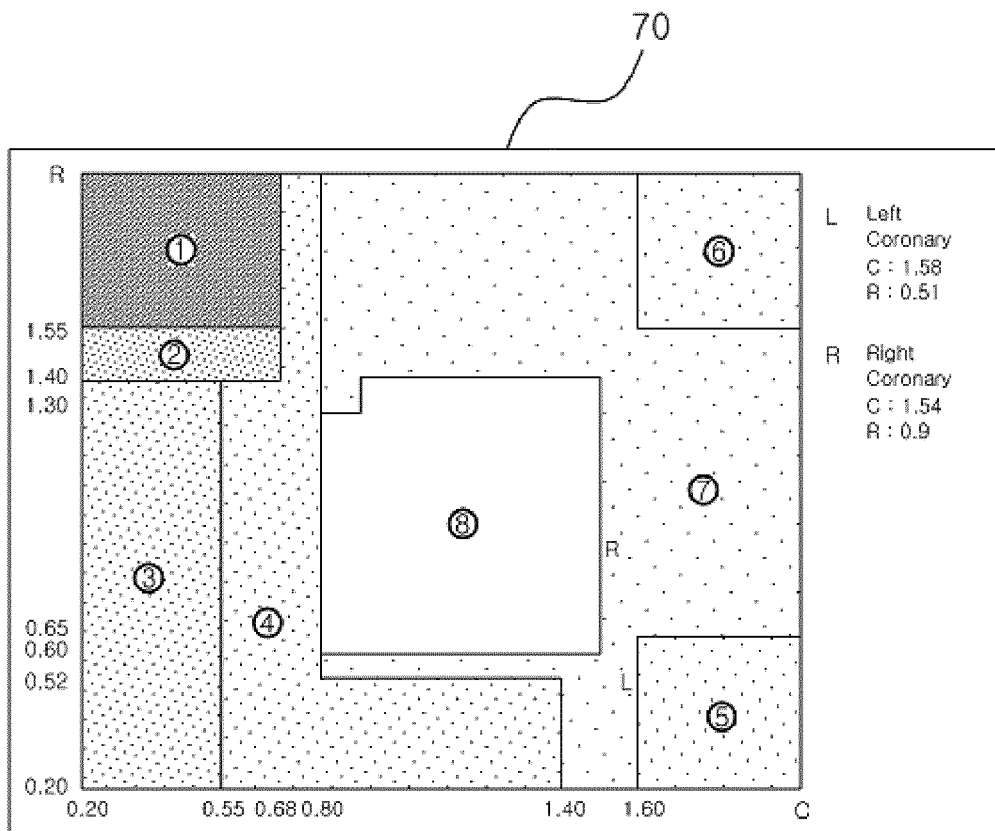
【Figure 14】



【Figure 15】



【Figure 16】





EUROPEAN SEARCH REPORT

Application Number
EP 16 15 6178

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A	US 2008/183232 A1 (VOSS GREGORY I [US] ET AL) 31 July 2008 (2008-07-31) * paragraphs [0123] - [0130] * -----	1-20	
A	US 6 120 442 A (HICKEY DONALD D [US]) 19 September 2000 (2000-09-19) * column 5, lines 23-55 * * column 13, lines 32-50 * * column 17, line 12 - column 18, line 9 * -----	1-20	
			TECHNICAL FIELDS SEARCHED (IPC)
			A61B
The present search report has been drawn up for all claims			
Place of search Berlin		Date of completion of the search 12 July 2016	Examiner Trachterna, Morten
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	

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ON EUROPEAN PATENT APPLICATION NO.

EP 16 15 6178

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For more details about this annex : see Official Journal of the European Patent Office, No. 12/82

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专利名称(译)	心血管分析仪		
公开(公告)号	EP3058868A1	公开(公告)日	2016-08-24
申请号	EP2016156178	申请日	2009-09-30
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当前申请(专利权)人(译)	IRUMEDI有限公司		
[标]发明人	KIM KWANG TAE HYEON SEOG SAN		
发明人	KIM, KWANG TAE HYEON, SEOG SAN		
IPC分类号	A61B5/02 A61B5/00 G16H10/60		
CPC分类号	A61B5/026 A61B5/02007 A61B5/7278		
代理机构(译)	柜CHAILLOT		
审查员(译)	TRACHTERNA , MORTEN		
优先权	1020080096524 2008-10-01 KR		
外部链接	Espacenet		

摘要(译)

心血管分析系统技术领域本发明涉及心血管分析系统，更具体地涉及能够及早检测心血管疾病并确定其原因的心血管分析仪。与传统的心电图不同，在左右冠状动脉的血管的每个分支中，心血管分析仪可以进一步测量血管的弹性系数（即，动脉硬化），显示有机变化，同时显示有机和功能变化的血管。，血流的体积，阻力和速度表现出血流的阻力特性。

[Figure 1]

